OW/JG/6250/11

23rd December 2011

Gil Levy
Claridge House
Suit 1
32 Davies Street
London
W1K 4ND

Dear Gil,

RE: 63 SHELTON STREET – DAYLIGHT & SUNLIGHT

Further to recent correspondence, GIA have undertaken a Daylight and Sunlight analysis of the proposed scheme from A3D Ltd Architects for 63 Shelton Street in relation to the surrounding properties. Our analysis considers the impact of the scheme in accordance with the BRE Guidelines methodology in regards to Daylight and Sunlight.

In terms of daylight, three different forms of analysis have been undertaken in accordance with the different methodologies outlined in the BRE Guidelines, and in respect of sunlight those windows and residential properties which face within 90° due south have been assessed in sunlight in accordance with the BRE Guidelines methodology.

The site is located at 63 Shelton Street, Camden. This is a dense urban location where the existing daylight potential in many of the surrounding properties is already very limited, as can be evidenced by the existing daylight levels shown in the results attached to this letter. The proposal entails the addition of one storey to the existing building at roof level. We have assessed the potential impact of this additional massing on those properties in the vicinity of the site with the potential to be affected. Daylight and Sunlight are only considered sensitively in relation to residential properties, and therefore it is the impact of the residential properties on which our analysis focuses. In this case, the only residential property within the vicinity of the site is 1 –28 Betterton House. This property is located to the rear of the site and has windows facing in a south-east direction towards the proposed massing. Drawings 6250/01 – 03 and 6250/07 – 09 (attached to this letter) illustrate the existing site and the proposed development and give an understanding of the 3D context of this area.

Our analysis of the proposal shows that in daylight terms almost all the windows in Betterton House will meet with the BRE Guidelines recommendations in respect of the Vertical Sky Component (VSC) form of daylight analysis. There are only five windows which do not meet the VSC recommendations however, these windows generally do so due to poor existing levels of daylight which are very low and all beneath 10% VSC. When even small reductions are expressed as a percentage of these already low existing values it is easy for the recommended 20% reduction margin in the BRE Guidelines to be breached, as is the case for these five windows. However, when the absolute reductions are considered, it can be seen that the loss as a result of the proposal is actually minimal.

We would consider these reductions to be typical for a dense urban location of this type and within the flexibility inferred in the BRE Guidelines, which were construed primarily in relation to a suburban environment. Therefore, we consider the daylight impact of the proposal to be acceptable.

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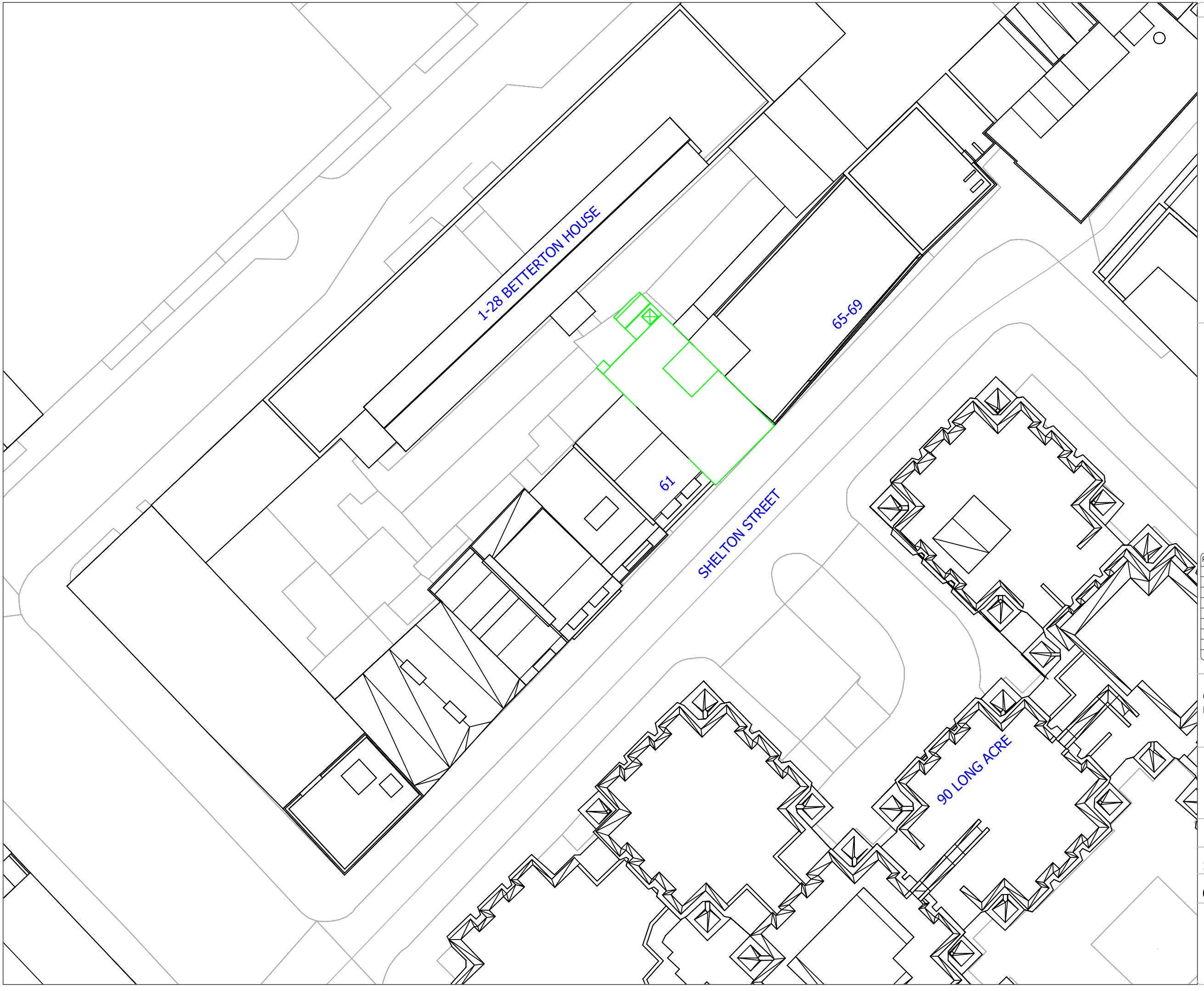
In sunlight terms, it is also the case that the majority of the windows which have been assessed meet the BRE Guidelines recommendations. However, there are a few windows that technically show reductions beyond the levels recommended in the BRE Guidelines. Again it is the case that the majority of these windows which exceed the reductions have very poor existing levels of sunlight which render compliance with the BRE Guidelines very difficult, particularly in respect of the winter levels of sunlight. In absolute terms it can be seen that the reductions as a result of the proposal are actually not excessive by any means and generally of a level of 2% or 3% APSH at most. Therefore, again we consider this slight reduction to be within the flexibility inferred in the BRE Guidelines for this type of dense urban location. Therefore, we consider the sunlight impact of the proposal to also be acceptable.

Therefore in summary, GIA have analysed the impact of the proposed development of the site upon the neighbouring residential property at Betterton House. Our analysis shows that generally the recommendations within the BRE guidelines will be complied with in respect of daylight and sunlight for all but a few windows. Generally those windows which exceed the recommendations do so due their poor existing levels of daylight and sunlight which reflect disproportionate reductions when expressed as a percentage of their very low existing values. However, in absolute terms the reductions are minimal and we consider them to be acceptable given the dense location of the site.

Kind regards,

Yours sincerely,
For and on behalf of GIA

OLIVER WESTLAKE
SURVEYOR
oliver.westlake@gia.uk.com



Sources of Information

GIA
PHOTOGRAPHS
IR1-6250 - FIND OS MAP

A3D LTD ARCHITECTS
IR2-6250 (13-12-11)
IR3-6250 (13-12-11)

Notes

Indicative Only

ALL HEIGHTS GIVEN IN mm AOD

Rev	Date	Description	Initials
A		Initial Issue	

Project

63 SHELTON STREET
LONDON

Title

SITE PLAN
EXISTING SCENARIO

Scale	Date
1:250 @ A3	DEC'11
Drawn	Checked
IA	JH

Drawing No.	Rel No.	Revision
6250-01	01	A

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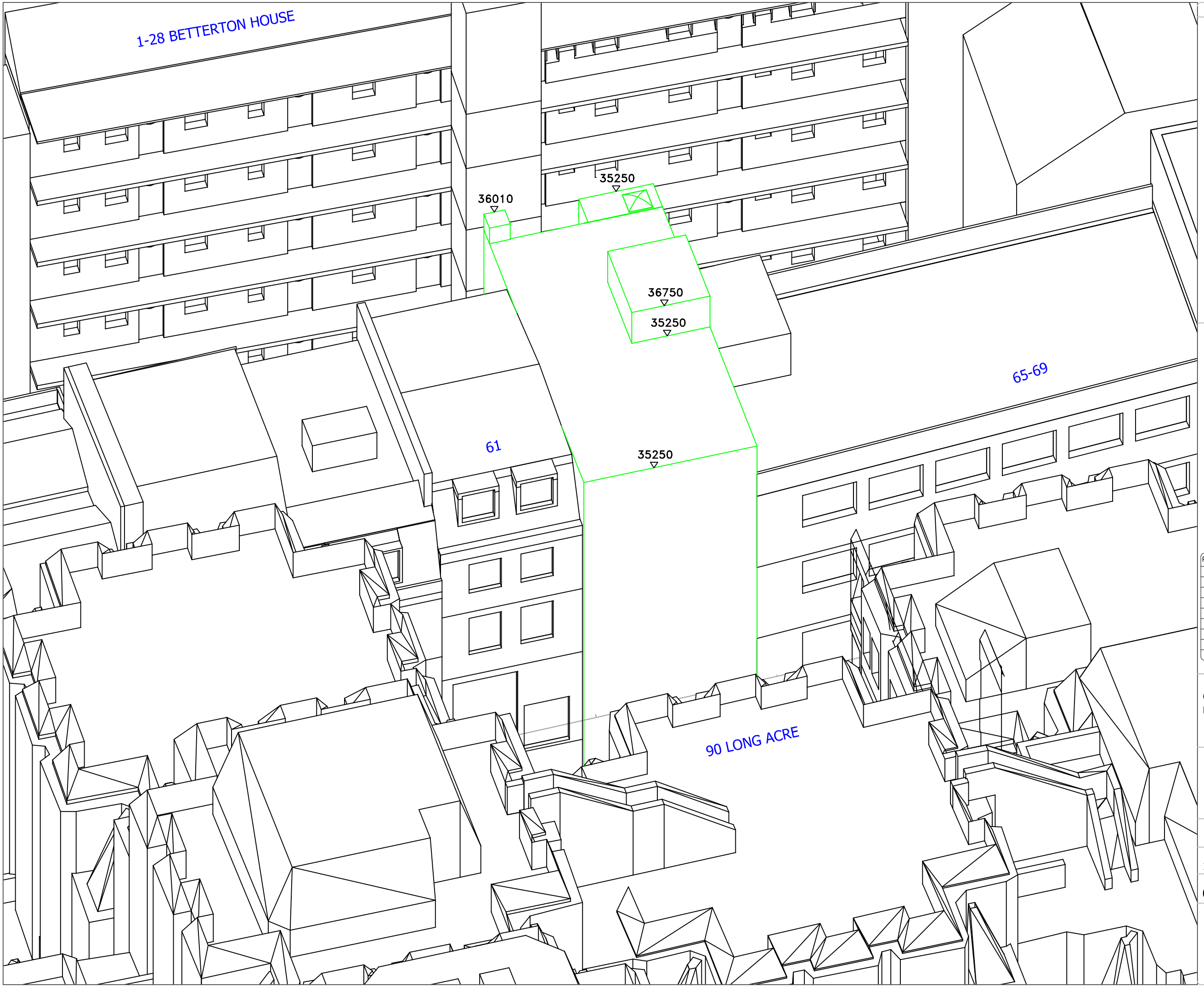

Sources of Information

GIA
PHOTOGRAPHS
IR1-6250 - FIND OS MAP

A3D LTD ARCHITECTS
IR2-6250 (13-12-11)
IR3-6250 (13-12-11)

Notes

N.B. DO NOT SCALE OFF THIS DRAWING

ALL HEIGHTS GIVEN IN mm AOD

Rev	Date	Description	Initials
A		Initial Issue	

Project

63 SHELTON STREET
LONDON

Title

3D VIEW
EXISTING SCENARIO

Scale	Date
NTS	DEC'11
Drawn	Checked
IA	JH

Drawing No.	Rel No.	Revision
6250-02	01	A

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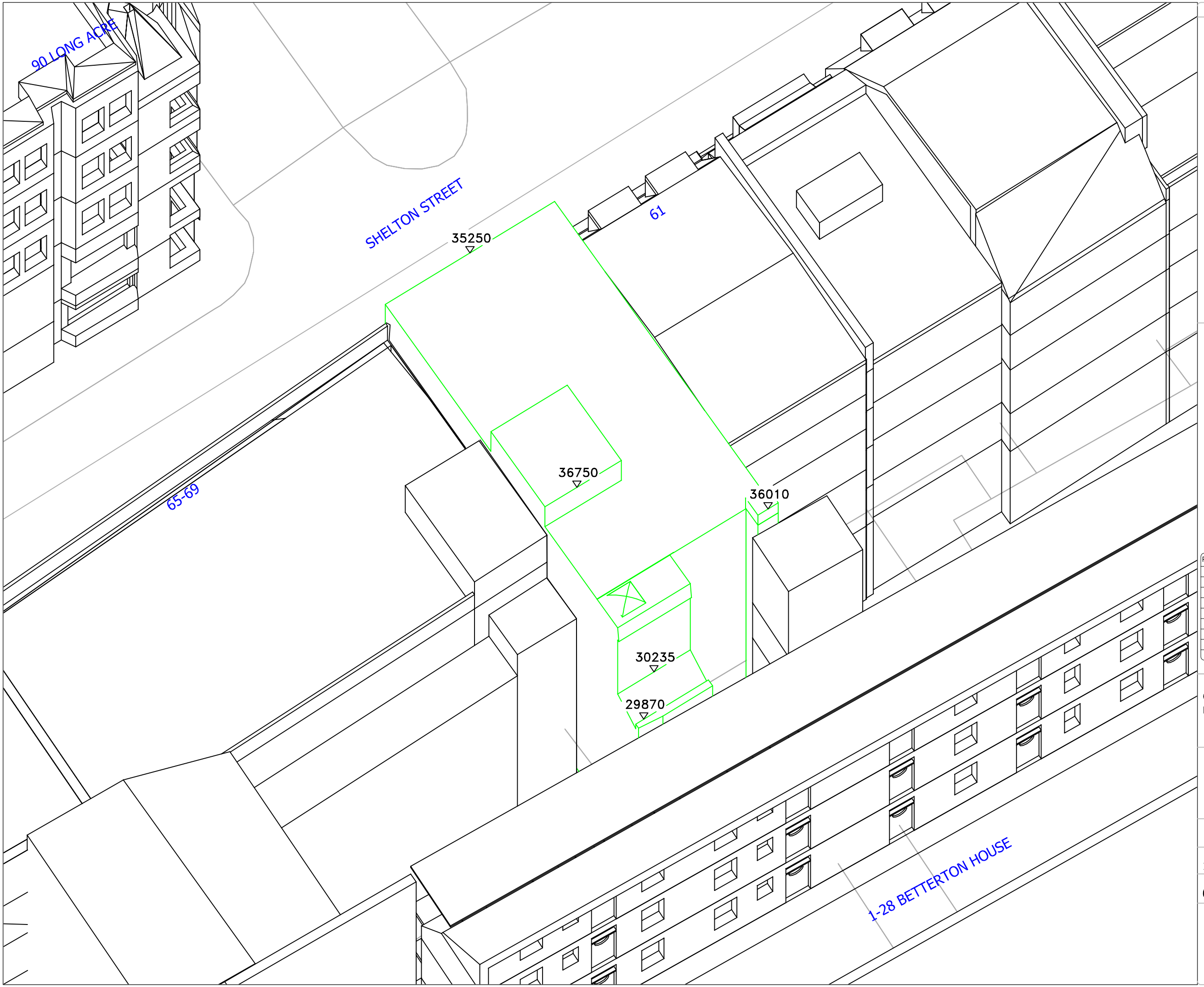

Sources of Information

GIA
PHOTOGRAPHS
IR1-6250 - FIND OS MAP

A3D LTD ARCHITECTS
IR2-6250 (13-12-11)
IR3-6250 (13-12-11)

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ALL HEIGHTS GIVEN IN mm AOD

Rev	Date	Description	Initials
A		Initial Issue	

Project

63 SHELTON STREET
LONDON

Title

3D VIEW
EXISTING SCENARIO

Scale	Date
NTS	DEC'11
Drawn	Checked
IA	JH

Drawing No.	Rel No.	Revision
6250-03	01	A

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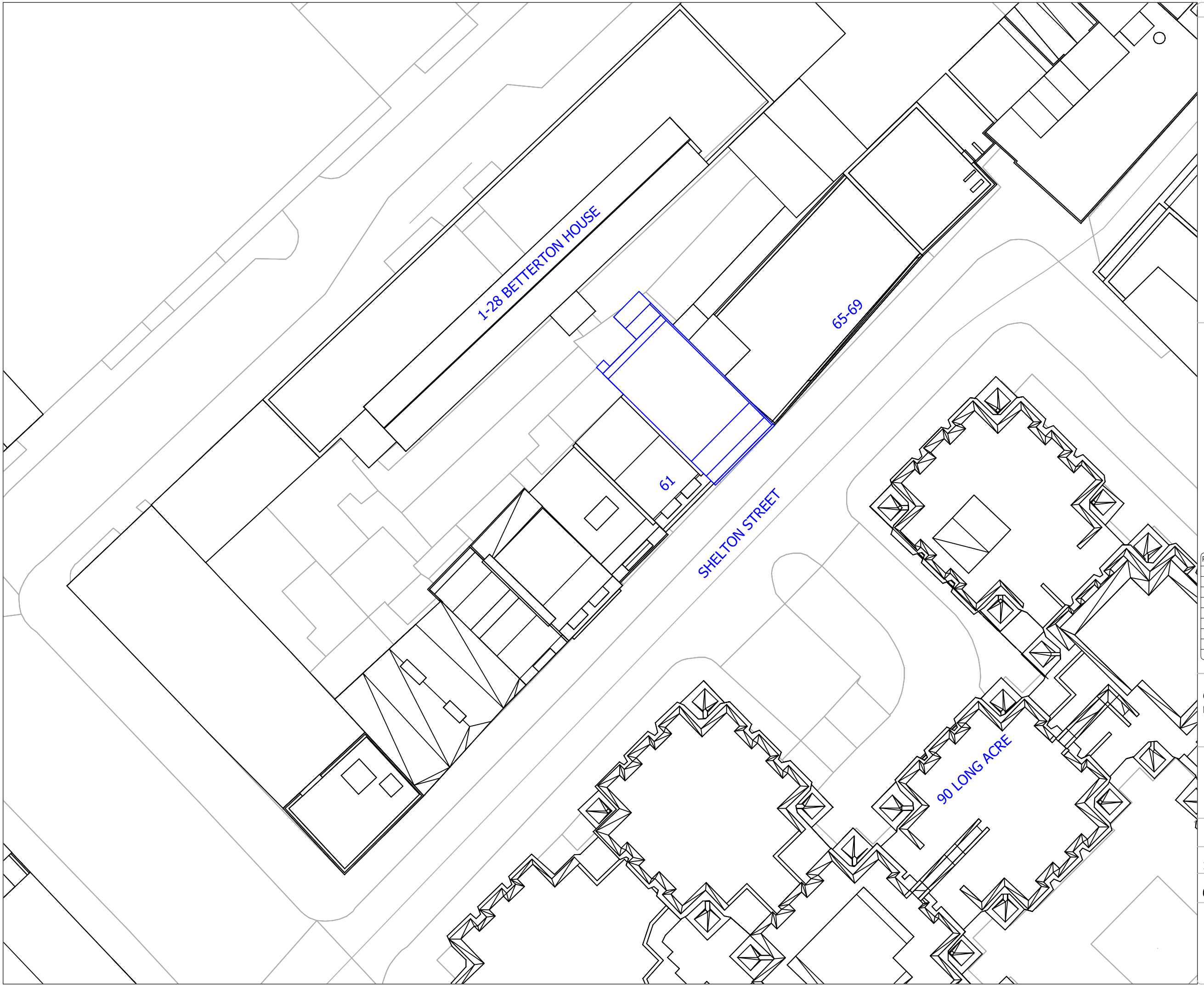

Sources of Information

GIA
PHOTOGRAPHS
IR1-6250 - FIND OS MAP

A3D LTD ARCHITECTS
IR2-6250 (13-12-11)
IR3-6250 (13-12-11)
IR4-6250 (13-12-11)
IR5-6250 (20-12-11)

Notes

N
Indicative Only

ALL HEIGHTS GIVEN IN mm AOD

Rev	Date	Description	Initials
A		Initial Issue	

Project
63 SHELTON STREET
LONDON

Title
SITE PLAN
PROPOSED SCENARIO
(20-12-11)

Scale	Date
1:250 @ A3	DEC'11
Drawn	Checked
IA	JH

Drawing No.	Rel No.	Revision
6250-07	02	A

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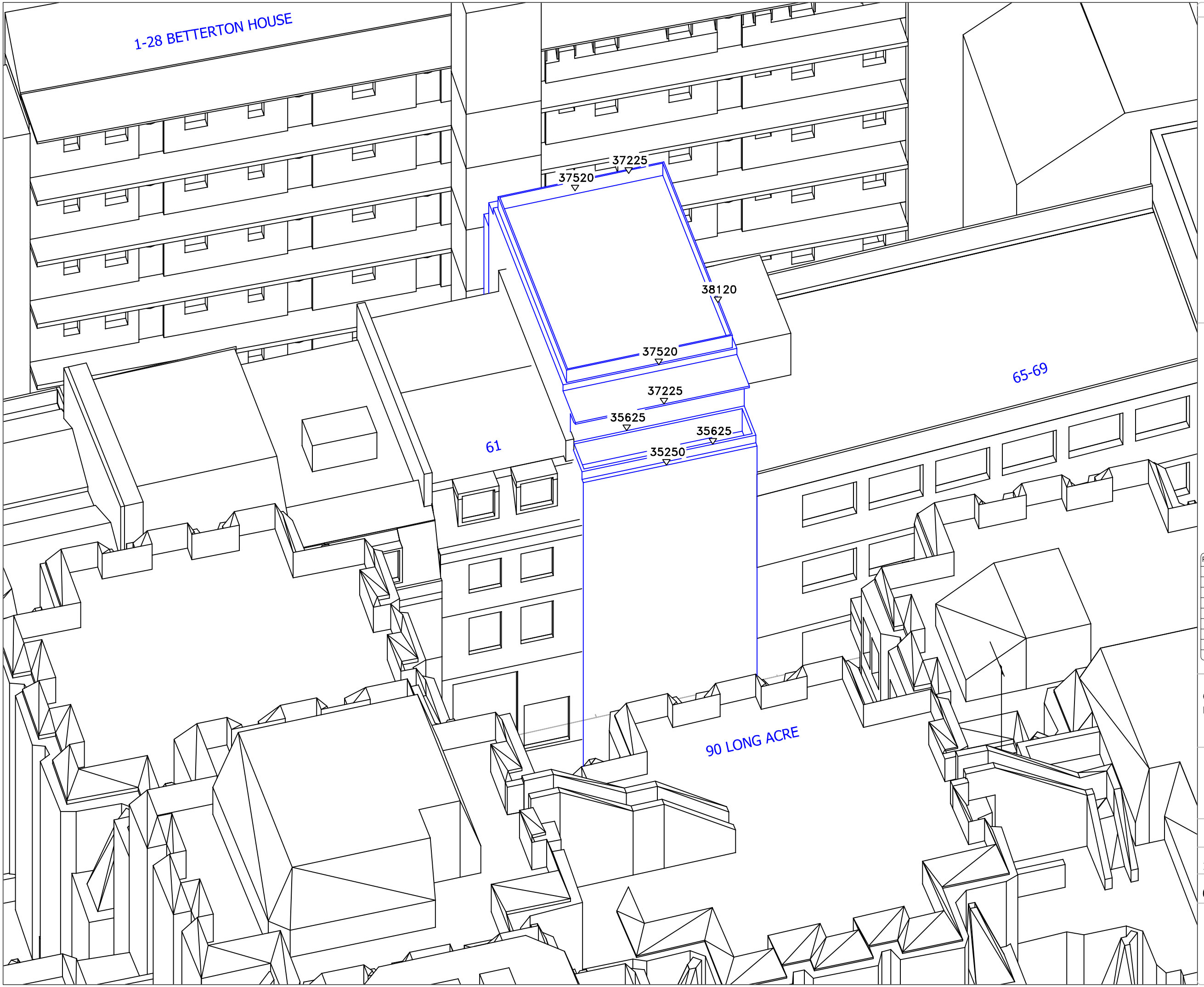

Sources of Information

GIA
PHOTOGRAPHS
IR1-6250 - FIND OS MAP

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IR3-6250 (13-12-11)
IR4-6250 (13-12-11)
IR5-6250 (20-12-11)

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A		Initial Issue	

Project

63 SHELTON STREET
LONDON

Title

3D VIEW
PROPOSED SCENARIO
(20-12-11)

Scale	Date
NTS	DEC'11
Drawn	Checked
IA	JH

Drawing No.	Rel No.	Revision
6250-08	02	B

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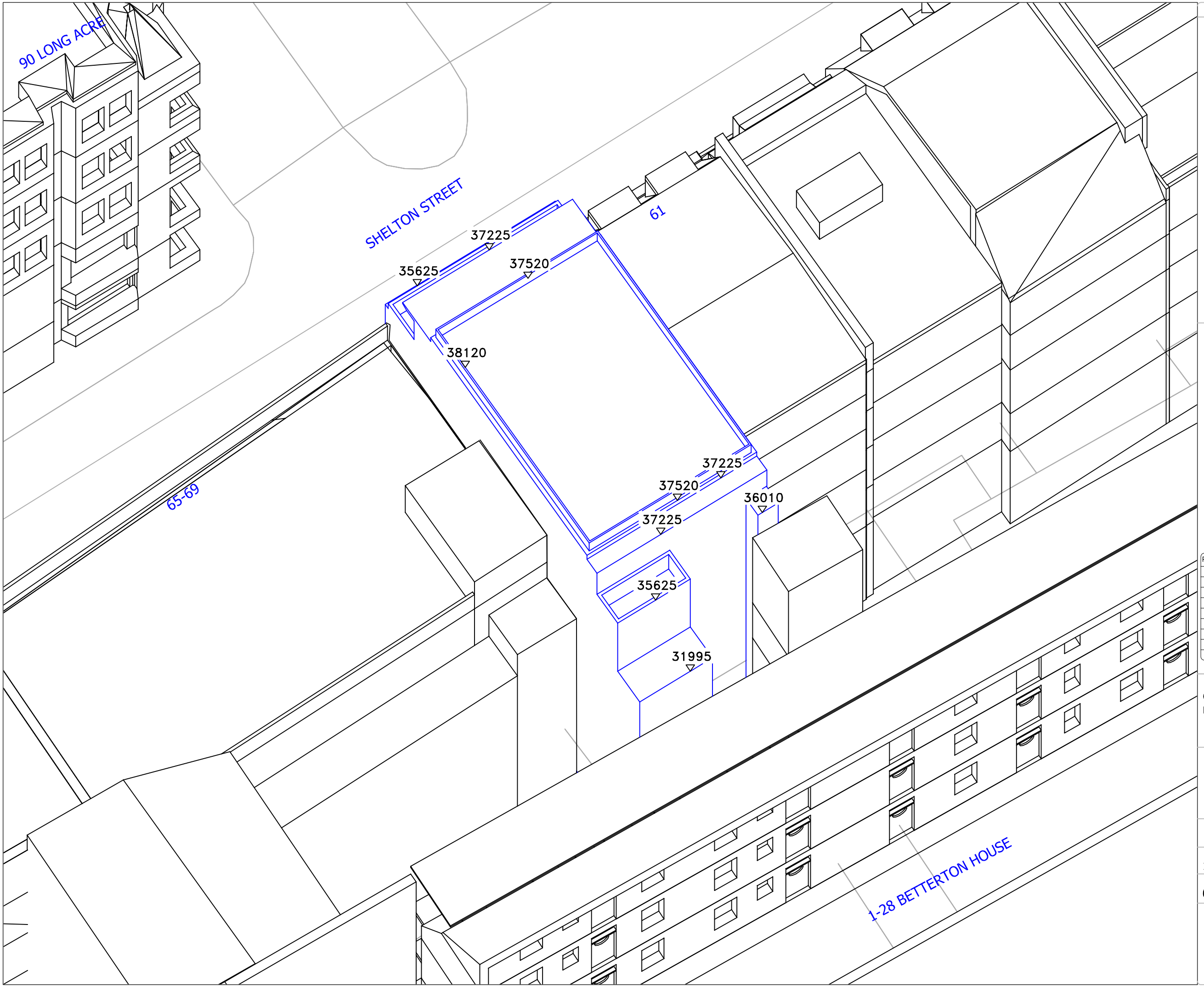

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PHOTOGRAPHS
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Project

63 SHELTON STREET
LONDON

Title

3D VIEW
PROPOSED SCENARIO
(20-12-11)

Scale	Date
NTS	DEC'11
Drawn	Checked
IA	JH

Drawing No.	Rel No.	Revision
6250-09	02	B

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Vertical Sky Component						Average Daylight Factor							
									Existing		Proposed		
Room	Window	Existing	Proposed	Loss	%	Room	Window	Room Use	ADF	Total	ADF	Total	Loss	%
BETTERTON HOUSE 1-28						**BETTERTON HOUSE 1-28**								
R1/100	**W1/100**	0.19	0.19	0.00	0.00	**R1/100**	**W1/100**		0.00		0.00			
R1/100	**W2/100**	0.03	0.03	0.00	0.00	**R1/100**	**W2/100**		0.00	0.00	0.00	0.00	0.00	-
R2/100	**W3/100**	0.00	0.00	0.00	0.00	**R2/100**	**W3/100**		0.00		0.00			
R2/100	**W4/100**	0.00	0.00	0.00	0.00	**R2/100**	**W4/100**		0.00	0.00	0.00	0.00	0.00	-
R3/100	**W5/100**	0.01	0.01	0.00	0.00	**R3/100**	**W5/100**		0.00	0.00	0.00	0.00	0.00	-
R4/100	**W6/100**	0.01	0.01	0.00	0.00	**R4/100**	**W6/100**		0.00	0.00	0.00	0.00	0.00	-
R5/100	**W7/100**	0.00	0.00	0.00	0.00	**R5/100**	**W7/100**		0.00		0.00			
R5/100	**W8/100**	0.00	0.00	0.00	0.00	**R5/100**	**W8/100**		0.00	0.00	0.00	0.00	0.00	-
R6/100	**W9/100**	0.01	0.01	0.00	0.00	**R6/100**	**W9/100**		0.00	0.00	0.00	0.00	0.00	-
R7/100	**W10/100**	0.00	0.00	0.00	0.00	**R7/100**	**W10/100**		0.00		0.00			
R7/100	**W11/100**	0.00	0.00	0.00	0.00	**R7/100**	**W11/100**		0.00	0.00	0.00	0.00	0.00	-
R8/100	**W12/100**	0.00	0.00	0.00	0.00	**R8/100**	**W12/100**		0.00		0.00			
R8/100	**W13/100**	0.00	0.00	0.00	0.00	**R8/100**	**W13/100**		0.00	0.00	0.00	0.00	0.00	-
R9/100	**W14/100**	0.00	0.00	0.00	0.00	**R9/100**	**W14/100**		0.00	0.00	0.00	0.00	0.00	-
R10/100	**W15/100**	0.00	0.00	0.00	0.00	**R10/100**	**W15/100**		0.00	0.00	0.00	0.00	0.00	-
R11/100	**W16/100**	0.00	0.00	0.00	0.00	**R11/100**	**W16/100**		0.00	0.00	0.00	0.00	0.00	-
R12/100	**W17/100**	0.00	0.00	0.00	0.00	**R12/100**	**W17/100**		0.00		0.00			
R12/100	**W18/100**	0.00	0.00	0.00	0.00	**R12/100**	**W18/100**		0.00	0.00	0.00	0.00	0.00	-
R13/100	**W19/100**	0.00	0.00	0.00	0.00	**R13/100**	**W19/100**		0.00	0.00	0.00	0.00	0.00	-
R14/100	**W20/100**	0.00	0.00	0.00	0.00	**R14/100**	**W20/100**		0.00	0.00	0.00	0.00	0.00	-
R15/100	**W21/100**	0.00	0.00	0.00	0.00	**R15/100**	**W21/100**		0.00	0.00	0.00	0.00	0.00	-
R1/101	**W1/101**	3.97	3.86	0.11	2.77	**R1/101**	**W1/101**		0.09		0.09			
R1/101	**W2/101**	3.41	3.29	0.12	3.52	**R1/101**	**W2/101**		0.13	0.22	0.13	0.22	0.00	0.00
R2/101	**W3/101**	2.78	2.68	0.10	3.60	**R2/101**	**W3/101**		0.11		0.11			
R2/101	**W4/101**	0.00	0.00	0.00	0.00	**R2/101**	**W4/101**		0.00	0.11	0.00	0.11	0.00	1.83
R3/101	**W5/101**	3.18	3.05	0.13	4.09	**R3/101**	**W5/101**		0.17	0.17	0.17	0.17	0.00	0.00
R4/101	**W6/101**	2.92	2.79	0.13	4.45	**R4/101**	**W6/101**		0.11	0.11	0.11	0.11	0.00	0.00
R5/101	**W7/101**	2.19	2.13	0.06	2.74	**R5/101**	**W7/101**		0.10		0.10			
R5/101	**W8/101**	0.00	0.00	0.00	0.00	**R5/101**	**W8/101**		0.00	0.10	0.00	0.10	0.00	1.04
R6/101	**W9/101**	2.20	2.16	0.04	1.82	**R6/101**	**W9/101**		0.08	0.08	0.08	0.08	0.00	0.00
R7/101	**W10/101**	1.38	1.38	0.00	0.00	**R7/101**	**W10/101**		0.07		0.07			
R7/101	**W11/101**	0.00	0.00	0.00	0.00	**R7/101**	**W11/101**		0.00	0.07	0.00	0.07	0.00	0.00
R8/101	**W12/101**	1.14	0.97	0.17	14.91	**R8/101**	**W12/101**		0.07		0.07			
R8/101	**W13/101**	0.00	0.00	0.00	0.00	**R8/101**	**W13/101**		0.00	0.07	0.00	0.07	0.01	7.04
R9/101	**W14/101**	0.61	0.59	0.02	3.28	**R9/101**	**W14/101**		0.00	0.00	0.00	0.00	0.00	-
R10/101	**W15/101**	2.25	2.25	0.00	0.00	**R10/101**	**W15/101**		0.20	0.20	0.20	0.20	0.00	0.00
R11/101	**W16/101**	2.96	2.90	0.06	2.03	**R11/101**	**W16/101**		0.21	0.21	0.21	0.21	0.00	0.47
R12/101	**W17/101**	2.80	2.73	0.07	2.50	**R12/101**	**W17/101**		0.11		0.11			
R12/101	**W18/101**	0.00	0.00	0.00	0.00	**R12/101**	**W18/101**		0.00	0.11	0.00	0.11	0.00	1.75
R13/101	**W19/101**	1.28	1.26	0.02	1.56	**R13/101**	**W19/101**		0.00	0.00	0.00	0.00	0.00	-
R14/101	**W20/101**	3.31	3.18	0.13	3.93	**R14/101**	**W20/101**		0.26	0.26	0.26	0.26	0.00	0.78
R15/101	**W21/101**	3.05	2.89	0.16	5.25	**R15/101**	**W21/101**		0.23	0.23	0.23	0.23	0.00	1.71
R1/102	**W1/102**	10.71	10.20	0.51	4.76	**R1/102**	**W1/102**		0.27		0.27			
R1/102	**W2/102**	10.03	9.39	0.64	6.38	**R1/102**	**W2/102**		0.41	0.68	0.40	0.67	0.01	1.76
R2/102	**W3/102**	9.13	8.43	0.70	7.67	**R2/102**	**W3/102**		0.22		0.21			
R2/102	**W4/102**	0.01	0.01	0.00	0.00	**R2/102**	**W4/102**		0.00	0.22	0.00	0.21	0.01	4.61
R3/102	**W5/102**	9.45	8.55	0.90	9.52	**R3/102**	**W5/102**		0.55	0.55	0.52	0.52	0.03	5.11
R4/102	**W6/102**	9.01	7.88	1.13	12.54	**R4/102**	**W6/102**		0.36	0.36	0.34	0.34	0.02	6.65
R5/102	**W7/102**	7.87	6.71	1.16	14.74	**R5/102**	**W7/102**		0.20		0.18			
R5/102	**W8/102**	0.01	0.01	0.00	0.00	**R5/102**	**W8/102**		0.00	0.20	0.00	0.19	0.02	7.92

Vertical Sky Component						Average Daylight Factor								
									Existing		Proposed			
Room	Window	Existing	Proposed	Loss	%	Room	Window	Room Use	ADF	Total	ADF	Total	Loss	%
R6/102	W9/102	7.48	6.26	1.22	16.31	R6/102	W9/102		0.35	0.35	0.32	0.32	0.03	7.78
R7/102	W10/102	4.73	4.56	0.17	3.59	R7/102	W10/102		0.15		0.15			
R7/102	W11/102	0.00	0.00	0.00	0.00	R7/102	W11/102		0.00	0.15	0.00	0.15	0.00	1.31
R8/102	W12/102	4.20	3.04	1.16	27.62	R8/102	W12/102		0.14		0.12			
R8/102	W13/102	0.30	0.30	0.00	0.00	R8/102	W13/102		0.04	0.18	0.04	0.16	0.02	10.93
R9/102	W14/102	3.70	3.13	0.57	15.41	R9/102	W14/102		0.29	0.29	0.29	0.29	0.00	0.34
R10/102	W15/102	7.58	6.05	1.53	20.18	R10/102	W15/102		0.50	0.50	0.47	0.47	0.02	4.65
R11/102	W16/102	9.07	7.72	1.35	14.88	R11/102	W16/102		0.51	0.51	0.48	0.48	0.02	4.36
R12/102	W17/102	8.90	7.77	1.13	12.70	R12/102	W17/102		0.22		0.20			
R12/102	W18/102	0.40	0.40	0.00	0.00	R12/102	W18/102		0.05	0.26	0.05	0.25	0.01	5.34
R13/102	W19/102	6.46	5.90	0.56	8.67	R13/102	W19/102		0.44	0.44	0.43	0.43	0.01	2.27
R14/102	W20/102	9.46	8.55	0.91	9.62	R14/102	W20/102		0.59	0.59	0.56	0.56	0.02	3.92
R15/102	W21/102	8.08	7.43	0.65	8.04	R15/102	W21/102		0.50	0.50	0.49	0.49	0.02	3.37
R1/103	W1/103	15.13	14.65	0.48	3.17	R1/103	W1/103		0.33		0.33			
R1/103	W2/103	14.45	13.85	0.60	4.15	R1/103	W2/103		0.53	0.86	0.52	0.85	0.01	1.05
R2/103	W3/103	13.54	12.82	0.72	5.32	R2/103	W3/103		0.27		0.26			
R2/103	W4/103	1.67	1.25	0.42	25.15	R2/103	W4/103		0.10	0.37	0.09	0.35	0.02	6.43
R3/103	W5/103	14.11	13.22	0.89	6.31	R3/103	W5/103		0.72	0.72	0.69	0.69	0.03	3.48
R4/103	W6/103	13.72	12.57	1.15	8.38	R4/103	W6/103		0.47	0.47	0.45	0.45	0.02	3.65
R5/103	W7/103	12.48	11.19	1.29	10.34	R5/103	W7/103		0.26		0.24			
R5/103	W8/103	1.28	0.73	0.55	42.97	R5/103	W8/103		0.09	0.35	0.07	0.31	0.04	11.14
R6/103	W9/103	11.84	10.46	1.38	11.66	R6/103	W9/103		0.49	0.49	0.45	0.45	0.04	8.74
R7/103	W10/103	7.17	6.89	0.28	3.91	R7/103	W10/103		0.19		0.19			
R7/103	W11/103	0.50	0.50	0.00	0.00	R7/103	W11/103		0.06	0.25	0.06	0.24	0.01	2.04
R8/103	W12/103	8.95	7.03	1.92	21.45	R8/103	W12/103		0.21		0.19			
R8/103	W13/103	1.24	1.16	0.08	6.45	R8/103	W13/103		0.09	0.30	0.09	0.27	0.03	9.60
R9/103	W14/103	8.50	6.81	1.69	19.88	R9/103	W14/103		0.51	0.51	0.42	0.42	0.09	17.39
R10/103	W15/103	12.74	11.29	1.45	11.38	R10/103	W15/103		0.71	0.71	0.65	0.65	0.06	8.09
R11/103	W16/103	13.97	13.11	0.86	6.16	R11/103	W16/103		0.68	0.68	0.65	0.65	0.03	4.15
R12/103	W17/103	13.50	12.86	0.64	4.74	R12/103	W17/103		0.27		0.27			
R12/103	W18/103	1.79	1.66	0.13	7.26	R12/103	W18/103		0.11	0.38	0.10	0.37	0.01	2.89
R13/103	W19/103	10.62	10.11	0.51	4.80	R13/103	W19/103		0.57	0.57	0.57	0.57	0.01	1.05
R14/103	W20/103	14.14	13.62	0.52	3.68	R14/103	W20/103		0.76	0.76	0.75	0.75	0.01	1.32
R15/103	W21/103	12.70	12.30	0.40	3.15	R15/103	W21/103		0.66	0.66	0.65	0.65	0.00	0.46
R1/104	W1/104	18.00	17.90	0.10	0.56	R1/104	W1/104		0.37		0.37			
R1/104	W2/104	17.26	17.14	0.12	0.70	R1/104	W2/104		0.59	0.97	0.59	0.97	0.00	0.00
R2/104	W3/104	16.26	16.11	0.15	0.92	R2/104	W3/104		0.30		0.30			
R2/104	W4/104	3.34	3.31	0.03	0.90	R2/104	W4/104		0.15	0.45	0.15	0.45	0.00	0.45
R3/104	W5/104	16.92	16.77	0.15	0.89	R3/104	W5/104		0.81	0.81	0.81	0.81	0.00	0.25
R4/104	W6/104	16.65	16.48	0.17	1.02	R4/104	W6/104		0.53	0.53	0.53	0.53	0.00	0.00
R5/104	W7/104	15.35	15.15	0.20	1.30	R5/104	W7/104		0.29		0.29			
R5/104	W8/104	2.96	2.93	0.03	1.01	R5/104	W8/104		0.14	0.43	0.14	0.43	0.00	0.70
R6/104	W9/104	14.47	14.39	0.08	0.55	R6/104	W9/104		0.57	0.57	0.57	0.57	0.00	0.18
R7/104	W10/104	8.92	8.92	0.00	0.00	R7/104	W10/104		0.21		0.21			
R7/104	W11/104	1.33	1.33	0.00	0.00	R7/104	W11/104		0.09	0.30	0.09	0.30	0.00	0.00
R8/104	W12/104	10.59	10.59	0.00	0.00	R8/104	W12/104		0.24		0.24			
R8/104	W13/104	2.63	2.63	0.00	0.00	R8/104	W13/104		0.13	0.36	0.13	0.36	0.00	0.00
R9/104	W14/104	10.53	10.53	0.00	0.00	R9/104	W14/104		0.60	0.60	0.60	0.60	0.00	0.00
R10/104	W15/104	15.13	15.13	0.00	0.00	R10/104	W15/104		0.80	0.80	0.80	0.80	0.00	0.00
R11/104	W16/104	16.85	16.84	0.01	0.06	R11/104	W16/104		0.78	0.78	0.78	0.78	0.00	0.00
R12/104	W17/104	16.52	16.47	0.05	0.30	R12/104	W17/104		0.31		0.31			
R12/104	W18/104	3.76	3.74	0.02	0.53	R12/104	W18/104		0.16	0.47	0.16	0.46	0.00	0.22
R13/104	W19/104	13.77	13.71	0.06	0.44	R13/104	W19/104		0.68	0.68	0.68	0.68	0.00	0.00
R14/104	W20/104	17.66	17.57	0.09	0.51	R14/104	W20/104		0.88	0.88	0.88	0.88	0.00	0.34
R15/104	W21/104	17.95	17.86	0.09	0.50	R15/104	W21/104		0.82	0.82	0.82	0.82	0.00	0.24

Room/ Floor	Room Use	Whole Room	Prev sq ft	New sq ft	Loss sq ft
BETTERTON HOUSE 1-28					
R1/100		149.0	12.5	12.5	0.0
R2/100		31.8	0.1	0.1	0.0
R3/100		88.1	6.2	6.2	0.0
R4/100		81.4	3.3	3.3	0.0
R5/100		31.8	0.0	0.0	0.0
R6/100		141.4	5.0	5.0	0.0
R7/100		31.8	0.0	0.0	0.0
R8/100		31.8	0.6	0.6	0.0
R9/100		28.6	0.0	0.0	0.0
R10/100		87.9	4.2	4.2	0.0
R11/100		103.8	5.1	5.1	0.0
R12/100		31.8	0.5	0.5	0.0
R13/100		28.6	0.0	0.0	0.0
R14/100		86.0	5.0	4.7	0.3
R15/100		95.0	4.4	4.2	0.2
R1/101		149.0	47.1	45.8	1.3
R2/101		31.8	11.1	11.0	0.1
R3/101		88.1	27.2	26.6	0.6
R4/101		81.4	20.1	19.4	0.7
R5/101		31.8	10.4	10.3	0.1
R6/101		141.4	25.3	24.7	0.7
R7/101		31.8	5.8	5.8	0.0
R8/101		31.8	2.8	2.4	0.5
R9/101		28.6	3.1	2.5	0.6
R10/101		87.9	17.5	17.5	0.0
R11/101		103.8	30.1	29.8	0.3
R12/101		31.8	12.7	12.3	0.4
R13/101		28.6	13.1	13.0	0.1
R14/101		86.0	28.1	26.6	1.4
R15/101		95.0	25.2	24.8	0.4
R1/102		149.0	117.0	116.6	0.4
R2/102		31.8	18.3	18.3	0.0
R3/102		88.1	52.7	52.7	0.0
R4/102		81.4	47.9	47.5	0.5
R5/102		31.8	19.7	19.7	0.0
R6/102		141.4	77.1	63.3	13.8
R7/102		31.8	15.2	14.7	0.5
R8/102		31.8	11.2	4.6	6.6
R9/102		28.6	14.8	6.0	8.8
R10/102		87.9	53.6	45.1	8.5
R11/102		103.8	80.7	75.2	5.5
R12/102		31.8	23.6	23.6	0.0
R13/102		28.6	21.9	21.9	0.0
R14/102		86.0	68.8	68.5	0.3
R15/102		95.0	80.3	80.3	0.0
R1/103		149.0	136.2	136.2	0.0
R2/103		31.8	22.1	22.1	0.0
R3/103		88.1	64.7	64.7	0.0
R4/103		81.4	60.9	60.9	0.0
R5/103		31.8	23.7	23.7	0.0
R6/103		141.4	106.9	105.7	1.1
R7/103		31.8	23.1	20.4	2.7
R8/103		31.8	23.7	14.8	9.0
R9/103		28.6	21.9	20.4	1.5
R10/103		87.9	75.9	65.2	10.6
R11/103		103.8	96.2	96.2	0.0
R12/103		31.8	25.9	25.9	0.0
R13/103		28.6	21.9	21.9	0.0
R14/103		86.0	81.2	81.2	0.0
R15/103		95.0	89.4	89.4	0.0
R1/104		149.0	143.6	143.6	0.0
R2/104		31.8	25.1	25.1	0.0
R3/104		88.1	81.6	81.6	0.0
R4/104		81.4	74.5	74.5	0.0
R5/104		31.8	25.7	25.7	0.0
R6/104		141.4	124.8	124.8	0.0
R7/104		31.8	24.4	24.4	0.0
R8/104		31.8	24.6	24.6	0.0
R9/104		28.6	21.7	21.7	0.0
R10/104		87.9	81.7	81.7	0.0
R11/104		103.8	99.8	99.8	0.0
R12/104		31.8	26.0	26.0	0.0
R13/104		28.6	21.9	21.9	0.0
R14/104		86.0	83.2	83.2	0.0
R15/104		95.0	91.4	91.4	0.0

Position	Room Use	Existing Summer	Existing Winter	Existing Total	Proposed Summer	Proposed Winter	Proposed Total	% Loss Winter	% Loss Total
BETTERTON HOUSE 1-28									
W1/100		1	1	2	1	1	2	0.00	0.00
W2/100		0	0	0	0	0	0	-	-
W3/100		0	0	0	0	0	0	-	-
W4/100		0	0	0	0	0	0	-	-
W5/100		0	0	0	0	0	0	-	-
W6/100		0	0	0	0	0	0	-	-
W7/100		0	0	0	0	0	0	-	-
W8/100		0	0	0	0	0	0	-	-
W9/100		0	0	0	0	0	0	-	-
W10/100		0	0	0	0	0	0	-	-
W11/100		0	0	0	0	0	0	-	-
W12/100		0	0	0	0	0	0	-	-
W13/100		0	0	0	0	0	0	-	-
W14/100		0	0	0	0	0	0	-	-
W15/100		0	0	0	0	0	0	-	-
W16/100		0	0	0	0	0	0	-	-
W17/100		0	0	0	0	0	0	-	-
W18/100		0	0	0	0	0	0	-	-
W19/100		0	0	0	0	0	0	-	-
W20/100		0	0	0	0	0	0	-	-
W21/100		0	0	0	0	0	0	-	-
W1/101		9	5	14	9	5	14	0.00	0.00
W2/101		8	3	11	7	3	10	0.00	9.09
W3/101		4	3	7	4	3	7	0.00	0.00
W4/101		0	0	0	0	0	0	-	-
W5/101		7	3	10	6	3	9	0.00	10.00
W6/101		7	2	9	6	2	8	0.00	11.11
W7/101		3	3	6	2	3	5	0.00	16.67
W8/101		0	0	0	0	0	0	-	-
W9/101		1	3	4	1	3	4	0.00	0.00
W10/101		0	4	4	0	4	4	0.00	0.00
W11/101		0	0	0	0	0	0	-	-
W12/101		6	0	6	4	0	4	-	33.33
W13/101		0	0	0	0	0	0	-	-
W14/101		1	0	1	1	0	1	-	0.00
W15/101		11	0	11	11	0	11	-	0.00
W16/101		12	1	13	12	1	13	0.00	0.00
W17/101		10	0	10	10	0	10	-	0.00
W18/101		0	0	0	0	0	0	-	-
W19/101		2	0	2	2	0	2	-	0.00
W20/101		9	0	9	9	0	9	-	0.00
W21/101		5	1	6	5	1	6	0.00	0.00
W1/102		18	12	30	17	12	29	0.00	3.33
W2/102		17	11	28	17	11	28	0.00	0.00
W3/102		15	10	25	15	10	25	0.00	0.00
W4/102		0	0	0	0	0	0	-	-
W5/102		18	8	26	14	8	22	0.00	15.38
W6/102		17	7	24	13	7	20	0.00	16.67
W7/102		12	7	19	10	7	17	0.00	10.53

Position	Room Use	Existing			Proposed			% Loss	
		Summer	Winter	Total	Summer	Winter	Total	Winter	Total
W8/102		0	0	0	0	0	0	-	-
W9/102		13	8	21	6	8	14	0.00	33.33
W10/102		3	8	11	3	8	11	0.00	0.00
W11/102		0	0	0	0	0	0	-	-
W12/102		15	0	15	12	0	12	-	20.00
W13/102		1	0	1	1	0	1	-	0.00
W14/102		9	1	10	9	0	9	100.00	10.00
W15/102		18	3	21	18	1	19	66.67	9.52
W16/102		19	5	24	18	3	21	40.00	12.50
W17/102		16	6	22	16	3	19	50.00	13.64
W18/102		1	1	2	1	1	2	0.00	0.00
W19/102		8	4	12	8	3	11	25.00	8.33
W20/102		16	8	24	16	5	21	37.50	12.50
W21/102		12	7	19	12	5	17	28.57	10.53
W1/103		23	17	40	22	17	39	0.00	2.50
W2/103		22	15	37	21	15	36	0.00	2.70
W3/103		20	13	33	18	13	31	0.00	6.06
W4/103		0	1	1	0	1	1	0.00	0.00
W5/103		22	13	35	20	13	33	0.00	5.71
W6/103		23	13	36	19	13	32	0.00	11.11
W7/103		19	12	31	15	12	27	0.00	12.90
W8/103		1	0	1	0	0	0	-	100.00
W9/103		18	13	31	15	13	28	0.00	9.68
W10/103		3	12	15	3	11	14	8.33	6.67
W11/103		0	0	0	0	0	0	-	-
W12/103		20	2	22	19	0	19	100.00	13.64
W13/103		1	1	2	1	1	2	0.00	0.00
W14/103		12	4	16	12	3	15	25.00	6.25
W15/103		23	8	31	23	6	29	25.00	6.45
W16/103		23	12	35	23	9	32	25.00	8.57
W17/103		20	14	34	20	12	32	14.29	5.88
W18/103		1	2	3	1	2	3	0.00	0.00
W19/103		11	11	22	11	9	20	18.18	9.09
W20/103		20	13	33	20	11	31	15.38	6.06
W21/103		16	13	29	16	12	28	7.69	3.45
W1/104		24	18	42	24	18	42	0.00	0.00
W2/104		23	17	40	23	17	40	0.00	0.00
W3/104		21	15	36	21	15	36	0.00	0.00
W4/104		1	3	4	1	3	4	0.00	0.00
W5/104		23	16	39	23	16	39	0.00	0.00
W6/104		23	15	38	23	15	38	0.00	0.00
W7/104		19	14	33	19	14	33	0.00	0.00
W8/104		1	1	2	1	1	2	0.00	0.00
W9/104		18	14	32	18	14	32	0.00	0.00
W10/104		3	13	16	3	13	16	0.00	0.00
W11/104		0	0	0	0	0	0	-	-
W12/104		21	3	24	21	3	24	0.00	0.00
W13/104		1	1	2	1	1	2	0.00	0.00
W14/104		14	6	20	14	6	20	0.00	0.00
W15/104		24	10	34	24	10	34	0.00	0.00
W16/104		24	14	38	24	14	38	0.00	0.00
W17/104		22	15	37	22	15	37	0.00	0.00
W18/104		1	3	4	1	3	4	0.00	0.00
W19/104		14	12	26	14	12	26	0.00	0.00
W20/104		23	16	39	23	16	39	0.00	0.00
W21/104		19	17	36	19	17	36	0.00	0.00