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Acoustic Survey

Investigation into

Existing Noise Environment Survey

At

Willing House, Gray's Inn Road

Date of Report: 10th October 2006

Compiled by: Mr. E. Brennan
MIOA

Revised by: Mr. D. Blacklock
BEng MSc CEng MIET MIOA

Copies to: Ole Smith, Heatherwick Studio,

Document Reference : dBA/SR/dB1837/EB/02

The Client.

Ole Smith
Heatherwick Studio
16 Acton St
London
WC1X 9NG

The Brief.

dB Attenuation were commissioned by Heatherwick Studio to carry out an acoustic survey of their proposed new premises in Grays Inn Road. The survey was requested as part of the planning application by Camden Planning Dept.

The existing and background noise levels to be established and presented in comparison with any contribution by the proposed air conditioning units.

The noise impact level to be calculated using the Sound Power Level of 83dB(A) - supplied by the manufacturer.

Summary.

The general noise level recorded in the roof area was relatively steady around 51–55dB, L_{Aeq} . The background noise level was from 48–51dB, L_{A90} . The increased noise level at location 2 when 1 condenser unit was operating from the Travelodge was +6dB(A).

The SWL of the proposed units combined is 83dB(A). There are no apparent tonal factors present with the units. The nearest bedroom window of the Travelodge is at a distance of some 7m from the intended location of the new unit. The predicted noise level at this window is some 57dB(A).

The predicted level at the penthouse flat on top of the adjacent Britannia Building is some 47dB(A).

Recommendations.

- Untreated, the proposed installation is predicted to have an impact on the noise levels in the vicinity of the roof area.
- The installation of a screen to shadow the directly affected areas has been suggested as a means to reduce the noise impact. Details are included in the report. This will reduce the impact of the noise of the plant to zero.

Theoretical and Methodology Information.

The survey was carried out between 17:30 and 20.00hrs on Monday 7th August 2006 by E. Brennan, MIOA. The weather was warm and still with no wind blowing in the quadrangle. The weather conditions were felt to be suitable for the purposes of the survey.

The equipment used was a CEL-593 Type 1 sound level analyser; calibration was checked with a CEL 284/2 acoustic calibrator. This instrument was supported on a tripod, with microphone level at 1.2m above ground and used at the various locations between the hours stated above.

There was some general background traffic activity in the area with intermittent local traffic, which remained relatively constant through out the survey.

The Sound level meter was set to 1/3 octave SPL_f reading and measurements were taken during an Environmental 5min assessment period. This allowed the operator to omit excessive background noise by comparing $L_{eq,5mins}$ with $L_{90,5mins}$. These are the mean equivalent noise levels and the minimum noise level recorded for 90% of the assessment period respectively.

Readings were taken at a distance of 1m away from and along the rear facing elevation of the Travelodge property as indicated in the layout sketch in the appendices. An additional reading was taken on the adjacent roof area that lays some 2m below the roof area in question.

An approximate sketch showing the location of the readings is included in the appendices at the end of this report.

BS4142 is the standard applicable noise generated from sources defined as industrial when present in a residential environment.

WHO Regulations are guidelines for generally all areas not covered by BS4142.

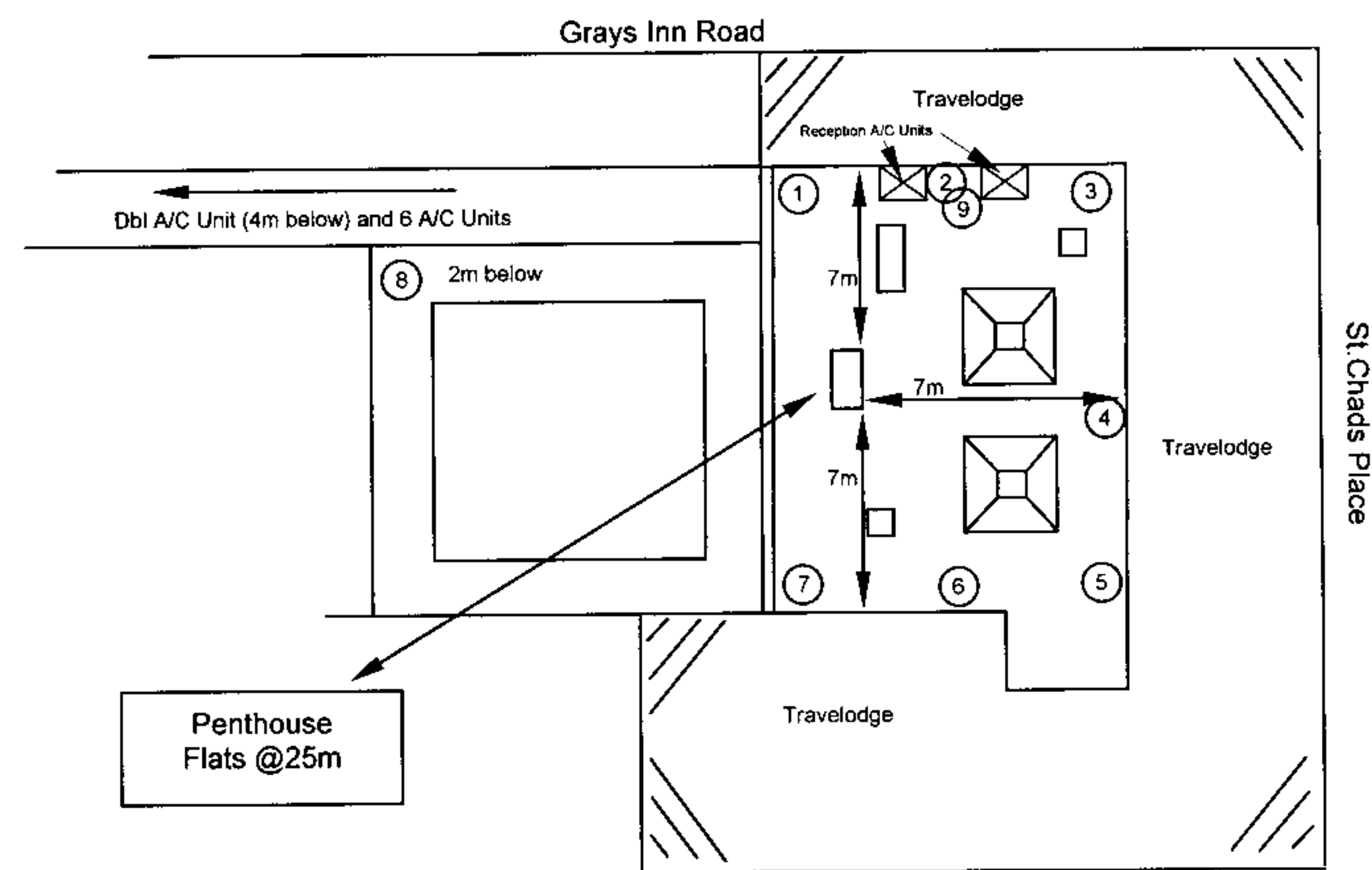
Tonal Noise is a peak in a frequency which can be defined as 5dB greater than the third octave above and below it.

Guidelines say that a weighting of +5dB should be added for tonal noise.

Discussion

The layout of the roof and the intended location of the proposed unit are shown in the sketch below. The roof area nominally measures 16 metres x 11 metres with 2 skylight windows into the studio and 3 access hatches to service areas. The roof of the studio has the Travelodge on three sides, is approximately 2 metres above the adjoining roof.

The approximate distance from this point to the nearest bedroom window of the Travelodge is some 7m in all directions. The bottom windows are at a level approximately equal to the proposed unit height.



There are 2 condenser units on the roof related to the reception area of the Travelodge, one unit operates spasmodically but according to the staff on duty they could not control it to operate during our survey, the second unit did not function at all and according to the staff has not worked for some time.

There are 6 single and a double air conditioning units outside the adjoining office block which were operating occasionally but, being located several metres below the studio roof could not be established how many were operating.

Aircraft noise is the major contributor to the general noise level peaks.

The noise from the building facing into Britannia St generates quite a lot of noise from voices, which was more prominent than normal due to the windows being open.

Results.

The results of the investigation are listed in full at the end of this report, but are shown in the summary table below.

Location	L_{Aeq}	L_{A90}
1	51	50
2	55	49
9(pos 2 with fan on)	61	48
3	50	48
4	50	49
5	54	48
6	50	48
7	50	49
8	55	51

The manufacturer's data shows individual SPL @1m of 57 and 63dB(A). At the worst incidence, the combined SPL will be 64dB(A).

For a unit that is 64dB(A) @1m, the SPL at 7m is given as;

- $SPL \text{ at } r_2 = SPL \text{ at } r_1 - 20\log(r_2/r_1)$ where $r_1=1m$ and $r_2=7m$
 - $SPL \text{ 7} = 64 - 20\log(7/1)$
 - $SPL@7m = 47dB(A)$

or

- Sound Power Level, $SWL = 20\log r + \text{Sound Pressure Level, SPL} + 7.9$
- $SWL_{(RXYQ8P)} = 20\log 1 + 57 + 7.9$
- $SWL_{(RXYQ8P)} = 65dB(A)$

- Sound Pressure Level, $SPL @7m = SWL - 20\log(7) - 7.9$
- $SPL@7m = 40dB(A)$

and

- $SWL_{(RXYQ18P)} = 20\log 1 + 63 + 7.9$
- $SWL_{(RXYQ8P)} = 71dB(A)$
- Sound Pressure Level, $SPL @7m = SWL - 20\log(7) - 7.9$
- $SPL@7m = 46dB(A)$

giving a combined $SPL@7m$ of $47dB(A)$.

However, further information provided by the manufacturer indicates a Sound Power Level of $83dB(A)$. This is extensively higher than that calculated from the given $SPL@1m$. To investigate the sound impact level worst case scenario, these two base figures should be used to compare the SPL at the nearest window.

- $SWL_{(RXYQ8P)} = 83dB(A)$
- $SWL, 83 = 20\log r + SPL + 7.9$
- $SPL@8m = 83 - 20\log 8 - 7.9$ (8m to centre of the plant)
- $SPL@8m = 57dB(A)$

Similarly, for the facing windows of Britannia House @26m

- $SPL@26m = 83 - 20\log 26 - 7.9$ (8m to centre of the plant)
- $SPL@26m = 47dB(A)$

There is clearly some difference in the two methods used to predict the noise impact of the plant, but in the situation where the worst case scenario is to be considered, the higher noise level must be assumed.

It should be considered that the manufacturer's data is from test conducted in an anechoic chamber. The actual installation location will give slightly higher readings due to floor and site reflections and could raise the readings by some 3dB.

Therefore to err on the side of safety, the noise level attributable to the proposed plant unit at the nearest Travelodge bedroom window is some 60dB(A). This compares marginally with the measured ambient noise level of 61dB(A) with a single Travelodge fan running, and would compare better still when both of them are in operation.

The other residential concern is the penthouse flats on the roof of the building adjacent to the roof area. This is some 25m away from the intended location of the proposed plant and under the previous calculation would have a direct noise level attributable to the new unit of some, 47dB(A), or a corrected 50dB(A).

Conclusions.

It can be seen from the sound power data and calculations above that the proposed plant would have an impact on the roof area with the present set up with existing ambient noise levels, fans and A/C units in the vicinity.

Predicted noise levels outside the windows are within the current 'operational' noise levels, but above the minimum background noise levels in the area. They have no apparent tonal identity.

Camden Council operates a 'non-creepage' policy which requires zero influence from new installations to control unwanted increase in background noise levels. Therefore the influence of the new plant should not impact on the 50dB(A) mean background noise level in the roof top area. The required SPL of the plant is therefore 10dB below current background – i.e. would be required to be as close to 40dB(A) as practicable.

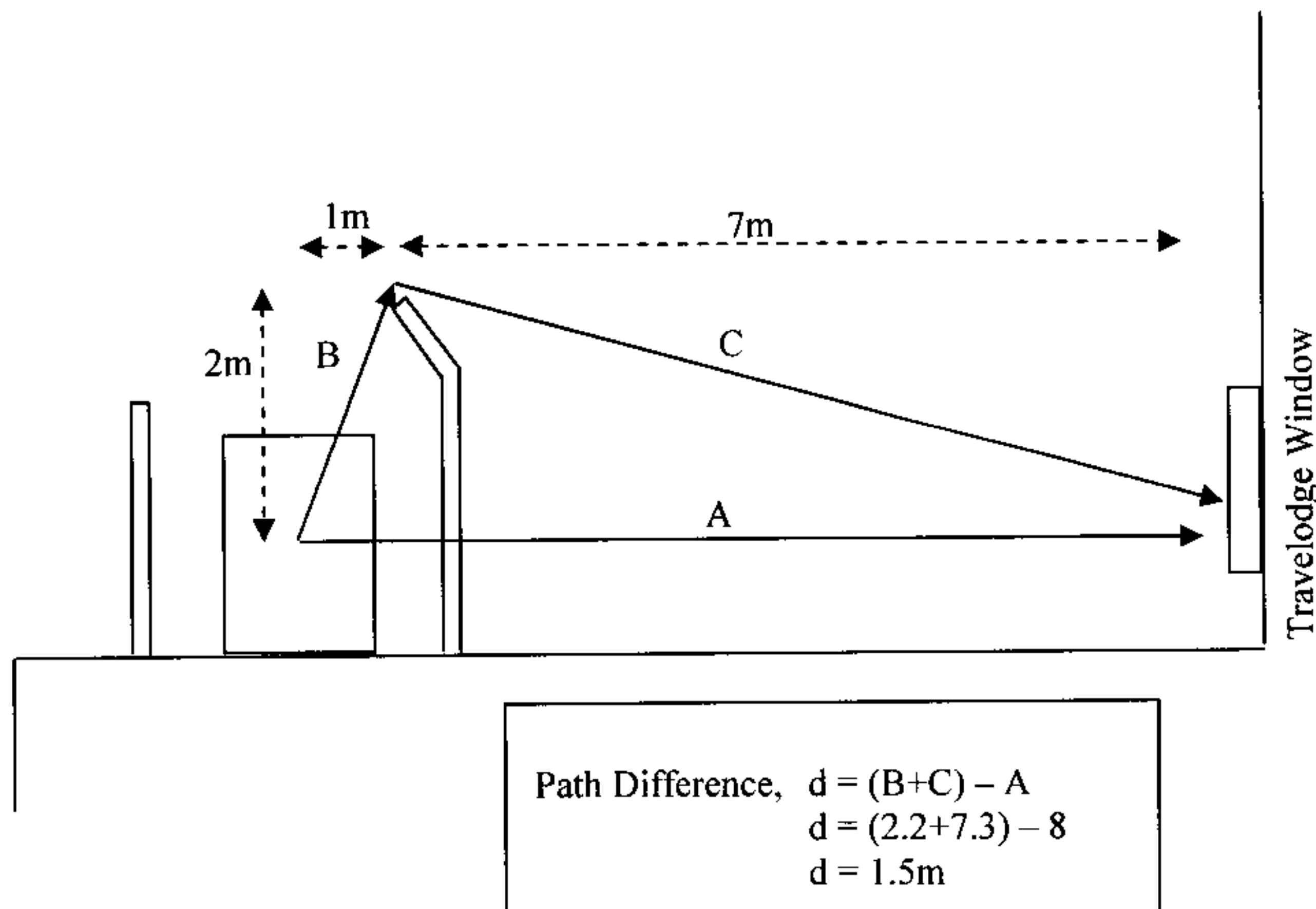
This is a reduction of a minimum of 10dB but a target level of 20dB from the predicted level of 60dB(A). In the direction of Britannia House, the reduction is only 0-10dB.

Recommendations.

To achieve this level of attenuation, this end a screen arrangement that is three sided and has a sloped roof section to protect the higher floors of the Travelodge could be considered to reduce further the noise levels of the equipment relative to the bedroom windows.

The size of the screen will be determined by the physical attributes of the plant plus ventilation and clearance requirements. Nominally, this give a structure some 3meters high, 3.7m across and 2.3m deep. To help in the protection of the higher placed windows, the top 600mm is angled inwards to increase the effective path difference caused by the screen, and allow for natural air convection movement within.

It is also proposed that the fourth side of the screen be only partial, providing access to the equipment, but limiting the effect of reflection towards the Travelodge windows. Although there will be some noise deflection toward the Britannia building, the requirement in this direction is less due to the distances involved and will be sufficient to provide the level of attenuation needed.



The given path difference of 1.5m will provide 17 and 20dB attenuation in the 250 and 500Hz octave band widths. These are the dominant mid frequency bandwidths, the 1000Hz and higher having a better attenuation with the path difference.

With the increase in height of the windows above the unit, the path difference does reduce somewhat, but is still around 14 and 17dB at these octave frequencies. With the additional attenuation for distance to the higher windows this is sufficient to compensate.

The structure of the screen should be such that it will have a barrier effect of not less than that of the path difference. The given sound reduction index for the structure of the screen is;

63	125	250	500	K	2K	4K	8K	Hz
21	24	27	36	43	44	47	49	dB

With these measures taken it is predicted that the noise impact of the newly proposed plant will be kept to a minimum, and it is not likely that residents in the Travelodge or adjoining buildings will have nuisance caused by the installation.

Appendix 1

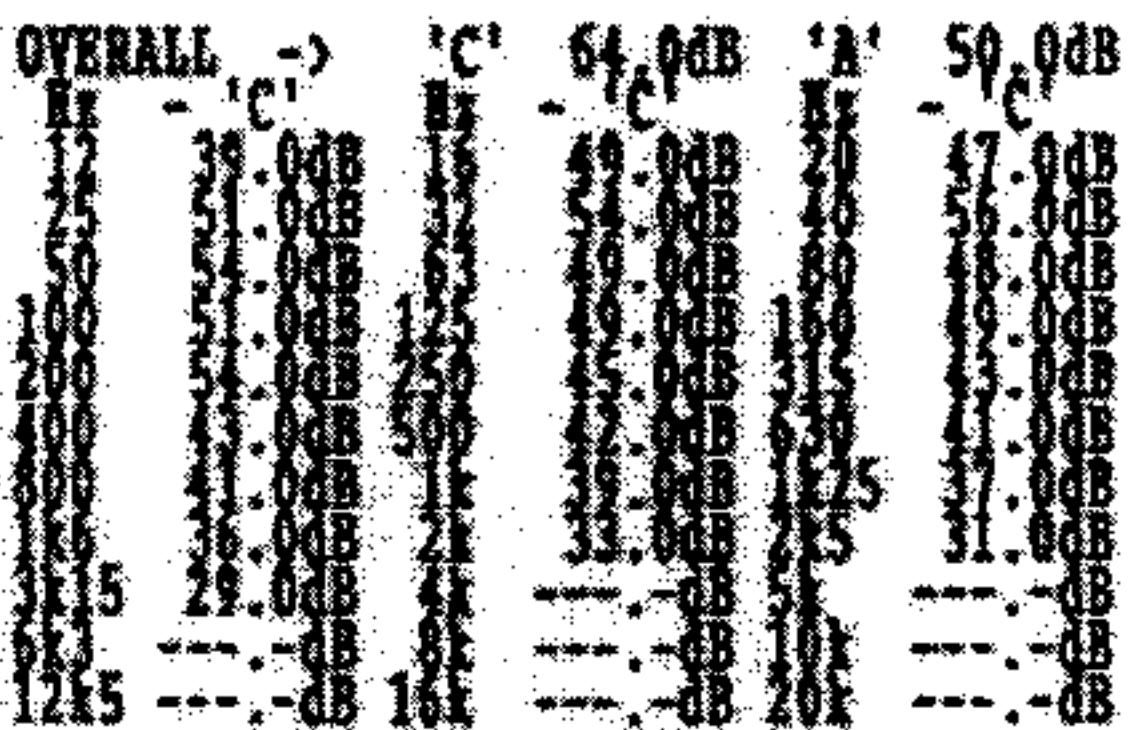
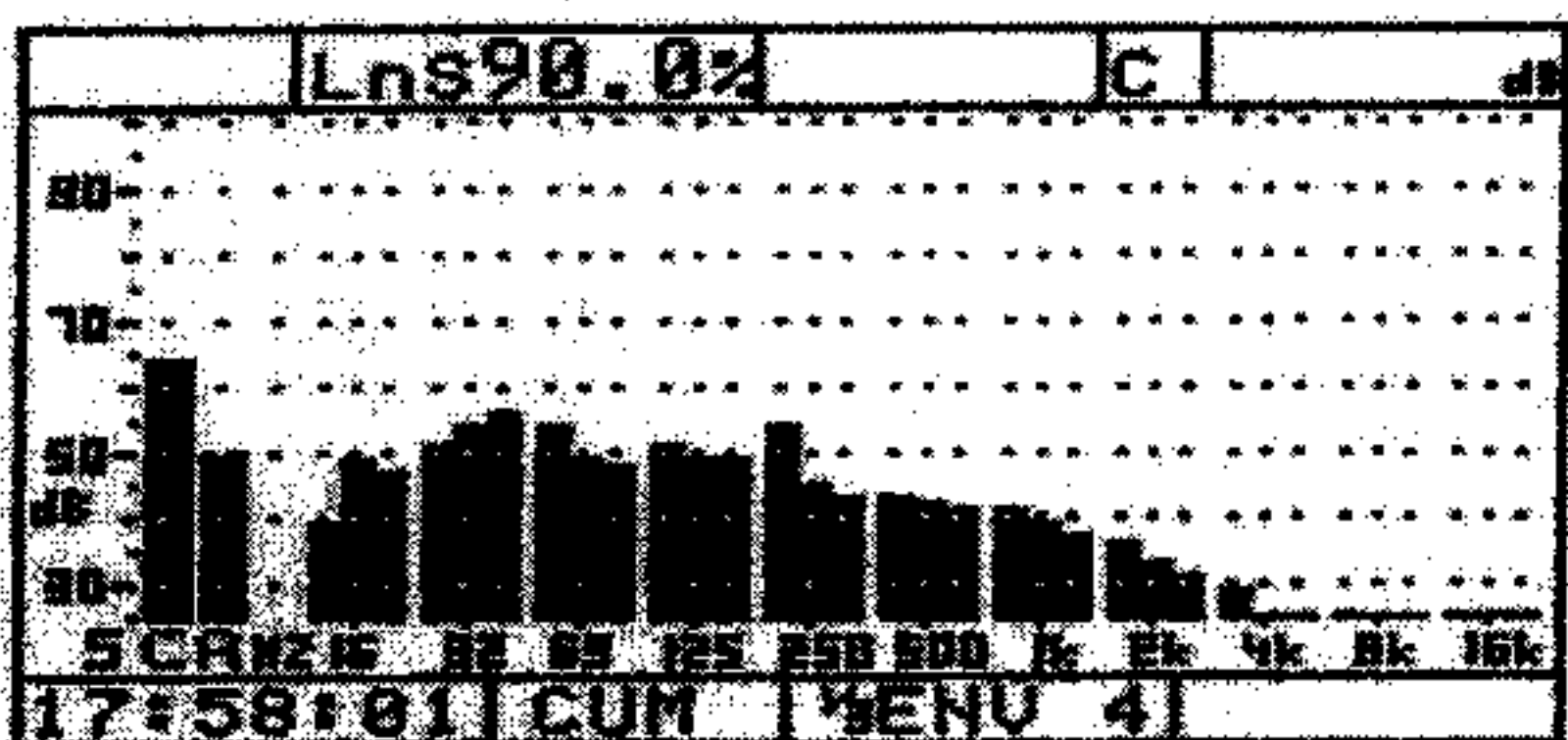
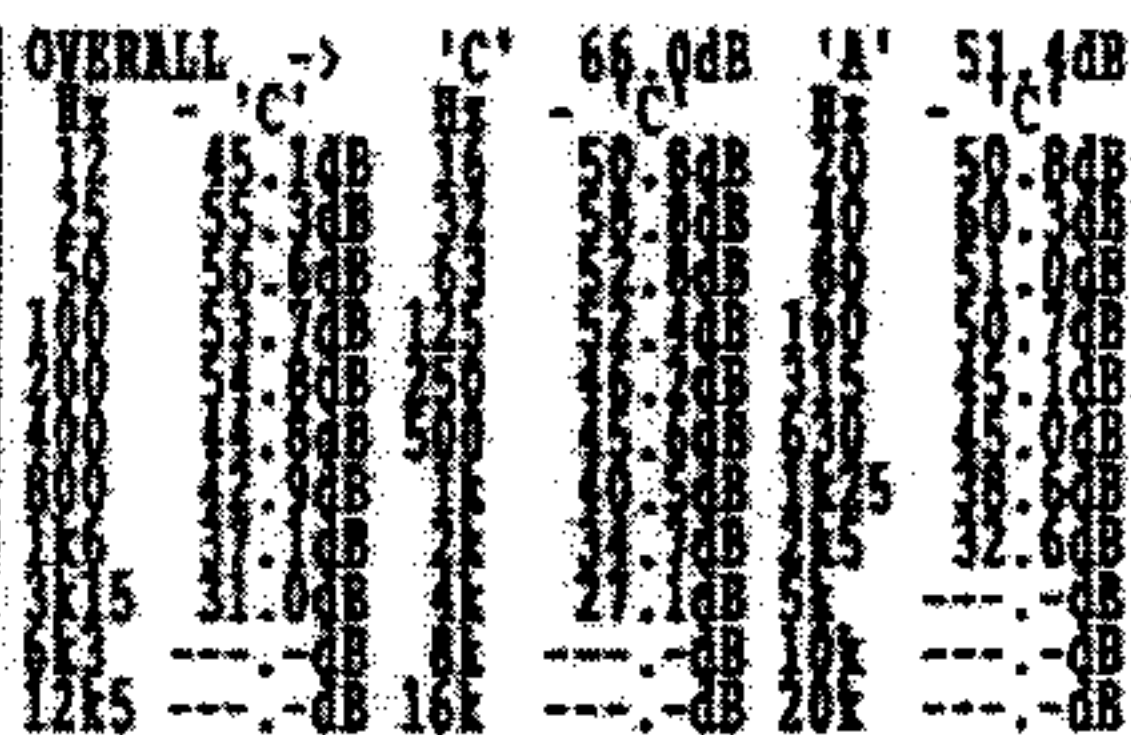
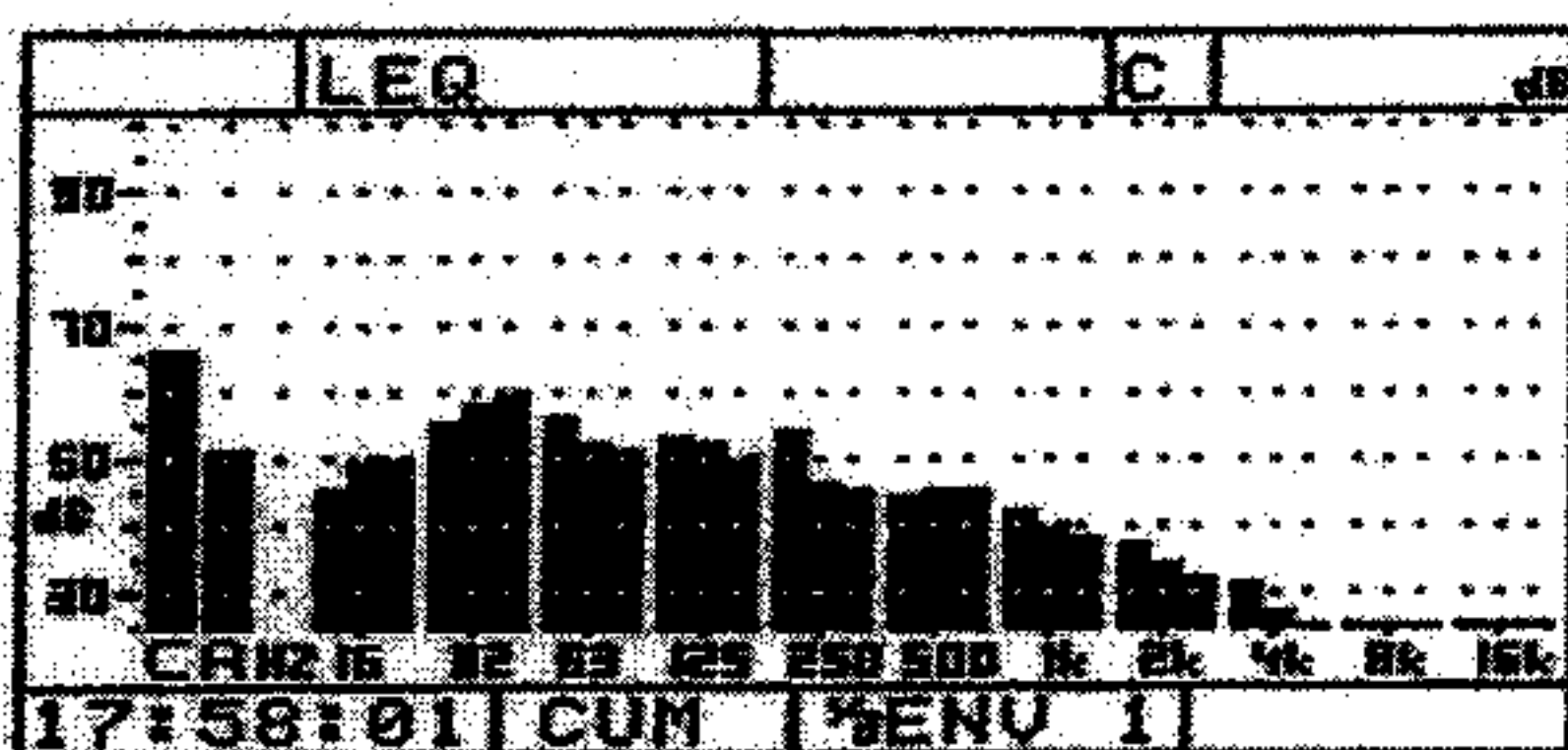
Sound level meter readings

and

locations

CEL 593.CIT v 5.5

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END	07-AUG-06	18:03:04
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TIMED RECS	1 PER	5min
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S	C.H 03	MENU

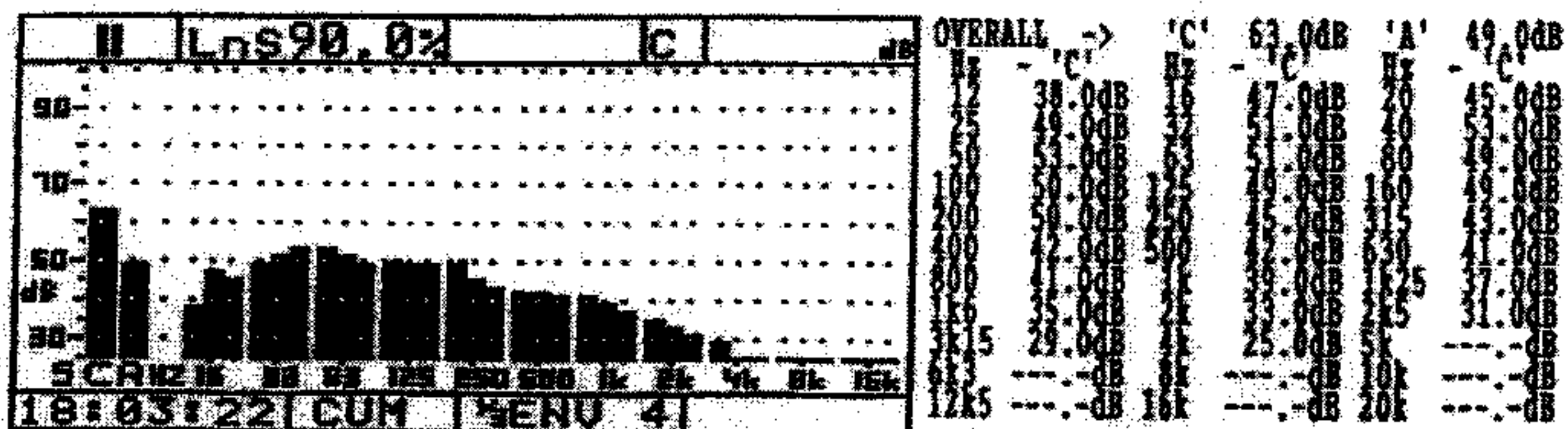
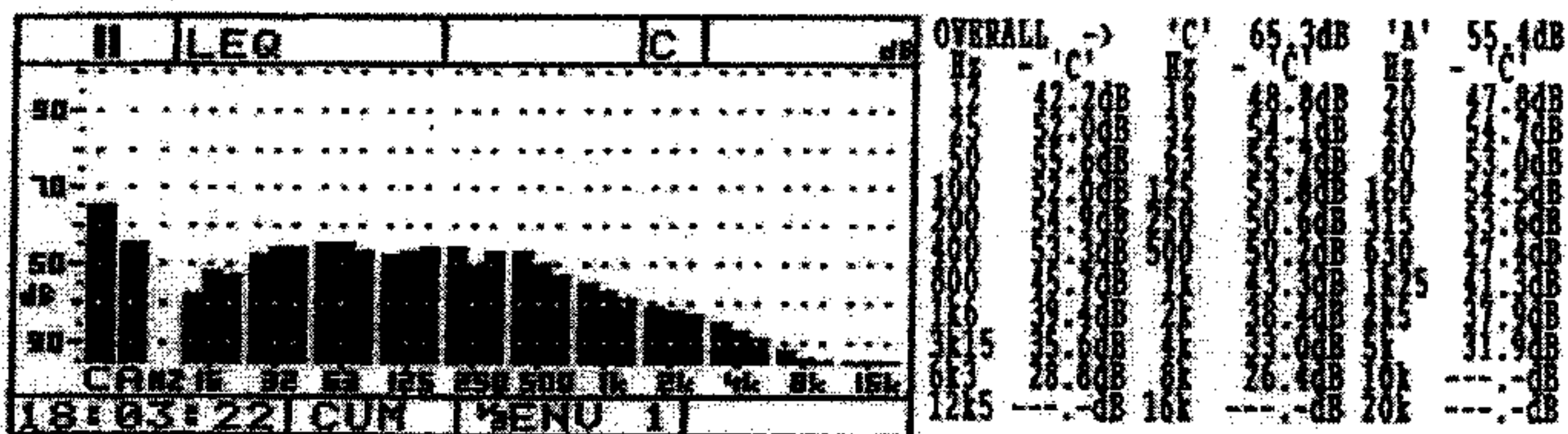


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CEL 593.CIT v 5.5

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 S C.A Q3 MENU

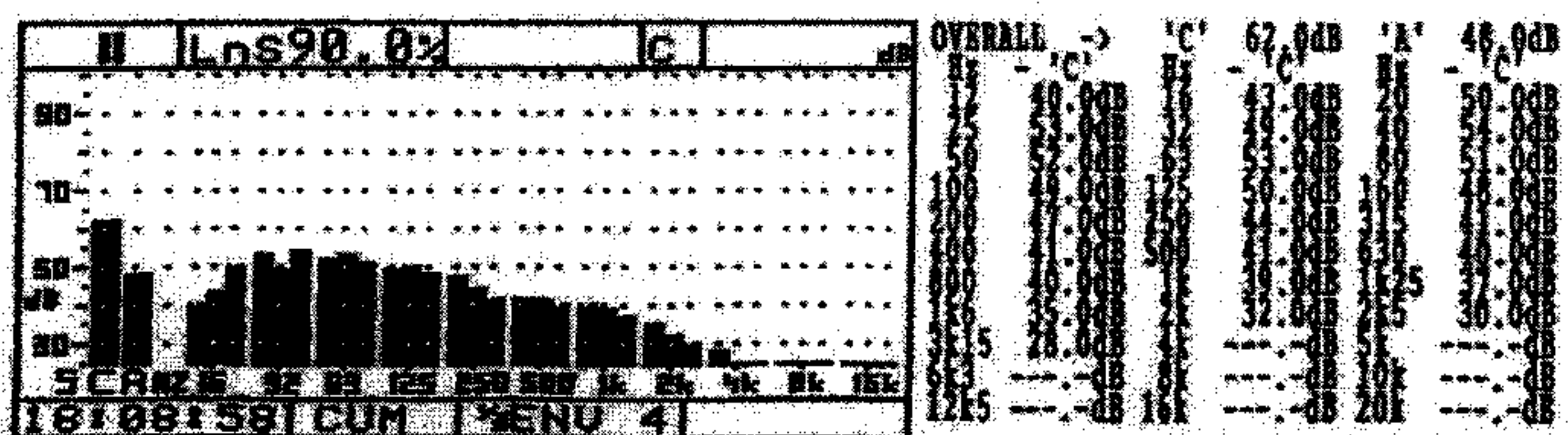
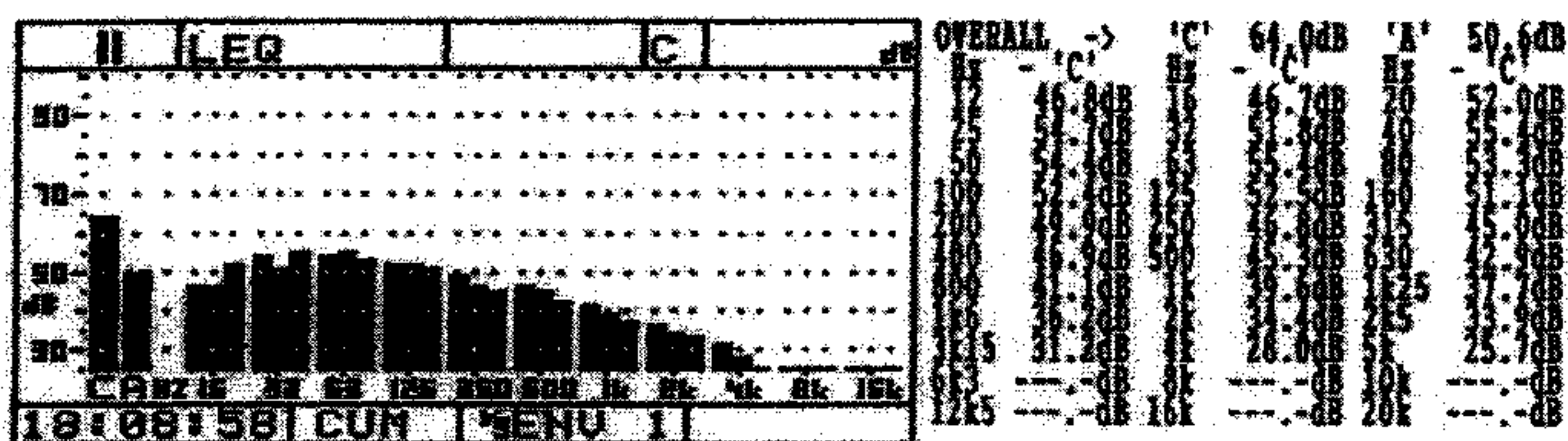


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 End 07-AUG-06 18:14:30
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 Mic Free Field 200v ON Period 5 minutes

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 END 07-AUG-06 18:14:30
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 S C.A Q3 MENU

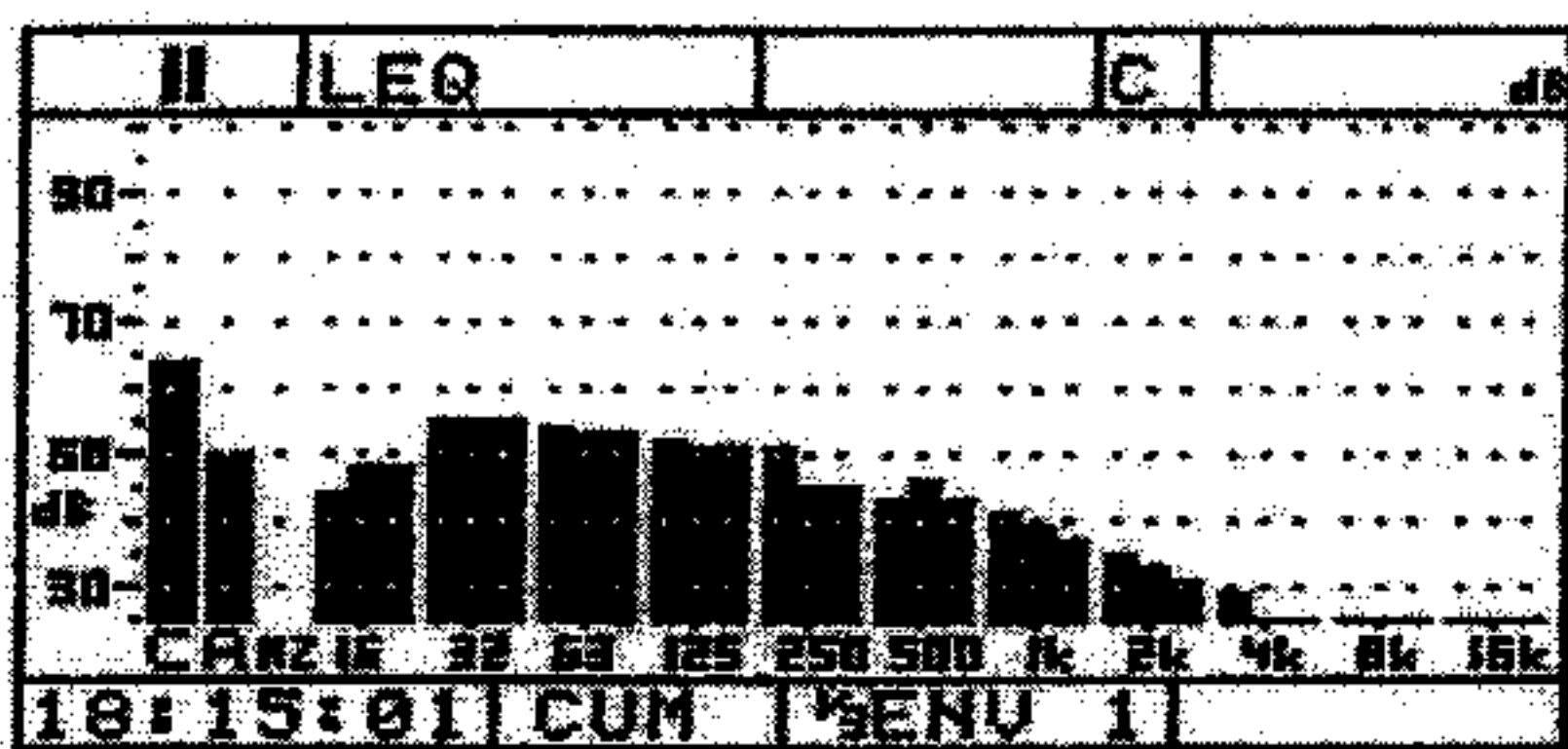


CEL Instruments Ltd.

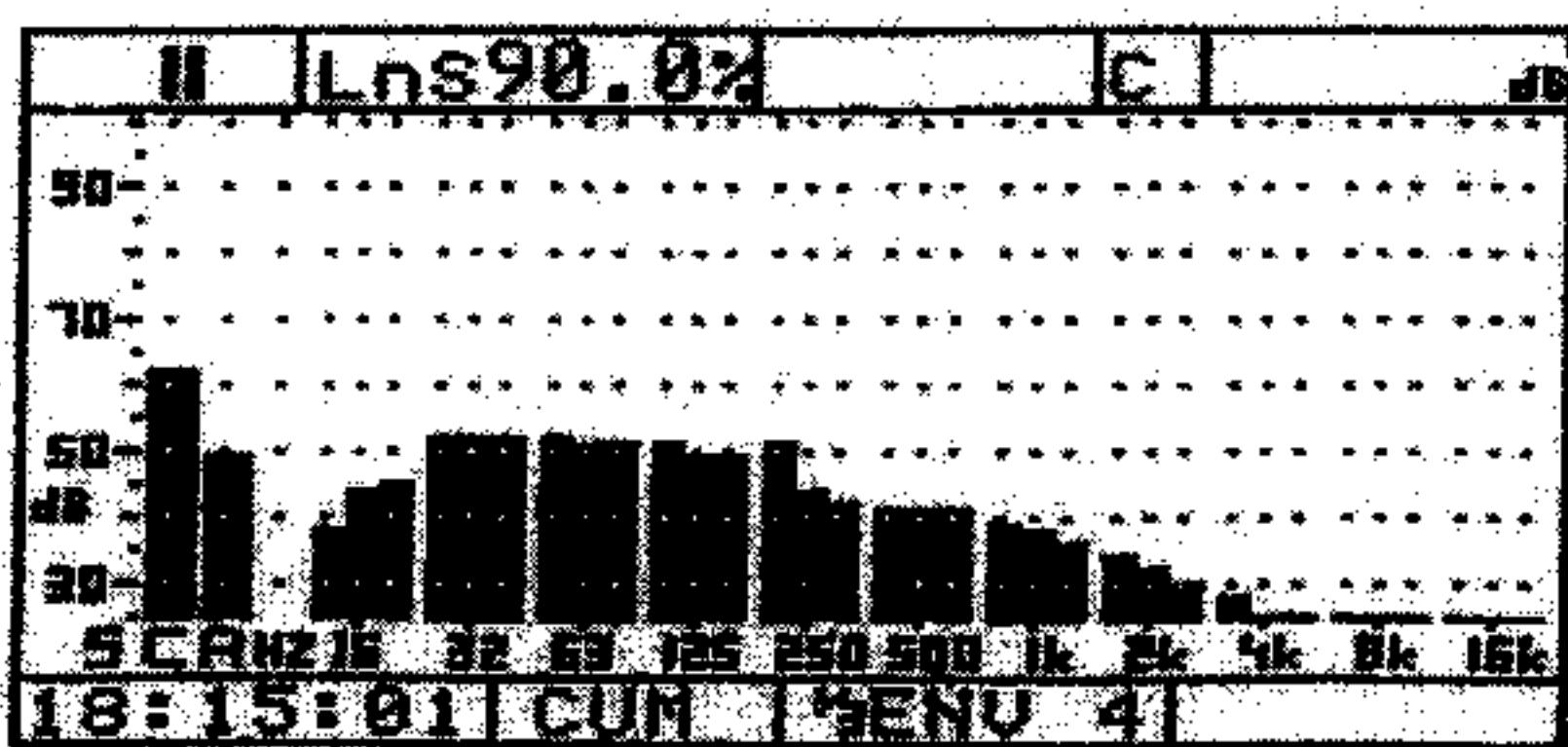
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 End 07-AUG-06 18:20:08
 Length 0 days 00:05:07
 Mic Free Field 200v ON Period 5 minutes

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 START 07-AUG-06 18:15:01
 END 07-AUG-06 18:20:08
 LENGTH 0 DAYS 00:05:07
 TIMED RECS 1 PER 5min
 MIC=FF 200U=ON TYPE=1
 S C.A Q3 I%ENU



OVERALL ->		'C'	64.0dB	'A'	50.4dB
Hz	-	Hz	-	Hz	-
125	44.9dB	16	48.0dB	20	48.3dB
250	55.1dB	32	55.5dB	40	55.0dB
500	52.2dB	63	52.2dB	80	53.2dB
1000	52.2dB	125	51.6dB	160	51.1dB
2000	43.1dB	250	45.9dB	315	45.2dB
4000	41.3dB	500	38.8dB	630	43.2dB
8000	35.4dB	1k	38.8dB	1k25	37.4dB
16k	29.3dB	2k	25.7dB	2k5	31.3dB
315	29.3dB	4k	25.7dB	5k	---
630	---	8k	---	10k	---
1250	---	16k	---	20k	---



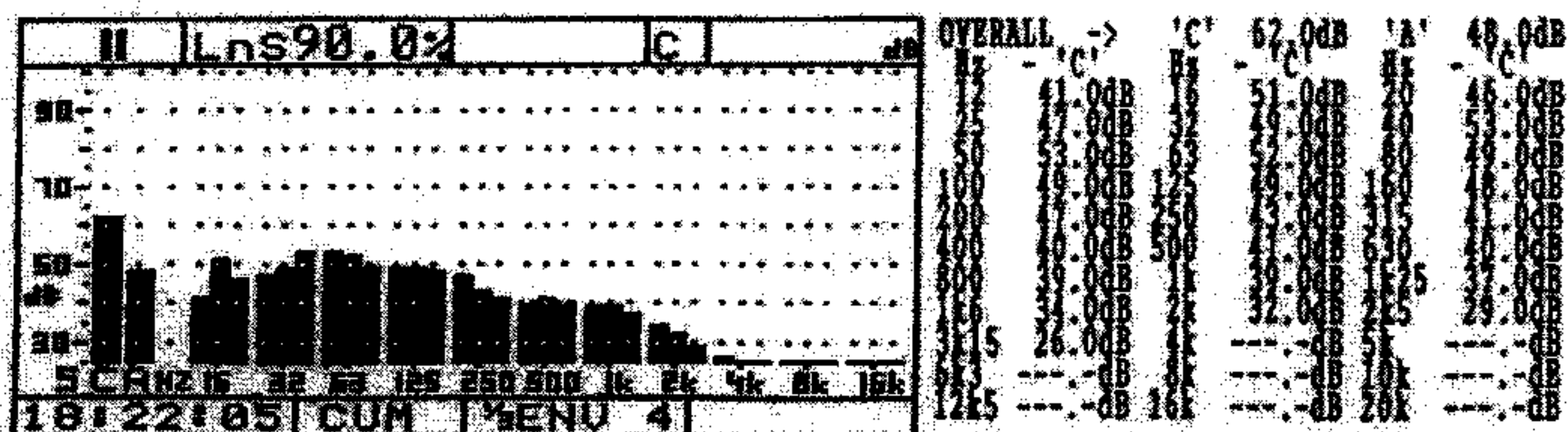
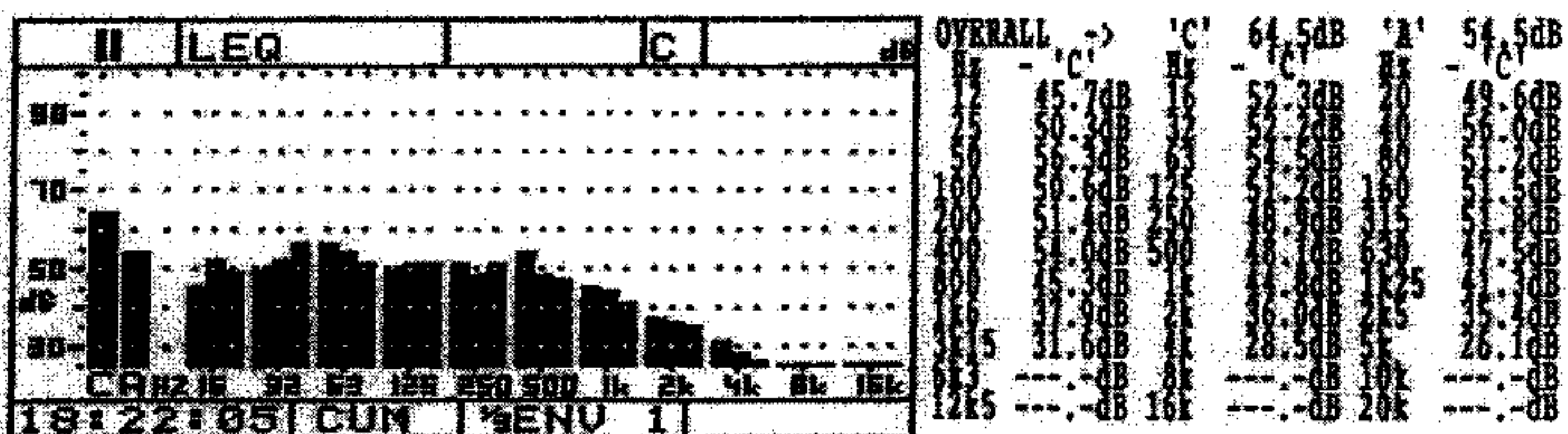
OVERALL ->		'C'	62.0dB	'A'	49.0dB
Hz	-	Hz	-	Hz	-
125	38.0dB	16	44.0dB	20	45.0dB
250	52.0dB	32	52.0dB	40	52.0dB
500	51.0dB	63	51.0dB	80	51.0dB
1000	51.0dB	125	48.0dB	160	49.0dB
2000	41.0dB	250	44.0dB	315	42.0dB
4000	39.0dB	500	41.0dB	630	41.0dB
8000	34.0dB	1k	38.0dB	1k25	38.0dB
16k	28.0dB	2k	32.0dB	2k5	30.0dB
315	28.0dB	4k	---	5k	---
630	---	8k	---	10k	---
1250	---	16k	---	20k	---

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CEL 593.CIT v 5.5

Start 07-AUG-06 18:22:05 Mode 1/3 ENV A005
 End 07-AUG-06 18:27:07
 Length 0 days 00:05:02
 Mic Free Field 200v ON Period 5 minutes

HEADER LAST CAL 16-JUN-06
 START 07-AUG-06 18:22:05
 END 07-AUG-06 18:27:07
 LENGTH 0 DAYS 00:05:02
 TIMED RECS 1 PER 5min
 MIC=FF 200U=ON TYPE=1
 S C.A Q3 MENU

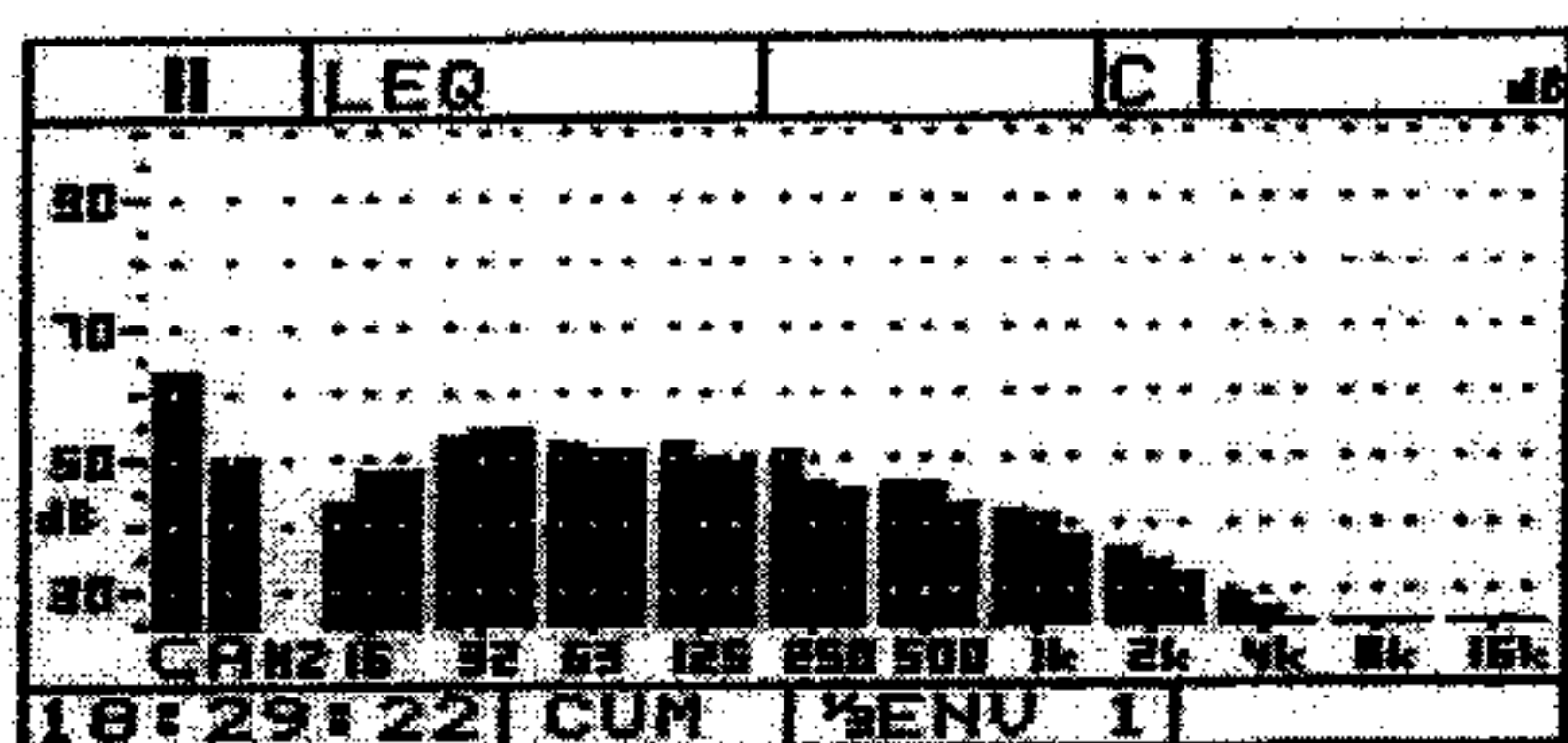


CEL Instruments Ltd.

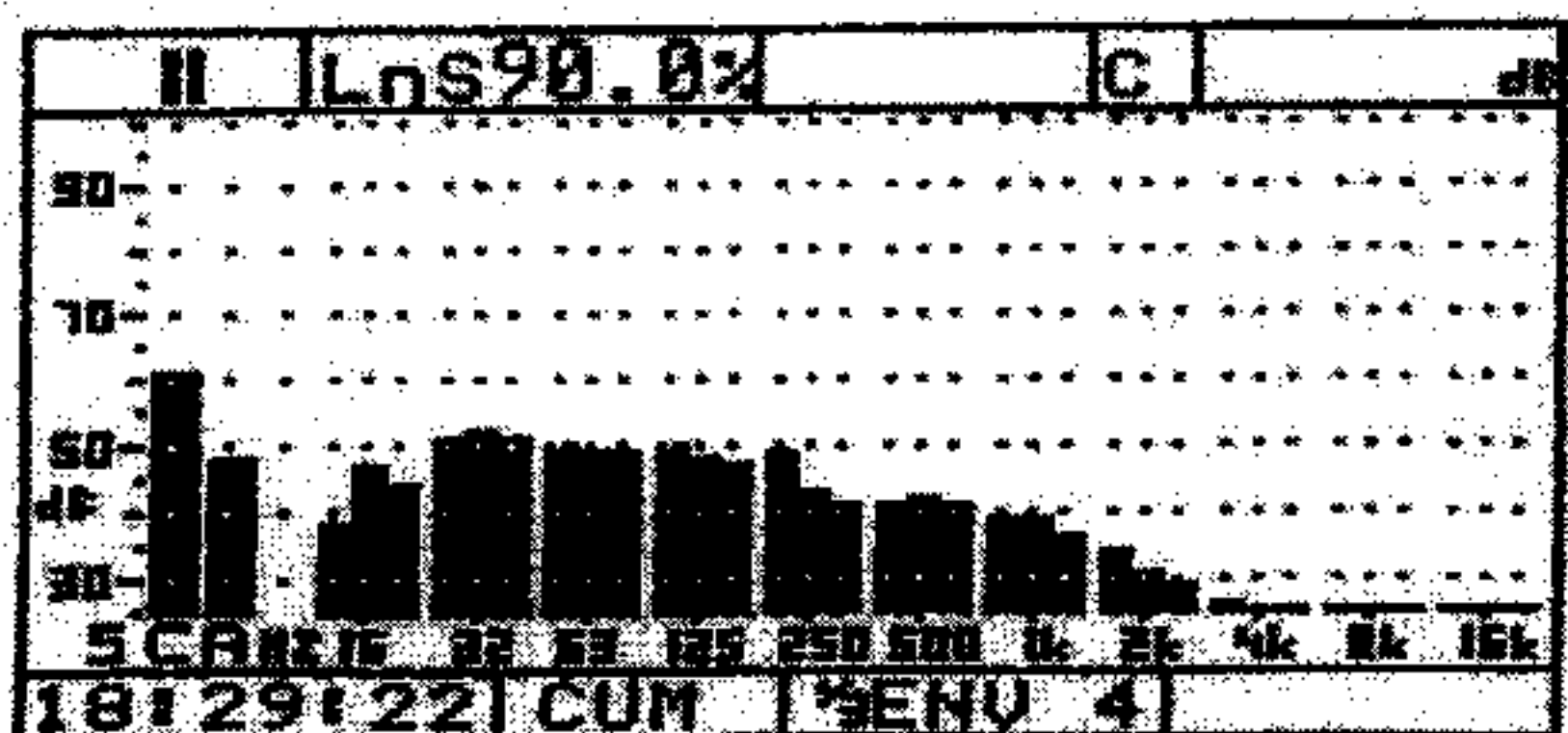
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 Mic Free Field 200v ON Period 5 minutes

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 START 07-AUG-06 18:29:22
 END 07-AUG-06 18:34:38
 LENGTH 0 DAYS 00:05:16
 TIMED RECS 1 PER 5min
 MIC=FF 200V=ON TYPE=1
 S C.A 03 %ENV



OVERALL	->	'C'	63.2dB	'A'	50.9dB
Hz		Hz		Hz	
125	43.5dB	125	48.9dB	20	48.6dB
250	43.7dB	250	54.8dB	40	54.6dB
500	42.7dB	500	51.7dB	80	51.9dB
1000	41.3dB	1000	49.0dB	160	50.0dB
2000	40.5dB	2000	46.7dB	315	45.3dB
4000	38.7dB	4000	41.1dB	630	43.3dB
8000	36.7dB	8000	38.8dB	1250	38.5dB
16000	35.7dB	16000	27.5dB	2500	32.2dB
31500	29.2dB	31500	27.5dB	5000	29.0dB
63000	26.0dB	63000	26.0dB	10000	26.0dB
125000	26.0dB	125000	26.0dB	20000	26.0dB



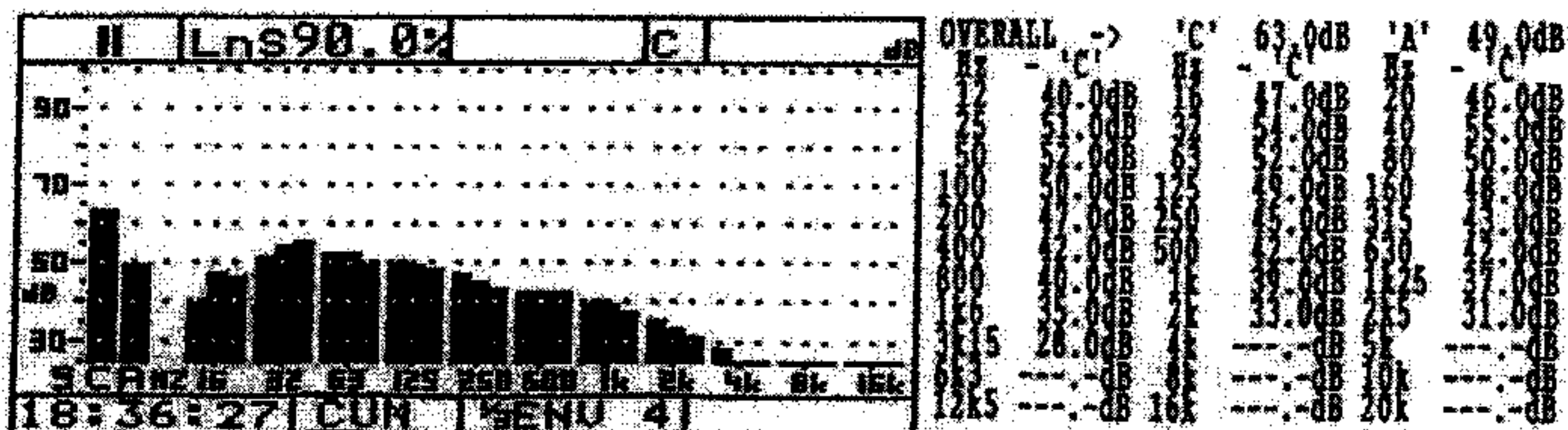
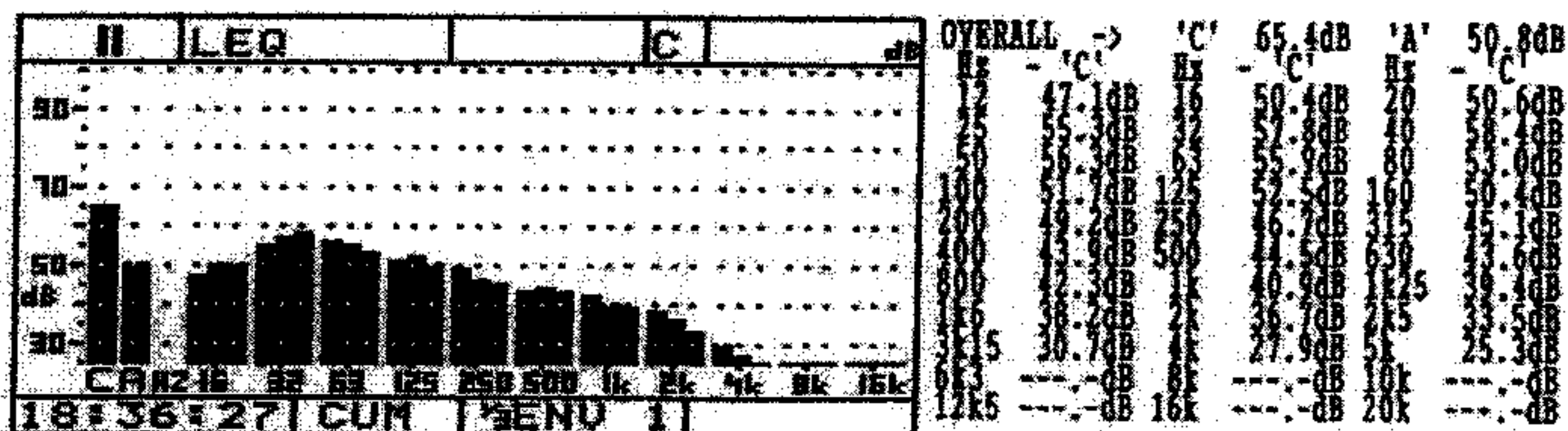
OVERALL	->	'C'	61.0dB	'A'	48.0dB
Hz		Hz		Hz	
125	38.0dB	125	47.0dB	20	44.0dB
250	31.0dB	250	52.0dB	40	51.0dB
500	30.0dB	500	48.0dB	80	49.0dB
1000	29.0dB	1000	43.0dB	160	47.0dB
2000	28.0dB	2000	43.0dB	315	41.0dB
4000	26.0dB	4000	31.0dB	630	36.0dB
8000	26.0dB	8000	31.0dB	1250	29.0dB
16000	26.0dB	16000	26.0dB	2500	26.0dB
31500	26.0dB	31500	26.0dB	5000	26.0dB
63000	26.0dB	63000	26.0dB	10000	26.0dB
125000	26.0dB	125000	26.0dB	20000	26.0dB

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CEL 593.CIT v 5.5

Start 07-AUG-06 18:36:27 Mode 1/3 ENV A007
 End 07-AUG-06 18:46:28
 Length 0 days 00:10:01
 Mic Free Field 200v ON Period 5 minutes

HEADER | LAST CAL 16-JUN-06
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 END 07-AUG-06 18:46:28
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 TIMED RECS 2 PER 5min
 MIC=FF 200V=ON TYPE=1
 S C.A 03 | SENU

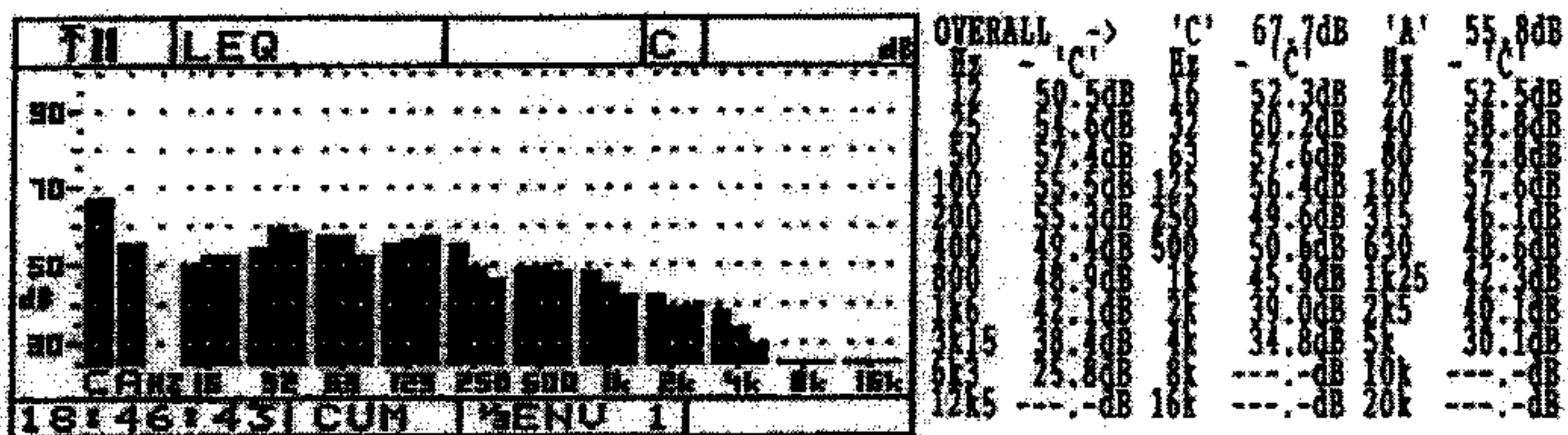


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CEL 593.CIT v 5.5

Start 07-AUG-06 18:46:43 Mode 1/3 ENV A008
 End 07-AUG-06 19:26:44
 Length 0 days 00:40:01
 Mic Free Field 200v ON Period 5 minutes

HEADER | LAST CAL 16-JUN-06
 START 07-AUG-06 18:46:43
 END 07-AUG-06 19:26:44
 LENGTH 0 DAYS 00:40:01
 TIMED RECS 8 PER 5min
 MIC=FF 200U=ON TYPE=1
 S C.A Q3 MENU

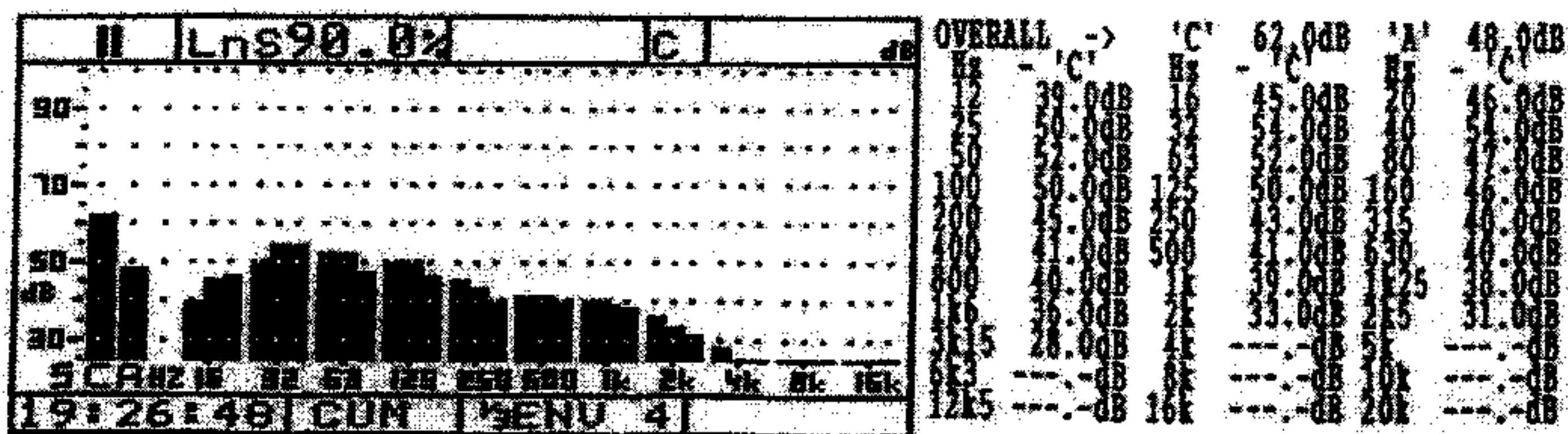
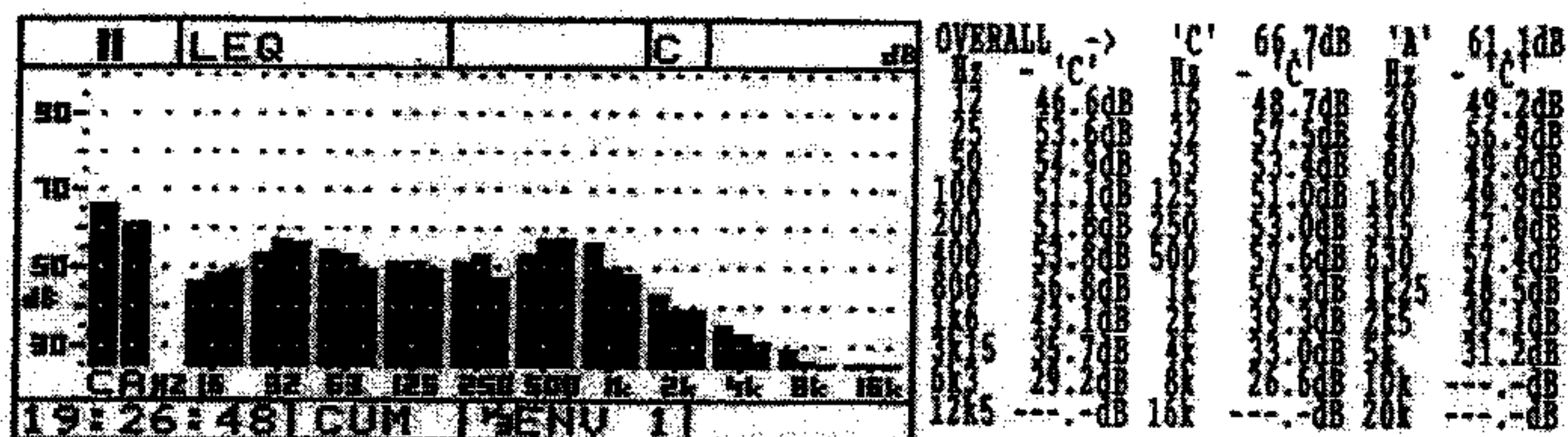


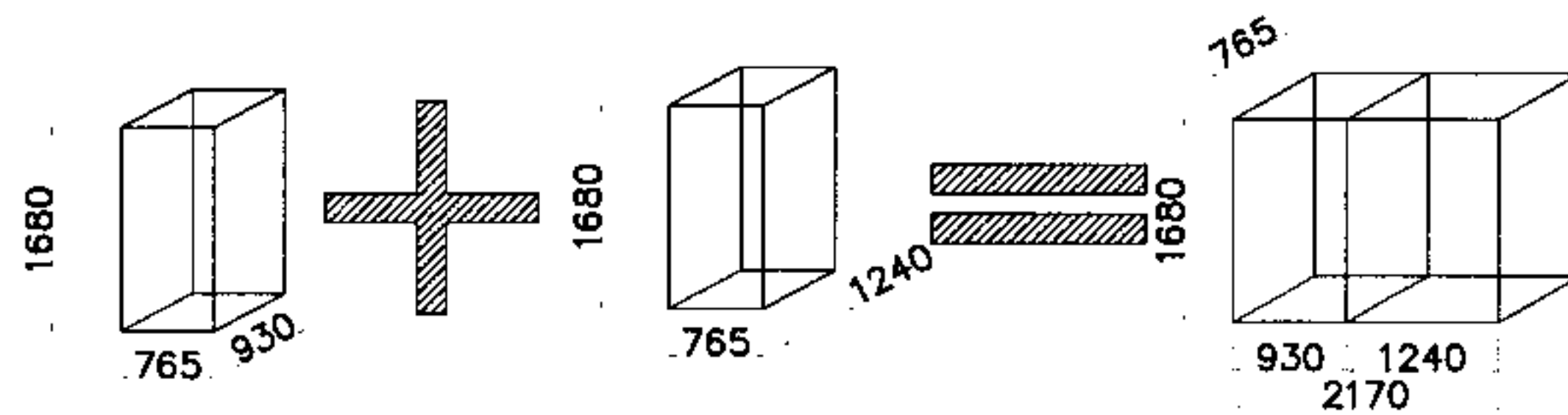
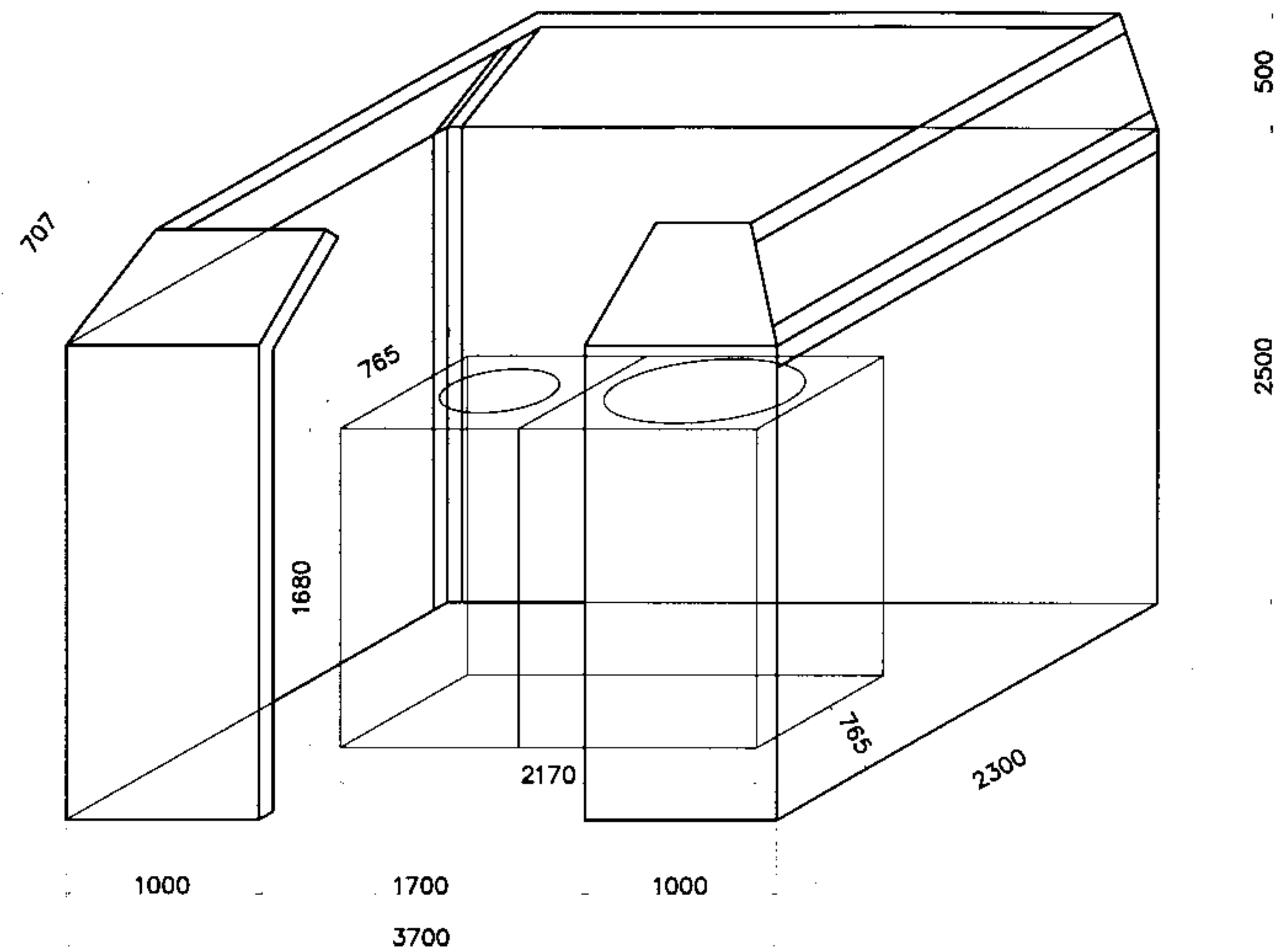
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CEL 593.CIT v 5.5


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Mic Free Field 200v ON Period 5 minutes

HEADER LAST CAL 16-JUN-06
START 07-AUG-06 19:26:48
END 07-AUG-06 19:31:50
LENGTH 0 DAYS 00:05:02
TIMED RECS 1 PER 5min
MIC=FF 200V=ON TYPE=1
S C.A 03 MENU 1





DO NOT SCALE

REV	DATE	DETAILS
CLIENT Heatherwick Studio	PROJECT Willing House, Grays Inn Road	DRAWN JDB
		CHECKED DJB
		SCALE A2, 1:100
TITLE General Arrangement of Proposed Acoustic Screen for Roof Plant		DATE 14/11/06
		DIMENSIONS MM
 dB Attenuation Ltd	Erskine House, Threshelfords Inworth Road, Feering Colchester, Essex CO5 9SE Tel : 01376 572787 Fax : 01376 572788 e-mail : design@dbattenuation.co.uk	
	Drawing No. dB1837/ga Revision No.	