

Now includes
'A' rated window

A

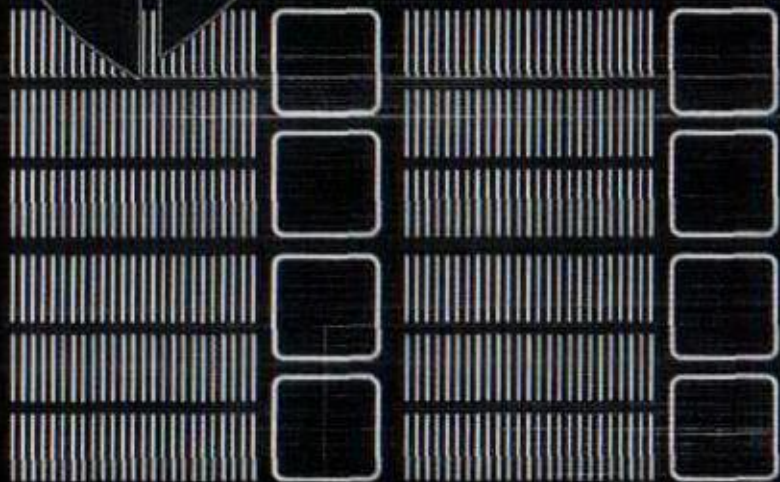
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SHIELD



SPECIFICATION GUIDE

Effective from February 2008

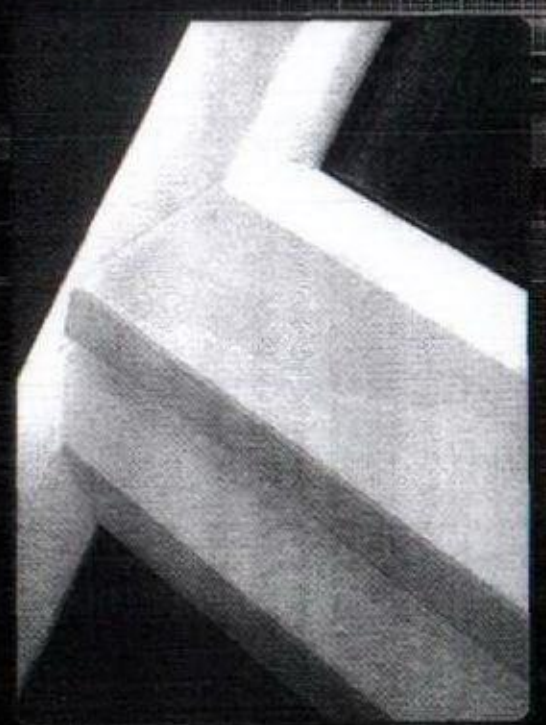
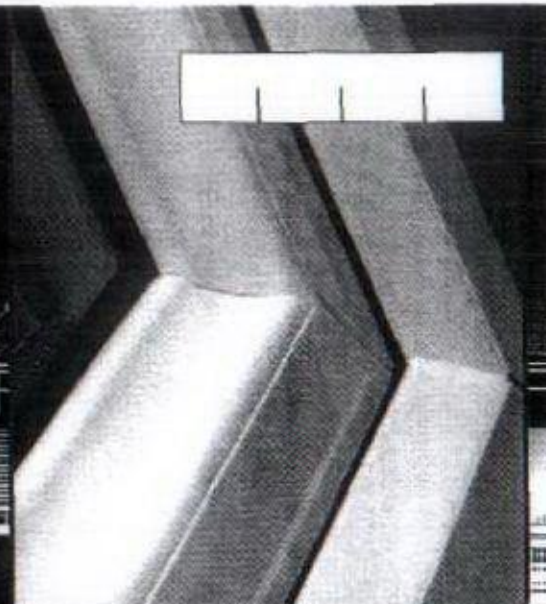


TECHNICAL DATA

ACCREDITATIONS

SCHEMATICS

FAQs





ABOUT SYNSEAL

Synseal is a systems company with a difference. It has been involved at all levels in the PVC-U window industry. It started in 1980 and within 18 months of opening the first shop Synseal had opened 13 showrooms across the East Midlands. Later Synseal added a fabrication facility and by 1987 1,000 frames were being fabricated a week with a nationwide customer base. In 1991 Synseal started extruding profile.

The success of the fabrication business meant Synseal was in direct competition with some customers. That's why it pulled

out of the domestic market in 1991. And why it pulled out of fabricating in 1995. At that time Synseal was fabricating 2,200 frames a week. This business was sold to JBS Industries - and is still a strong business today.

Today Synseal is number one in window and conservatories an achievement no other company has attained. More fabricators choose Synseal than any other company. So it's hardly surprising that one-in-every windows and one-in-four conservatory roofs are made with Synseal products.

The Shield window and door system was launched in 1999. This guide contains details of the accreditations, frequently asked questions, schematics and technical data.

In addition to the window system, Shield offers a conservatory roof system.



All information in this manual is provided for guidance only. Synseal Ltd cannot be held responsible for the way in which the information in this manual is interpreted.

We reserve the right to alter specifications and descriptions without prior notice as part of our policy of continuous development. All dimensions are in millimetres. 1:10 not to scale drawings.

SHIELD



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Details of the accreditation of Synseal Ltd and its subsidiaries and their products and services.

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FAQS

Frequently Asked Questions relating to technical aspects, quality assurance and window/door performance.

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Cross section drawings of Shield windows and doors.

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TECHNICAL DATA

Technical data relating to window and door performance.

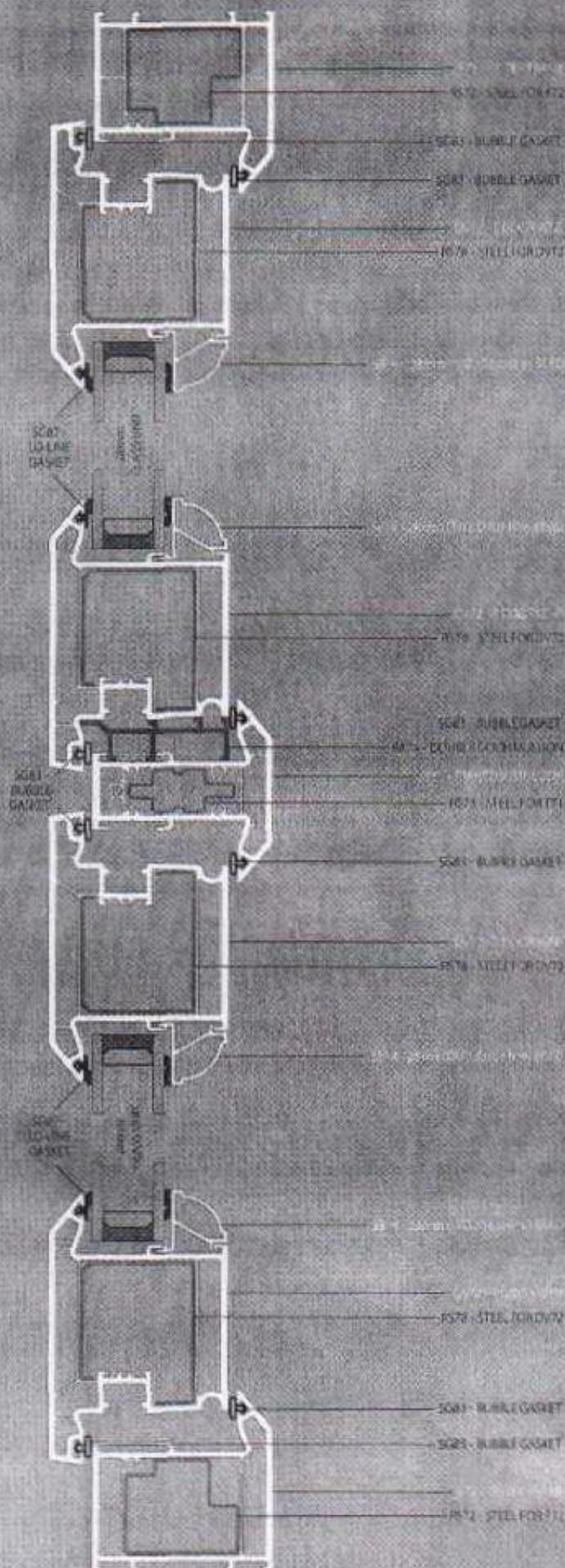
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SCHEMATICS

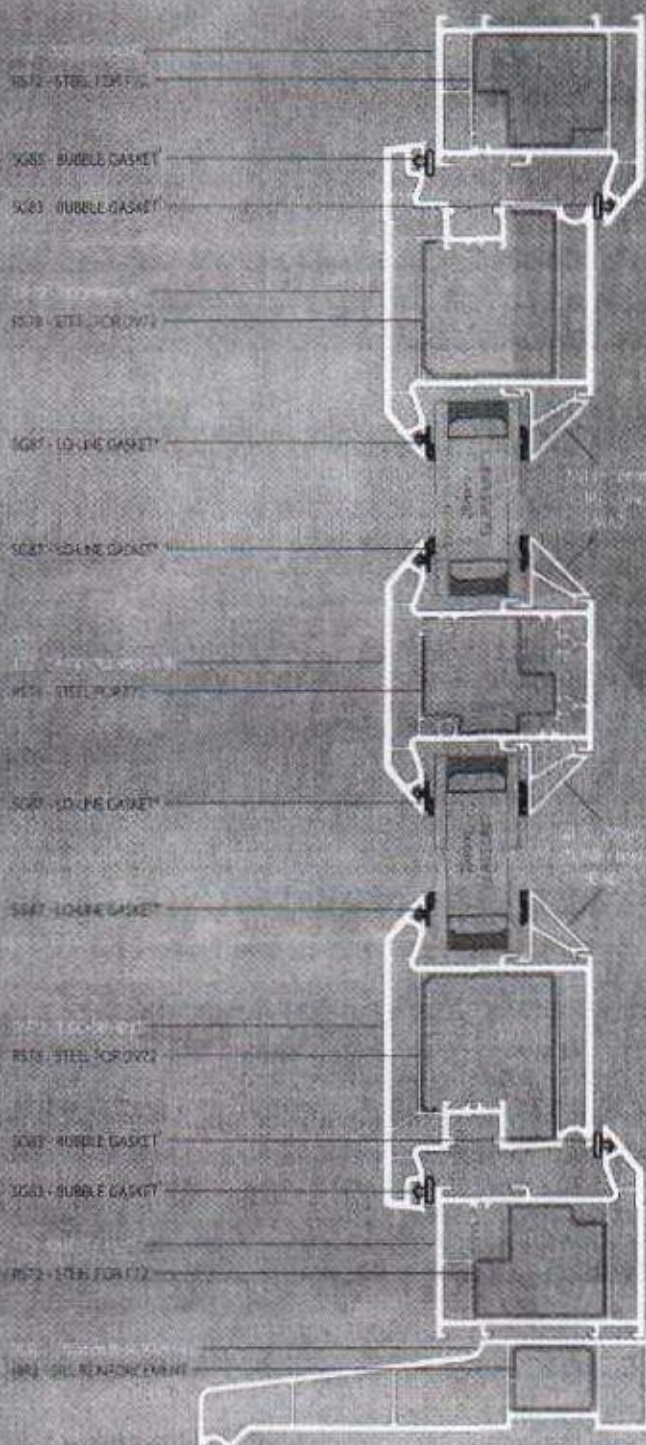
KEY: = PLASTIC = ALUMINIUM = RUBBER = STEEL = FOAM = GLASS = SEALANT = VARIOUS/OTHER

Please note: not both levels of different blurring possible at the same time

DOUBLE DOOR



RESIDENTIAL DOOR



© 2000 by The McGraw-Hill Companies

7244 Buck Creek is available in only 2 other crv.

Department of Civil and Environmental Engineering

NGH • ZEPHYRUS • 1959 • THE UNIVERSITY OF MICHIGAN • KAPLAN • 1959



TECHNICAL DATA

MAIN TECHNICAL DETAILS

Name	Shield Join System for windows and doors
Grade Reference	SYN10 White 01
Material	Acrylic modified high quality impact resistant white in plastic and Polyurethane extrusion to produce a rigid multi-chambered structure.
Physical Properties	Comply with BS EN 12608:2001
Colours	Marigold, White, Cherrywood, Golden Oak, Anthracite Grey, Black Brown, Dark Red, Burgundy, Steel Blue (Oxford) and Dark Green (Brookland)
Appearance	Smooth finish, No obvious joint surface/finishing
Surface Finish	Resistant against UV light to prevent excessive colour drift. Meets requirements of BS EN 12608 when used in the EU Moderate climate.
Weldability	For the determination of the weldability of profiles, welded joints are tested in accordance with EN 12608. The calculated mean stress at maximum of each corner shall not be <25 N/mm ² for the tensile bending test of BS 5135. For the compression bending test, each individual value shall not be <20 N/mm ² for the tensile bending test and not be <30 N/mm ² for the compression bending strength.
Glass & Glazing	Subject to manufacture in accordance with the Special Technical Manual recommended by the manufacturer. Windows and doors will comply with the requirements of the standard.

Physical Properties of PVC-U Type A Material Grade Ref. SYN10 White 01	
Sound Insulation	>30dB in vacuum
Thermal Conductivity at 20°C	Typical test value 0.15 W/m deg C. PVC-U has a low thermal conductivity and is virtually constant over a wide temperature range.
Heat Reversion	To BS EN 12608 Clause 5.5 (Test method 1) at 120°C. When tested in accordance with Annex B, the mean reversion reversion value for individual samples shall not be greater than 2% for profiles and greater than 1% for the variation between individual four sides of the same sample shall not be greater than 0.4% for profiles and 0.2% for glazing beads.
Heat Aging	To BS EN 12608 Clause 5.7 (Test method 3) at 150°C. When tested in accordance with Annex B, the profile shall show no bubbles, cracks or delamination.
Resistance of impact at low temperature	To BS EN 12608 Clause 5.6 (Annex 2 - Test method 1) from -15 N/mm ² at -10°C. When manufacturing, sun of equipment used with profiles are tested in accordance with EN 471, no more than one sample shall exhibit cracking through the entire wall thickness of the profile in either face.
Heat Resistance/Softening Point	To BS EN 12608. When tested to ISO 830 method B, Minimum heat softening point 73°C. Typical result 82°C. This is well above the requirements of the UK wall Glazing specifications.
Apparent Modulus of Elasticity	To BS EN 12608 minimum requirement 2200 mpa value, when tested to ISO 178 typical result 2350 mpa.

Resistance of impact Strength after Artificial Ageing	To BS EN 12608:2001. Minimum 50% of original value specified when tested to EN 573
Colour Fastness	After exposure in accordance with EN 513 moderate B2 climate zone the change in colour between the unexposed test specimens expressed in ΔE* that not be >4.2 for test 3.3. The demarcation of the change in colour is in accordance with EN 513.
Bulk Density of Powder Blend	Typical test value 0.91 g/cm ³ . Minimum requirement: None specified.
Specific Gravity of Profile	Typical test 1.072 g/cm ³ . Minimum requirement: None specified.

PROFILE STORAGE

Profile Storage:

The profiles should be stored in a suitable area preferably under cover, not in direct sunlight. If the profile is stored on racks, it must be supported at least 1 metre intervals of the entire profile length. If stored on the floor, the floor must be even and the profile placed on a protective board base.

The stock storage temperature should be maintained between 10°C and 20°C. Working with profiles in colder conditions can result in warpage.

If the profile has been stored in a separate storage area with lower temperatures, it must be allowed for the profile to reach working temperature.

Profile cut ends by working should be stored in a dry area with the same ambient temperature of 10°C-25°C. Care must be taken if profiles are stored vertically so as not to damage the point of the mixer (check concentration of these particles to working).

All cut profiles must be worked within 48 hours as this will avoid contamination of the cut ends and avoid any absorption of moisture, which could have an effect on the weld strength.

AVAILABLE PROFILE COLOURS*



White
C121



Mahogany
(Also available for roofs)
2097/53



Golden Oak
(Also available for roofs)
80001



Cherrywood
(Also available for roofs)
8015/36/17



Dark Green (Brookland)
5125



Anthracite Grey
7316



Black Brown
8518



Dark Red (Burgundy)
3081



Steel Blue (Oxford)
5150

*Please note: the tools for this page should be used as a guide only and are not intended to be a permanent record.



TECHNICAL DATA

SAFE WORKING CAPACITIES OF REINFORCEMENTS

FROM BPF CODE OF PRACTICE FOR THE SURVEY OF PVC & ALUMINIUM DOORS

KEY: ALUMINIUM

Bay-pole Load-bearing Capacity

The load-bearing capacity of a bay pole depends upon two factors:

1. The Least Radius of Gyration
2. The Effective Length of the pole

The Least Radius of Gyration is given by:

$$r = \sqrt{\frac{I}{A}}$$

where I is the moment of inertia (Joules) and A is the cross-sectional area of the pole.

The effective length of a pole is determined by the fixity of its ends. If the pole is fixed in position at both ends, but not restrained in direction, then the effective length is the actual length of the pole divided by the cosine of the angle.

If the pole is effectively held in position and restrained at both ends, then the effective length is only 70% of the actual length (this condition will only apply if the pole is fixed to the structure so that it will not move until the column starts to buckle).

The Slenderness Ratio of the bay pole can then be calculated by dividing the effective length by the least radius of gyration. The maximum permissible stress for that length of bay pole can then be obtained from the graph below. The actual load that can be applied is then given by multiplying the allowable stress by the cross-sectional area.

CW have done this for the most commonly used standard bay poles and posts, see tables and graphs in this section.

52.5mm dia BAY POLE - RA75

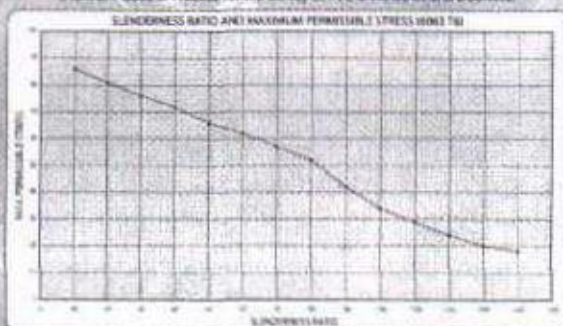
Data supplied by Sider & Bates - Consulting Civil & Structural Engineers - Nottingham

HEIGHT (mm)	SLENDERNESS RATIO	PERMISSIBLE STRESS (N/mm ²)	CAPACITY (kN)
100	27.9	24.1	15.1
200	55.8	20.3	19.0
300	83.7	18.8	24.5
400	111.6	18.2	31.9
500	139.5	17.7	40.7
600	167.4	17.2	50.7
700	195.3	16.7	61.9
800	223.2	16.2	74.3
900	251.1	15.7	87.9
1000	279.0	15.2	102.7
1100	306.9	14.7	118.7
1200	334.8	14.2	135.9
1300	362.7	13.7	154.3
1400	390.6	13.2	173.9
1500	418.5	12.7	194.7
1600	446.4	12.2	216.7
1700	474.3	11.7	239.9
1800	502.2	11.2	264.3
1900	530.1	10.7	289.9
2000	558.0	10.2	316.7



SLENDERNESS RATIO AND MAXIMUM PERMISSIBLE STRESS (ALUMINIUM GRADE 6063 T6)

From BPF Code of Practice for the Survey of PVC & ALUMINIUM DOORS



SAFE WORKING CAPACITY OF 52.5mm dia BAY POLE - RA75



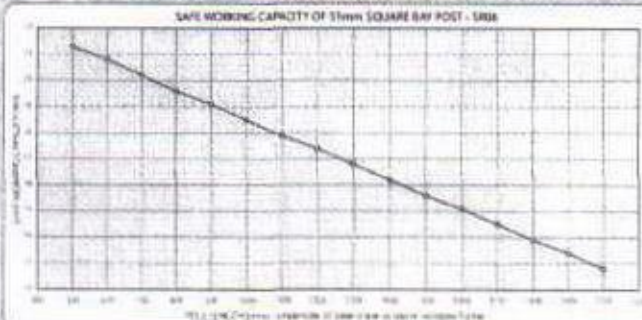
55mm SQUARE BAY POST - SR06

Data supplied by Sider & Bates - Consulting Civil & Structural Engineers - Nottingham

HEIGHT (mm)	SLENDERNESS RATIO	PERMISSIBLE STRESS (N/mm ²)	CAPACITY (kN)
100	27.9	24.1	15.1
200	55.8	20.3	19.0
300	83.7	18.8	24.5
400	111.6	18.2	31.9
500	139.5	17.7	40.7
600	167.4	17.2	50.7
700	195.3	16.7	61.9
800	223.2	16.2	74.3
900	251.1	15.7	87.9
1000	279.0	15.2	102.7
1100	306.9	14.7	118.7
1200	334.8	14.2	135.9
1300	362.7	13.7	154.3
1400	390.6	13.2	173.9
1500	418.5	12.7	194.7
1600	446.4	12.2	216.7
1700	474.3	11.7	239.9
1800	502.2	11.2	264.3
1900	530.1	10.7	289.9
2000	558.0	10.2	316.7



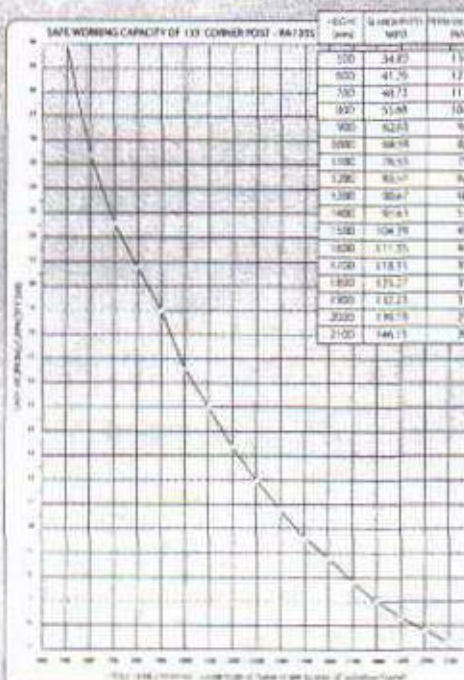
SAFE WORKING CAPACITY OF 55mm SQUARE BAY POST - SR06



135° CORNER POST - RA1355

Data supplied by Sider & Bates - Consulting Civil & Structural Engineers - Nottingham
Based on: Working Stress on Aluminium

HEIGHT (mm)	SLENDERNESS RATIO	PERMISSIBLE STRESS (N/mm ²)	WORKING CAPACITY (kN)	FIXED CAPACITY (kN)
100	27.9	24.1	15.1	26.4
200	55.8	20.3	19.0	35.3
300	83.7	18.8	24.5	45.7
400	111.6	18.2	31.9	58.7
500	139.5	17.7	40.7	74.3
600	167.4	17.2	50.7	92.7
700	195.3	16.7	61.9	113.9
800	223.2	16.2	74.3	137.9
900	251.1	15.7	87.9	164.7
1000	279.0	15.2	102.7	194.3
1100	306.9	14.7	118.7	226.7
1200	334.8	14.2	135.9	261.9
1300	362.7	13.7	154.3	300.3
1400	390.6	13.2	173.9	341.9
1500	418.5	12.7	194.7	386.7
1600	446.4	12.2	216.7	434.7
1700	474.3	11.7	239.9	485.9
1800	502.2	11.2	264.3	540.3
1900	530.1	10.7	289.9	597.9
2000	558.0	10.2	316.7	658.7





SAFE WORKING CAPACITIES OF REINFORCEMENTS

ORDER INFORMATION: Table of data on the safety of PVC-U window and doors.

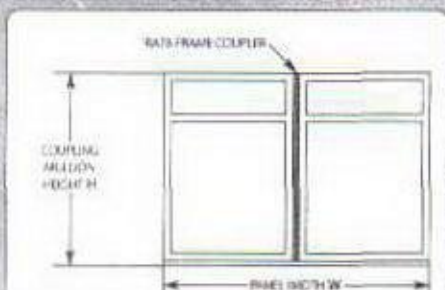
KEY: ALUMINIUM

ALUMINIUM COUPLER - RA76

Data supplied by: Schweizer Aluminium Ltd - Structural Engineers - UK/Italy

Graph colour key: ● 1.2kN ● 1.5kN ○ 2.0kN ○ 2.5kN

MAX PANEL WIDTH (mm) W	1.2kN	1.5kN	2.0kN	2.5kN	1.2kN	1.5kN
1,200	1805	4073	2862	2562	1480	1060
1,500	4288	3055	2244	1560	1096	799
2,000	3519	2444	1795	1248	877	633
2,500	2932	2035	1486			

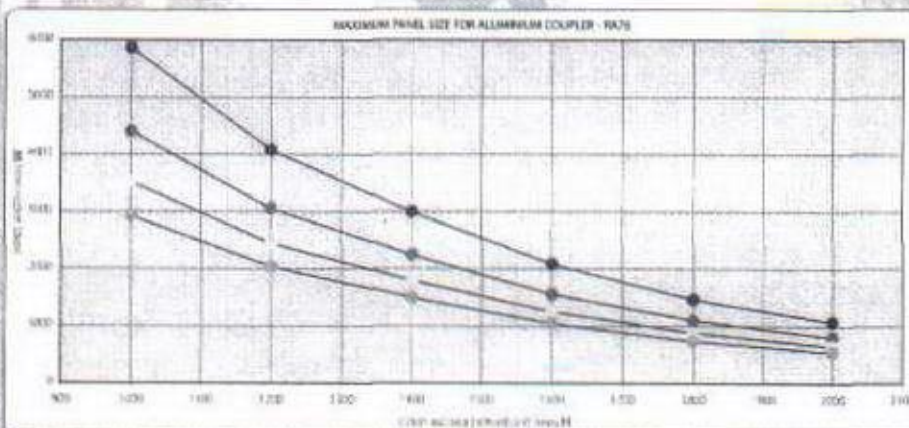


Min maximum panel width is equal to the combination of both frames and the chosen RA76 Coupling Profile.

Information is not applicable for conservatories (outer frame must be fixed to structure at either side using standard required window industry fixing practices).

The panel loading only sections are constrained to be laterally supported by glazing panel and/or transoms.

None of the calculated maximum panel width includes the strength of the two outer frames which will make a contribution to the combined strength.



PVC-U WINDOWS IN FIRES

Information from Langate Technology Ltd

Introduction

PVC-U exhibits specific fire behaviour and does not burn once the source of heat or flame has been removed.

Building Regulations

UK Building Regulations do not stipulate any fire performance standards for the material used in window frames, whilst no degree of fire resistance (as defined by BS 476 part 2) can be achieved by PVC-U window units, the large scale fire tests carried out show no difference between PVC-U and wood under the conditions of test.

PVC-U can, when correctly formulated, achieve high ratings (usually Class 1 surface spread of flame) when performance is assessed to BS 476 part 6 and 7.

Ignition and burning response

PVC-U is very difficult to ignite using commonly available ignition sources (match, cigarette, etc.). Tests with a wide variety of sources, varying in heat intensity and impingement area, on PVC-U window frames show that the product only burns whilst the source is applied. When the source is removed there is no residual flame on the product. In terms of ignitability, the temperature required to ignite PVC-U is more than 120°C higher than that of pine wood (0.8°C for PVC-U and 260°C for wood as defined for BS 476 part 6). Once a material has been ignited the flammability can be defined in terms of the Limiting Oxygen Index (LOI).

This defines the amount of oxygen that needs to be present for a material to burn freely. A material with an LOI of 21 will burn freely in air which contains 21% oxygen and one with an LOI of more than 21 will not burn in air at room temperature.

PVC-U has an LOI of approximately 32, compared with wood at an LOI of 21. This shows that PVC-U will not sustain combustion in air at room temperature and is better than wood in this test.

The limited burning of PVC-U is confirmed in a variety of other standard tests which measure specific parameters, such as rate of heat release and flame spread under different conditions.

The conclusions are clear:

1) The rate of heat release and total heat released by PVC-U are significantly lower than most other building materials.

2) When flames do contact PVC-U, it forms a protective charred layer which insulates the material below and excludes the oxygen necessary for combustion. This restricts the burning zone to a depth of only a few millimetres in a combustion situation.

3) PVC-U is very difficult to ignite using common ignition sources.

Smoke and fumes

Smoke is the result of incomplete burning of a material and consists of solid or liquid particles in the combustion gases. Smoke densities are similar to wood under unshielding conditions, but smoke under flaming conditions. The combustion gases (CO, HCl) may lead to more confusion of materials, materials, but not to a significant increase in the toxicity of the combustion gases of PVC-U. A smoke test, and certainly not significantly worse than those of many natural materials, the bulk of PVC-U samples will be less than those of many natural materials of a similar toxic potency. The rate of generation and quantity of smoke and fumes produced by a PVC-U window will depend on the severity of the source applied. The smoke and fumes emitted will be confined to the area of the product affected by the source and then transport away from the impingement zone will depend on local factors such as ventilation and survival of the glazing.

In a typical domestic fire the PVC-U window frames will not markedly affect the progress of the fire or the possibility of personal injury. Most deaths in fires are caused by smoke or fume inhalation. In a typical domestic fire the occupants are likely to suffer from the inhalation effects from burning carpets, curtains, etc. before the PVC-U in the window frames has even begun to emit smoke or fumes.



Fire resistance

The fire resistance of a glazed window is mainly influenced by the failure behaviour of the glazing at high temperatures. The fire resistance of glazed PVC-U window frames is generally found to be similar to that of glazed wood window frames.

Large scale fire tests

In a research programme carried out by the Fire Research Station, the performance of PVC-U window frames in fires was compared with that of traditional wood frames in a typical domestic room. All windows were double glazed and both a large fuel load (non-ventilated controlled fire) and a medium fuel load (ventilation controlled fire) were used.

The conclusions of the report were:

- 1) Little damage was evident to both PVC-U and wood windows until the glass panes were displaced at approximately 200°C to 400°C. Glass panes failed by cracking and falling out in a random manner.
- 2) After failure of one glass pane the increased ventilation changed the mode of the fire and accelerated the fire growth. In most tests the other panes fell out soon after.
- 3) Wood frames burned after the displacement of the glass while the PVC-U window frames collected and the complete specimens fell out. There was some evidence of combustion of the PVC-U, but PVC-U windows did not show any adverse effects which would create new supplies in the burning buildings.
- 4) Smoke products produced mainly from the wooden fuel under low ventilation conditions was the major factor tested in each test and was produced in volumes that would prove lethal in regions where ambient temperatures would allow survival.
- 5) The concentrations of carbon monoxide were noticeably lower in the fire involving only PVC-U frames. This was possibly caused by a lower rate of burning in this test.

Summary

The basic PVC-U material has good fire properties and PVC-U windows give a satisfactory performance in fires compared with other materials.

SOUND TRANSMISSION THROUGH WINDOWS

SHIELD Canada's Building Division and the U.S. Coast



Introduction

In addition to their primary function as visual openings, windows also transmit sound. This is of concern not only for the exterior surfaces of a building but also for interior applications ranging from office spaces to control booths in recording studios. Sound transmitted through windows often limits the overall acoustical insulation.

Sound transmission through windows is governed by the same physical principles that affect walls, but practical noise control measures are influenced by the properties of glass and the characteristics of the window assemblies. Increasing the glass thickness, for example, gives greater noise reduction at most frequencies, but the stiffness of glass limits the improvement. Using multiple layers (double or triple glazing) increases noise reduction at most frequencies, but this is dependent on the separation of the layers.

As with most building assemblies, transmission of sound through walls may drastically reduce the effective noise reduction. This is of particular concern for operable windows even windows with good weatherstripping have reduced noise reduction because of air leakage. Most of the data presented in this report are for sealed windows.

The acoustic terms used in this report are as follows:
decibels (abbreviated to dB)

Sound Transmission Loss (TL) which is a standardized measure of the noise reduction in decibels for specific frequency ranges.

Sound Transmission Class (STC) is a single figure rating of sound insulation, calculated by fitting a standard contour to the TL data. It is most commonly used in North America.

Sealed single glazing

The TL for a large thin plate would theoretically increase by 6 dB for each doubling of the sound frequency or the mass if the effect of stiffness was ignored. Although single glazing does approach this mass law behaviour at some frequencies, the stiffness of the glass and the limited use of typical windows cause significant deviations from this prediction (see fig. 1 on page 23).

The sharp decrease in TL at specific frequencies is called the "coincidence dip" and is caused by bending waves in the glass panel. Above the coincidence frequency, laminated glass can provide much higher TL than solid glass. This is apparently due to damping (dissipation of vibrational energy) by the plastic interlayer.

Sealed double glazing

The TL of double glazing is strongly dependent on the masses of the cavity between the two layers of glass. The STC rating increases as the air space increases (see fig. 2 on page 23). On each doubling of the air space, the STC increases by approximately 3. The STC also increases with increasing glass thickness.

If the separation between the panes is small, the STC rating is only slightly higher than that for a single pane of the same glass. This occurs because the air in the space between the two panes acts like a spring, transferring vibrational energy from one pane to the other. This resonance falls within the range of 250 to 400 Hz for a unit with a small air gap (see fig. 3 on page 23). Most of the energy from aircraft or heavy traffic falls within this frequency range, but by increasing the air space and using heavier glass, the resonant frequency can be lowered to improve the insulation against such noise sources.

Sealed triple glazing

Despite the widespread belief that adding another layer of glass must be beneficial, triple glazing provides essentially the same noise reduction as double glazing unless the air gap is very large. Figure 4 (on page 23) compares TL data for a double glazed window with that for a triple glazed window of similar total thickness.

Designing for noise control

In most cases where substantial noise control is required, double glazing is the most sensible choice. The airspace should be sufficiently large to provide the desired TL.

Using differing thicknesses of glass for double glazing gives greater noise reduction. The highest STC values shown in figure 2 are for double 6mm glass windows with 1mm substituted for one of the 6mm panes would have equal or higher STC ratings.

The use of laminated glass has also been shown to reduce sound transmission.

Figure 1
Sound transmission loss (TL) for sealed single glazing

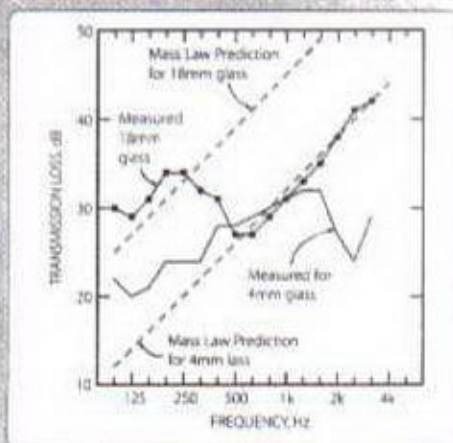


Figure 2
Sound transmission class (STC) versus interpane spacing for double glazing

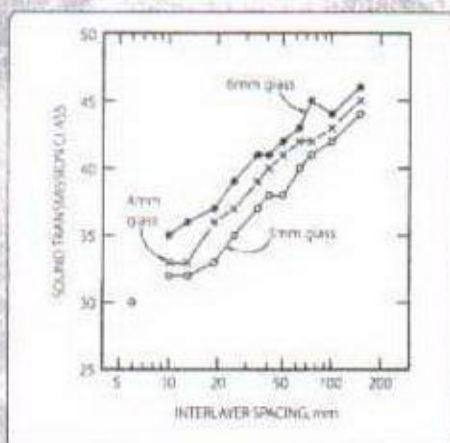


Figure 3
The effect of a small airspace on TL of double glazing

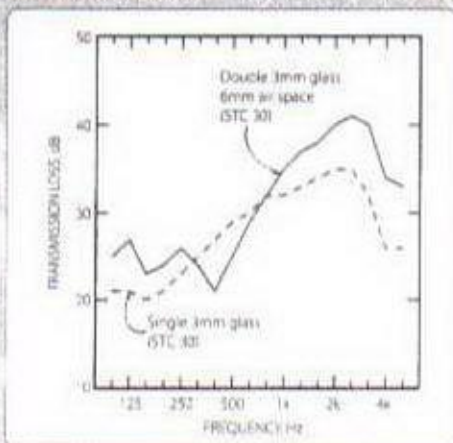


Figure 4
TL of double and triple glazed windows

