

MANSFIELD ASSOCIATES

Structural Design Consultants

Contract 21 Chester Terrace.

Job No. 06484

Sheet No G-1.

Locate how.

Date Feb '07

Prepared by PM.

Groundwork loadings

See Roof Calculation Sheet R/1.

2nd, 2nd, 1st & Grd Floor.

$W = 1.50 \text{ kN/m}^2$

$U = \text{Boarding} = 0.15$

$\text{Dirt} = 0.17$

$\text{Carpet} = 0.16$

$\text{Total} = 0.48 \text{ kN/m}^2$ $\text{By } 2.00 \text{ kN/m}^2$

Shed walls

$2 \text{ layers Plaster} = 0.32$

$\text{Shed} = 0.14$

0.460 kN/m^2

NB. Halloway

Ad. 3rd floor = 0.72

$= 2.72 \text{ kN/m}^2$

Ground Floor
Halloway.

Proposed Alteration to lower Ground Floor

Beam < G/3 > Spc 1.8m

loading to Grd floor construction.

$\text{Plan} = 2.00 \times 3.4/2 = 3.40 \text{ kN}$

$+ \text{Shed wall} = (0.41 \times 3 \times 1.8) = (2.22 \text{ kN})$

$\therefore \text{So Max load} = 2.2 + (3.4 \times 1.8) = 8.32 \text{ kN/m}$

$\therefore M = 8.32 \times 1.8/8 = 1.87 \text{ kNm}$

$\text{Defl} = 8.32 \times 1.8^3 \times 2.23 = 60.11 \text{ mm}$

$\text{In } 178 \times 102 \text{ UB, } L = 180 \text{ mm, } r_y = 2.37 = 75.9 \text{ mm, } P_k = 22$

$\therefore M = 153 \times 154 \times 10^{-3} = 23.56 \text{ kNm} > 1.87 \text{ kNm}$

$\therefore \text{Use } 178 \times 102 \text{ UB}$

$\text{Buckling stress} = 0.42 \times 1.8 = 0.63 = 8.32/2 / 0.63 \times 100 = 66$

$\text{Use } 225 \times 145 \text{ mm UB}$
 use 9 plates

RECEIVED
21 MAR 2007

MANSFIELD ASSOCIATES

Structural Design Consultants

Contract 21 Chester Terrace

Job No. 06485

Sheet No G2

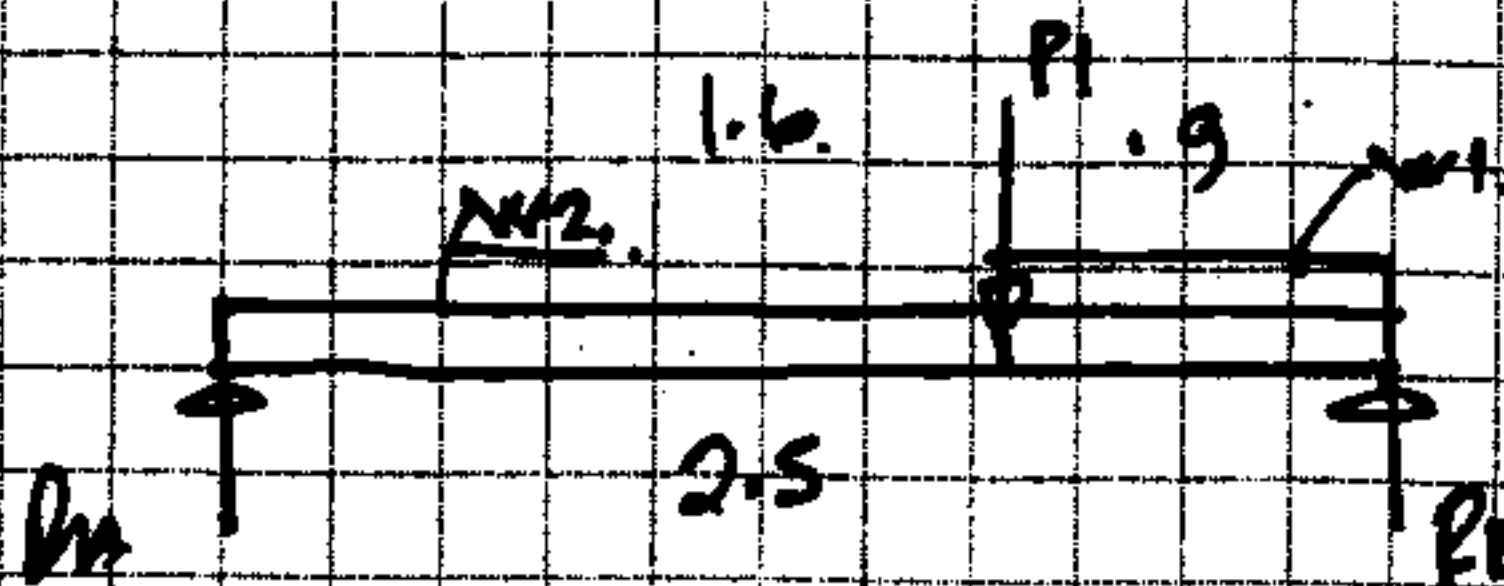
Regent Inn

Date Feb'07

Prepared by PM.

Beam $\langle G/1 \rangle$

span 2.5m.



P. Statical Imposed load (im.) (4.0 m.)

$$\text{flow} = 2.72 \times 1.3/2 = 1.76 \text{ kN}$$

weak to 1/2 up light

$$= 2.10 \times 1.5 \text{ m} = 3.150 \text{ kN} / 4.91 \text{ kN}$$

$$\therefore 4.91 \leq 6.0 \times 4/2 = 12 \text{ kN} = P_1$$

$$W_2 = 2.72 \times 3 \text{ m} = 8.16 \text{ kN}$$

$$W_1 = \text{Static - up } 3.2 \text{ kN}^2 \times 2 = 6.4 \text{ kN}$$

$$R_A = (8.16 \times 1.25) + \frac{12 \times 0.9}{2.5} + \frac{(6.4 \times 0.9)}{2.5} \times 0.45$$

$$= 10.20 + 4.32 + 1.036 = 15.55 \text{ kN}$$

$$R_B = 10.20 + 7.68 + 4.72 = 22.60 \text{ kN}$$

$$\therefore P_2 = 15.55 / 8.16 = 1.9 \therefore \text{Whole PL.}$$

$$\therefore M = 15.55 \times 1.6 - 8.16 \times 1.6/2 = 24.88 - 10.44 = 14.43 \text{ kNm}$$

$$\text{Q. up } 14.43 \times 8 / 2.5 = 46.19 \text{ kN}$$

$$I. L. 46.19 \times 2.5^2 \times 2.23 = 643.8 \text{ cm}^4$$

$$I. 203 \times 133. U.B. 30. L. 250 r_y = 3.17 = 78.8$$

$$\therefore W_2 = 150 \times 280 \times 10^{-3} = 42 \text{ kN} > 14.43$$

$$\text{Squash} = 22.60 \times 10^3 / 0.65 \times 100 = 358$$

Use 203x133x30UB

$$15.55 \times 10^3 / 0.65 \times 100 = 246 = \frac{400 \times 100 \times 246 \text{ kN}}{300 \times 100 \times 180 \text{ kN}} \text{ spread}$$

RECEIVED
21 MAR 2007

MANSFIELD ASSOCIATES

Structural Design Consultants

Contract 21 Chester Row

Job No. 06485

Sheet No G3

Royce Park

Date Feb '07

Prepared by PM.

Beam < G27

Span 4.2m

loady: wall. Col - 1st. (b/w) 2.5 x 3.3. 8.25

Wall load: $2.72 \times 2.5/2 = 3.50$

Min. W. load: $2.0 \times 1.3 = 0.6$

12.350 kN/m

$\therefore$ Total load = $12.35 \times 4.2 = 51.87 \text{ kN}$

12.35 kN

Max $52 \times 4.2/8 = 27.3 \text{ kNm}$

I req. $52 \times 4.2^2 \times 2.23 = 2045 \text{ cm}^4$

In $203 \times 133 \times 30 \text{ UB}$. $420/3.17 = 132$. $1/11.5$ Allow

$\therefore M = 280 \times 110 \times 10^{-3} = 30.8 \text{ kNm} >$

However In $203 \times 203 \text{ UC } 46$. $I = 4168 > 2045$

$L = 420/5.13 = 81.8$. $1/18.7$. $1/60 \text{ UB}$

$\therefore M = 150 \times 450 \times 10^{-3} = 67.5 \text{ kNm} > 27.3 \text{ kNm}$

$\therefore$ Use $203 \times 203 \times 46 \text{ UC}$

Beam h beam: $25 \times 1.48 = 38.4 \text{ kN}$ further load

Use 20.4 N/mm^2 steel is $1:4$

In 215×215 plain steel to resist walls

$\therefore$ Use with 340 mm (eff.) area 215×215

$f_k = 6.4 \text{ N/mm}^2$. $\gamma_m = 3.5$. $B = 2500/340 = 7.35$. $\therefore$ 0.88

Max load: 0.76 . $\therefore \frac{6.4 \times 215 \times 215 \times 0.88 \times 0.76}{3.5} = 56.5 \text{ kN} > 38.4$

$\therefore$ OK Use

$215 \times 215 \text{ plain}$

RECEIVED
21 MAR 2007

MANSFIELD ASSOCIATES

Structural Design Consultants

Contract 21 Chester Terrace

Job No. 06485

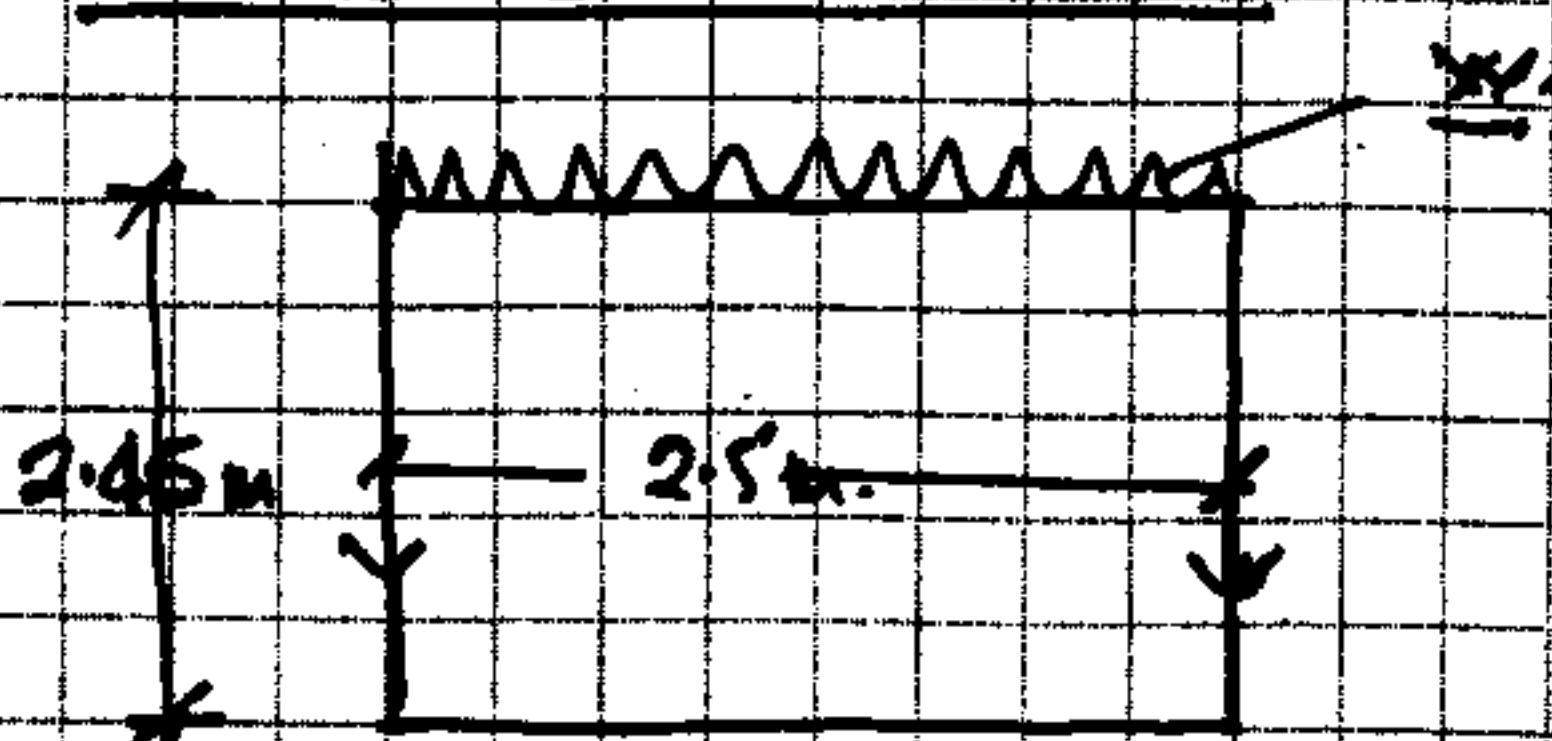
Sheet No G4.

Regents Park

Date Feb '07

Prepared by. R.M.

Box Frame A°



Loads

Roof = 0.

3rd Flr = $2.0 \times 7/2 = 7.0$

2nd Flr. = $2.0 \times 7/2 = 7.0$

1st Flr = $2.0 \times 7/2 = 7.0$

Grd Flr = $2.72 \times 1.3/2 = 1.76$

Wall Grd - 3rd Flr. $10.2 \times 2.8 = 28.56 / 48.26 \text{ kN/m}$

in E/F. Partitions = $3 \times 3.5 \times (1.2 \text{ kN/m}^2) = 12.60$
 60.86 kN

$\therefore$ Grd Flr Beam = $60.86 \times 2.5 = 152 \text{ kN}$ Reactions = 76 kN

$M = 152 \times 2.5/8 = 47.5 \text{ kNm}$

Beam supports 215mm wall. T_1 203x203x4 UC

$I_x = 250$ $y = 5.13 = 48.73$ $D/t = 18.72$ $P_{ex} = 180 \text{ kN}$

$\therefore$ $M_x = 180 \times 48 \times 10^{-3} = 8.64 \text{ kNm} > 47.5 \text{ kNm}$ Use 203x203x4 UC

Check Col. 2. Imposed load = 10% vehic load = 15.2 kN

$\therefore M = 15.2 \times 1.2/2 = 9.12 \text{ kNm}$ Reactions = 4.56 kN

(Contd)

RECEIVED
21 MAR 2007

MANSFIELD ASSOCIATES

Structural Design Consultants

Contract 21 Chester Towace.

Job No. 06 485

Sheet No GS'

Recons from

Date. Feb. 07.

Prepared by. Lm.

Col. Cuts

Try 203x203 UC 46

$P = 76 \text{ kN}$

Area 58.7 cm^2 $I_x = 450$

$r_y = 5.13$

$L = 2400 \times 8\% = 2040 \text{ mm}$

$P_{cr} = 180 \text{ kN}$

$L/r = 2040/5.13 = 397$

$\lambda = 139 \text{ N/mm}^2$

$M = 10 \text{ kNm}$

$$f_c = \frac{76 \times 10^3}{58.7 \times 10^2} = 12.9 \text{ N/mm}^2$$

$$12.9 / 139 = 0.093$$

$$f_{cr} = 10 \times 10^3 / 180 = 55.6 \text{ N/mm}^2$$

22.5

$$22.5 / 180 = 0.125$$

$$0.216 < 1.0$$

$\therefore$ Col Beam as Beam at Col Plate level

$203 \times 203 \times 46 \text{ UC}$

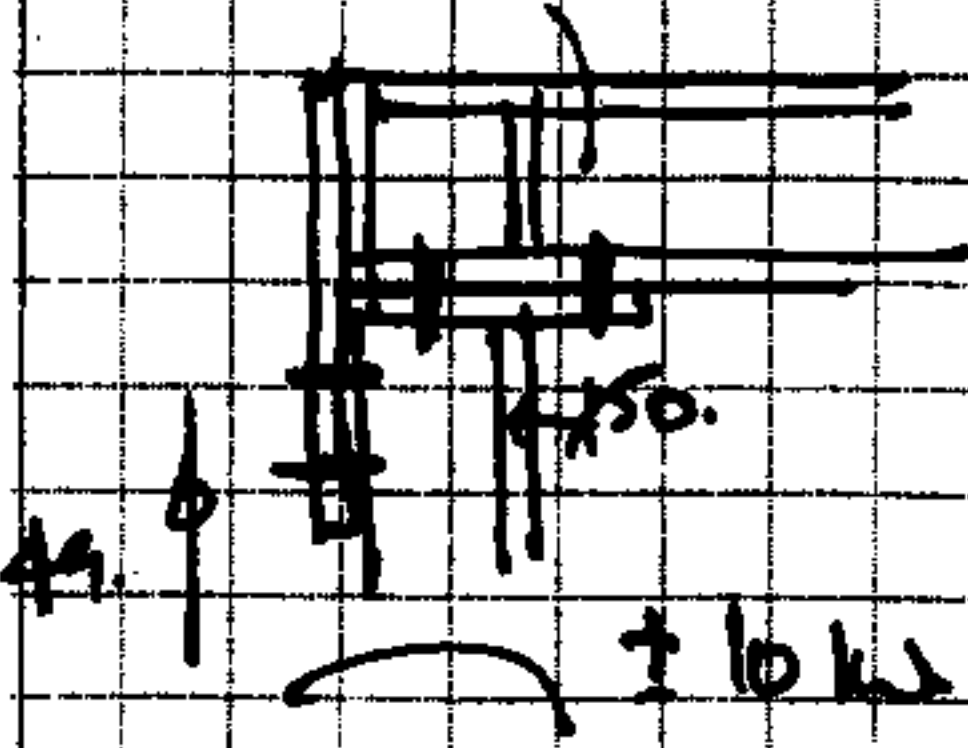
Connections:

Use M20 grade 8.8 bolts

$$10 / 203 = 49 \text{ kN}$$

Provide 12mm plate welded to UC beams.

from full profile fitted weld



Use grade 8.8 bolts

to resist shear 49 kN

Provide 4 M20 grade 8.8 bolts

$$Capacity = 200 \text{ kN}$$

Check tension 20 kN

$$10 / 253 = 39 \text{ kN}$$

$$19.1 \text{ kN/bolt}$$

$\therefore$ Use 4

M20 grade 8.8 bolts

cap d base plate

$$20 \text{ bolts} = 137.4 \text{ kN}$$

$$> 39 \text{ kN}$$

Check plate:

RECEIVED
21 MAR 2007

MANSFIELD ASSOCIATES

Structural Design Consultants

Contract 21 Cluster Terrace

Job No. 06485

Sheet No GB

Report Rev.

Date Feb '07

Prepared by PM.

Base plate calc.

Design: Two bolts 39.1kN @ 0.09m
from edge of web.

$\therefore M, 39.0 \times 0.09 = 1.98 \text{ kNm}$ (moment in plate)

$\therefore 200 \text{ mm} \quad \sqrt{\frac{1.98 \times 6}{200 \times 180}} = 18.03 \text{ mm}$

Use 20mm thick Cap & base
plate welded to UC with full
profile butt fillet welds.