

## APPENDIX 3

### Chord Environmental Groundwater Impact Report

# 59 Maresfield Gardens

## Groundwater Impact Assessment

59 Maresfield Gardens  
London  
NW3 5TE

Site NGR: TQ 264 851

Prepared for:  
Stefanie Drews & Colin Rowat

**Chord Environmental Ltd**

Report no. 1102/R1

November 2012

# 59 Maresfield Gardens Groundwater Impact Assessment

## Site Address

**59 Maresfield Gardens**

**London**

**NW3 5TE**

**Site NGR: TQ 264 851**

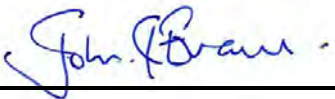
## Document Control Sheet

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The report is confidential to Stefanie Drews & Colin Rowat. Chord Environmental Ltd. accepts no responsibility of any nature to any third party to whom this report or any part thereof is made known.

**Chord Environmental Ltd**

<b>Prepared by:</b>	John Evans MSc FGS CGeol				
<b>Report no:</b>	1102/R1	<b>Issue no:</b>	3	<b>Date:</b>	12 <sup>th</sup> November 2012

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# 59 Maresfield Gardens

## Groundwater Impact Assessment

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# 1 Introduction

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## 1.1 Background

Stefanie Drews and Colin Rowat are applying for Planning Consent to demolish the existing end terrace, split level two-storey house at 59 Maresfield Gardens and construct a new detached two-storey building with a double level basement and additional swimming pool level. Formation level for the proposed basement is understood to be at an approximate level of 76.5 m OD, c.6.5m below existing site levels adjacent to the house.

Site investigation works have been undertaken by Ian Farmer Associates (IFA) in 2008<sup>1</sup> and Geotechnical and Environmental Associates (GEA) Ltd in 2011<sup>2</sup>. The work comprised detailed Ground Investigations and this assessment should be read in conjunction with both the IFA and GEA site investigation reports.

Chord Environmental has been commissioned by Elliott Wood Partnership on behalf of Stefanie Drews & Colin Rowat, to carry out a groundwater assessment for the proposed development at 59 Maresfield Gardens, London, NW3 5TE, to meet the requirements of London Borough of Camden's "Guidance for Subterranean Development"<sup>3</sup>.

## 1.2 Scope and Approach

This report reviews the proposed development at 59 Maresfield Gardens within the context of the conceptual understanding of its site setting which has been informed through both desk study and review of site investigation findings. The report will identify potential groundwater impacts the development may have. Appropriate mitigating measures can then be developed and adopted to avoid or minimise these affects where identified.

This report is limited to the groundwater flow component of the Basement Impact Assessment, as specified by the London Borough of Camden's "Guidance for Subterranean Development". The Author of this report is a qualified Hydrogeologist, Chartered Geologist and Fellow of the Geological Society of London, as required by the Guidance.

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<sup>1</sup> Report on Phase 2 Site Investigation – 59 Maresfield Gardens, London NW3 5TE. Ian Farmer Associates. July 2008.

<sup>2</sup> Site Investigation and Impact Assessment Report – 59 Maresfield Gardens, London NW3. Geotechnical and Environmental Associates Ltd. May 2012.

<sup>3</sup> Camden Geological, Hydrogeological and Hydrological study - Guidance for Subterranean Development. Ove Arup & Partners Ltd., November 2010

### 1.3 Limitations

The conclusions and recommendations made in this report are limited to those that can be made on the basis of the site information obtained from the client or other third parties and the results of the work should be viewed in the context of the range of data sources consulted. No liability can be accepted for information in other data sources or conditions not revealed by the information provided. There may be conditions prevailing at the Site which have not been disclosed by the site investigations undertaken. Any comments made on the basis of information obtained from the client or other third parties are given in good faith on the assumption that the information is accurate; no independent validation of such information has been made by Chord Environmental Ltd.

## **2 Proposed Development**

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The Site occupied by 59 Maresfield Gardens, South Hampstead, London (National Grid Reference TQ 264 851) is a residential property approximately rectangular in shape and 30m by 8m in area. The existing split level, two-storey, end terraced house is located on the middle part of the site. The property fronts on to Maresfield Gardens to the east and is bounded by the adjoining terrace of No.57 Maresfield Gardens to the south. There is a driveway, garden and courtyard to the front of the property and small garden to the rear. The elevation of the site drops sharply by 3.5m from c.85.5m above Ordnance Datum (OD) at the front of the property to c.81.75m OD within the front courtyard and rear garden areas.

The proposal is to demolish the existing house at 59 Maresfield Gardens and construct a new detached two-storey house with double level basement and additional swimming pool level. The basement formation level will extend to a depth of up to 8m below existing lower site levels and be approximately double the existing building footprint in area. A secant pile wall foundation would be constructed around the proposed basement with female piles extending to 72.5m OD (c.9.5m below ground level) and male piles extending to 67m OD (c.15m bgl). Areas of hard standing will increase by approximately 35% from 106m<sup>2</sup> to 130m<sup>2</sup>.

## 3 Site Setting

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The Site is located on the northern end of Maresfield Gardens in the South Hampstead area of London, NW3 5TE and National Grid Reference TQ 2642 8517.

### 3.1 Topography

The majority of the Site lies at an elevation of approximately c.82m OD rising sharply to c.85.5m OD to the east of the site fronting on to Maresfield Gardens. Locally the topography falls away to the southwest across the site to c.40m OD at the River Thames, c.2km to the south and rising to an elevation of 134m OD on Hampstead Heath, c.1.5km north of the site. Within the Site itself the ground from the rear garden through to the front courtyard is relatively level and is c.3.5m below the level of Maresfield Gardens and the eastern part of the site comprising a garden area and driveway.

### 3.2 Hydrology and Drainage

The Site lies within the surface water catchment of the upper Westbourne stream, a tributary of the River Thames, and outside of the catchment of the Hampstead Heath chain of ponds. The Westbourne is entirely covered and culverted and forms part of the surface water sewerage system, running beneath South Hampstead to where it discharges into the Thames to the west of Chelsea Bridge. According to historic maps<sup>4, 5</sup> (1870-71) a small headwater tributary of the Westbourne flowed across the north-western corner of the Site which rose from a pond 20m north of the Site. The area was undeveloped at this time. By 1896 the area is shown to be developed with the current road infrastructure in place and the pond and headwater tributary entirely removed.

There are no surface water features marked on current Ordnance Survey mapping (1:25,000 scale) within 1km of the Site. The site is not located within a Flood Zone as defined by the Environment Agency and Maresfield Gardens has not been identified as a street at risk of surface water flooding as a result of sewer surcharging within the London Borough of Camden.

### 3.3 Geology

According to the British Geological Survey (BGS) 1:50,000 scale sheet for the area (Sheet 256, North London. 2006) and the associated geological memoir, The Geology of London (BGS 2004), the Site is underlain by the clays, silts and fine grained sands of the Eocene Claygate Member, the upper unit of the London Clay Formation. The Eocene silty clay of the London Clay outcrops c.30m down gradient to the west of the Site and the sands of the

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<sup>4</sup> The Lost Rivers of London: a study of their effects upon London and Londoners, and the effects of London and Londoners upon them. N. Barton. 1962.

<sup>5</sup> Report on Phase 1 Desk Study – 59 Maresfield Gardens, London NW3 5TE. Ian Farmer Associates. June 2008.



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## 59 Maresfield Gardens

### Groundwater Impact Assessment

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Bagshot Formation outcrop up topographic gradient, 300m north beneath Hampstead village.

The Site lies 30m to the east of an area denoted by the BGS as likely to be covered by Quaternary Head deposits. This is disturbed material which has been mobilised from higher ground.

The London Clay is underlain by the Cretaceous Chalk at a depth of over 100m beneath the Site.

Site specific geological data from the IFA and GEA site investigations<sup>1,2</sup>, have established the presence of between 0.2m and 3.0m thickness of made ground beneath the Site locally. Claygate Member silty, sandy clay was proved to depths of 8.3m (73.4m OD) and 12.0m (72.5m OD) and stiff dark grey silty London Clay was then proved to a depth of 20m below ground level (61.7m OD). A thin layer of sand (0.15m) was present within one borehole in the east of the site however this was not established in any of the other boreholes.

Alluvium comprising silty clayey sand over sandy clay was established beneath made ground in the western part of the site. This corresponds with the location of the headwater stream on the 1871 historic map.

A geological cross section of the site showing the existing building and proposed basement in relation to the ground conditions encountered has been prepared by GEA<sup>2</sup> and is included as an appendix to this report.

## 3.4 Hydrogeology

The Environment Agency classifies the Claygate Member and overlying Bagshot Beds as Secondary A Aquifer, which have permeable layers capable of supporting water supplies at a local rather than strategic scale, and in some cases forming an important source of base flow to rivers. These are generally aquifers formerly classified as minor aquifers.

Although the Claygate Member is classified a Secondary Aquifer, a majority of the springs in the area (arising on Highgate and Hampstead Heath) occur at the boundary between the sands of the Bagshot Formation and the lower permeability clay rich Claygate Member. The Claygate Member's Secondary Aquifer classification is due to the presence of beds of glauconitic silty fine sand; however as these have been proved to be absent beneath the site, the silty clays encountered can be considered as Non-Productive strata.

London Clay is classified as Non-Productive Strata (formerly Non Aquifer), i.e. not capable of providing useable quantities of water. The Cretaceous Chalk is classified as a Principal (formerly Major) Aquifer however it is highly confined and not generally used for drinking water supply in the central London area due to its poor water quality.

The Site lies approximately 600m north of a Source Protection Zone as designated by the Environment Agency. This is for a licensed public water supply abstraction from the Chalk.

## 59 Maresfield Gardens Groundwater Impact Assessment

### Groundwater Levels

During the GEA site investigation, groundwater was generally encountered as seepages within the Claygate Member at depths of between 2.0 m (80.0 m OD) and 6.0 m (79.3 m OD), whilst a slow inflow was recorded in Borehole No 1 at a depth of 4.5 m (77.2 m OD), rising to 4.3 m (77.4 m OD) after a period of 20 minutes.

Monitoring undertaken within installed boreholes across the Site is summarised in the table below.

Location	BH1		BH2		BH3	
	mbgl	m OD	mbgl	m OD	mbgl	m OD
December 2011	1.96	79.74	3.56	80.94	4.40	80.90
October 2012	1.90	79.80	3.53	80.97	4.51	80.79

There is very little change in groundwater levels despite winter 2011 being a period of very limited rainfall leading to drought conditions by the spring of 2012 followed by over six months of exceptionally wet conditions. Recharge through the Claygate Member and London Clay Formation strata is expected to be limited to approximately 50mm per annum where clay strata dominates, severely limiting vertical flow and groundwater levels are anticipated to vary by less than 0.5m annually.

### Groundwater Flow

Groundwater within the Claygate Member is considered to be dominated by intergranular flow through the thin horizons of fine silty sand (where present) and fissure flow through silty clay beds. Groundwater present within the Claygate Member will be confined by the very low vertical permeability clay beds which separate the more permeable silty and sandy clays.

Rising head tests were undertaken by GEA during October 2012 to estimate the permeability of the Claygate Member strata beneath the site. The results and analysis of the rising head tests are appended to this report and summarised in the table below.

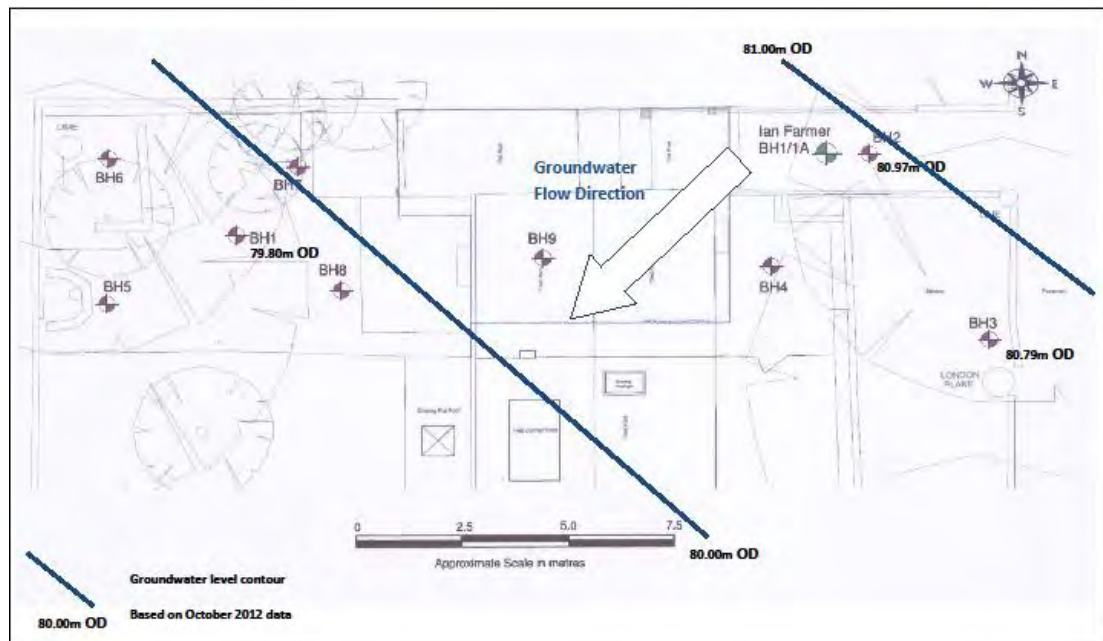
Borehole	Test Section (m bgl)	Permeability ( $\text{ms}^{-1}$ )
BH1	1.90 – 7.84	$2.07 \times 10^{-8}$
BH2	3.53 – 10.22	$2.19 \times 10^{-8}$
BH3	4.51 – 8.65	$6.66 \times 10^{-8}$

These results are consistent with published permeabilities for London Clay Formation strata and represent the highest permeability encountered throughout each borehole. It is highly unlikely that any excavation beneath the Site will encounter any saturated high permeability strata as none was encountered within the ten boreholes drilled across the site. Any such strata would not be laterally continuous and would have very limited water bearing potential.

## 59 Maresfield Gardens Groundwater Impact Assessment

IFA also undertook rising head tests within one borehole (BH1/BH1A) which yielded permeabilities of between  $4.8 \times 10^{-7} \text{ ms}^{-1}$  and  $2.9 \times 10^{-7} \text{ ms}^{-1}$ . However the test results presented show that the water level in BH1A stopped recovering after 15 minutes placing some doubt on the borehole's hydraulic continuity with the aquifer. The rising head tests for BH1 were not analysed within the IFA report however subsequent analysis indicates a permeability of  $c.8.0 \times 10^{-9} \text{ ms}^{-1}$  for strata between 6 and 12m below ground level.

A groundwater contour plan prepared using groundwater monitoring data collected during October 2012 is presented below.



Monitored groundwater levels and interpreted groundwater level contours indicate a groundwater flow direction to the southwest. This coincides with the local topographic gradient as would be expected. The hydraulic gradient across the Site is approximately 0.1.

The Westbourne stream and its associated headwater tributary, which historically crossed the northwest part of the site, are considered to rise from springs and seepages from the Bagshot Formation sands on Hampstead Heath and to be perched on the Claygate Member and London Clay. Alluvium associated with this tributary was found to comprise 1m of desiccated silty clayey sand within BH6 indicating that the flow path has most likely been collected by surface water drainage up gradient of the Site.

## **4 Screening**

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The London Borough of Camden’s “Guidance for subterranean development” states that any development proposal which includes a subterranean basement should be screened in order to determine whether there is a requirement for a BIA to be carried out.

### **4.1 Screening Assessment**

Appendix E of the guidance document details six Basement Impact Assessment screening questions, each of which is stated and answered below:

- **Question 1a: Is the site located directly above an aquifer?**
- Yes. The Site is underlain by the Claygate Member which is designated as Secondary Aquifer by the Environment Agency and considered capable of supporting local water supplies and baseflow to watercourses. However, site investigation information shows the Claygate Member to comprise silty sandy clays and to have a very low permeability exhibiting the hydraulic properties of Non Productive strata.
- **Question 1b: Will the proposed basement extend beneath the water table surface?**

Based on the findings of the site investigation, the basement would extend beneath the water table surface (i.e. saturated Claygate Member). The proposed basement would extend to a depth of approximately 6.5m below existing ground level. An 8m deep secant pile wall foundation would be constructed. The monitoring standpipes installed during the site investigation indicated groundwater within the Claygate Member to be 1.90m below ground level during October 2012 following a very wet summer and autumn. Groundwater levels are not expected to vary by more than 0.5m throughout the year. Refer to Section 3.4.

- **Question 2: Is the site within 100m of a watercourse, well (used/disused) or potential spring line?**

No. According to historic maps<sup>4,5</sup>, a headwater tributary of the Westbourne flowed across the northwest of the Site, rising from a pond c.20m north of the site. This stream is not present at surface and is considered to have been culverted to form part of the local surface water sewer up stream of the Site. Site investigation findings established the presence of dry alluvium in the west of the Site however no shallow flow was encountered in this area. The low permeability of the Claygate Member and London Clay strata does not support groundwater flows to the headwater tributary and are effectively hydraulically isolated from it. The Site is not within a street which has been identified as being at risk of surface water flooding as a result of sewer surcharging within the London Borough of Camden. Refer to Section 3.2 and 3.4.

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## 59 Maresfield Gardens

### Groundwater Impact Assessment

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- **Question 3: Is the site within the catchment of the pond chains on Hampstead Heath?**

No. The Site is outside the catchment of Hampstead Heath ponds. Refer to Section 3.2.

- **Question 4: Will the proposed development result in a change in the proportion of hard surfaced / paved area?**

Yes. Areas of hard standing will increase by 35% from 106m<sup>2</sup> to 130m<sup>2</sup>.

- **Question 5: As part of the site drainage, will more surface water (e.g. rainfall and run-off) than at present be discharged to ground (e.g. via soakaways and/or SUDS)?**

No. The low permeability nature of the Claygate Member strata is unsuitable for receiving significant surface water discharge to ground.

- **Is the lowest point of the proposed excavation (allowing for any drainage and foundation space under the basement floor) close to, or lower than, the mean water level in any local pond (not just the pond chains on Hampstead Heath) or spring line?**

- No. There are no ponds or spring lines present within 100m of the Site.

## 4.2 Screening Conclusions

The screening exercise has identified the following potential issue which should be assessed:

1. The Site is underlain by the Claygate Member, classified a Secondary Aquifer by the Environment Agency, capable of supporting local water supplies and baseflow to watercourses.
2. The basement structure would extend into saturated Claygate Member and London Clay Formation strata.
3. The proposal will increase the hardstanding area by 35% from 106m<sup>2</sup> to 130m<sup>2</sup>.

## 5 Scoping and Site Investigation

Scoping is the activity of defining in further detail the matters to be investigated as part of the impact assessment. Potential impacts should be ascertained for each of the matters of concern identified during the screening process.

The investigation of the potential impacts is undertaken through a site investigation. In this instance, a desk study and site investigation has been undertaken to establish ground conditions for geotechnical assessment purposes. The investigation included the installation of three groundwater monitoring installations to depths between 8m and 12m below ground level. This assessment relies upon the findings of the desk study and site investigation.

### 5.1 Potential Impacts

The following potential impacts have been identified:

Potential Impact	Relevant Site Investigation conclusions
<p>The basement structure would extend into saturated ground.</p> <p>The groundwater flow regime may be altered by the proposed basement. Change in flow regime could potentially cause the groundwater level within the zone encompassed by the new flow route to increase (causing up hydraulic gradient mounding) or decrease down gradient locally. For existing nearby structures the degree of dampness or seepage may potentially increase as a result of changes in groundwater level.</p>	<p>The ground investigation has confirmed the presence of Claygate Member and London Clay beneath the Site. It has also identified confined groundwater levels within the Claygate Member and London Clay formation, and the basement would extend beneath this piezometric groundwater level.</p> <p>The Claygate Member is classified as a Secondary Aquifer however site investigation findings have established it to be predominantly comprised of very low permeability silty sandy clay exhibiting the hydraulic properties of Non Productive strata.</p>
<p>The Site is underlain by a Secondary Aquifer.</p> <p>The proposed development may reduce baseflow to watercourses or reduce the supply of local water supplies.</p>	<p>The Claygate Member is considered to be a Secondary Aquifer however site investigation findings have established it to be predominantly comprised of silty sandy clay. Groundwater encountered during the site investigations entered boreholes very slowly reflecting low permeability (<math>c.5 \times 10^{-8} \text{ ms}^{-1}</math>). The silty sandy clays encountered cannot store or transmit significant quantities of groundwater and exhibit hydraulic properties of Non Productive strata which cannot support baseflow to springs or streams.</p>

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The proposal will increase areas of hard standing by 35% from 106m<sup>2</sup> to 130m<sup>2</sup>. The sealing of the ground surface to rainfall will result in decreased recharge to the underlying ground. In areas underlain by an aquifer, this may impact upon groundwater flow or levels. In areas of non-aquifer or Unproductive Strata (i.e. the London Clay), this may mean changes in the degree of wetness which in turn may affect stability.

The ground investigation has confirmed the presence of Claygate Member and London Clay beneath the Site, designated a Secondary Aquifer and Non Productive Strata or a “non-aquifer” respectively.

The lithological logs and site investigation findings indicate that soakaway drainage is not appropriate for the Site due to the very low permeability clayey nature of the soils beneath the site.

## 6 Groundwater Impact Assessment

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The screening process identified three potential impacts. The results of the desk study and site investigation have been used below to address these concerns and assess the likelihood of a negative impact occurring. These are:

1. Altering of the groundwater flow regime as a result of the proposed basement development.

### **Long Term Built Impact**

The proposed basement formation level will extend to a depth of up to 8m below existing lower site levels. A secant pile wall foundation would be constructed around the proposed basement with female piles extending to 72.5m OD (c.9.5m below ground level) and male piles extending to 67m OD (c.15m bgl).

It has been established that the basement would extend beneath the piezometric surface (or confined groundwater level) within the Claygate Member and London Clay Formation strata. Once constructed, the proposed basement and its secant pile wall foundation would not allow the flow of groundwater beneath the site to the depth of the female piles. The potential impact of this is that the groundwater could potentially mound against the basement structure as groundwater is prevented from flowing along its natural path.

The site investigation has established that the geological formation into which the basement would be constructed comprises very low permeability silty sandy clay. The hydrogeological properties of the Claygate Member and London Clay present beneath the Site are such that free flowing groundwater is not present in significant quantities and is flowing at very low rates.

Additionally, based on the groundwater levels available, groundwater flows from northeast to southwest across the site. The proposed basement would therefore present a c.10m wide blockage to groundwater flow in this direction. When considering the width of the proposed basement, it is considered very unlikely that the structure would cause a significant damming of groundwater to occur.

Using established numerical tools it can be shown that the radius of influence to a change in groundwater level within low permeability strata is very small (Sichardt and Bear unconfined and confined respectively, radius of influence solutions<sup>6</sup>). Given a permeability of  $5 \times 10^{-8} \text{ ms}^{-1}$  based on site specific tests, a change (increase or decrease) in groundwater level of 2m due to a potential damming affect adjacent to the proposed basement would not affect the groundwater level at a distance beyond 10mnd any change would decay rapidly away from the basement structure. The calculations using Sichardt's and Bear's solutions are appended to this report.

Additionally, groundwater within the Claygate Member is confined by numerous interbedded low permeability clay beds and any increase in hydraulic pressure (piezometric surface) would be at a depth of several metres. On this basis, it is highly

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<sup>6</sup> Hydrogeological impact appraisal for dewatering abstractions. Science Report SC040020. Environment Agency. 2007.



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unlikely that there would be any adverse affects from a local change in groundwater level resulting from the proposed basement development.

There are no adjacent neighbouring basement structures which could be affected by a small local rise in groundwater level. A swimming pool is located on higher ground within 40 Netherhall Gardens beyond the Site's northern boundary. The pool is approximately 2.0 m from the site boundary and has a basal elevation of c.81.5m OD, similar to the existing ground level of the Site. It would not be affected by and changes to groundwater level or flow beneath the Site as a result of the proposed basement development.

#### **Short Term Construction Impact**

During construction, groundwater has the potential to enter the excavation. As measured permeability is of the order of  $5 \times 10^{-8} \text{ ms}^{-1}$ , inflow rates are expected to be slow but prolonged whilst the excavation remains open. Given the depth and breadth of the site investigation, it is considered unlikely that significant higher permeable layers will be encountered, however it is possible that saturated pockets or inter-connected layers of groundwater could be encountered resulting in higher inflow rates.

On this basis, we agree with the GEA report that if the adopted method of temporary support during excavations is not watertight, it would be prudent for the chosen contractor to have a contingency plan in place to deal with more significant inflows as a precautionary measure. We also agree with GEA's recommendation that it would also be prudent to carry out a number of trial excavations, to depths as close to the full basement depth as possible, to provide an indication of the likely groundwater inflow conditions.

**Based on the findings of the site investigation and subsequent data analysis, it is considered highly unlikely that the proposed development would result in significant changes to the groundwater flow regime surrounding the Site.**

#### 2. Reducing flow to watercourses and groundwater supplies developing within an Aquifer.

Although the Claygate Member is classified a Secondary Aquifer due to the presence of water bearing sand horizons, the site investigations have established that the Claygate Member beneath the site of the proposed basement is comprised of silty sandy clay and no significant water bearing sandy beds were encountered. It is apparent from the site investigation findings that groundwater is not present in significant quantities within the geological formations into which the basement would be constructed due to their lowly permeable hydrogeological properties. No groundwater abstractions have been identified within 500m and the Westbourne stream and the headwater stream identified on the historic map are fed by discharge from the Bagshot Beds outcrop 300m to the north of the site and are no flow near to the Site.

**It is therefore considered highly unlikely that the proposed development will result in reduced groundwater flow to watercourses and abstractions.**

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## 59 Maresfield Gardens

### Groundwater Impact Assessment

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Altering of the rate of groundwater recharge or changes in the degree of wetness through the creation of additional hard surfaces.

Due to the clayey nature of the soils, recharge to the lower Claygate Member and London Clay is likely to be negligible (of the order of c.50mm/a) due to the very low ( $<1 \times 10^{-9}$  m/s) vertical permeability of the underlying clay dominated strata. In addition, the lowly permeable properties of these strata negate the possibility of significant discharging of surface water drainage to ground.

As the ground is unsuitable for a soakaway system, surface water drainage from the Site would be via existing surface water drains to the mains sewerage system.

**Due to the nature of the soils beneath the site and the relatively small area of development, groundwater recharge (which is naturally highly restricted due to the low permeability of the Claygate Member and London Clay present beneath the site) would not be significantly affected by the proposed development.**

## 7 Conclusions

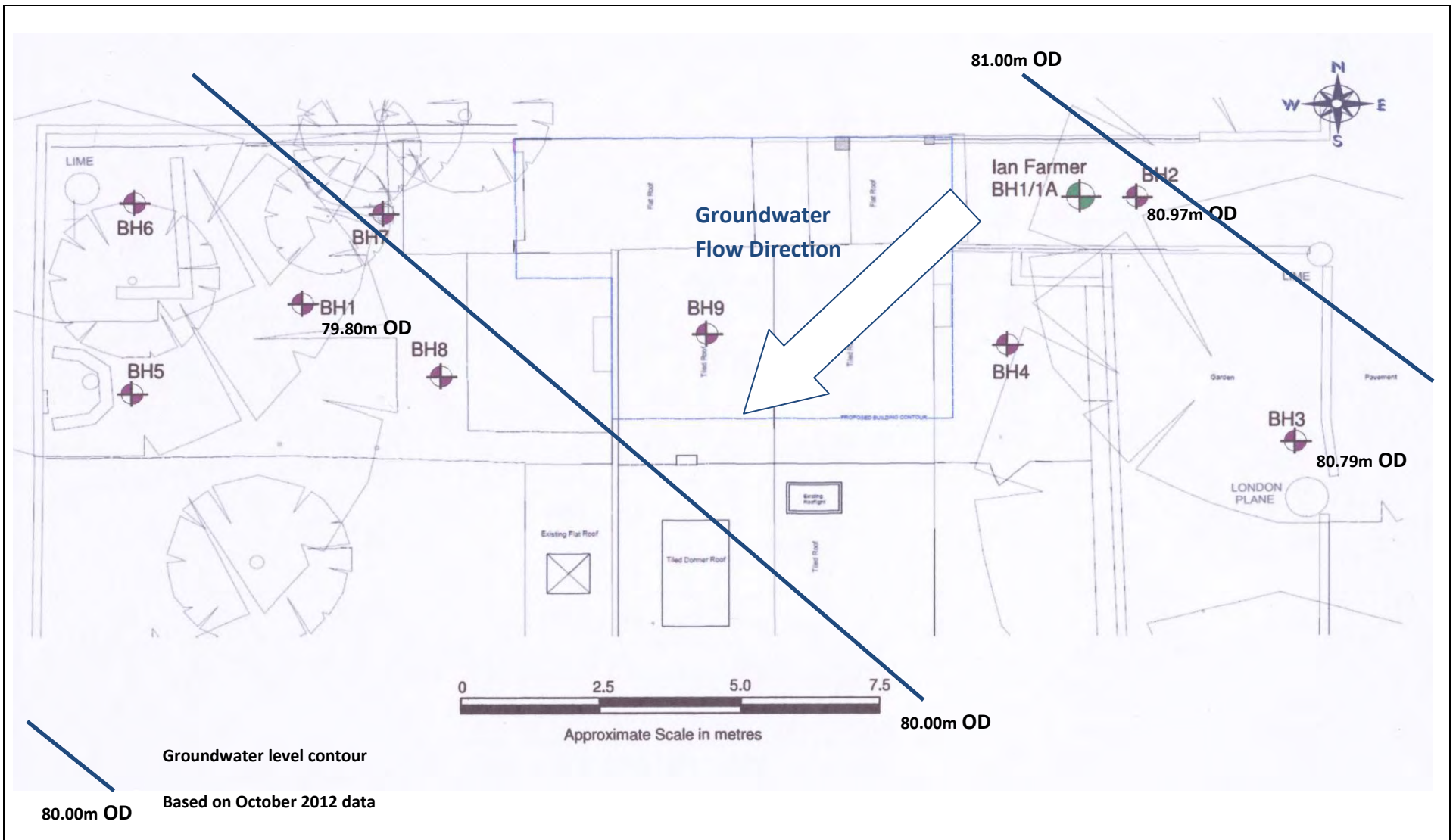
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A groundwater impact assessment of the proposed development has been undertaken. The assessment has been based on information and guidance published by the London Borough of Camden<sup>3</sup> and on site investigation information<sup>1,2,3</sup>.

Detailed site investigation information has established the presence of low permeability clays beneath the Site. Rates of groundwater flow are therefore very low (estimated at c.3m/a) and the underlying strata are incapable of supporting flow to water features such as streams or spring lines down gradient of the Site.

Changes in groundwater level due to potential damming effect adjacent to the proposed basement development would not occur beyond a few metres because of the very lowly permeable Claygate Member and London Clay Formation strata present beneath the Site.

It is concluded that the proposed basement development is unlikely to result in significant changes to the groundwater regime beneath or adjacent to the Site. No potential adverse impacts have been identified as a result of the groundwater impact assessment.



Site	59 Maresfield Gardens	Job Number	1102
Client	Stefanie Drews & Colin Rowat	Drawing Date	09-11-12
Engineer	Elliott Wood		



Geotechnical &  
Environmental  
Associates

Tythenhanger House  
Coursers Road  
St Albans  
Herts AL4 0PG

### Cross-Section

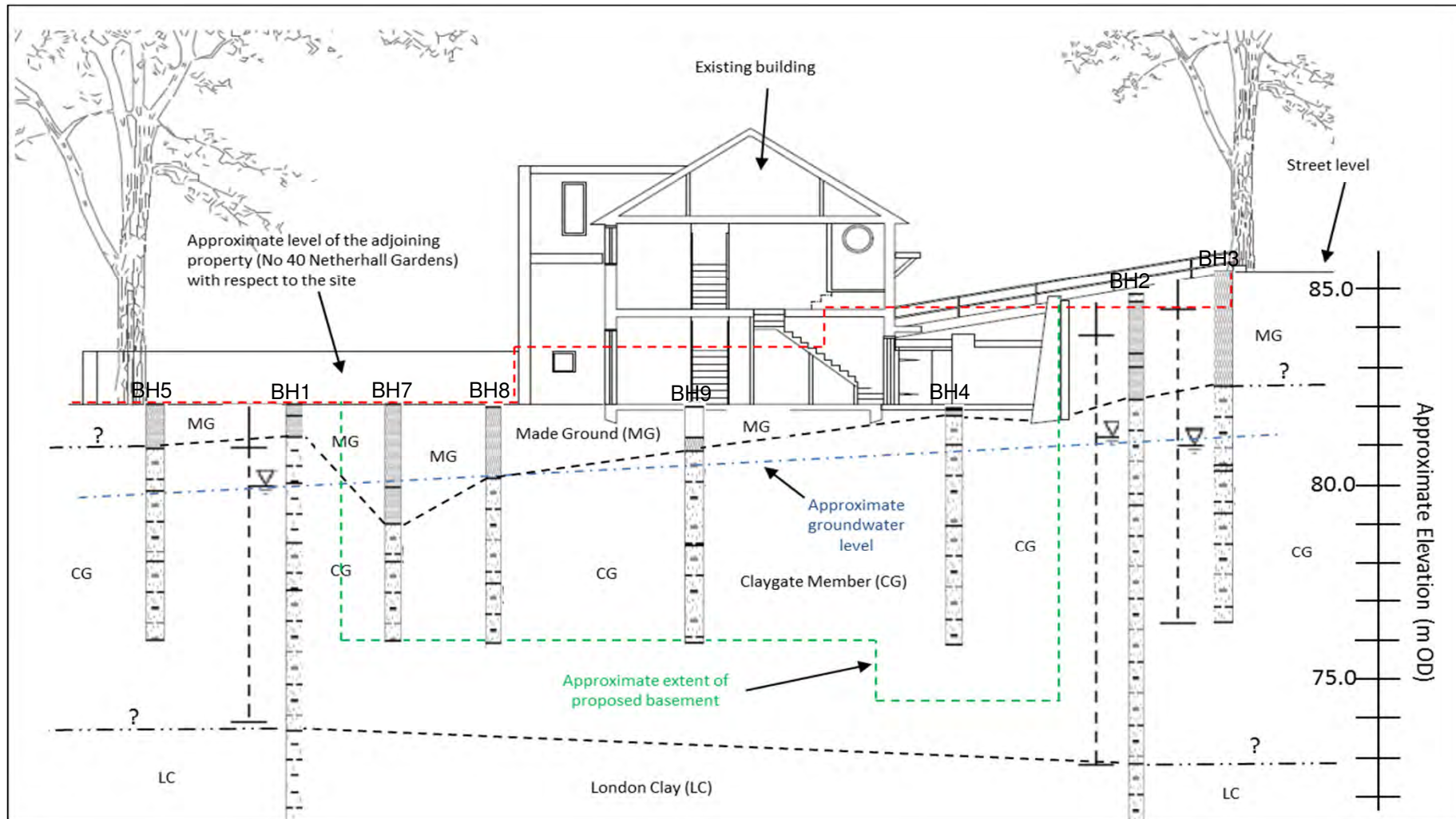
**Site** 59 Maresfield Gardens, London, NW3 5TE

**Client** Stefanie Drews & Colin Rowat

**Engineer** Elliott Wood

**Job Number**  
J11251

**Sheet**  
1 / 1



Site 59 Maresfield Gardens, London, NW3 5TE

Client Stefanie Drews & Colin Rowat

Engineer Elliott Wood

Job Number

J11251

Sheet

1/3

Rising Head Permeability Test.

<b>BOREHOLE No</b>	BH1
<b>TEST NO</b>	1
<b>DATE</b>	22/10/2012

<i>AT START OF TEST</i>	
<b>BH Depth</b>	7.84
<b>Casing Depth</b>	
<b>Water Level (m)</b>	1.90

<i>TIME</i>	<i>WATER LEVEL (m)</i>
0 min	5.22
1 min	4.94
2 min	4.80
3 min	4.71
4 min	4.64
5 min	4.57
10 min	4.33
15 min	4.14
20 min	4.01
25 min	3.91
30 min	3.82
45 min	3.57
1 hr	3.35
1 hr 30 min	3.18
2 hr	3.13

<b>Borehole Depth at End of Test (m)</b>	7.82
--	------

REMARKS

Site 59 Maresfield Gardens, London, NW3 5TE

Job Number

J11251

Client Stefanie Drews & Colin Rowat

Sheet

2/3

Engineer Elliott Wood

Rising Head Permeability Test.

<b>BOREHOLE No</b>	BH2
<b>TEST NO</b>	1
<b>DATE</b>	22/10/2012

<i>AT START OF TEST</i>	
<b>BH Depth</b>	10.22
<b>Casing Depth</b>	
<b>Water Level (m)</b>	3.53

<i>TIME</i>	<i>WATER LEVEL (m)</i>
<b>0 min</b>	3.87
<b>1 min</b>	3.87
<b>2 min</b>	3.87
<b>3 min</b>	3.86
<b>4 min</b>	3.86
<b>5 min</b>	3.86
<b>10 min</b>	3.85
<b>15 min</b>	3.84
<b>20 min</b>	3.83
<b>25 min</b>	3.82
<b>30 min</b>	3.81
<b>45 min</b>	3.79
<b>1 hr</b>	3.77

<i>Borehole Depth at End of Test (m)</i>	10.34
--	-------

**REMARKS**

*An obstruction or kink in the standpipe results in the 50 mm diameter bailer being obstructed and therefore a 19 mm diameter bailer must be used.*

Site 59 Maresfield Gardens, London, NW3 5TE

Job Number  
J11251

Client Stefanie Drews & Colin Rowat

Sheet  
3/3

Engineer Elliott Wood

Rising Head Permeability Test.

<b>BOREHOLE No</b>	BH3
<b>TEST NO</b>	1
<b>DATE</b>	22/10/2012

<i>AT START OF TEST</i>	
<b>BH Depth</b>	8.65
<b>Casing Depth</b>	
<b>Water Level (m)</b>	4.51

<i>TIME</i>	<i>WATER LEVEL (m)</i>
0 min	8.30
1 min	8.26
2 min	8.23
3 min	8.20
4 min	8.17
5 min	8.14
10 min	8.00
15 min	7.85
20 min	7.69
25 min	7.57
30 min	7.44
45 min	7.05
1 hr	6.68
1 hr 30 min	6.00
2 hr	5.41

<i>Borehole Depth at End of Test (m)</i>	8.70
--	------

REMARKS



**Chord Environmental**  
**Rising Head Data - Calculations using Horslev Test (1951)**

**Client:** Geotechnical and Environmental Associates  
**Project:** 59 Maresfield Gardens  
**Project No.:** 1102  
**Borehole No.:** BH1

**Abbreviations**  
L Length of test section  
D Borehole diameter  
d Stand Pipe diameter  
m Permeability transformation ratio  
h0 = excess head at time t0 (m)  
h = excess head at time t (m)  
t1 = time at t1 (minutes)  
h1 = excess head at time t1 (m)  
t2 = time at t2 (minutes)  
h2 = excess head at time t2 (m)  
K = hydraulic conductivity (m/d)  
All depths in metres below datum (borehole cover).

**Calculations**  
**FORMULA APPLIED =**  $k = d^2 \cdot \ln(2mL/D) \cdot \ln(h_1/h_2) / 8 \cdot L \cdot (t_2 - t_1)$   
**NB** Only applicable when  $mL/D > 4$  See Horslev 1951, pg 44 equation G.

**Analysis**

BH1	Section Tested	1.90 - 7.84	mBD
	Borehole Depth	7.84	mBD
	Length of test section (L)	5.94	m
	Borehole diameter (D)	0.1	m
	Standpipe diameter (d)	0.05	m
	Transformation ratio (m)	1	
	Depth to rest water level	1.90	mBD
	Water level at test start (mbd)	3.69	mBD

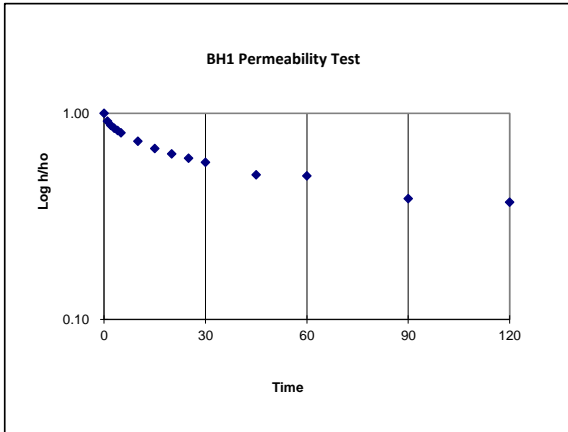
**Selected Values**

t1=	30.00	minutes
h1=	1.92	m
t2=	120.00	minutes
h2=	1.23	m

**PERMEABILITY OF BOREHOLE SECTION:** **0.001791 m/day**  
**2.07E-08 m/sec**

**Prepared by:** John Evans **Date:** 30-Oct-12  
**Reference:** Horslev 1951  
Time Lag and Soil Permeability in Groundwater Observations  
Bulletin No. 36, Waterways Experiment Station, Mississippi.

Time (seconds)	TIME (minutes)	h (metres)	h/h0
0	0.00	3.32	1.00
60	1.00	3.04	0.92
120	2.00	2.9	0.87
180	3.00	2.81	0.85
240	4.00	2.74	0.83
300	5.00	2.67	0.80
600	10.00	2.43	0.73
900	15.00	2.24	0.67
1200	20.00	2.11	0.64
1500	25.00	2.01	0.61
1800	30.00	1.92	0.58
2700	45.00	1.67	0.50
3600	60.00	1.65	0.50
5400	90.00	1.28	0.39
7200	120.00	1.23	0.37



**Chord Environmental**  
**Rising Head Data - Calculations using Horslev Test (1951)**

**Client:** Geotechnical and Environmental Associates  
**Project:** 59 Maresfield Gardens  
**Project No.:** 1102  
**Borehole No.:** BH2

**Abbreviations**  
L Length of test section  
D Borehole diameter  
d Stand Pipe diameter  
m Permeability transformation ratio

h0 = excess head at time t0 (m)  
h = excess head at time t (m)  
t1 = time at t1 (minutes)  
h1 = excess head at time t1 (m)  
t2 = time at t2 (minutes)  
h2 = excess head at time t2 (m)  
K = hydraulic conductivity (m/d)

All depths in metres below datum (borehole cover).

**Calculations**  
**FORMULA APPLIED =**  $k = d^2 \cdot \ln(2mL/D) \cdot \ln(h_1/h_2) / 8 \cdot L(t_2 - t_1)$   
**NB** Only applicable when  $mL/D > 4$  See Horslev 1951, pg 44 equation G.

**Analysis**

BH2	Section Tested	3.53 - 10.22	mBD
	Borehole Depth	10.22	mBD
	Length of test section (L)	6.69	m
	Borehole diameter (D)	0.1	m
	Standpipe diameter (d)	0.05	m
	Transformation ratio (m)	1	
	Depth to rest water level	3.53	mBD
	Water level at test start (mbd)	3.87	mBD

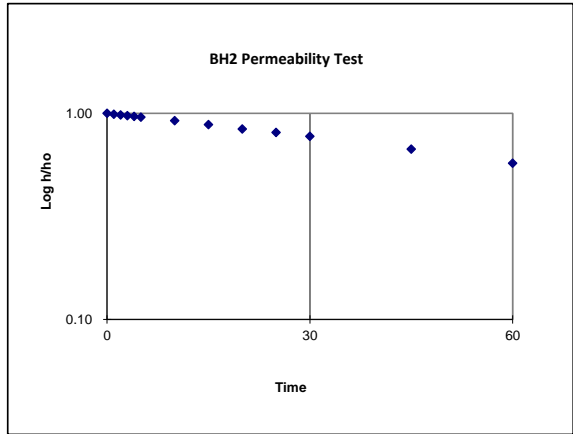
**Selected Values**

t1=	10.00	minutes
h1=	0.32	m
t2=	60.00	minutes
h2=	0.24	m

**PERMEABILITY OF BOREHOLE SECTION:** **0.001895 m/day**  
**2.19E-08 m/sec**

**Prepared by:** John Evans **Date:** 30-Oct-12  
**Reference:** Horslev 1951  
Time Lag and Soil Permeability in Groundwater Observations  
Bulletin No. 36, Waterways Experiment Station, Mississippi.

Time (seconds)	TIME (minutes)	h (metres)	h/h0
0	0.00	0.34	1.00
60	1.00	0.34	1.00
120	2.00	0.34	1.00
180	3.00	0.33	0.97
240	4.00	0.33	0.97
300	5.00	0.33	0.97
600	10.00	0.32	0.94
900	15.00	0.31	0.91
1200	20.00	0.30	0.88
1500	25.00	0.29	0.85
1800	30.00	0.28	0.82
2700	45.00	0.26	0.76
3600	60.00	0.24	0.71



**Chord Environmental**  
**Rising Head Data - Calculations using Horslev Test (1951)**

**Client:** Geotechnical and Environmental Associates  
**Project:** 59 Maresfield Gardens  
**Project No.:** 1102  
**Borehole No.:** BH3

**Abbreviations**  
L Length of test section  
D Borehole diameter  
d Stand Pipe diameter  
m Permeability transformation ratio

h<sub>0</sub> = excess head at time t<sub>0</sub> (m)  
h = excess head at time t (m)  
t<sub>1</sub> = time at t<sub>1</sub> (minutes)  
h<sub>1</sub> = excess head at time t<sub>1</sub> (m)  
t<sub>2</sub> = time at t<sub>2</sub> (minutes)  
h<sub>2</sub> = excess head at time t<sub>2</sub> (m)  
K = hydraulic conductivity (m/d)

All depths in metres below datum (borehole cover).

**Calculations**  
**FORMULA APPLIED =**  $k = d^2 \cdot \ln(2mL/D) \cdot \ln(h_1/h_2) / 8 \cdot L(t_2 - t_1)$   
**NB** Only applicable when  $mL/D > 4$  See Horslev 1951, pg 44 equation G.

**Analysis**

BH3	Section Tested	4.51 - 8.65	mBD
	Borehole Depth	8.65	mBD
	Length of test section (L)	4.14	m
	Borehole diameter (D)	0.1	m
	Standpipe diameter (d)	0.05	m
	Transformation ratio (m)	1	
	Depth to rest water level	4.51	mBD
	Water level at test start (mbd)	8.30	mBD

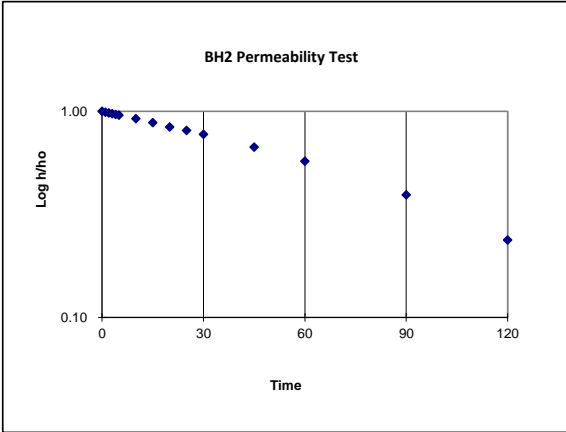
**Selected Values**

t <sub>1</sub> =	0.00	minutes
h <sub>1</sub> =	3.79	m
t <sub>2</sub> =	120.00	minutes
h <sub>2</sub> =	0.90	m

**PERMEABILITY OF BOREHOLE SECTION:** **0.005751 m/day**  
**6.66E-08 m/sec**

**Prepared by:** John Evans **Date:** 30-Oct-12  
**Reference:** Horslev 1951  
Time Lag and Soil Permeability in Groundwater Observations  
Bulletin No. 36, Waterways Experiment Station, Mississippi.

Time (seconds)	TIME (minutes)	h (metres)	h/h <sub>0</sub>
0	0.00	3.79	1.00
60	1.00	3.75	0.99
120	2.00	3.72	0.98
180	3.00	3.69	0.97
240	4.00	3.66	0.97
300	5.00	3.63	0.96
600	10.00	3.49	0.92
900	15.00	3.34	0.88
1200	20.00	3.18	0.84
1500	25.00	3.06	0.81
1800	30.00	2.93	0.77
2700	45.00	2.54	0.67
3600	60.00	2.17	0.57
5400	90.00	1.49	0.39
7200	120.00	0.9	0.24



Radius of influence (Sichardt)

$$R_0 = Cs\sqrt{K}$$

Essential input

Empirical equation based on drawdown and permeability

Optional input

		expected	min	max
Drawdown in well	s	2 m	1 m	5 m
Hydraulic conductivity	K	5E-08 m/s	5E-09 m/s	5E-07 m/s
		0.00432 m/d	0.000432 m/d	0.0432 m/d
Factor	C	1750	3000 for radial flow 1500-2000 for line flow to trenches or wellpoints	
Radius of influence	R <sub>0</sub>	0.8 m	0.1 m	6.2 m

The following assumptions apply to this equation

- the aquifer is unconfined
- the aquifer has infinite areal extent
- the aquifer is homogeneous, isotropic and of uniform thickness
- flat initial water table
- the aquifer is pumped at a constant discharge rate
- the pumping well is fully penetrating, therefore receiving water from the entire saturated thickness of the aquifer
- the flow to the well is in a steady state

Data sources (to complete an audit trail)

Drawdown in well	s	Assumed - increase close to existing ground level
Hydraulic conductivity	K	Calculated from site specific rising head tests
Factor	C	Linear nature of structure.



Radius of influence (Bear)

$$R_0(t) = 1.5 \sqrt{\left(\frac{Tt}{S}\right)}$$

Radius of influence for a pumping well in an infinite confined aquifer

Essential input

Optional input

Calculated

Transmissivity of aquifer	T	expected 0.04 m <sup>2</sup> /d	min 0.1 m <sup>2</sup> /d	max 0.1 m <sup>2</sup> /d
Storage coefficient	S	0.2	0.2	0.2
Time from start of abstraction	t	182 d	182 d	182 d
Radius of influence at time t	R <sub>0</sub>	9.0 m	0.6 m	20.2 m

The following assumptions apply to this equation

- the aquifer is confined
- the aquifer has infinite areal extent
- the aquifer is homogeneous, isotropic and of uniform thickness

Data sources (to complete an audit trail)

Transmissivity of aquifer	T	Calculated permeability multiplied by assumed 10m effective aquifer thickness
Storage coefficient	S	Assumed intergranular storage through sandier horizons
Time from start of abstraction	t	Assume six month period

## APPENDIX 4

### Summary Sheets from Retaining Wall Design Calculations

Temporary license on loan from Geosolve | Sheet No.  
 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types			
		Active side		Passive side	
1	84.00	1	Made Ground / Alluv	1	Made Ground / Alluv
2	76.00	2	Claygate Beds	2	Claygate Beds
3	73.50	3	London Clay	3	London Clay

**SOIL PROPERTIES**

-- Soil type -- No. Description (Datum elev.)	Bulk density kN/m3	Young's Modulus Eh, kN/m2 (dEh/dy)	At rest coeff. Ko (dKo/dy)	Consol state. NC/OC ( Nu )	Active limit Ka ( Kac )	Passive limit Kp ( Kpc )	Cohesion kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 ( 2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 ( 2.390)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (2.476)	1.000 ( 2.477)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 ( 5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.253 ( 4.831)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.351 (1.391)	3.440 ( 5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

----- Soil type ----- No. Description	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.500	0.00
3 London Clay	0.00	0.670	0.00	0.00	0.670	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.500	0.00
6 London Clay Drained	25.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile no.	Active side				Passive side			
	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	73.00	73.00	0.0 MC
4	1	82.00	82.00	0.0	1	73.20	73.20	0.0 WC



**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.80 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 7.0700E-03 m4/m run  
 E.I = 197960 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	84.40	6.00	0.010000	2.000E+08	5.00	0.00	0	No
2	82.00	6.00	0.010000	2.000E+08	5.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	1.00	0.00	0	No
4	74.75	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5	79.50	6.00	0.100000	2.000E+08	5.00	0.00	0	No
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	3.000E+07	1.00	0.00	0	No
8	76.30	6.00	0.010000	2.000E+08	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- kN/m2 ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	84.00	0.00(A)	8.00	20.00	5.00	=	N/A	1.00 Var
2	84.00	5.00(A)	8.00	15.00	5.00	=	N/A	1.00 Var
3	84.00	1.00(A)	8.00	4.00	0.00	17.00	N/A	1.00 P/U
4	73.20	-0.00(P)	8.00	10.00	70.00	=	N/A	1.00 -
5	74.00	-0.00(P)	10.00	10.00	70.00	=	N/A	1.00 -
6	84.00	5.00(A)	10.00	15.00	17.00	=	N/A	1.00 P/U
7	83.00	5.00(A)	2.00	2.00	25.00	=	N/A	1.00 P/U

Note: A = Active side, P = Passive side

A trapezoidal surcharge is defined by two values:

N = at edge near to wall, F = at edge far from wall

Limit State Categories P/U = Permanent Unfavourable

P/F = Permanent Favourable

Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 84.00 No analysis at this stage
2	Apply surcharge no.2 at elevation 84.00 No analysis at this stage
3	Apply surcharge no.3 at elevation 84.00 No analysis at this stage
4	Apply surcharge no.6 at elevation 84.00 No analysis at this stage
5	Apply surcharge no.7 at elevation 83.00 No analysis at this stage
6	Install strut or anchor no.1 at elevation 84.40
7	Excavate to elevation 81.50 on PASSIVE side
8	Install strut or anchor no.2 at elevation 82.00
9	Apply water pressure profile no.1 ( Mod. Conserv. )
10	Excavate to elevation 77.50 on PASSIVE side
11	Install strut or anchor no.3 at elevation 78.00
12	Apply water pressure profile no.3 ( Mod. Conserv. )
13	Excavate to elevation 74.00 on PASSIVE side
14	Install strut or anchor no.4 at elevation 74.75
15	Apply surcharge no.4 at elevation 73.20
16	Install strut or anchor no.5 at elevation 79.50
17	Remove strut or anchor no.3 at elevation 78.00
18	Install strut or anchor no.6 at elevation 78.90
19	Remove strut or anchor no.5 at elevation 79.50
20	Install strut or anchor no.7 at elevation 81.65
21	Remove strut or anchor no.2 at elevation 82.00
22	Remove strut or anchor no.1 at elevation 84.40
23	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
24	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
25	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: Serviceability Limit State  
All loads and soil strengths are unfactored

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 6.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

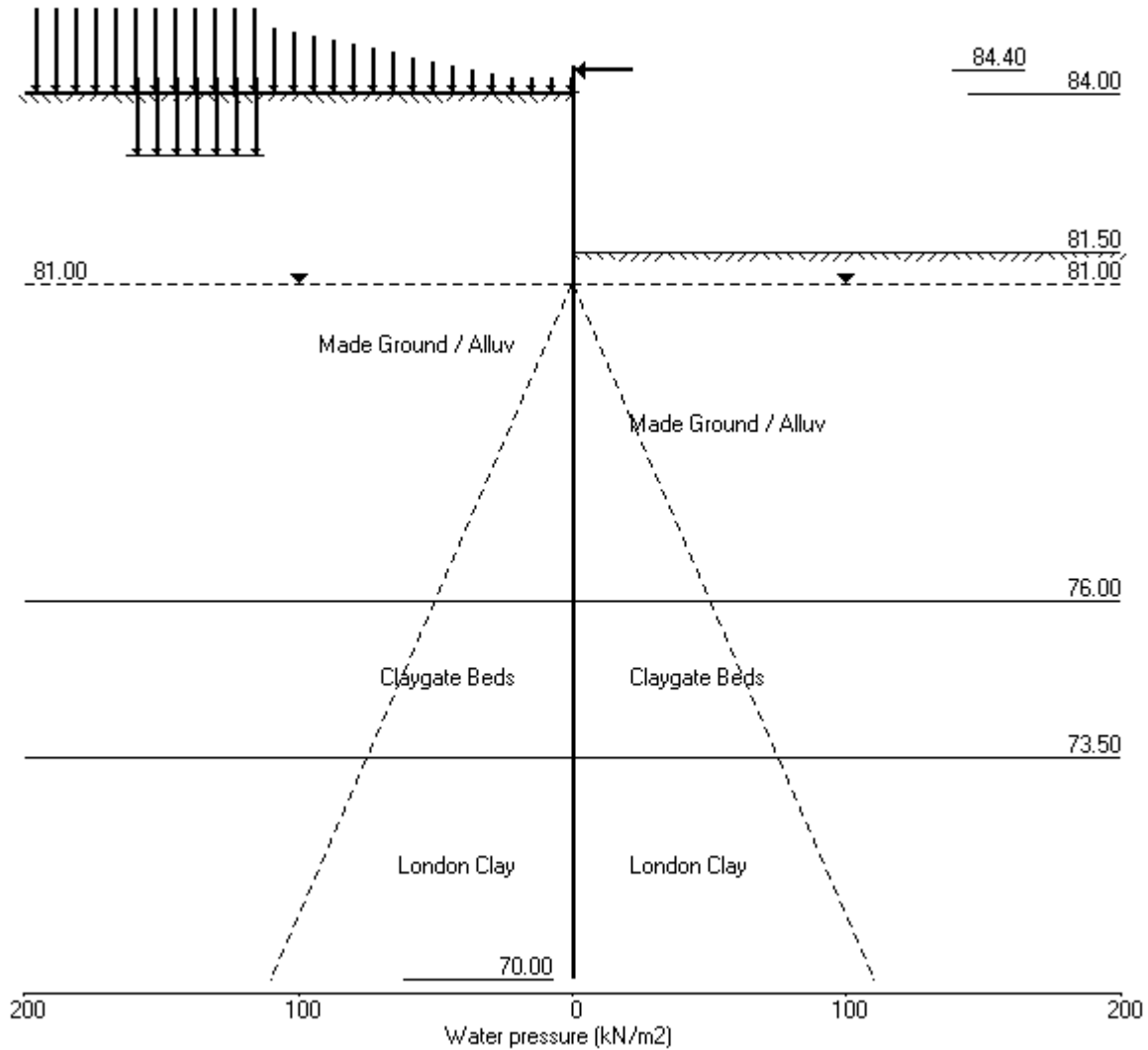
**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 84.00	No	No	No
2	Apply surcharge no.2 at elev. 84.00	No	No	No
3	Apply surcharge no.3 at elev. 84.00	No	No	No
4	Apply surcharge no.6 at elev. 84.00	No	No	No
5	Apply surcharge no.7 at elev. 83.00	No	No	No
6	Install strut no.1 at elev. 84.40	No	No	No
7	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
8	Install strut no.2 at elev. 82.00	No	No	No
9	Apply water pressure profile no.1	No	No	No
10	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
11	Install strut no.3 at elev. 78.00	No	No	No
12	Apply water pressure profile no.3	No	No	No
13	Excav. to elev. 74.00 on PASSIVE side	Yes	No	Yes
14	Install strut no.4 at elev. 74.75	No	No	No
15	Apply surcharge no.4 at elev. 73.20	No	No	No
16	Install strut no.5 at elev. 79.50	No	No	No
17	Remove strut no.3 at elev. 78.00	No	No	No
18	Install strut no.6 at elev. 78.90	No	No	No
19	Remove strut no.5 at elev. 79.50	No	No	No
20	Install strut no.7 at elev. 81.65	No	No	No
21	Remove strut no.2 at elev. 82.00	No	No	No
22	Remove strut no.1 at elev. 84.40	No	No	No
23	Change soil type 1 to soil type 4	No	No	No
24	Change soil type 2 to soil type 5	No	No	No
25	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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Units: kN,m

Stage No.7 Excav. to elev. 81.50 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 7 Excavate to elevation 81.50 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	FoS for toe elev. = 70.00	Moment of equil. at elev.	Toe elev. for FoS = 1.000	Wall Penetr- ation
7	84.00 81.50	84.40	7.328	n/a	81.31	0.19

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**  
**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.37E-03	-26.3	0.0	26.3
2	84.00	0.00	0.002	-1.36E-03	-26.3	-10.5	
3	83.50	2.50	0.003	-1.32E-03	-25.7	-23.6	
4	83.00	5.00	0.003	-1.25E-03	-23.8	-36.0	
5	82.50	7.50	0.004	-1.14E-03	-20.7	-47.2	
6	82.00	10.00	0.004	-1.01E-03	-16.3	-56.5	
7	81.65	11.77	0.005	-9.10E-04	-12.5	-61.3	
8	81.50	12.79	0.005	-8.63E-04	-10.7	-63.0	
		0.10	0.005	-8.63E-04	-10.7	-63.0	
9	81.00	2.34	0.005	-6.97E-04	-10.1	-68.1	
10	80.25	4.09	0.006	-4.27E-04	-7.6	-74.6	
11	79.50	9.48	0.006	-1.37E-04	-2.6	-78.5	
12	78.90	12.36	0.006	1.00E-04	4.0	-78.2	
13	78.45	12.89	0.006	2.74E-04	9.7	-75.1	
14	78.00	13.83	0.006	4.39E-04	15.7	-69.5	
15	77.50	15.32	0.005	6.02E-04	23.0	-59.9	
16	76.75	18.27	0.005	7.88E-04	35.6	-38.4	
17	76.00	21.71	0.004	8.74E-04	50.6	-6.7	
		-35.84	0.004	8.74E-04	50.6	-6.7	
18	75.38	-29.25	0.004	8.56E-04	30.2	17.8	
19	74.75	-22.36	0.003	7.79E-04	14.1	31.0	
20	74.00	-14.63	0.003	6.54E-04	0.2	35.2	
21	73.50	-10.10	0.002	5.67E-04	-6.0	33.4	
22	73.20	-7.53	0.002	5.18E-04	-8.6	31.1	
23	73.00	-5.94	0.002	4.88E-04	-10.0	29.3	
24	72.50	-2.36	0.002	4.21E-04	-12.0	23.5	
25	72.00	0.75	0.002	3.70E-04	-12.4	17.2	
26	71.20	5.15	0.001	3.20E-04	-10.1	7.3	
27	70.60	8.34	0.001	3.06E-04	-6.0	2.2	
28	70.00	11.72	0.001	3.03E-04	0.0	0.0	
Strut force at elev.			84.40 =	26.32 kN/m run =	157.89 kN/strut		

(continued)

Stage No.7 Excavate to elevation 81.50 on PASSIVE side

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective stresses Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	5.00	0.00	69.28	0.00	0.00a	3265
3	83.50	Total>	13.59	2.50m	77.87	2.50	2.50a	3265
4	83.00	Total>	22.49	5.00m	86.77	5.00	5.00a	3265
5	82.50	Total>	31.59	7.50m	95.87	7.50	7.50a	3265
6	82.00	Total>	40.74	10.00m	105.02	10.00	10.00a	3265
7	81.65	Total>	47.13	11.75m	111.41	11.77	11.77	3265
8	81.50	Total>	49.85	12.50m	114.13	12.79	12.79	3265
9	81.00	Total>	58.88	15.00m	123.16	16.31	16.31	3265
10	80.25	Total>	72.26	18.75m	136.54	25.71	25.71	3265
11	79.50	Total>	85.46	22.50m	149.73	35.60	35.60	3265
12	78.90	Total>	95.88	31.62	160.16	43.91	43.91	3265
13	78.45	Total>	103.64	39.38	167.92	50.38	50.38	3265
14	78.00	Total>	111.35	47.09	175.63	57.06	57.06	3265
15	77.50	Total>	119.87	55.61	184.15	64.69	64.69	3265
16	76.75	Total>	132.57	68.31	196.85	76.50	76.50	3265
17	76.00	Total>	145.19	80.93	209.47	88.57	88.57	3265
		Total>	145.19	40.00m	324.43	60.97	60.97	9796
18	75.38	Total>	156.29	43.13m	344.50	73.18	73.18	10286
19	74.75	Total>	167.36	46.25m	364.53	85.54	85.54	10776
20	74.00	Total>	180.62	50.00m	388.54	100.14	100.14	11364
21	73.50	Total>	189.45	52.50m	404.54	109.57	109.57	11756
		Total>	189.45	52.50m	412.37	162.57	162.57	11756
22	73.20	Total>	195.04	54.00m	421.83	169.66	169.66	11960
23	73.00	Total>	198.77	55.00m	428.13	174.33	174.33	12096
24	72.50	Total>	208.09	57.50m	443.89	185.81	185.81	12437
25	72.00	Total>	217.40	60.00m	459.65	197.06	197.06	12778
26	71.20	Total>	232.31	64.00m	484.85	214.77	214.77	13323
27	70.60	Total>	243.49	67.00m	503.76	228.01	228.01	13732
28	70.00	Total>	254.67	70.00m	522.67	241.33	241.33	14140

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective stresses Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	64.28	12.70	12.70	3431
9	81.00	Total>	8.50	2.50m	72.78	13.97	13.97	3431
10	80.25	Total>	21.28	6.25m	85.56	21.62	21.62	3431
11	79.50	Total>	34.14	10.00m	98.42	26.12	26.12	3431
12	78.90	Total>	44.49	13.00m	108.77	31.55	31.55	3431
13	78.45	Total>	52.31	15.25m	116.59	37.49	37.49	3431
14	78.00	Total>	60.17	17.50m	124.45	43.23	43.23	3431
15	77.50	Total>	68.97	20.00m	133.24	49.37	49.37	3431
16	76.75	Total>	82.26	23.75m	146.54	58.23	58.23	3431

(continued)

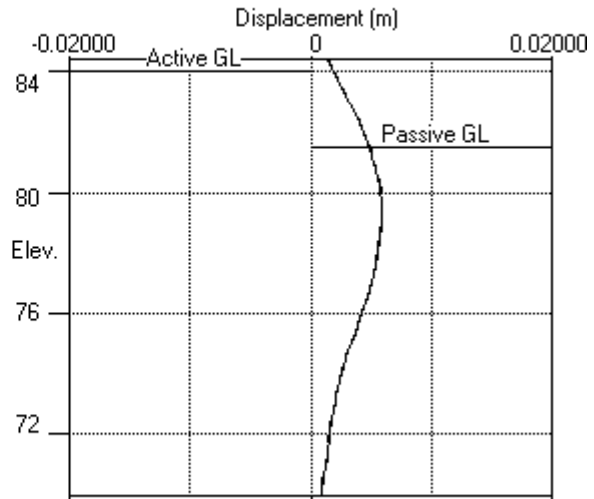
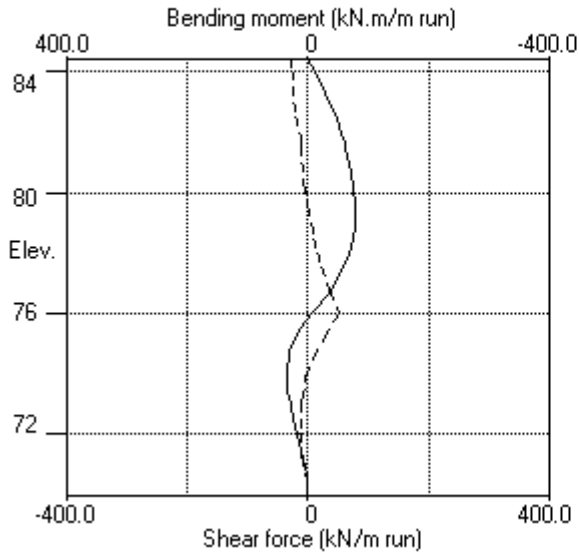
Stage No.7 Excavate to elevation 81.50 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure	Soil stiffness coeff.
		Water press.	Vertical	Effective Active limit	Effective Passive limit	Earth pressure		
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3	
17	76.00	Total>	95.68	31.42	159.96	66.86	3431	
		Total>	95.68	27.50m	274.93	96.81	10293	
18	75.38	Total>	107.57	30.63m	295.78	102.43	10808	
19	74.75	Total>	119.52	33.75m	316.69	107.90	11322	
20	74.00	Total>	133.92	37.50m	341.85	114.77	11940	
21	73.50	Total>	143.56	40.00m	358.65	119.67	12351	
		Total>	143.56	40.00m	366.48	172.67	12351	
22	73.20	Total>	149.65	41.50m	376.43	177.19	12566	
23	73.00	Total>	153.71	42.50m	383.07	180.27	12709	
24	72.50	Total>	163.87	45.00m	399.68	188.16	13067	
25	72.00	Total>	174.05	47.50m	416.29	196.30	13425	
26	71.20	Total>	190.33	51.50m	442.87	209.62	13998	
27	70.60	Total>	202.54	54.50m	462.81	219.67	14427	
28	70.00	Total>	214.74	57.50m	482.74	229.61	14857	

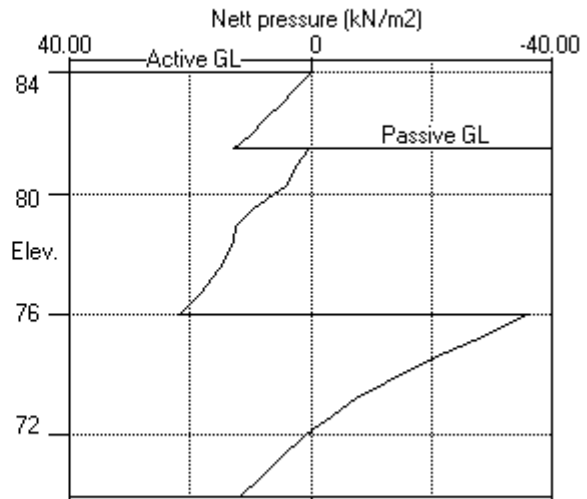
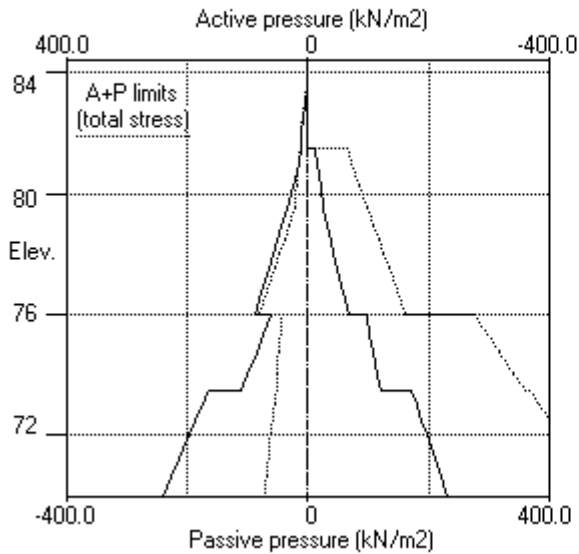
Note: 10.00a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.7 Excav. to elev. 81.50 on PASSIVE side



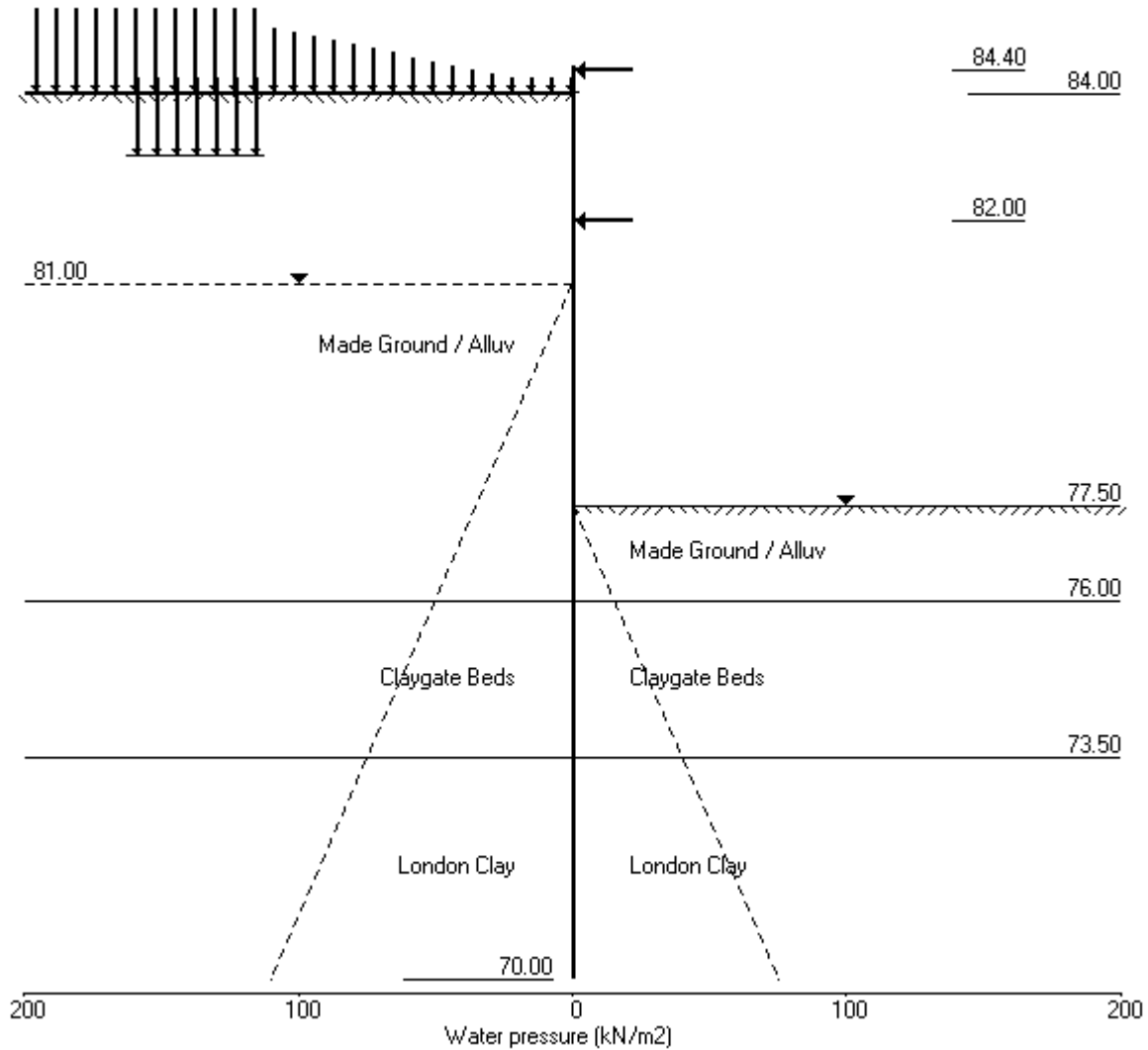
Stage No.7 Excav. to elev. 81.50 on PASSIVE side





Units: kN,m

Stage No.10 Excav. to elev. 77.50 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 10 Excavate to elevation 77.50 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

				FoS for toe	Toe elev. for
				elev. = 70.00	FoS = 1.000
				-----	-----
Stage	--- G.L. ---	Strut	Factor	Moment	Toe
No.	Act. Pass.	Elev.	of	of equilib.	Wall
			Safety	at elev.	Penetr
			at elev.		-ation
10	84.00 77.50		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**  
**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-2.05E-03	0.0	0.0	-0.0
2	84.00	0.00	0.002	-2.05E-03	0.0	-0.0	
		8.14	0.002	-2.05E-03	0.0	-0.0	
3	83.50	2.50	0.003	-2.05E-03	2.7	1.1	
4	83.00	5.00	0.004	-2.06E-03	4.5	2.9	
5	82.50	7.50	0.005	-2.07E-03	7.7	5.9	
6	82.00	10.00	0.006	-2.09E-03	12.0	10.8	93.0
		10.00	0.006	-2.09E-03	-81.0	10.8	
7	81.65	11.75	0.006	-2.08E-03	-77.2	-16.7	
8	81.50	12.50	0.007	-2.07E-03	-75.4	-28.1	
9	81.00	15.00	0.008	-1.95E-03	-68.5	-64.1	
10	80.25	18.75	0.009	-1.62E-03	-55.9	-110.6	
11	79.50	22.50	0.010	-1.13E-03	-40.4	-146.8	
12	78.90	31.62	0.011	-6.60E-04	-24.2	-166.4	
13	78.45	39.38	0.011	-2.74E-04	-8.2	-173.8	
14	78.00	47.09	0.011	1.20E-04	11.3	-173.3	
15	77.50	55.61	0.011	5.43E-04	37.0	-161.5	
		34.61	0.011	5.43E-04	37.0	-161.5	
16	76.75	43.94	0.010	1.08E-03	66.4	-123.5	
17	76.00	54.10	0.009	1.43E-03	103.2	-60.9	
		-46.53	0.009	1.43E-03	103.2	-60.9	
18	75.38	-46.82	0.008	1.53E-03	74.0	-6.1	
19	74.75	-46.00	0.007	1.49E-03	45.0	30.4	
20	74.00	-36.53	0.006	1.33E-03	14.1	54.7	
21	73.50	-26.83	0.006	1.19E-03	-1.8	57.1	
22	73.20	-21.10	0.005	1.11E-03	-9.0	55.4	
23	73.00	-17.50	0.005	1.05E-03	-12.8	53.2	
24	72.50	-9.24	0.005	9.33E-04	-19.5	44.5	
25	72.00	-1.90	0.004	8.35E-04	-22.3	33.5	
26	71.20	8.62	0.003	7.37E-04	-19.6	14.8	



(continued)

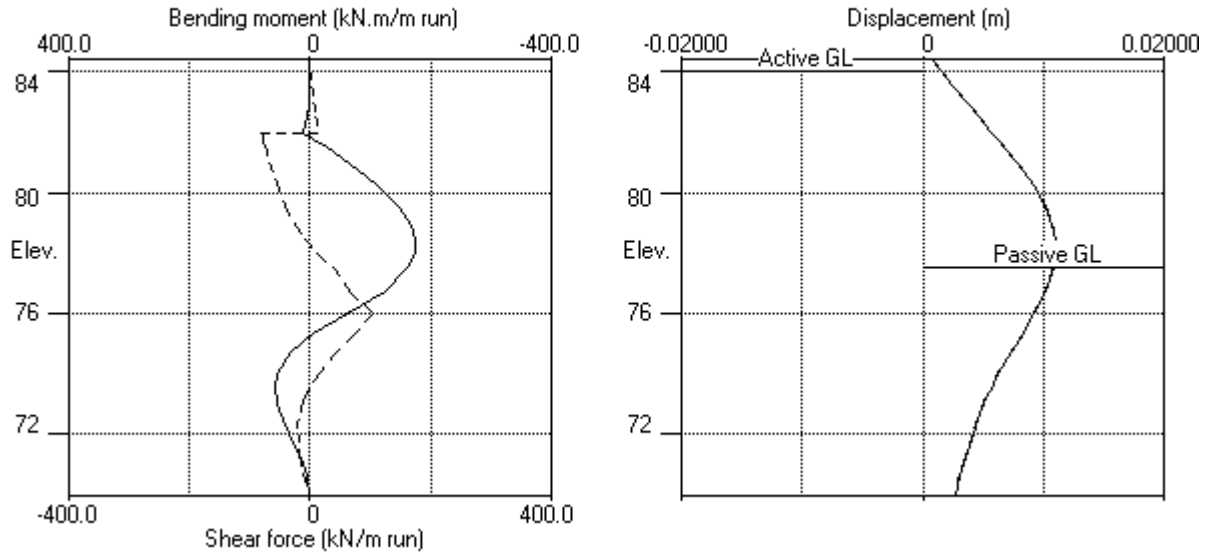
Stage No.10 Excavate to elevation 77.50 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	64.28	21.00	21.00	3859
16	76.75	Total>	12.77	3.75m	77.05	24.36	24.36	3859
17	76.00	Total>	25.65	7.50m	89.93	26.83	26.83	3859
		Total>	25.65	7.50m	204.90	86.53	86.53	11578
18	75.38	Total>	37.18	10.63m	225.39	89.94	89.94	12157
19	74.75	Total>	48.89	13.75m	246.06	92.25	92.25	12735
20	74.00	Total>	63.25	17.50m	271.17	94.85	94.85	13430
21	73.50	Total>	73.01	20.00m	288.11	97.01	97.01	13893
		Total>	73.01	20.00m	295.93	150.01	150.01	13893
22	73.20	Total>	79.24	21.50m	306.03	152.88	152.88	14135
23	73.00	Total>	83.42	22.50m	312.78	154.92	154.92	14296
24	72.50	Total>	93.98	25.00m	329.78	160.45	160.45	14698
25	72.00	Total>	104.67	27.50m	346.91	166.52	166.52	15101
26	71.20	Total>	122.02	31.50m	374.57	176.99	176.99	15745
27	70.60	Total>	135.20	34.50m	395.48	185.05	185.05	16228
28	70.00	Total>	148.50	37.50m	416.50	192.98	192.98	16711

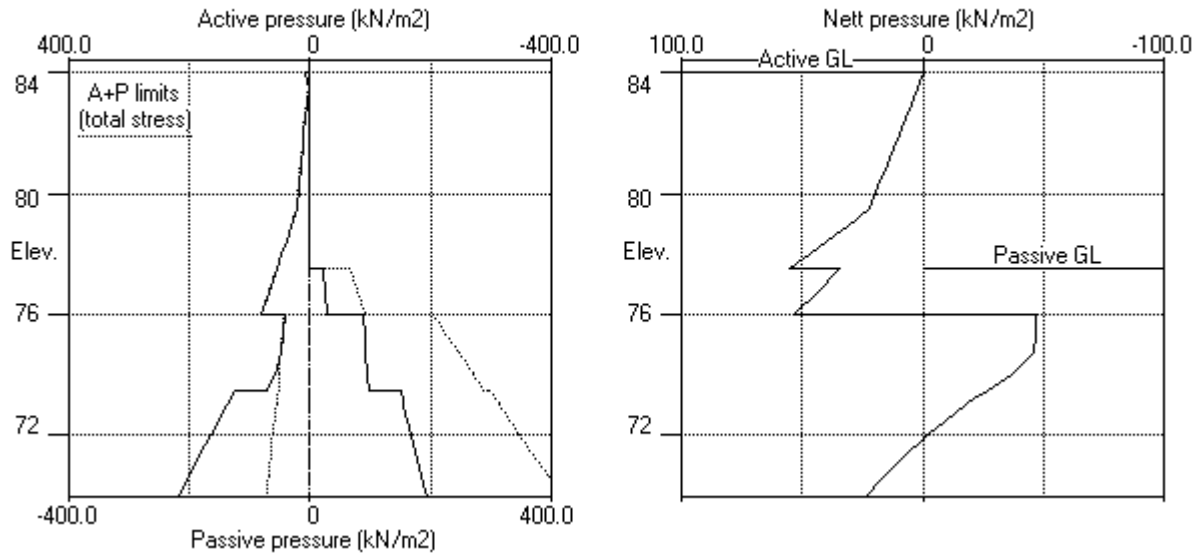
Note: 46.25a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.10 Excav. to elev. 77.50 on PASSIVE side

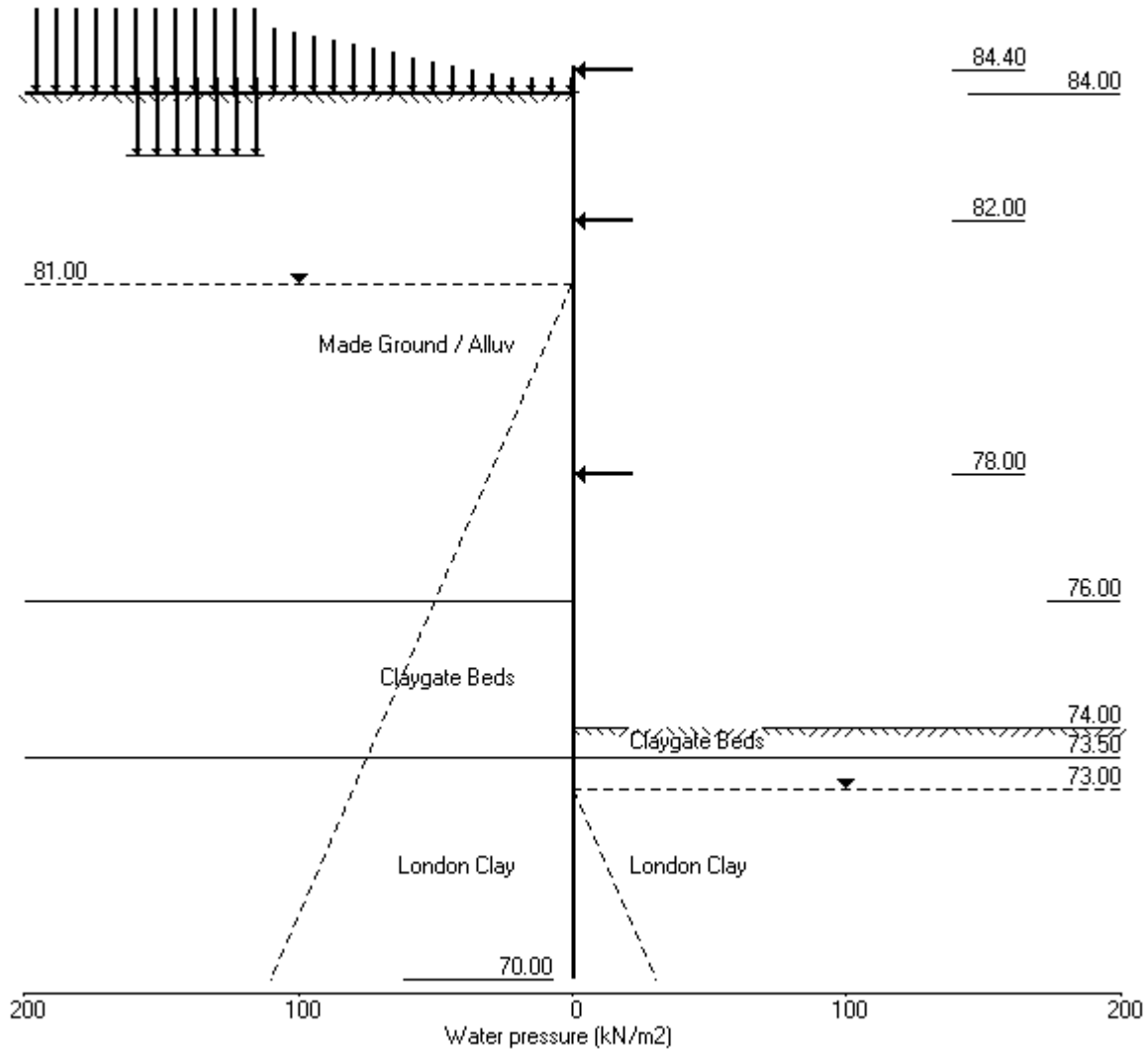


Stage No.10 Excav. to elev. 77.50 on PASSIVE side



Units: kN,m

Stage No.13 Excav. to elev. 74.00 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 13 Excavate to elevation 74.00 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

				FoS for toe	Toe elev. for
				elev. = 70.00	FoS = 1.000
				-----	-----
Stage	--- G.L. ---	Strut	Factor	Moment	Toe
No.	Act. Pass.	Elev.	of	of equilib.	Wall
			Safety	at elev.	Penetr
			at elev.		-ation
13	84.00 74.00		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**  
**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.85E-03	0.0	0.0	-0.0
2	84.00	0.00	0.002	-1.85E-03	0.0	-0.0	
		8.07	0.002	-1.85E-03	0.0	-0.0	
3	83.50	2.93	0.003	-1.85E-03	2.8	1.1	
4	83.00	5.88	0.003	-1.86E-03	5.0	3.0	
5	82.50	8.83	0.004	-1.87E-03	8.6	6.3	
6	82.00	11.77	0.005	-1.89E-03	13.8	11.8	67.1
		11.77	0.005	-1.89E-03	-53.3	11.8	
7	81.65	13.82	0.006	-1.90E-03	-48.9	-5.8	
8	81.50	14.70	0.006	-1.89E-03	-46.7	-13.0	
9	81.00	17.53	0.007	-1.83E-03	-38.7	-34.3	
10	80.25	21.44	0.009	-1.66E-03	-24.0	-57.8	
11	79.50	24.66	0.010	-1.42E-03	-6.8	-69.3	
12	78.90	32.65	0.010	-1.21E-03	10.4	-68.4	
13	78.45	39.38	0.011	-1.06E-03	26.6	-60.1	
14	78.00	47.09	0.011	-9.49E-04	46.1	-43.9	164.4
		47.09	0.011	-9.49E-04	-118.3	-43.9	
15	77.50	55.61	0.012	-7.71E-04	-92.6	-96.9	
16	76.75	68.31	0.012	-3.03E-04	-46.2	-149.9	
17	76.00	80.93	0.012	2.92E-04	9.8	-164.6	
		40.00	0.012	2.92E-04	9.8	-164.6	
18	75.38	43.13	0.012	7.90E-04	35.8	-151.1	
19	74.75	46.25	0.011	1.21E-03	63.7	-120.8	
20	74.00	50.00	0.010	1.55E-03	99.8	-56.9	
		-46.76	0.010	1.55E-03	99.8	-56.9	
21	73.50	-44.88	0.009	1.64E-03	76.9	-13.2	
		-76.85	0.009	1.64E-03	76.9	-13.2	
22	73.20	-68.04	0.009	1.65E-03	55.2	6.4	
23	73.00	-61.90	0.009	1.63E-03	42.2	16.0	
24	72.50	-46.22	0.008	1.58E-03	15.1	29.4	





(continued)

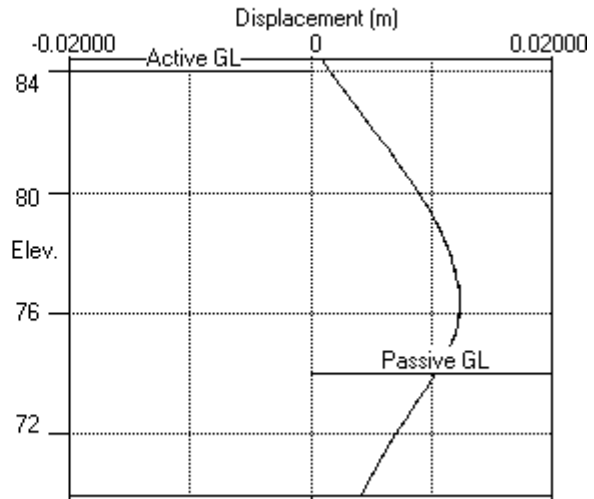
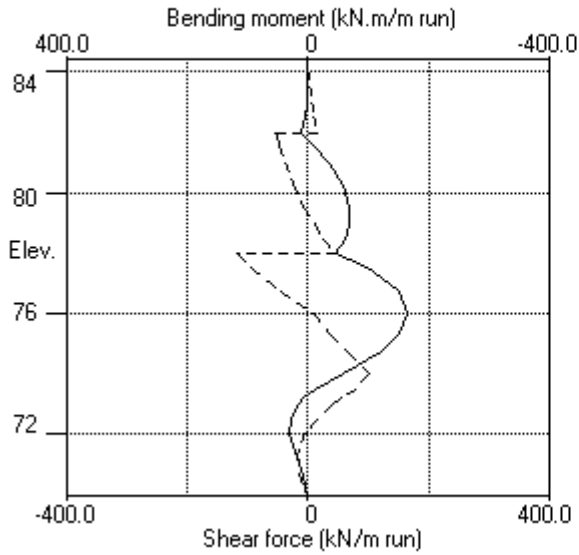
Stage No.13 Excavate to elevation 74.00 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
7	81.65	0.00	0.00	0.00	0.00	0.00	0.0	
8	81.50	0.00	0.00	0.00	0.00	0.00	0.0	
9	81.00	0.00	0.00	0.00	0.00	0.00	0.0	
10	80.25	0.00	0.00	0.00	0.00	0.00	0.0	
11	79.50	0.00	0.00	0.00	0.00	0.00	0.0	
12	78.90	0.00	0.00	0.00	0.00	0.00	0.0	
13	78.45	0.00	0.00	0.00	0.00	0.00	0.0	
14	78.00	0.00	0.00	0.00	0.00	0.00	0.0	
15	77.50	0.00	0.00	0.00	0.00	0.00	0.0	
16	76.75	0.00	0.00	0.00	0.00	0.00	0.0	
17	76.00	0.00	0.00	0.00	0.00	0.00	0.0	
18	75.38	0.00	0.00	0.00	0.00	0.00	0.0	
19	74.75	0.00	0.00	0.00	0.00	0.00	0.0	
20	74.00	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	207.93	96.76	15938	
21	73.50	Total>	9.01	2.50m	224.10	97.38	16488	
		Total>	9.01	2.50m	231.93	150.38	16488	
22	73.20	Total>	14.74	4.00m	241.52	151.26	16775	
23	73.00	Total>	18.57	5.00m	247.94	151.68	16966	
24	72.50	Total>	28.24	7.50m	264.04	152.67	17444	
25	72.00	Total>	38.06	10.00m	280.30	153.54	17921	
26	71.20	Total>	54.16	14.00m	306.71	155.03	18686	
27	70.60	Total>	66.62	17.00m	326.89	156.11	19259	
28	70.00	Total>	79.41	20.00m	347.41	156.88	19832	

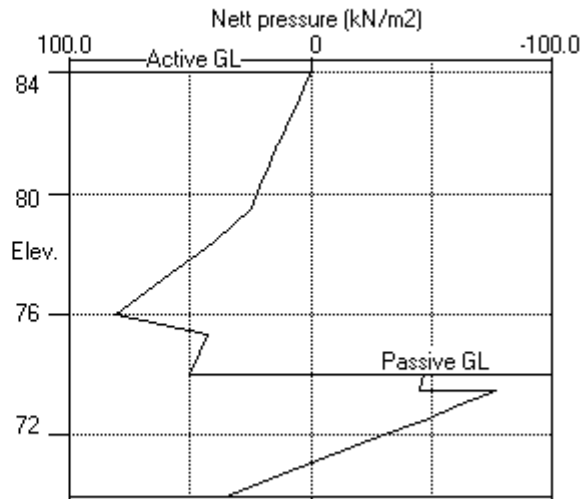
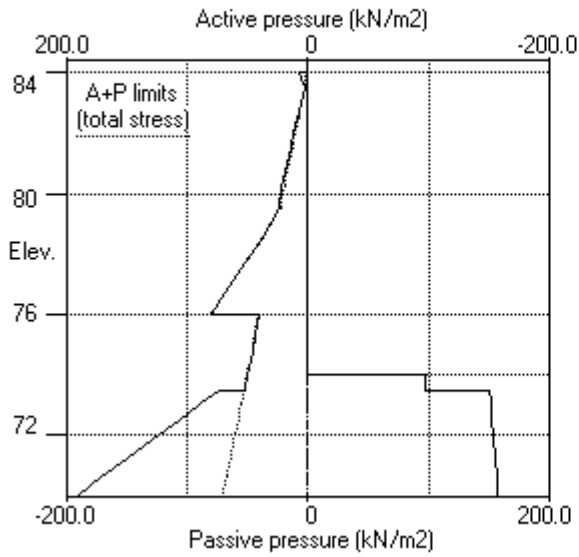
Note: 52.50a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.13 Excav. to elev. 74.00 on PASSIVE side

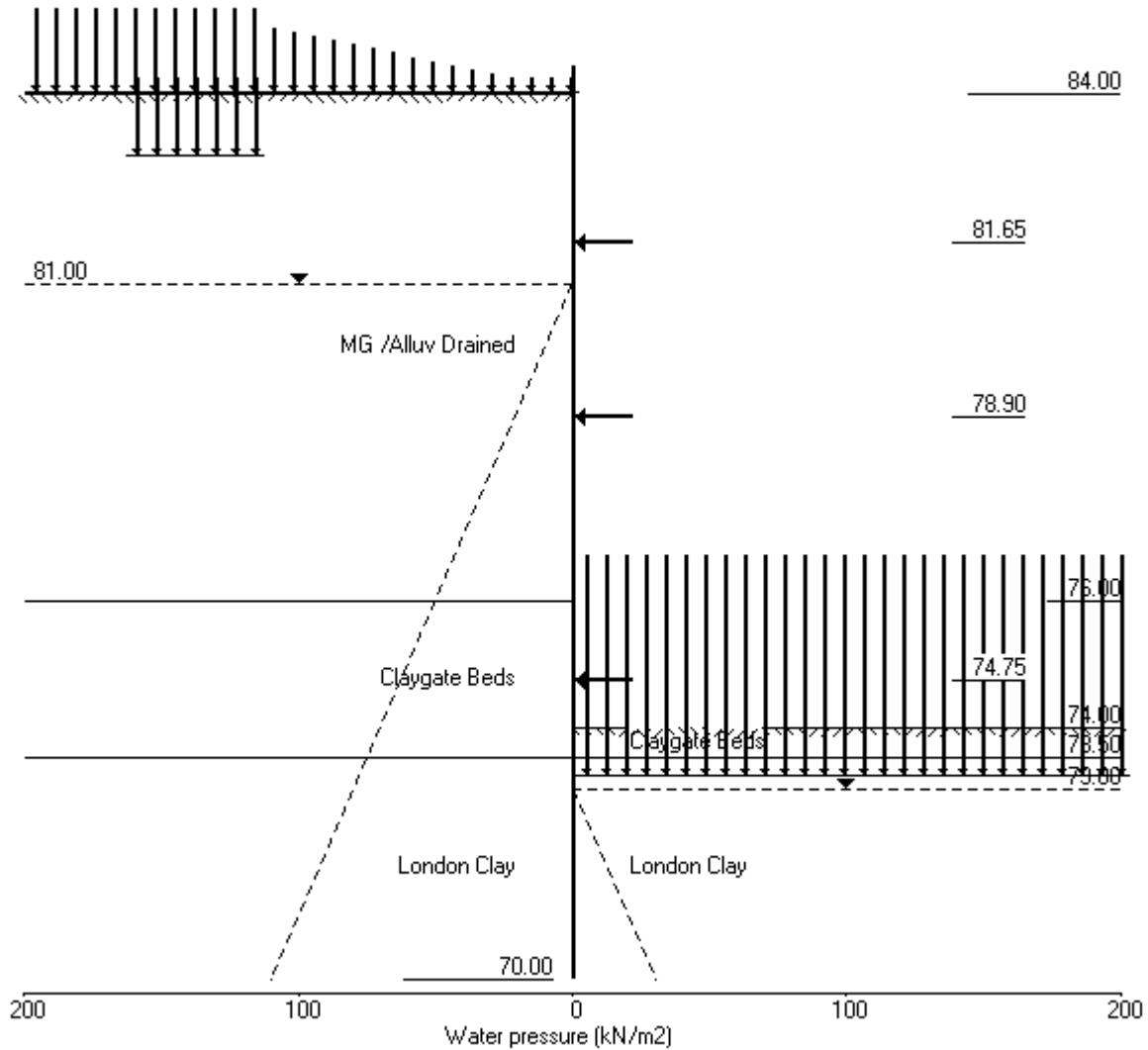


Stage No.13 Excav. to elev. 74.00 on PASSIVE side



Units: kN,m

Stage No.23 Change soil type 1 to soil type 4



Temporary license on loan from Geosolve | Sheet No.  
 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	FoS for toe elev. = 70.00	Moment of equilib. at elev.	Toe elev. for FoS = 1.000	Wall Penetr -ation
23	84.00 74.00			More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor  
 of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.84E-03	0.0	-0.0	
2	84.00	0.00	0.002	-1.84E-03	0.0	-0.0	
		7.76	0.002	-1.84E-03	0.0	-0.0	
3	83.50	6.64	0.002	-1.84E-03	3.6	1.2	
4	83.00	11.46	0.003	-1.85E-03	8.1	4.1	
5	82.50	16.38	0.004	-1.87E-03	15.1	9.7	
6	82.00	21.31	0.005	-1.90E-03	24.5	19.5	
7	81.65	24.72	0.006	-1.95E-03	32.6	29.7	99.6
		24.72	0.006	-1.95E-03	-67.1	29.7	
8	81.50	26.17	0.006	-1.97E-03	-63.2	19.9	
9	81.00	30.95	0.007	-1.98E-03	-49.0	-8.1	
10	80.25	41.77	0.009	-1.90E-03	-21.7	-34.8	
11	79.50	52.49	0.010	-1.76E-03	13.6	-38.1	
12	78.90	60.97	0.011	-1.67E-03	47.7	-20.0	221.7
		60.97	0.011	-1.67E-03	-174.0	-20.0	
13	78.45	67.28	0.012	-1.55E-03	-145.2	-91.9	
14	78.00	73.55	0.012	-1.27E-03	-113.5	-150.3	
15	77.50	80.51	0.013	-8.36E-04	-75.0	-197.6	
16	76.75	90.96	0.013	-2.54E-05	-10.7	-230.6	
17	76.00	101.45	0.013	8.14E-04	61.5	-212.6	
		47.89	0.013	8.14E-04	61.5	-212.6	
18	75.38	50.92	0.012	1.41E-03	92.3	-165.3	
19	74.75	54.35	0.011	1.82E-03	125.2	-97.9	72.2
		54.35	0.011	1.82E-03	53.0	-97.9	
20	74.00	64.80	0.010	2.08E-03	97.7	-39.8	
		-32.73	0.010	2.08E-03	97.7	-39.8	
21	73.50	-18.40	0.009	2.13E-03	84.9	4.6	
		-50.36	0.009	2.13E-03	84.9	4.6	
22	73.20	-34.64	0.008	2.10E-03	72.2	27.8	
		-101.89	0.008	2.10E-03	72.2	27.8	

(continued)

Stage No.23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
23	73.00	-91.38	0.008	2.07E-03	52.8	40.2	
24	72.50	-66.01	0.007	1.95E-03	13.5	55.2	
25	72.00	-41.79	0.006	1.81E-03	-13.5	53.6	
26	71.20	-3.40	0.004	1.64E-03	-31.5	29.6	
27	70.60	25.96	0.003	1.58E-03	-24.8	10.1	
28	70.00	56.67	0.002	1.57E-03	0.0	0.0	
Strut force at elev.			81.65 =	99.62 kN/m	run =	99.62 kN/strut	
Strut force at elev.			78.90 =	221.73 kN/m	run =	221.73 kN/strut	
Strut force at elev.			74.75 =	72.24 kN/m	run =	72.24 kN/strut	

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	5.00	1.62	18.00	7.76	7.76	4144
3	83.50	0.00	14.09	4.56	50.72	6.64	6.64	4144
4	83.00	0.00	23.49	7.61	84.57	11.46	11.46	4144
5	82.50	0.00	33.09	10.72	119.16	16.38	16.38	4144
6	82.00	0.00	42.74	13.85	153.90	21.31	21.31	4144
7	81.65	0.00	49.48	16.03	178.14	24.72	24.72	4144
8	81.50	0.00	52.35	16.96	188.50	26.17	26.17	4144
9	81.00	0.00	61.88	20.05	222.81	30.95	30.95	3141
10	80.25	7.50	68.51	22.20	246.69	34.27	41.77	3141
11	79.50	15.00	74.96	24.29	269.89	37.49	52.49	3141
12	78.90	21.00	79.98	25.92	287.99	39.97	60.97	1510
13	78.45	25.50	83.69	27.12	301.35	41.78	67.28	1510
14	78.00	30.00	87.35	28.30	314.53	43.55	73.55	1510
15	77.50	35.00	91.37	29.61	328.99	45.51	80.51	1510
16	76.75	42.50	97.32	31.53	350.40	48.46	90.96	1510
17	76.00	50.00	103.19	33.44	371.54	51.45	101.45	1510
		Total>	153.19	40.00m	332.43	47.89	47.89	9966
18	75.38	Total>	164.29	43.13m	352.50	50.92	50.92	10464
19	74.75	Total>	175.36	46.25m	372.53	54.35	54.35	10962
20	74.00	Total>	188.62	50.00m	396.54	64.80	64.80	11560
21	73.50	Total>	197.45	52.50m	412.54	71.81	71.81	11959
		Total>	197.45	52.50m	420.37	92.84	92.84	11959
22	73.20	Total>	203.04	54.00m	429.83	105.18	105.18	12167
23	73.00	Total>	206.77	55.00m	436.13	113.48	113.48	12306
24	72.50	Total>	216.09	57.50m	451.89	134.40	134.40	12652
25	72.00	Total>	225.40	60.00m	467.65	155.25	155.25	12999
26	71.20	Total>	240.31	64.00m	492.85	187.96	187.96	13553
27	70.60	Total>	251.49	67.00m	511.76	212.47	212.47	13969
28	70.00	Total>	262.67	70.00m	530.67	237.48	237.48	14385

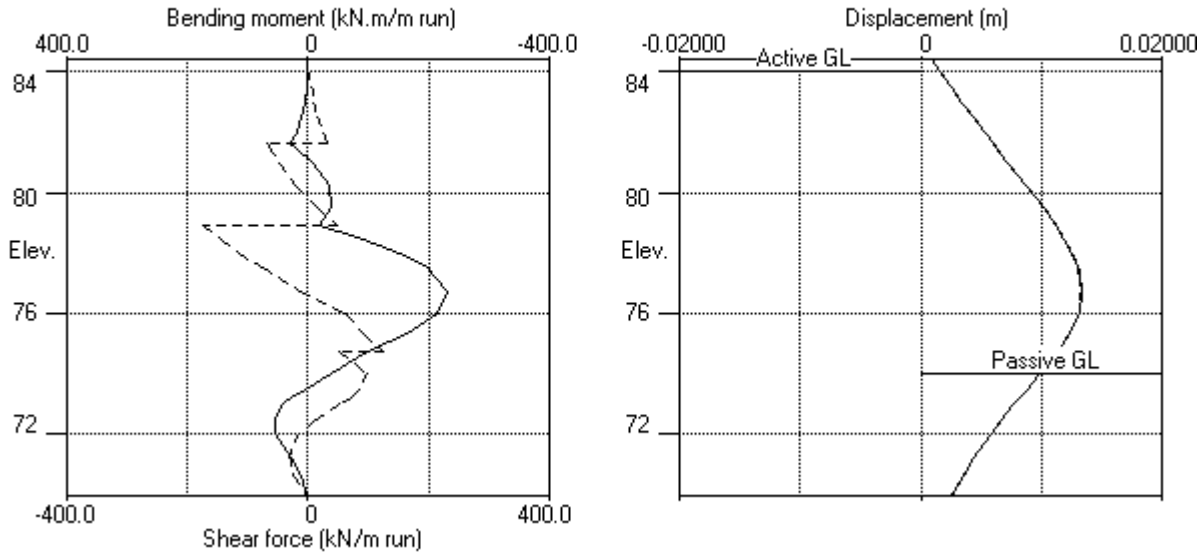
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Stage No.23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

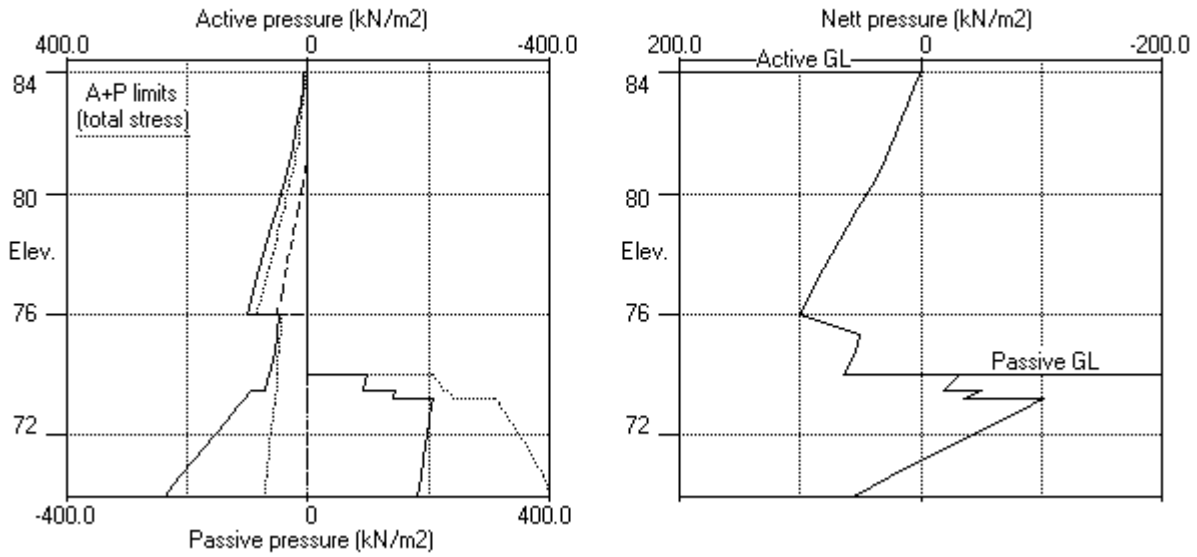
Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
16	76.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
17	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	207.93	97.52	97.52	20859
21	73.50	Total>	9.01	2.50m	224.10	90.21	90.21	21579
		Total>	9.01	2.50m	231.93	143.21	143.21	21579
22	73.20	Total>	14.74	4.00m	241.52	139.82	139.82	21954
		Total>	84.74	4.00m	311.52	207.07	207.07	21954
23	73.00	Total>	88.56	5.00m	317.93	204.86	204.86	22204
24	72.50	Total>	98.08	7.50m	333.88	200.41	200.41	22829
25	72.00	Total>	107.31	10.00m	349.55	197.04	197.04	23455
26	71.20	Total>	121.23	14.00m	373.78	191.37	191.37	24455
27	70.60	Total>	131.10	17.00m	391.37	186.51	186.51	25205
28	70.00	Total>	140.73	20.00m	408.73	180.81	180.81	25956

Units: kN,m

Stage No.23 Change soil type 1 to soil type 4

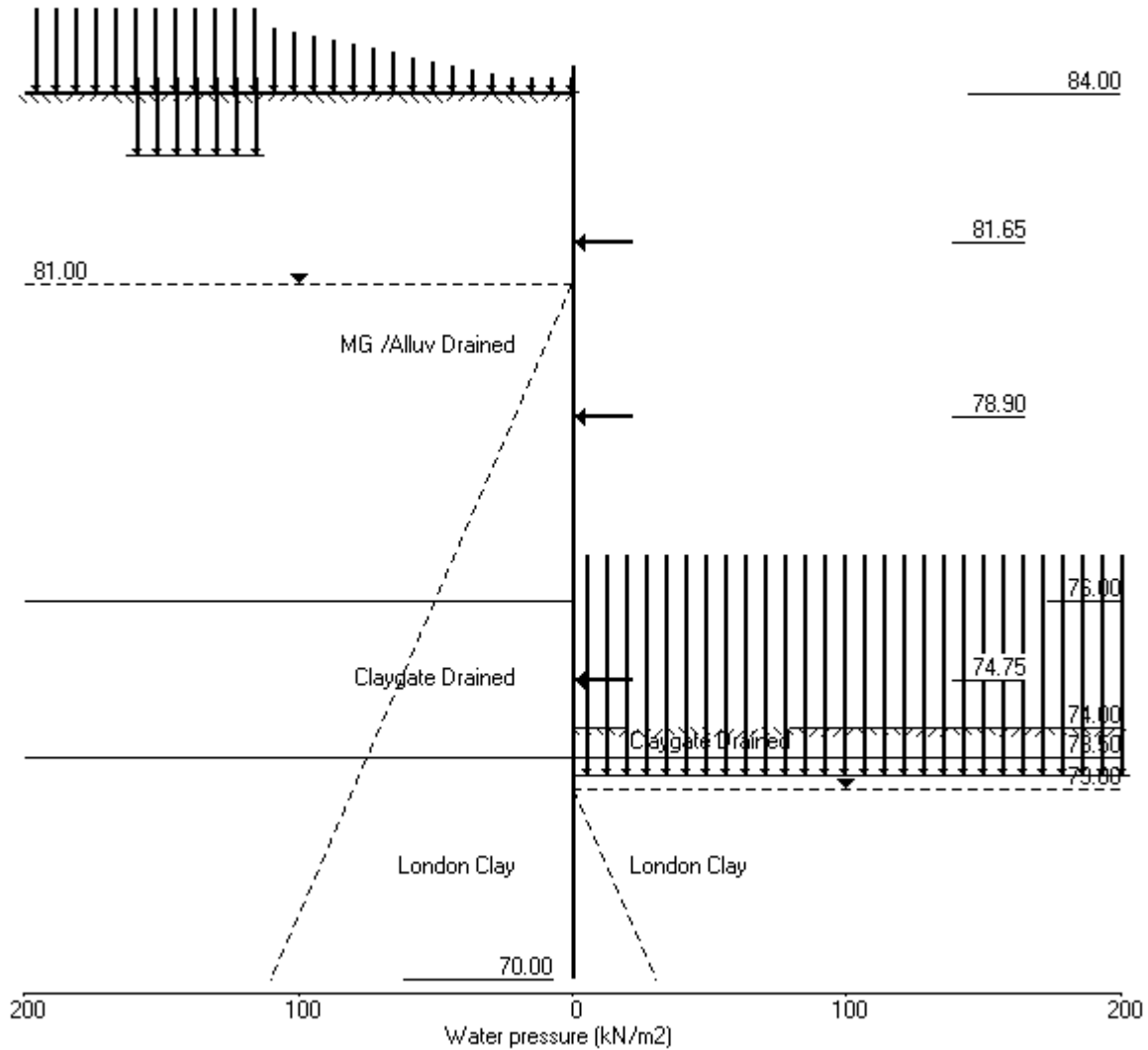


Stage No.23 Change soil type 1 to soil type 4



Units: kN,m

Stage No.24 Change soil type 2 to soil type 5





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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	FoS for toe elev. = 70.00	Moment of equilib. at elev.	Toe elev. for FoS = 1.000	Wall Penetr -ation
24	84.00 74.00			More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.83E-03	0.0	-0.0	
2	84.00	0.00	0.002	-1.83E-03	0.0	-0.0	
		7.69	0.002	-1.83E-03	0.0	-0.0	
3	83.50	6.58	0.003	-1.83E-03	3.6	1.2	
4	83.00	11.42	0.003	-1.84E-03	8.1	4.0	
5	82.50	16.36	0.004	-1.86E-03	15.0	9.7	
6	82.00	21.30	0.005	-1.90E-03	24.4	19.4	
7	81.65	24.72	0.006	-1.94E-03	32.5	29.5	98.0
		24.72	0.006	-1.94E-03	-65.5	29.5	
8	81.50	26.17	0.006	-1.96E-03	-61.7	20.0	
9	81.00	30.97	0.007	-1.97E-03	-47.4	-7.3	
10	80.25	41.80	0.009	-1.90E-03	-20.1	-32.8	
11	79.50	52.51	0.010	-1.77E-03	15.2	-34.9	
12	78.90	60.97	0.011	-1.69E-03	49.3	-15.8	228.3
		60.97	0.011	-1.69E-03	-179.1	-15.8	
13	78.45	67.25	0.012	-1.57E-03	-150.2	-90.0	
14	78.00	73.50	0.013	-1.30E-03	-118.5	-150.6	
15	77.50	80.43	0.013	-8.60E-04	-80.0	-200.5	
16	76.75	90.86	0.013	-3.15E-05	-15.8	-237.3	
17	76.00	101.36	0.013	8.40E-04	56.3	-223.2	
		152.93	0.013	8.40E-04	56.3	-223.2	
18	75.38	164.15	0.012	1.44E-03	155.4	-158.1	
19	74.75	175.17	0.011	1.73E-03	261.4	-28.6	377.2
		175.17	0.011	1.73E-03	-115.8	-28.6	
20	74.00	187.56	0.010	1.91E-03	20.2	-62.9	
21	73.50	166.53	0.009	2.02E-03	108.8	-31.2	
		-57.59	0.009	2.02E-03	108.8	-31.2	
22	73.20	-42.76	0.008	2.05E-03	93.7	-1.1	
		-110.01	0.008	2.05E-03	93.7	-1.1	

(continued)

Stage No.24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
23	73.00	-99.85	0.008	2.04E-03	72.7	15.4	
24	72.50	-74.70	0.007	1.97E-03	29.1	39.3	
25	72.00	-49.95	0.006	1.87E-03	-2.1	44.5	
26	71.20	-9.81	0.005	1.72E-03	-26.0	26.9	
27	70.60	21.29	0.004	1.67E-03	-22.5	9.6	
28	70.00	53.90	0.003	1.65E-03	0.0	0.0	
Strut force at elev.			81.65 =	97.99 kN/m	run =	97.99 kN/strut	
Strut force at elev.			78.90 =	228.33 kN/m	run =	228.33 kN/strut	
Strut force at elev.			74.75 =	377.18 kN/m	run =	377.18 kN/strut	

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	5.00	1.62	18.00	7.69	7.69	3884
3	83.50	0.00	14.09	4.56	50.72	6.58	6.58	3884
4	83.00	0.00	23.49	7.61	84.57	11.42	11.42	3884
5	82.50	0.00	33.09	10.72	119.16	16.36	16.36	3884
6	82.00	0.00	42.74	13.85	153.90	21.30	21.30	3884
7	81.65	0.00	49.48	16.03	178.14	24.72	24.72	2987
8	81.50	0.00	52.35	16.96	188.50	26.17	26.17	2987
9	81.00	0.00	61.88	20.05	222.81	30.97	30.97	2987
10	80.25	7.50	68.51	22.20	246.69	34.30	41.80	2987
11	79.50	15.00	74.96	24.29	269.89	37.51	52.51	2987
12	78.90	21.00	79.98	25.92	287.99	39.97	60.97	2081
13	78.45	25.50	83.69	27.12	301.35	41.75	67.25	2081
14	78.00	30.00	87.35	28.30	314.53	43.50	73.50	2081
15	77.50	35.00	91.37	29.61	328.99	45.43	80.43	2081
16	76.75	42.50	97.32	31.53	350.40	48.36	90.86	2081
17	76.00	50.00	103.19	33.44	371.54	51.36	101.36	2081
		50.00	103.19	36.25	335.65	102.93	152.93	6058
18	75.38	56.25	108.04	37.95	351.42	107.90	164.15	6361
19	74.75	62.50	112.86	39.64	367.11	112.67	175.17	6664
20	74.00	70.00	118.62	41.67	385.84	117.56	187.56	7027
21	73.50	75.00	122.45	43.01	398.29	120.84	195.84	7270
		Total>	197.45	52.50m	420.37	89.26	89.26	16165
22	73.20	Total>	203.04	54.00m	429.83	101.16	101.16	16447
23	73.00	Total>	206.77	55.00m	436.13	109.29	109.29	16634
24	72.50	Total>	216.09	57.50m	451.89	130.10	130.10	17102
25	72.00	Total>	225.40	60.00m	467.65	151.21	151.21	17571
26	71.20	Total>	240.31	64.00m	492.85	184.80	184.80	18320
27	70.60	Total>	251.49	67.00m	511.76	210.15	210.15	18882
28	70.00	Total>	262.67	70.00m	530.67	236.11	236.11	19445

(continued)

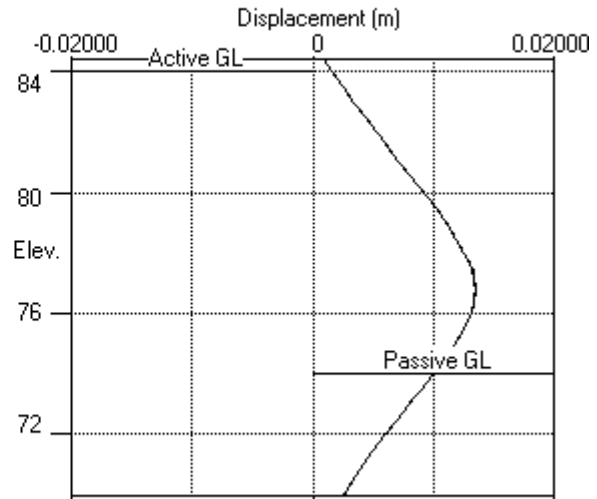
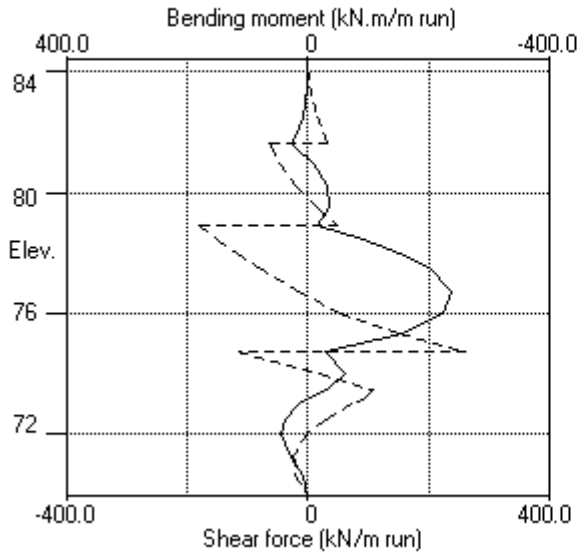
Stage No.24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
16	76.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
17	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	0.00	0.00	0.00	0.00	0.00	7178
21	73.50	0.00	9.01	3.16	29.30	29.30	29.30p	7426
		Total>	9.01	2.50m	231.93	146.86	146.86	16498
22	73.20	Total>	14.74	4.00m	241.52	143.92	143.92	16785
		Total>	84.74	4.00m	311.52	211.17	211.17	16785
23	73.00	Total>	88.56	5.00m	317.93	209.14	209.14	16976
24	72.50	Total>	98.08	7.50m	333.88	204.80	204.80	17454
25	72.00	Total>	107.31	10.00m	349.55	201.16	201.16	17932
26	71.20	Total>	121.23	14.00m	373.78	194.60	194.60	18697
27	70.60	Total>	131.10	17.00m	391.37	188.87	188.87	19271
28	70.00	Total>	140.73	20.00m	408.73	182.21	182.21	19844

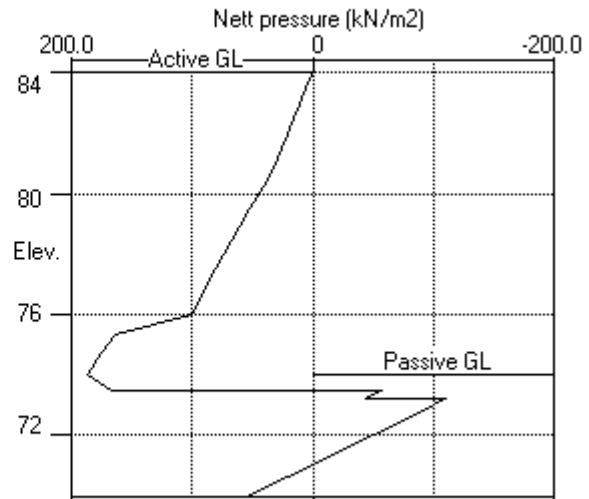
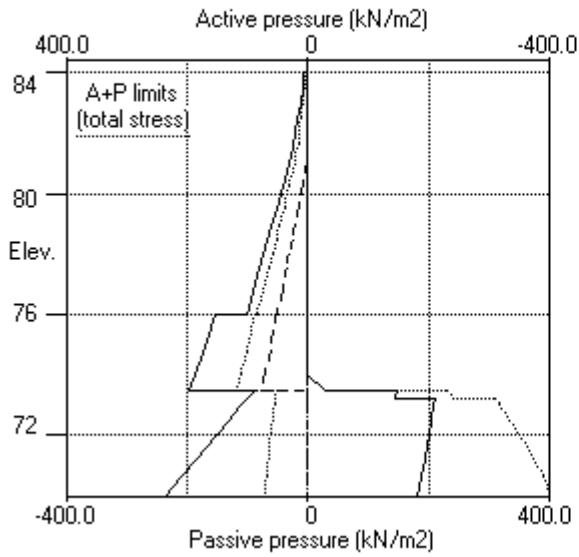
Note: 12.34a Soil pressure at active limit  
 29.30p Soil pressure at passive limit

Units: kN,m

Stage No.24 Change soil type 2 to soil type 5

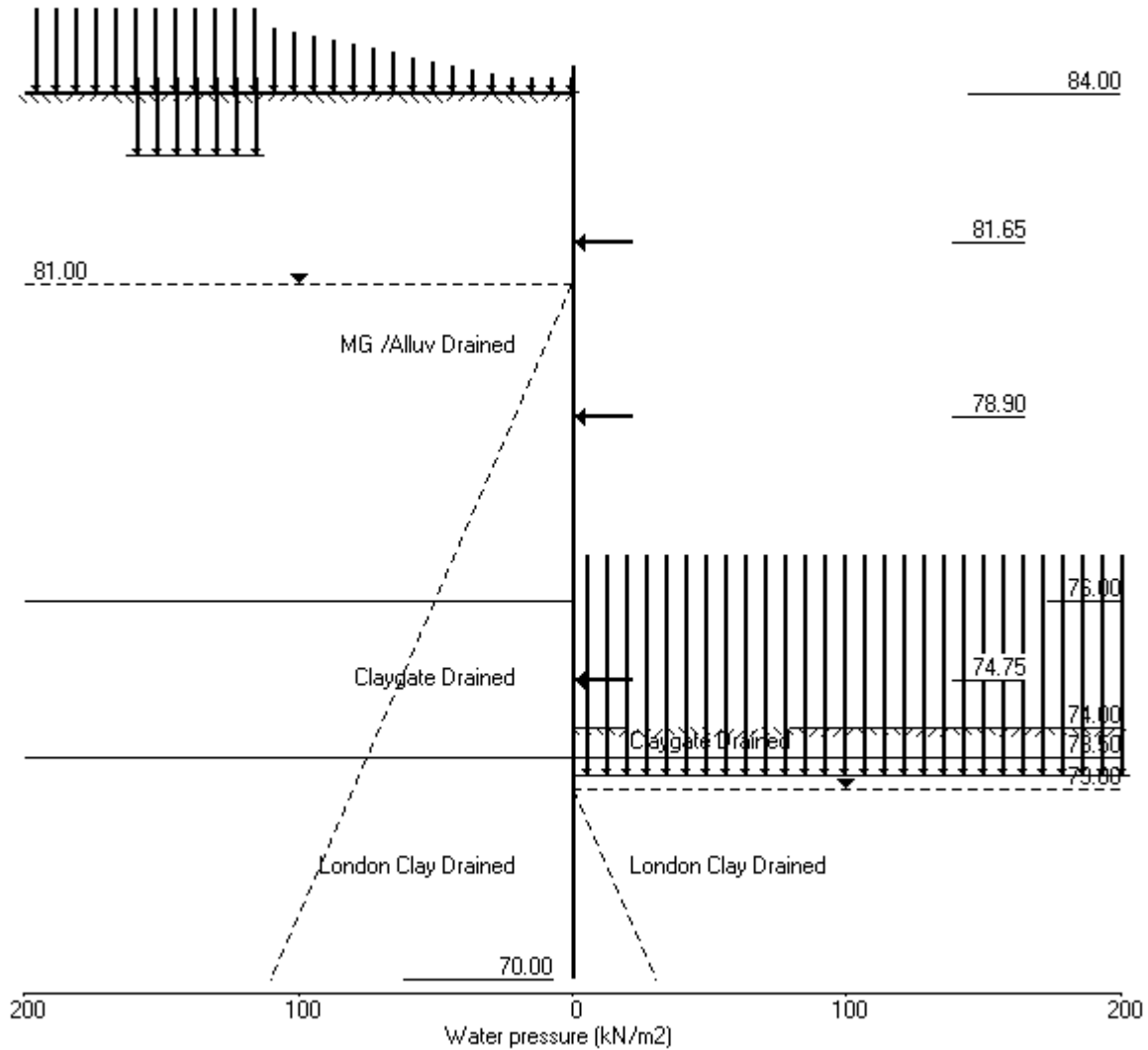


Stage No.24 Change soil type 2 to soil type 5



Units: kN,m

Stage No.25 Change soil type 3 to soil type 6



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 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 25 Change properties of soil type 3 to soil type 6  
 Ko pressures will be reset

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	FoS for toe elev. = 70.00	Moment of equil. at elev.	Toe elev. for FoS = 1.000	Wall Penetration
25	84.00 74.00			More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.90E-03	0.0	-0.0	
2	84.00	0.00	0.001	-1.90E-03	0.0	-0.0	
		8.28	0.001	-1.90E-03	0.0	-0.0	
3	83.50	7.04	0.002	-1.90E-03	3.8	1.3	
4	83.00	11.76	0.003	-1.91E-03	8.5	4.3	
5	82.50	16.57	0.004	-1.92E-03	15.6	10.2	
6	82.00	21.38	0.005	-1.96E-03	25.1	20.3	
7	81.65	24.72	0.006	-2.01E-03	33.2	30.7	111.1
		24.72	0.006	-2.01E-03	-77.9	30.7	
8	81.50	26.14	0.006	-2.03E-03	-74.1	19.3	
9	81.00	30.83	0.007	-2.03E-03	-59.9	-14.3	
10	80.25	41.57	0.009	-1.91E-03	-32.7	-49.2	
11	79.50	52.34	0.010	-1.70E-03	2.5	-60.8	
12	78.90	60.99	0.011	-1.54E-03	36.5	-49.4	180.7
		60.99	0.011	-1.54E-03	-144.2	-49.4	
13	78.45	67.47	0.012	-1.36E-03	-115.3	-107.9	
14	78.00	73.96	0.012	-1.06E-03	-83.5	-152.8	
15	77.50	81.17	0.013	-6.41E-04	-44.7	-185.0	
16	76.75	91.91	0.013	7.90E-05	20.2	-195.1	
17	76.00	102.44	0.013	7.39E-04	93.1	-153.7	
		156.08	0.013	7.39E-04	93.1	-153.7	
18	75.38	166.43	0.012	1.08E-03	193.9	-65.0	
19	74.75	175.07	0.011	1.04E-03	300.6	89.0	517.2
		175.07	0.011	1.04E-03	-216.6	89.0	
20	74.00	182.33	0.011	9.18E-04	-82.6	-20.9	
21	73.50	156.94	0.010	9.96E-04	2.2	-41.3	
22	73.20	140.05	0.010	1.05E-03	46.7	-34.0	
		-32.73	0.010	1.05E-03	46.7	-34.0	
23	73.00	-30.55	0.010	1.08E-03	40.4	-25.3	



(continued)

Stage No.25 Change properties of soil type 3 to soil type 6  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
16	76.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
17	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	0.00	0.00	0.00	0.00	0.00	7895
21	73.50	0.00	9.01	3.16	29.30	29.30	29.30p	8167
		0.00	9.01	3.16	30.99	30.99	30.99p	8167
22	73.20	0.00	14.74	5.18	50.69	50.69	50.69p	8309
		0.00	84.74	29.77	291.49	223.47	223.47	8309
23	73.00	0.00	88.56	31.11	304.65	223.23	223.23	8404
24	72.50	5.00	93.08	32.70	320.19	218.21	223.21	8640
25	72.00	10.00	97.31	34.18	334.75	213.59	223.59	8877
26	71.20	18.00	103.23	36.26	355.12	204.85	222.85	9256
27	70.60	24.00	107.10	37.62	368.41	197.24	221.24	9540
28	70.00	30.00	110.73	38.90	380.91	188.74	218.74	9824

Note: 12.34a Soil pressure at active limit  
 50.69p Soil pressure at passive limit





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 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

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 Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: Serviceability Limit State  
 All loads and soil strengths are unfactored

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	G.L.		Strut Elev.	FoS for toe elev. = 70.00		Toe elev. for FoS = 1.000	
	Act.	Pass.		Factor of Safety	Moment of equilib. at elev.	Toe elev.	Wall Penetration
1	84.00	84.00	Cant.	Conditions not suitable for FoS calc.			
2	84.00	84.00		No analysis at this stage			
3	84.00	84.00		No analysis at this stage			
4	84.00	84.00		No analysis at this stage			
5	84.00	84.00	Cant.	Conditions not suitable for FoS calc.			
6	84.00	84.00		No analysis at this stage			
7	84.00	81.50	84.40	7.328	n/a	81.31	0.19
8	84.00	81.50		No analysis at this stage			

All remaining stages have more than one strut - FoS calculation n/a

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 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		---- Bending moment ----				----- Shear force -----			
		max.	min.	Calculated		Factored		Calculated		Factored	
				max.	min.	max.	min.	max.	min.	max.	min.
		m	m	kN.m/m		kN.m/m		kN/m		kN/m	
1	84.40	0.001	0.000	0	-0	0	-0	0	-26	0	-36
2	84.00	0.002	0.000	0	-11	0	-14	0	-26	0	-36
3	83.50	0.003	0.000	1	-24	2	-32	4	-26	5	-35
4	83.00	0.004	0.000	4	-36	6	-49	9	-24	12	-32
5	82.50	0.005	0.000	10	-47	14	-64	16	-21	21	-28
6	82.00	0.006	0.000	20	-56	27	-76	25	-81	34	-109
7	81.65	0.006	0.000	31	-61	41	-83	33	-78	45	-105
8	81.50	0.007	0.000	20	-63	27	-85	0	-75	0	-102
9	81.00	0.008	0.000	0	-68	0	-92	0	-69	0	-92
10	80.25	0.009	0.000	0	-111	0	-149	1	-56	2	-75
11	79.50	0.010	0.000	0	-147	0	-198	18	-131	25	-177
12	78.90	0.011	0.000	0	-166	0	-225	49	-179	67	-242
13	78.45	0.012	0.000	0	-174	0	-235	27	-150	36	-203
14	78.00	0.013	0.000	0	-173	0	-234	46	-123	62	-166
15	77.50	0.013	0.000	0	-200	0	-271	37	-97	50	-131
16	76.75	0.013	0.000	1	-237	1	-320	66	-51	90	-68
17	76.00	0.013	0.000	2	-223	3	-301	103	0	139	0
18	75.38	0.012	0.000	18	-171	24	-231	194	0	262	0
19	74.75	0.011	0.000	89	-139	120	-188	301	-217	406	-292
20	74.00	0.011	0.000	55	-72	74	-97	111	-83	149	-112
21	73.50	0.010	0.000	57	-41	77	-56	109	-6	147	-8
22	73.20	0.010	0.000	55	-34	75	-46	94	-9	126	-12
23	73.00	0.010	0.000	53	-25	72	-34	73	-13	98	-17
24	72.50	0.009	0.000	57	-9	76	-13	29	-20	39	-26
25	72.00	0.009	0.000	55	0	75	0	15	-22	20	-30
26	71.20	0.008	0.000	31	0	41	0	2	-33	3	-44
27	70.60	0.007	0.000	11	0	14	0	0	-26	0	-35
28	70.00	0.006	0.000	0	0	0	0	0	-0	0	-0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment						Shear force					
	Calculated				Factored		Calculated				Factored	
	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.
	kN.m/m	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m
1	3	74.75	-1	79.50	5	-2	2	76.00	-1	72.50	3	-1
2	No calculation at this stage											
3	No calculation at this stage											
4	No calculation at this stage											
5	6	74.00	-10	78.45	8	-13	8	76.00	-3	81.50	11	-4
6	No calculation at this stage											
7	35	74.00	-79	79.50	47	-106	51	76.00	-26	84.40	68	-36
8	No calculation at this stage											
9	35	74.00	-78	79.50	47	-106	50	76.00	-26	84.40	68	-35
10	57	73.50	-174	78.45	77	-235	103	76.00	-81	82.00	139	-109
11	No calculation at this stage											
12	56	73.50	-173	78.45	76	-233	102	76.00	-81	82.00	138	-109
13	31	72.00	-165	76.00	42	-222	100	74.00	-118	78.00	135	-160
14	No calculation at this stage											
15	45	72.00	-180	76.00	61	-244	108	74.00	-123	78.00	146	-166
16	No calculation at this stage											
17	57	72.50	-221	76.75	76	-299	107	74.00	-131	79.50	145	-177
18	No calculation at this stage											
19	55	72.50	-210	76.75	74	-283	111	74.00	-126	78.90	149	-170
20	No calculation at this stage											
21	55	72.50	-211	76.75	74	-285	110	74.00	-125	78.90	149	-169
22	55	72.50	-211	76.75	74	-285	110	74.00	-125	78.90	149	-169
23	55	72.50	-231	76.75	74	-311	125	74.75	-174	78.90	169	-235
24	44	72.00	-237	76.75	60	-320	261	74.75	-179	78.90	353	-242
25	89	74.75	-195	76.75	120	-263	301	74.75	-217	74.75	406	-292

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum m	Displacement elev.	Displacement minimum m	Displacement elev.	Stage description
1	0.001	84.40	0.000	84.40	Apply surcharge no.1 at elev. 84.00
2	No calculation at this stage				Apply surcharge no.2 at elev. 84.00
3	No calculation at this stage				Apply surcharge no.3 at elev. 84.00
4	No calculation at this stage				Apply surcharge no.6 at elev. 84.00
5	0.001	80.25	0.000	84.40	Apply surcharge no.7 at elev. 83.00
6	No calculation at this stage				Install strut no.1 at elev. 84.40
7	0.006	78.90	0.000	84.40	Excav. to elev. 81.50 on PASSIVE side
8	No calculation at this stage				Install strut no.2 at elev. 82.00
9	0.006	78.90	0.000	84.40	Apply water pressure profile no.1
10	0.011	78.00	0.000	84.40	Excav. to elev. 77.50 on PASSIVE side
11	No calculation at this stage				Install strut no.3 at elev. 78.00
12	0.011	78.00	0.000	84.40	Apply water pressure profile no.3
13	0.012	76.00	0.000	84.40	Excav. to elev. 74.00 on PASSIVE side
14	No calculation at this stage				Install strut no.4 at elev. 74.75
15	0.012	76.75	0.000	84.40	Apply surcharge no.4 at elev. 73.20
16	No calculation at this stage				Install strut no.5 at elev. 79.50
17	0.013	76.75	0.000	84.40	Remove strut no.3 at elev. 78.00
18	No calculation at this stage				Install strut no.6 at elev. 78.90
19	0.013	76.75	0.000	84.40	Remove strut no.5 at elev. 79.50
20	No calculation at this stage				Install strut no.7 at elev. 81.65
21	0.013	76.75	0.000	84.40	Remove strut no.2 at elev. 82.00
22	0.013	76.75	0.000	84.40	Remove strut no.1 at elev. 84.40
23	0.013	76.75	0.000	84.40	Change soil type 1 to soil type 4
24	0.013	76.75	0.000	84.40	Change soil type 2 to soil type 5
25	0.013	76.75	0.000	84.40	Change soil type 3 to soil type 6

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Strut forces at each stage (horizontal components)**

Stage no.	----- Strut no. 1 ----- at elev. 84.40			----- Strut no. 2 ----- at elev. 82.00			----- Strut no. 3 ----- at elev. 78.00		
	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut
7	26	158	213	---	---	---	---	---	---
9	26	157	212	0	0	0	---	---	---
10	slack	slack	slack	93	558	754	---	---	---
12	slack	slack	slack	93	557	752	1	6	8
13	slack	slack	slack	67	403	544	164	986	1332
15	slack	slack	slack	69	411	555	167	1003	1354
17	slack	slack	slack	47	281	379	---	---	---
19	slack	slack	slack	61	366	495	---	---	---
21	slack	slack	slack	---	---	---	---	---	---

Stage no.	----- Strut no. 4 ----- at elev. 74.75			----- Strut no. 5 ----- at elev. 79.50			----- Strut no. 6 ----- at elev. 78.90		
	--Calculated-- kN per m run	--Factored-- kN per strut	Factor kN per strut	--Calculated-- kN per m run	--Factored-- kN per strut	Factor kN per strut	--Calculated-- kN per m run	--Factored-- kN per strut	Factor kN per strut
15	slack	slack	slack	---	---	---	---	---	---
17	35	35	48	149	895	1209	---	---	---
19	22	22	30	---	---	---	143	143	193
21	23	23	32	---	---	---	134	134	181
22	23	23	32	---	---	---	134	134	181
23	72	72	98	---	---	---	222	222	299
24	377	377	509	---	---	---	228	228	308
25	517	517	698	---	---	---	181	181	244

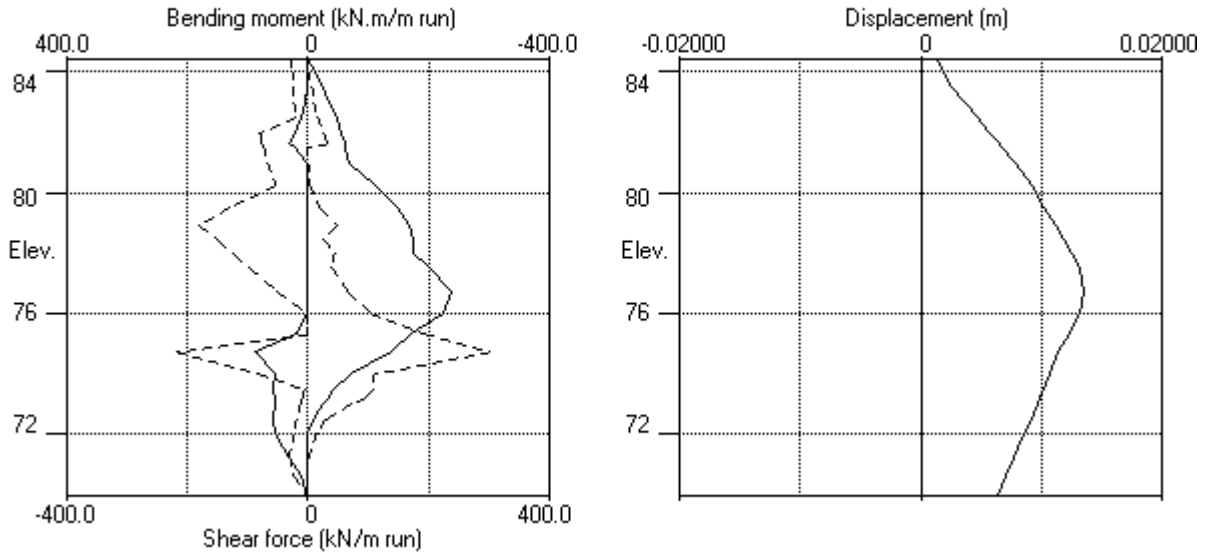
Stage no.	----- Strut no. 7 ----- at elev. 81.65		
	--Calculated--		Factored
	kN per m run	kN per strut	kN per strut
21	67	67	90
22	67	67	90
23	100	100	134
24	98	98	132
25	111	111	150



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Data filename/Run ID: 59 Maresfield Gdns East Wall Final_SLS	Date: 6-12-2012
59 Maresfield Gardens	Checked :
East Wall	

Units: kN,m

Bending moment, shear force, displacement envelopes



Temporary license on loan from Geosolve | Sheet No.  
 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	84.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES (Unfactored SLS soil strengths)**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.390)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (2.476)	1.000 (2.477)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.253 (4.831)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.500	0.00
3 London Clay	0.00	0.670	0.00	0.00	0.670	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.500	0.00
6 London Clay Drained	25.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile		Active side			Passive side			
Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	73.00	73.00	0.0 MC
4	1	82.00	82.00	0.0	1	73.20	73.20	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.80 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 7.0700E-03 m4/m run  
 E.I = 197960 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	84.40	6.00	0.010000	2.000E+08	5.00	0.00	0	No
2	82.00	6.00	0.010000	2.000E+08	5.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	1.00	0.00	0	No
4	74.75	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5	79.50	6.00	0.100000	2.000E+08	5.00	0.00	0	No
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	3.000E+07	1.00	0.00	0	No
8	76.30	6.00	0.010000	2.000E+08	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- kN/m2 ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	84.00	0.00(A)	8.00	20.00	5.00	=	N/A	1.10 Var
2	84.00	5.00(A)	8.00	15.00	5.00	=	N/A	1.10 Var
3	84.00	1.00(A)	8.00	4.00	0.00	17.00	N/A	1.00 P/U
4	73.20	-0.00(P)	8.00	10.00	70.00	=	N/A	1.00 -
5	74.00	-0.00(P)	10.00	10.00	70.00	=	N/A	1.00 -
6	84.00	5.00(A)	10.00	15.00	17.00	=	N/A	1.00 P/U
7	83.00	5.00(A)	2.00	2.00	25.00	=	N/A	1.00 P/U

Note: A = Active side, P = Passive side

A trapezoidal surcharge is defined by two values:

N = at edge near to wall, F = at edge far from wall

Limit State Categories P/U = Permanent Unfavourable

P/F = Permanent Favourable

Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 84.00 No analysis at this stage
2	Apply surcharge no.2 at elevation 84.00 No analysis at this stage
3	Apply surcharge no.3 at elevation 84.00 No analysis at this stage
4	Apply surcharge no.6 at elevation 84.00 No analysis at this stage
5	Apply surcharge no.7 at elevation 83.00 No analysis at this stage
6	Install strut or anchor no.1 at elevation 84.40
7	Excavate to elevation 81.50 on PASSIVE side
8	Install strut or anchor no.2 at elevation 82.00
9	Apply water pressure profile no.1 ( Mod. Conserv. )
10	Excavate to elevation 77.50 on PASSIVE side
11	Install strut or anchor no.3 at elevation 78.00
12	Apply water pressure profile no.3 ( Mod. Conserv. )
13	Excavate to elevation 74.00 on PASSIVE side
14	Install strut or anchor no.4 at elevation 74.75
15	Apply surcharge no.4 at elevation 73.20
16	Install strut or anchor no.5 at elevation 79.50
17	Remove strut or anchor no.3 at elevation 78.00
18	Install strut or anchor no.6 at elevation 78.90
19	Remove strut or anchor no.5 at elevation 79.50
20	Install strut or anchor no.7 at elevation 81.65
21	Remove strut or anchor no.2 at elevation 82.00
22	Remove strut or anchor no.1 at elevation 84.40
23	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
24	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
25	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: ULS DA1 Combination 1

Water pressures : Moderately Conservative

Partial factor on C' = 1.000

Partial factor on Phi' = 1.000

Partial factor on Cu = 1.000

Partial factor on Soil Modulus = 1.000

Partial factor on Permanent Unfavourable loads = 1.000

Partial factor on Permanent Favourable loads = 1.000

Partial factor on Permanent Variable loads = 1.100

Design factor on calculated Bending Moments = 1.350

Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>

Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients

Open Tension Crack analysis? - No

Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:

Length of wall (normal to plane of analysis) = 6.00 m

Width of excavation on active side of wall = 20.00 m

Width of excavation on passive side of wall = 10.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

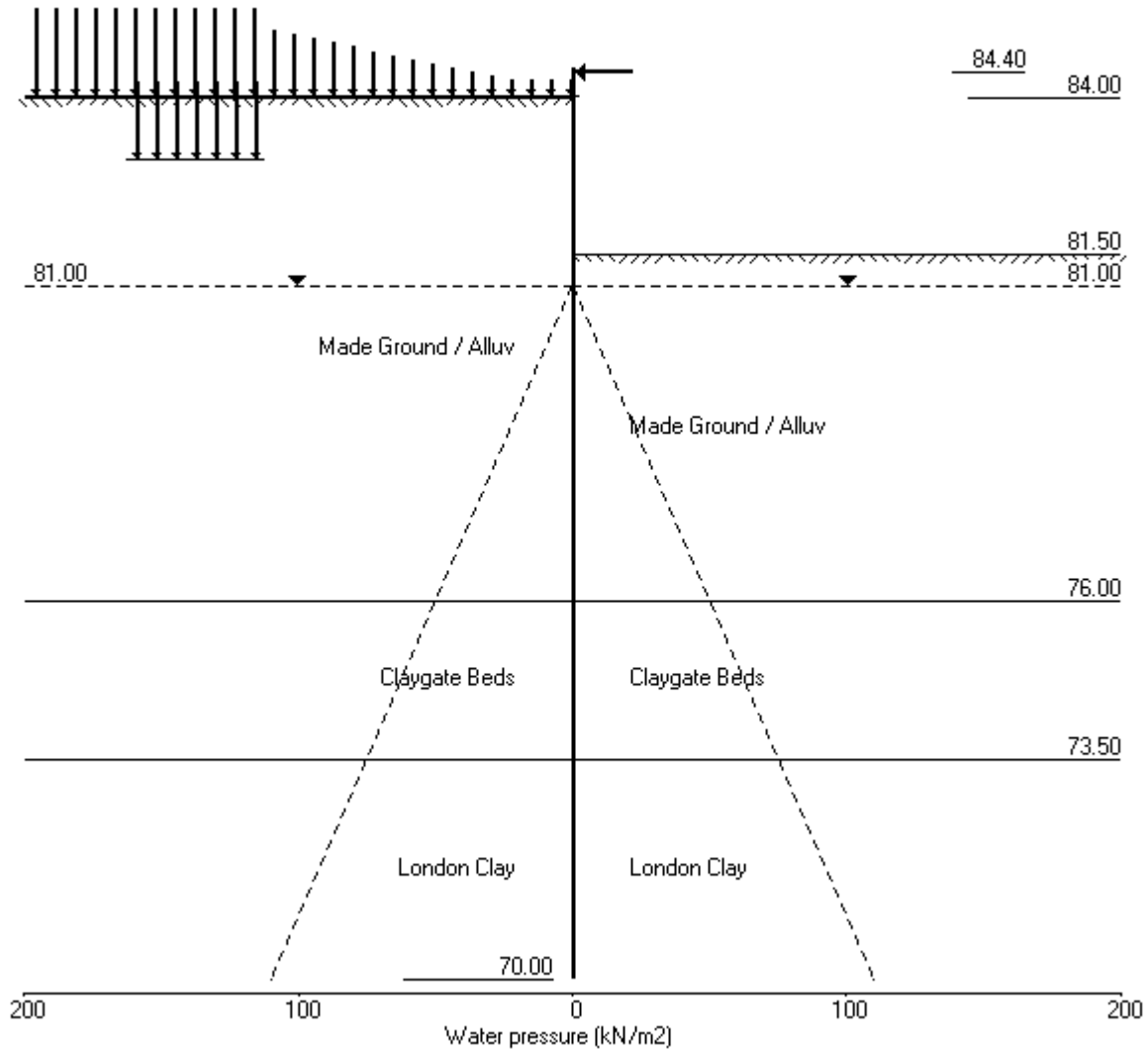
**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 84.00	No	No	No
2	Apply surcharge no.2 at elev. 84.00	No	No	No
3	Apply surcharge no.3 at elev. 84.00	No	No	No
4	Apply surcharge no.6 at elev. 84.00	No	No	No
5	Apply surcharge no.7 at elev. 83.00	No	No	No
6	Install strut no.1 at elev. 84.40	No	No	No
7	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
8	Install strut no.2 at elev. 82.00	No	No	No
9	Apply water pressure profile no.1	No	No	No
10	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
11	Install strut no.3 at elev. 78.00	No	No	No
12	Apply water pressure profile no.3	No	No	No
13	Excav. to elev. 74.00 on PASSIVE side	Yes	No	Yes
14	Install strut no.4 at elev. 74.75	No	No	No
15	Apply surcharge no.4 at elev. 73.20	No	No	No
16	Install strut no.5 at elev. 79.50	No	No	No
17	Remove strut no.3 at elev. 78.00	No	No	No
18	Install strut no.6 at elev. 78.90	No	No	No
19	Remove strut no.5 at elev. 79.50	No	No	No
20	Install strut no.7 at elev. 81.65	No	No	No
21	Remove strut no.2 at elev. 82.00	No	No	No
22	Remove strut no.1 at elev. 84.40	No	No	No
23	Change soil type 1 to soil type 4	No	No	No
24	Change soil type 2 to soil type 5	No	No	No
25	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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Units: kN,m

Stage No.7 Excav. to elev. 81.50 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 7 Excavate to elevation 81.50 on PASSIVE side

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DAL Combination 1**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor  
 of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.37E-03	-26.5	-0.0	26.5
2	84.00	0.00	0.002	-1.36E-03	-26.5	-10.6	
3	83.50	2.50	0.003	-1.32E-03	-25.9	-23.7	
4	83.00	5.00	0.003	-1.25E-03	-24.0	-36.2	
5	82.50	7.50	0.004	-1.14E-03	-20.9	-47.5	
6	82.00	10.00	0.004	-1.01E-03	-16.5	-56.9	
7	81.65	11.97	0.005	-9.07E-04	-12.6	-61.8	
8	81.50	12.99	0.005	-8.60E-04	-10.8	-63.5	
		0.24	0.005	-8.60E-04	-10.8	-63.5	
9	81.00	2.48	0.005	-6.93E-04	-10.1	-68.7	
10	80.25	4.22	0.006	-4.20E-04	-7.6	-75.1	
11	79.50	9.62	0.006	-1.28E-04	-2.4	-79.0	
12	78.90	12.33	0.006	1.09E-04	4.2	-78.5	
13	78.45	12.88	0.006	2.84E-04	9.9	-75.4	
14	78.00	13.84	0.006	4.49E-04	15.9	-69.7	
15	77.50	15.36	0.005	6.13E-04	23.2	-60.0	
16	76.75	18.35	0.005	7.99E-04	35.8	-38.3	
17	76.00	21.83	0.004	8.84E-04	50.9	-6.4	
		-36.18	0.004	8.84E-04	50.9	-6.4	
18	75.38	-29.51	0.004	8.65E-04	30.4	18.3	
19	74.75	-22.54	0.003	7.87E-04	14.1	31.5	
20	74.00	-14.73	0.003	6.59E-04	0.1	35.6	
21	73.50	-10.15	0.002	5.72E-04	-6.1	33.8	
22	73.20	-7.56	0.002	5.22E-04	-8.7	31.5	
23	73.00	-5.95	0.002	4.92E-04	-10.1	29.6	
24	72.50	-2.34	0.002	4.24E-04	-12.2	23.8	
25	72.00	0.79	0.002	3.72E-04	-12.6	17.3	
26	71.20	5.21	0.001	3.22E-04	-10.2	7.4	
27	70.60	8.42	0.001	3.08E-04	-6.1	2.2	
28	70.00	11.82	0.001	3.04E-04	0.0	-0.0	
Strut force at elev. 84.40 =			26.49 kN/m run =		158.95 kN/strut		

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness coeff. kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.0	
2	84.00	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	5.50	0.00	69.78	0.00	0.00a	
3	83.50	Total>	14.09	2.50m	78.37	2.50	2.50a	

(continued)

Stage No.7 Excavate to elevation 81.50 on PASSIVE side

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
4	83.00	Total>	22.99	5.00m	87.27	5.00	5.00a	3266
5	82.50	Total>	32.09	7.50m	96.38	7.50	7.50a	3266
6	82.00	Total>	41.23	10.00m	105.52	10.00	10.00a	3266
7	81.65	Total>	47.61	11.75m	111.90	11.97	11.97	3266
8	81.50	Total>	50.33	12.50m	114.62	12.99	12.99	3266
9	81.00	Total>	59.35	15.00m	123.64	16.50	16.50	3266
10	80.25	Total>	72.71	18.75m	137.01	25.90	25.90	3266
11	79.50	Total>	85.89	22.50m	150.18	35.79	35.79	3266
12	78.90	Total>	96.30	32.02	160.60	44.11	44.11	3266
13	78.45	Total>	104.05	39.77	168.35	50.58	50.58	3266
14	78.00	Total>	111.75	47.47	176.05	57.26	57.26	3266
15	77.50	Total>	120.25	55.97	184.56	64.90	64.90	3266
16	76.75	Total>	132.93	68.65	197.24	76.72	76.72	3266
17	76.00	Total>	145.54	81.25	209.84	88.81	88.81	3266
		Total>	145.54	40.00m	324.81	60.97	60.97	9798
18	75.38	Total>	156.63	43.13m	344.86	73.21	73.21	10288
19	74.75	Total>	167.69	46.25m	364.88	85.61	85.61	10778
20	74.00	Total>	180.93	50.00m	388.88	100.24	100.24	11366
21	73.50	Total>	189.75	52.50m	404.87	109.69	109.69	11758
		Total>	189.75	52.50m	412.70	162.69	162.69	11758
22	73.20	Total>	195.34	54.00m	422.15	169.79	169.79	11962
23	73.00	Total>	199.06	55.00m	428.45	174.46	174.46	12098
24	72.50	Total>	208.37	57.50m	444.20	185.95	185.95	12439
25	72.00	Total>	217.68	60.00m	459.95	197.21	197.21	12780
26	71.20	Total>	232.57	64.00m	485.15	214.93	214.93	13325
27	70.60	Total>	243.74	67.00m	504.05	228.17	228.17	13734
28	70.00	Total>	254.91	70.00m	522.95	241.50	241.50	14143

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	64.28	12.75	12.75	3432
9	81.00	Total>	8.50	2.50m	72.78	14.02	14.02	3432
10	80.25	Total>	21.28	6.25m	85.57	21.67	21.67	3432
11	79.50	Total>	34.14	10.00m	98.42	26.17	26.17	3432
12	78.90	Total>	44.49	13.00m	108.78	31.78	31.78	3432
13	78.45	Total>	52.31	15.25m	116.60	37.70	37.70	3432
14	78.00	Total>	60.17	17.50m	124.46	43.42	43.42	3432
15	77.50	Total>	68.97	20.00m	133.25	49.54	49.54	3432
16	76.75	Total>	82.26	23.75m	146.55	58.38	58.38	3432
17	76.00	Total>	95.68	31.41	159.97	66.98	66.98	3432
		Total>	95.68	27.50m	274.94	97.15	97.15	10297
18	75.38	Total>	107.57	30.63m	295.79	102.72	102.72	10812
19	74.75	Total>	119.52	33.75m	316.70	108.15	108.15	11326



(continued)

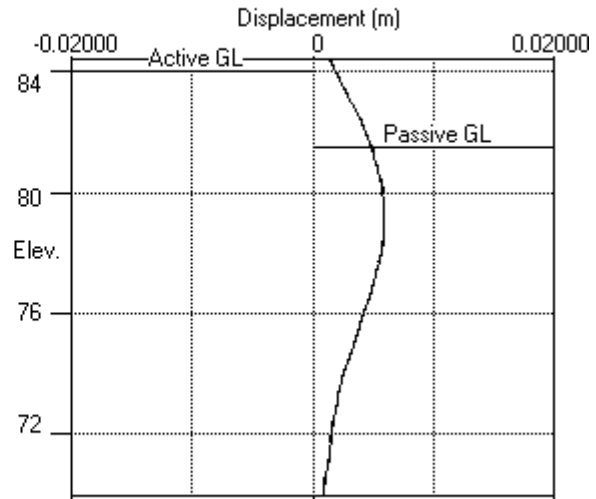
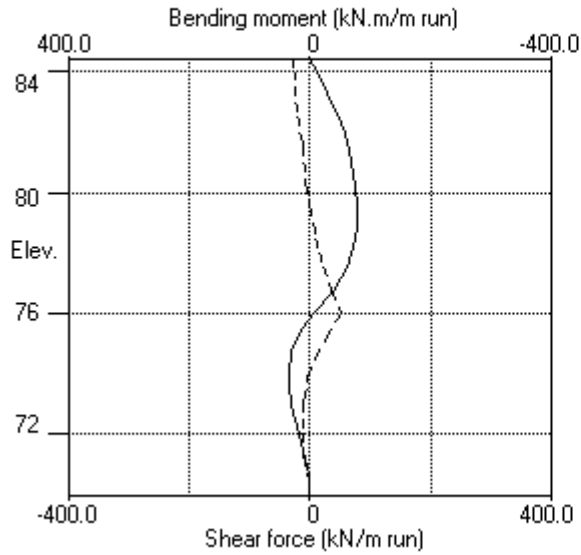
Stage No.7 Excavate to elevation 81.50 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure	Soil stiffness coeff.
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
20	74.00	Total>	133.92	37.50m	341.86	114.97	114.97	11944
21	73.50	Total>	143.56	40.00m	358.67	119.84	119.84	12356
		Total>	143.56	40.00m	366.50	172.84	172.84	12356
22	73.20	Total>	149.65	41.50m	376.45	177.35	177.35	12571
23	73.00	Total>	153.71	42.50m	383.09	180.42	180.42	12714
24	72.50	Total>	163.87	45.00m	399.70	188.29	188.29	13072
25	72.00	Total>	174.05	47.50m	416.31	196.42	196.42	13430
26	71.20	Total>	190.33	51.50m	442.90	209.72	209.72	14003
27	70.60	Total>	202.54	54.50m	462.84	219.75	219.75	14433
28	70.00	Total>	214.74	57.50m	482.77	229.68	229.68	14863

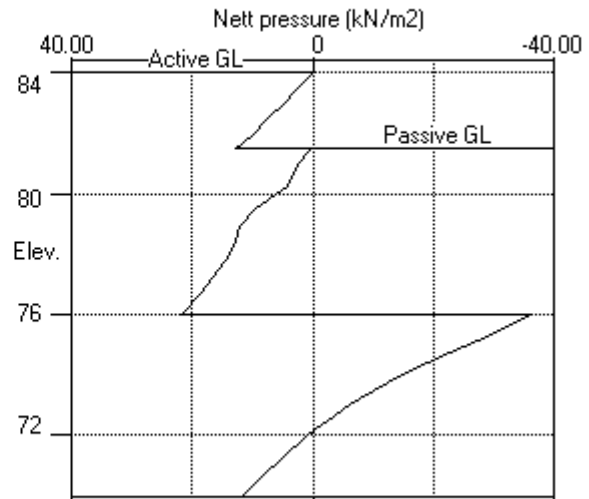
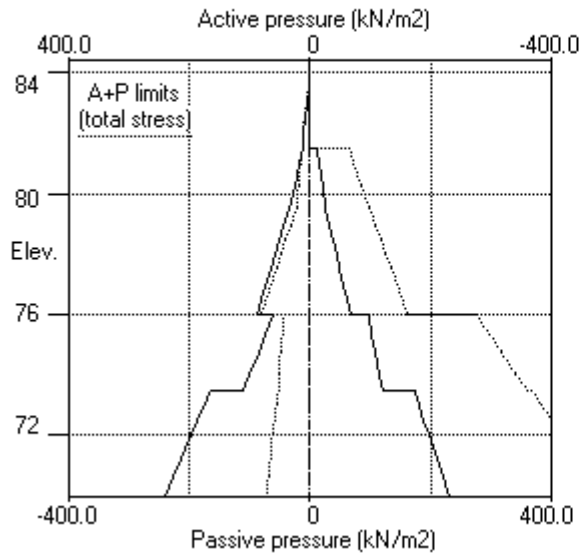
Note: 10.00a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.7 Excav. to elev. 81.50 on PASSIVE side

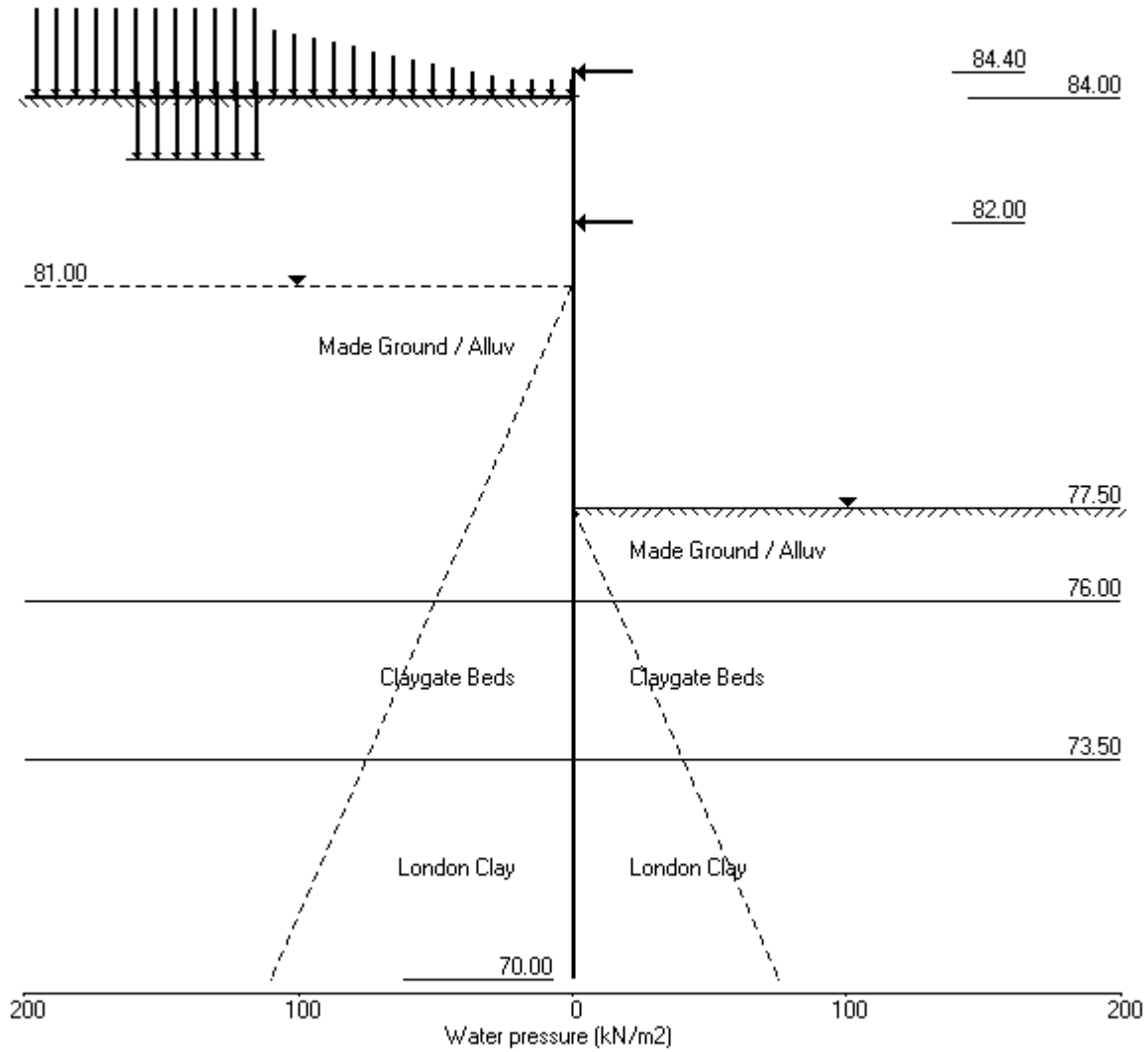


Stage No.7 Excav. to elev. 81.50 on PASSIVE side



Units: kN,m

Stage No.10 Excav. to elev. 77.50 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 10 Excavate to elevation 77.50 on PASSIVE side

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor  
 of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-2.05E-03	0.0	-0.0	-0.0
2	84.00	0.00	0.002	-2.05E-03	0.0	-0.0	
		8.11	0.002	-2.05E-03	0.0	-0.0	
3	83.50	2.50	0.003	-2.05E-03	2.7	1.1	
4	83.00	5.00	0.004	-2.06E-03	4.5	2.9	
5	82.50	7.50	0.005	-2.07E-03	7.7	5.9	
6	82.00	10.00	0.006	-2.09E-03	12.0	10.7	93.3
		10.00	0.006	-2.09E-03	-81.3	10.7	
7	81.65	11.75	0.007	-2.08E-03	-77.5	-16.8	
8	81.50	12.50	0.007	-2.07E-03	-75.7	-28.3	
9	81.00	15.00	0.008	-1.95E-03	-68.8	-64.4	
10	80.25	18.75	0.009	-1.62E-03	-56.1	-111.1	
11	79.50	22.50	0.010	-1.13E-03	-40.7	-147.5	
12	78.90	32.02	0.011	-6.54E-04	-24.3	-167.2	
13	78.45	39.77	0.011	-2.65E-04	-8.2	-174.7	
14	78.00	47.47	0.011	1.30E-04	11.5	-174.1	
15	77.50	55.97	0.011	5.55E-04	37.3	-162.2	
		34.88	0.011	5.55E-04	37.3	-162.2	
16	76.75	44.20	0.010	1.09E-03	67.0	-123.8	
17	76.00	54.36	0.009	1.44E-03	103.9	-60.7	
		-47.10	0.009	1.44E-03	103.9	-60.7	
18	75.38	-47.30	0.008	1.55E-03	74.4	-5.6	
19	74.75	-46.40	0.007	1.51E-03	45.2	31.1	
20	74.00	-36.77	0.006	1.34E-03	14.0	55.4	
21	73.50	-26.98	0.006	1.20E-03	-2.0	57.8	
22	73.20	-21.20	0.005	1.11E-03	-9.2	56.0	
23	73.00	-17.58	0.005	1.06E-03	-13.1	53.7	
24	72.50	-9.25	0.005	9.38E-04	-19.8	44.9	
25	72.00	-1.86	0.004	8.39E-04	-22.5	33.8	
26	71.20	8.73	0.003	7.40E-04	-19.8	14.9	
27	70.60	16.42	0.003	7.11E-04	-12.3	4.5	
28	70.00	24.45	0.003	7.04E-04	0.0	0.0	

The strut at elev. 84.40 is slack

Strut force at elev. 82.00 = 93.32 kN/m run = 559.90 kN/strut

(continued)

Stage No.10 Excavate to elevation 77.50 on PASSIVE side

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure	Soil stiffness coeff.
		Water press.	Vertic -al	Effective Active limit	Effective Passive limit	Earth pressure		
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	5.50	0.00	69.78	8.11	8.11	30201
3	83.50	Total>	14.09	2.50m	78.37	2.50	2.50a	3264
4	83.00	Total>	22.99	5.00m	87.27	5.00	5.00a	3264
5	82.50	Total>	32.09	7.50m	96.38	7.50	7.50a	3264
6	82.00	Total>	41.23	10.00m	105.52	10.00	10.00a	3264
7	81.65	Total>	47.61	11.75m	111.90	11.75	11.75a	3264
8	81.50	Total>	50.33	12.50m	114.62	12.50	12.50a	3264
9	81.00	Total>	59.35	15.00m	123.64	15.00	15.00a	3264
10	80.25	Total>	72.71	18.75m	137.01	18.75	18.75a	3264
11	79.50	Total>	85.89	22.50m	150.18	22.50	22.50a	3264
12	78.90	Total>	96.30	32.02	160.60	32.02	32.02a	3264
13	78.45	Total>	104.05	39.77	168.35	39.77	39.77a	3264
14	78.00	Total>	111.75	47.47	176.05	47.47	47.47a	3264
15	77.50	Total>	120.25	55.97	184.56	55.97	55.97a	3264
16	76.75	Total>	132.93	68.65	197.24	68.65	68.65a	3264
17	76.00	Total>	145.54	81.25	209.84	81.25	81.25a	3264
		Total>	145.54	40.00m	324.81	40.00	40.00a	9791
18	75.38	Total>	156.63	43.13m	344.86	43.13	43.13a	10281
19	74.75	Total>	167.69	46.25m	364.88	46.25	46.25a	10770
20	74.00	Total>	180.93	50.00m	388.88	58.38	58.38	11358
21	73.50	Total>	189.75	52.50m	404.87	70.27	70.27	11749
		Total>	189.75	52.50m	412.70	123.27	123.27	11749
22	73.20	Total>	195.34	54.00m	422.15	131.89	131.89	11954
23	73.00	Total>	199.06	55.00m	428.45	137.54	137.54	12090
24	72.50	Total>	208.37	57.50m	444.20	151.36	151.36	12430
25	72.00	Total>	217.68	60.00m	459.95	164.79	164.79	12771
26	71.20	Total>	232.57	64.00m	485.15	185.81	185.81	13316
27	70.60	Total>	243.74	67.00m	504.05	201.53	201.53	13724
28	70.00	Total>	254.91	70.00m	522.95	217.46	217.46	14133

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure	Soil stiffness coeff.
		Water press.	Vertic -al	Effective Active limit	Effective Passive limit	Earth pressure		
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	64.28	21.09	21.09	3866
16	76.75	Total>	12.77	3.75m	77.05	24.45	24.45	3866

(continued)

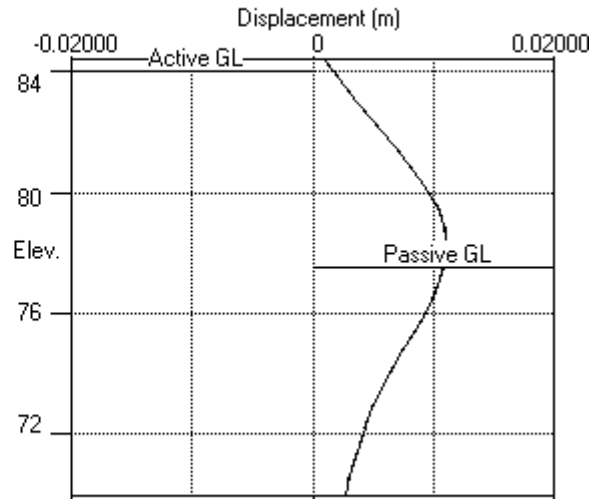
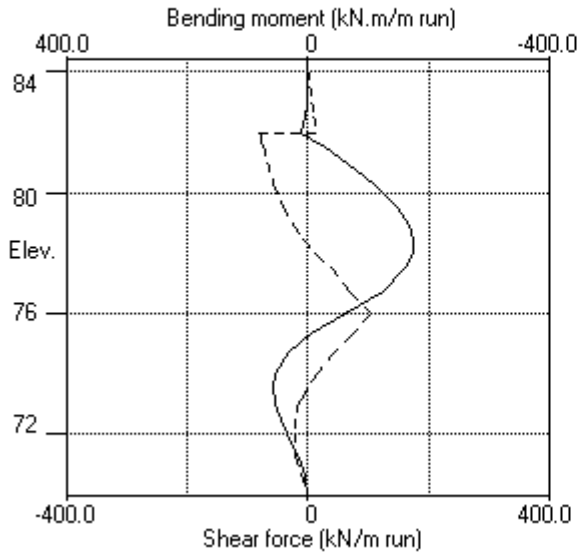
Stage No.10 Excavate to elevation 77.50 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure	Soil stiffness
		Water press.	Vertical	Effective Active limit	Effective Passive limit	Earth pressure		
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3	
17	76.00	Total>	25.65	7.50m	89.94	26.90	26.90	3866
		Total>	25.65	7.50m	204.90	87.10	87.10	11597
18	75.38	Total>	37.18	10.63m	225.39	90.42	90.42	12176
19	74.75	Total>	48.89	13.75m	246.07	92.65	92.65	12756
20	74.00	Total>	63.25	17.50m	271.18	95.15	95.15	13452
21	73.50	Total>	73.01	20.00m	288.11	97.26	97.26	13916
		Total>	73.01	20.00m	295.94	150.26	150.26	13916
22	73.20	Total>	79.24	21.50m	306.03	153.09	153.09	14158
23	73.00	Total>	83.42	22.50m	312.79	155.12	155.12	14319
24	72.50	Total>	93.98	25.00m	329.79	160.61	160.61	14722
25	72.00	Total>	104.67	27.50m	346.92	166.65	166.65	15126
26	71.20	Total>	122.02	31.50m	374.58	177.08	177.08	15771
27	70.60	Total>	135.20	34.50m	395.50	185.11	185.11	16255
28	70.00	Total>	148.50	37.50m	416.52	193.01	193.01	16739

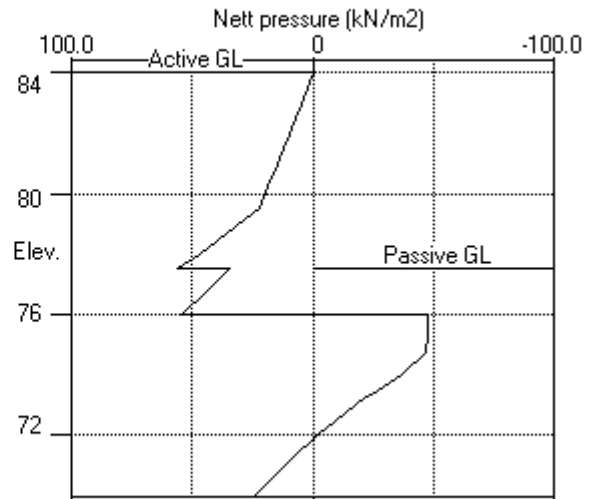
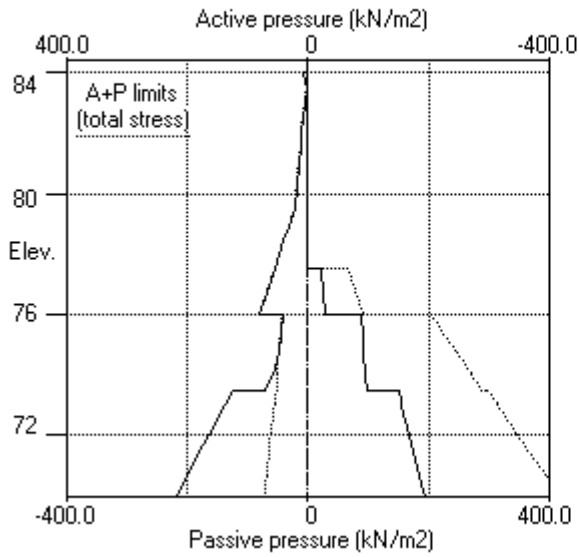
Note: 46.25a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.10 Excav. to elev. 77.50 on PASSIVE side

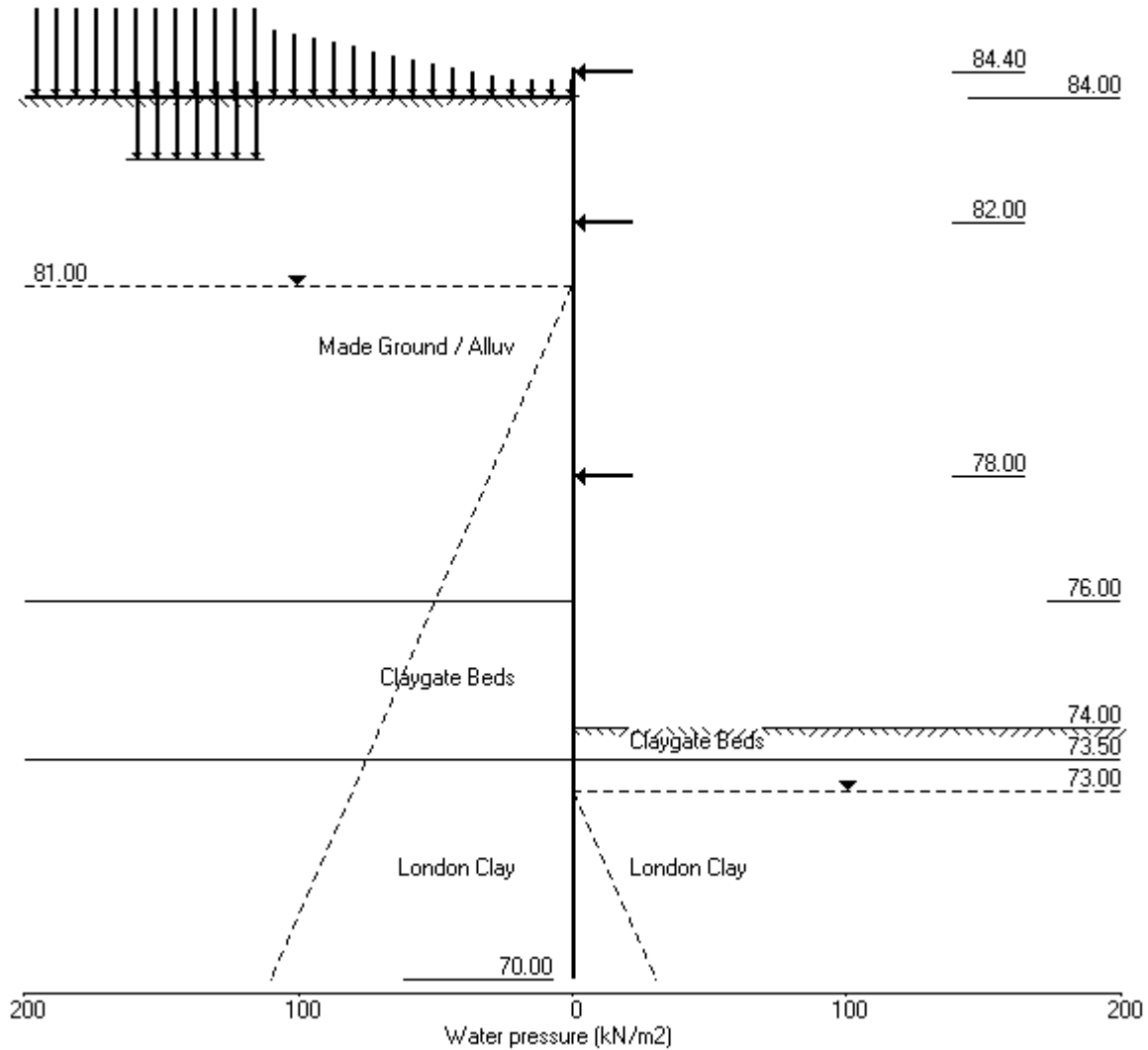


Stage No.10 Excav. to elev. 77.50 on PASSIVE side



Units: kN,m

Stage No.13 Excav. to elev. 74.00 on PASSIVE side





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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 13 Excavate to elevation 74.00 on PASSIVE side

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.85E-03	0.0	-0.0	-0.0
2	84.00	0.00	0.002	-1.85E-03	0.0	-0.0	
		8.05	0.002	-1.85E-03	0.0	-0.0	
3	83.50	2.94	0.003	-1.85E-03	2.7	1.1	
4	83.00	5.88	0.004	-1.86E-03	5.0	3.0	
5	82.50	8.83	0.004	-1.87E-03	8.6	6.3	
6	82.00	11.78	0.005	-1.89E-03	13.8	11.8	67.3
		11.78	0.005	-1.89E-03	-53.5	11.8	
7	81.65	13.83	0.006	-1.90E-03	-49.0	-5.9	
8	81.50	14.70	0.006	-1.89E-03	-46.9	-13.1	
9	81.00	17.54	0.007	-1.83E-03	-38.8	-34.5	
10	80.25	21.45	0.009	-1.66E-03	-24.2	-58.1	
11	79.50	24.67	0.010	-1.41E-03	-6.9	-69.8	
12	78.90	33.05	0.011	-1.20E-03	10.4	-68.9	
13	78.45	39.77	0.011	-1.06E-03	26.8	-60.7	
14	78.00	47.47	0.012	-9.41E-04	46.4	-44.4	165.0
		47.47	0.012	-9.41E-04	-118.6	-44.4	
15	77.50	55.97	0.012	-7.62E-04	-92.7	-97.5	
16	76.75	68.65	0.012	-2.92E-04	-46.0	-150.4	
17	76.00	81.25	0.012	3.04E-04	10.2	-165.0	
		40.00	0.012	3.04E-04	10.2	-165.0	
18	75.38	43.13	0.012	8.03E-04	36.2	-151.2	
19	74.75	46.25	0.011	1.23E-03	64.1	-120.6	
20	74.00	50.00	0.010	1.56E-03	100.2	-56.5	
		-47.28	0.010	1.56E-03	100.2	-56.5	
21	73.50	-45.33	0.009	1.65E-03	77.1	-12.7	
		-77.30	0.009	1.65E-03	77.1	-12.7	
22	73.20	-68.41	0.009	1.66E-03	55.2	6.9	
23	73.00	-62.22	0.009	1.64E-03	42.1	16.6	
24	72.50	-46.42	0.008	1.58E-03	15.0	29.9	
25	72.00	-30.37	0.007	1.51E-03	-4.2	31.6	
26	71.20	-4.65	0.006	1.41E-03	-18.2	18.3	
27	70.60	14.99	0.005	1.37E-03	-15.1	6.5	
28	70.00	35.46	0.004	1.36E-03	0.0	0.0	

The strut at elev. 84.40 is slack

Strut force at elev. 82.00 = 67.31 kN/m run = 403.86 kN/strut  
 Strut force at elev. 78.00 = 165.00 kN/m run = 990.00 kN/strut



(continued)

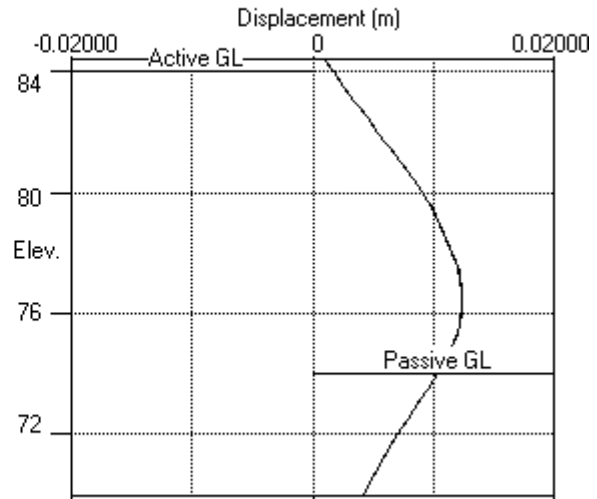
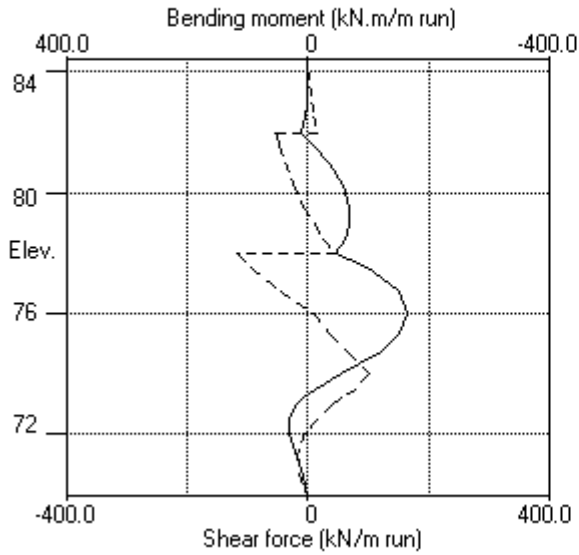
Stage No.13 Excavate to elevation 74.00 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
18	75.38	0.00	0.00	0.00	0.00	0.00	0.0	
19	74.75	0.00	0.00	0.00	0.00	0.00	0.0	
20	74.00	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	207.93	97.28	15962	
21	73.50	Total>	9.01	2.50m	224.11	97.83	16513	
		Total>	9.01	2.50m	231.93	150.83	16513	
22	73.20	Total>	14.74	4.00m	241.53	151.65	16800	
23	73.00	Total>	18.57	5.00m	247.94	152.05	16991	
24	72.50	Total>	28.24	7.50m	264.05	152.96	17470	
25	72.00	Total>	38.06	10.00m	280.31	153.76	17948	
26	71.20	Total>	54.16	14.00m	306.72	155.16	18714	
27	70.60	Total>	66.62	17.00m	326.90	156.15	19288	
28	70.00	Total>	79.41	20.00m	347.42	156.85	19862	

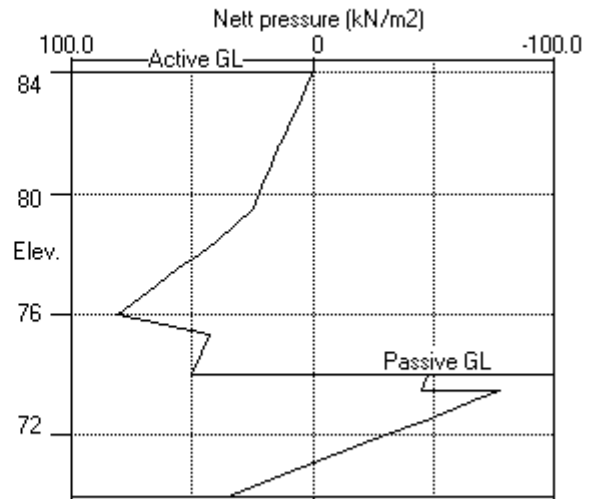
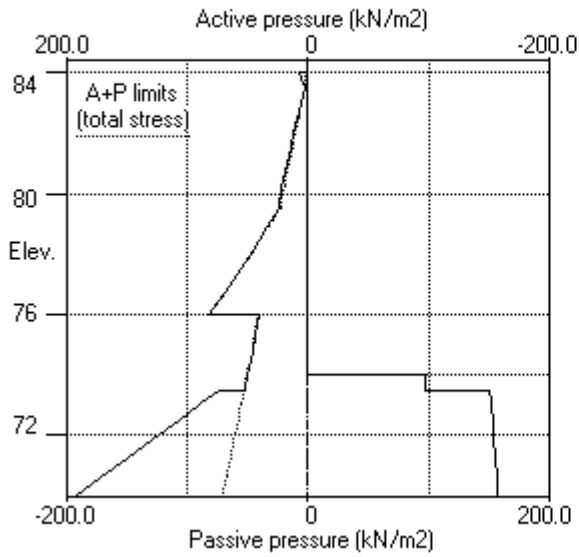
Note: 52.50a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.13 Excav. to elev. 74.00 on PASSIVE side

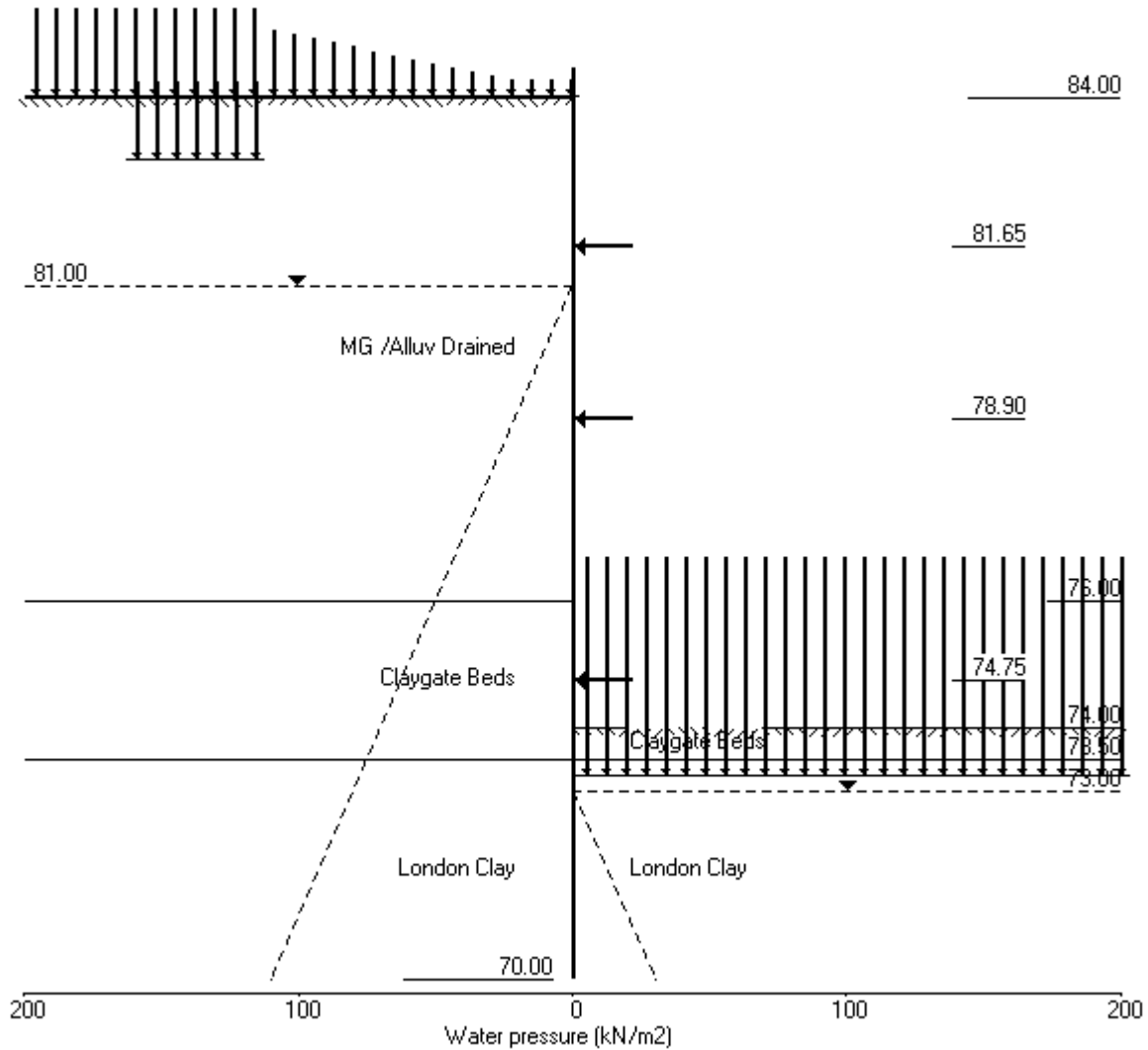


Stage No.13 Excav. to elev. 74.00 on PASSIVE side



Units: kN,m

Stage No.23 Change soil type 1 to soil type 4



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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.84E-03	0.0	-0.0	
2	84.00	0.00	0.002	-1.84E-03	0.0	-0.0	
		7.72	0.002	-1.84E-03	0.0	-0.0	
3	83.50	6.87	0.003	-1.84E-03	3.6	1.2	
4	83.00	11.70	0.003	-1.85E-03	8.3	4.1	
5	82.50	16.62	0.004	-1.86E-03	15.4	9.9	
6	82.00	21.55	0.005	-1.90E-03	24.9	19.8	
7	81.65	24.96	0.006	-1.95E-03	33.0	30.2	100.8
		24.96	0.006	-1.95E-03	-67.8	30.2	
8	81.50	26.41	0.006	-1.96E-03	-63.9	20.3	
9	81.00	31.18	0.007	-1.98E-03	-49.5	-8.1	
10	80.25	41.99	0.009	-1.90E-03	-22.1	-35.1	
11	79.50	52.70	0.010	-1.76E-03	13.4	-38.6	
12	78.90	61.18	0.011	-1.67E-03	47.6	-20.6	221.8
		61.18	0.011	-1.67E-03	-174.2	-20.6	
13	78.45	67.48	0.012	-1.54E-03	-145.3	-92.6	
14	78.00	73.75	0.013	-1.26E-03	-113.5	-151.0	
15	77.50	80.70	0.013	-8.27E-04	-74.9	-198.3	
16	76.75	91.15	0.013	-1.37E-05	-10.4	-231.2	
17	76.00	101.63	0.013	8.27E-04	61.9	-212.9	
		47.90	0.013	8.27E-04	61.9	-212.9	
18	75.38	50.93	0.012	1.42E-03	92.8	-165.4	
19	74.75	54.35	0.011	1.83E-03	125.7	-97.7	72.3
		54.35	0.011	1.83E-03	53.4	-97.7	
20	74.00	64.80	0.010	2.09E-03	98.1	-39.3	
		-33.26	0.010	2.09E-03	98.1	-39.3	
21	73.50	-18.83	0.009	2.14E-03	85.0	5.2	
		-50.81	0.009	2.14E-03	85.0	5.2	
22	73.20	-34.99	0.008	2.11E-03	72.2	28.4	
		-102.24	0.008	2.11E-03	72.2	28.4	
23	73.00	-91.67	0.008	2.08E-03	52.8	40.8	
24	72.50	-66.19	0.007	1.96E-03	13.3	55.7	
25	72.00	-41.86	0.006	1.82E-03	-13.7	54.0	
26	71.20	-3.32	0.004	1.65E-03	-31.8	29.8	
27	70.60	26.16	0.003	1.59E-03	-24.9	10.2	
28	70.00	56.99	0.002	1.57E-03	0.0	0.0	
Strut force at elev.			81.65 =	100.84 kN/m run =	100.84 kN/strut		
Strut force at elev.			78.90 =	221.78 kN/m run =	221.78 kN/strut		
Strut force at elev.			74.75 =	72.28 kN/m run =	72.28 kN/strut		



(continued)

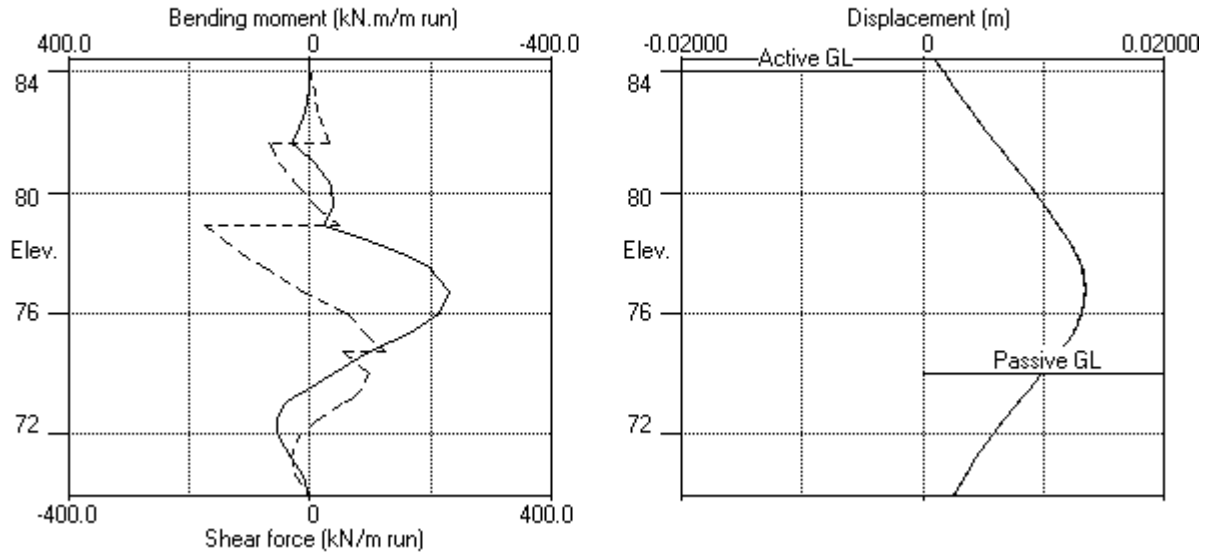
Stage No.23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure	Soil stiffness
		Water press.	Vertical	Effective Active limit	Effective Passive limit	Earth pressure		
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3
17	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	207.93	98.06	98.06	20831
21	73.50	Total>	9.01	2.50m	224.11	90.64	90.64	21549
		Total>	9.01	2.50m	231.93	143.64	143.64	21549
22	73.20	Total>	14.74	4.00m	241.53	140.19	140.19	21924
		Total>	84.74	4.00m	311.54	207.45	207.45	21924
23	73.00	Total>	88.56	5.00m	317.95	205.20	205.20	22174
24	72.50	Total>	98.08	7.50m	333.91	200.70	200.70	22798
25	72.00	Total>	107.31	10.00m	349.58	197.26	197.26	23423
26	71.20	Total>	121.23	14.00m	373.81	191.49	191.49	24422
27	70.60	Total>	131.10	17.00m	391.40	186.55	186.55	25171
28	70.00	Total>	140.73	20.00m	408.76	180.78	180.78	25921

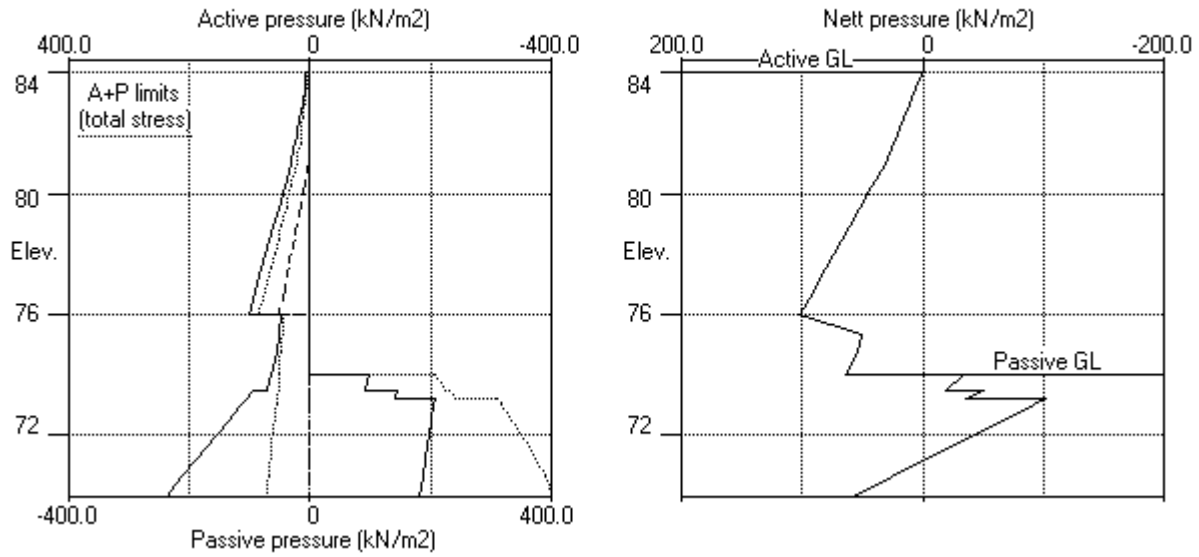


Units: kN,m

Stage No.23 Change soil type 1 to soil type 4

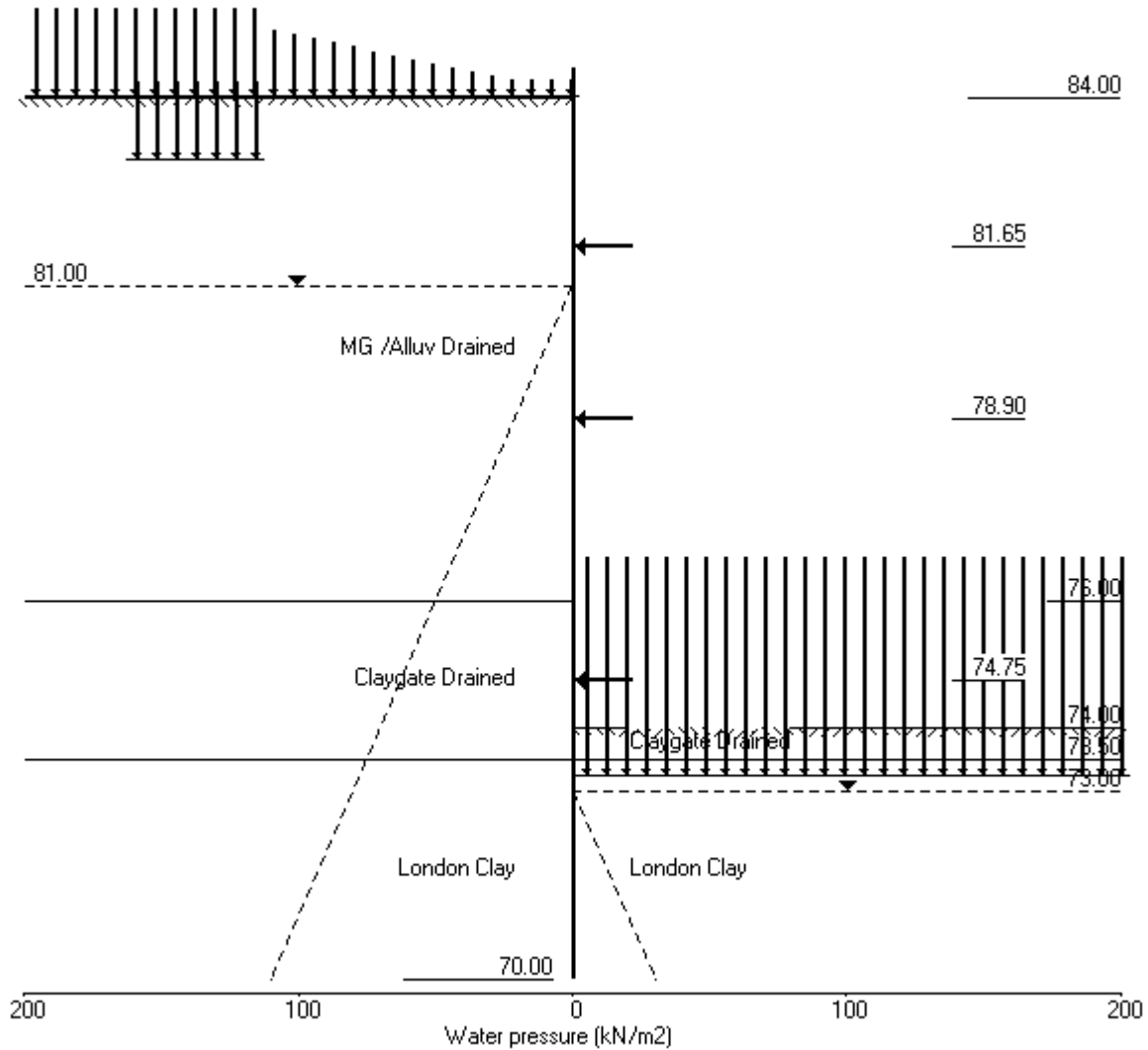


Stage No.23 Change soil type 1 to soil type 4



Units: kN,m

Stage No.24 Change soil type 2 to soil type 5



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor  
 of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.83E-03	0.0	-0.0	
2	84.00	0.00	0.002	-1.83E-03	0.0	-0.0	
		7.64	0.002	-1.83E-03	0.0	-0.0	
3	83.50	6.81	0.003	-1.83E-03	3.6	1.2	
4	83.00	11.65	0.004	-1.84E-03	8.2	4.1	
5	82.50	16.59	0.004	-1.86E-03	15.3	9.8	
6	82.00	21.54	0.005	-1.89E-03	24.8	19.7	
7	81.65	24.96	0.006	-1.94E-03	33.0	30.0	99.2
		24.96	0.006	-1.94E-03	-66.2	30.0	
8	81.50	26.41	0.006	-1.96E-03	-62.4	20.4	
9	81.00	31.20	0.007	-1.97E-03	-48.0	-7.2	
10	80.25	42.02	0.009	-1.90E-03	-20.5	-33.1	
11	79.50	52.73	0.010	-1.77E-03	15.0	-35.4	
12	78.90	61.18	0.011	-1.69E-03	49.2	-16.4	228.4
		61.18	0.011	-1.69E-03	-179.2	-16.4	
13	78.45	67.46	0.012	-1.57E-03	-150.3	-90.7	
14	78.00	73.70	0.013	-1.29E-03	-118.5	-151.3	
15	77.50	80.62	0.013	-8.51E-04	-79.9	-201.1	
16	76.75	91.04	0.013	-1.98E-05	-15.6	-237.8	
17	76.00	101.54	0.013	8.54E-04	56.7	-223.5	
		153.28	0.013	8.54E-04	56.7	-223.5	
18	75.38	164.49	0.012	1.45E-03	156.0	-158.1	
19	74.75	175.49	0.011	1.75E-03	262.2	-28.2	378.2
		175.49	0.011	1.75E-03	-116.0	-28.2	
20	74.00	187.87	0.010	1.92E-03	20.3	-62.5	
21	73.50	166.83	0.009	2.04E-03	109.0	-30.7	
		-58.06	0.009	2.04E-03	109.0	-30.7	
22	73.20	-43.14	0.008	2.06E-03	93.8	-0.7	
		-110.39	0.008	2.06E-03	93.8	-0.7	
23	73.00	-100.18	0.008	2.05E-03	72.7	15.9	
24	72.50	-74.91	0.007	1.98E-03	29.0	39.7	
25	72.00	-50.06	0.006	1.87E-03	-2.3	44.8	
26	71.20	-9.75	0.005	1.73E-03	-26.2	27.1	
27	70.60	21.47	0.004	1.67E-03	-22.7	9.7	
28	70.00	54.20	0.003	1.66E-03	0.0	0.0	
Strut force at elev.			81.65 =	99.20 kN/m run =	99.20 kN/strut		
Strut force at elev.			78.90 =	228.39 kN/m run =	228.39 kN/strut		
Strut force at elev.			74.75 =	378.17 kN/m run =	378.17 kN/strut		

(continued)

Stage No.24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	
		0.00	5.50	1.78	19.80	7.64	3884	
3	83.50	0.00	14.59	4.73	52.52	6.81	3884	
4	83.00	0.00	23.99	7.77	86.37	11.65	3884	
5	82.50	0.00	33.59	10.88	120.94	16.59	3884	
6	82.00	0.00	43.23	14.01	155.66	21.54	3884	
7	81.65	0.00	49.96	16.19	179.88	24.96	2987	
8	81.50	0.00	52.83	17.12	190.22	26.41	2987	
9	81.00	0.00	62.35	20.20	224.50	31.20	2987	
10	80.25	7.50	68.96	22.35	248.31	34.52	2987	
11	79.50	15.00	75.39	24.43	271.44	37.73	2987	
12	78.90	21.00	80.40	26.05	289.50	40.18	2081	
13	78.45	25.50	84.10	27.25	302.81	41.96	2081	
14	78.00	30.00	87.75	28.43	315.95	43.70	2081	
15	77.50	35.00	91.75	29.73	330.38	45.62	2081	
16	76.75	42.50	97.68	31.65	351.73	48.54	2081	
17	76.00	50.00	103.54	33.55	372.81	51.54	2081	
		50.00	103.54	36.37	336.79	103.28	6058	
18	75.38	56.25	108.38	38.07	352.52	108.24	6361	
19	74.75	62.50	113.19	39.76	368.16	112.99	6664	
20	74.00	70.00	118.93	41.78	386.85	117.87	7027	
21	73.50	75.00	122.75	43.12	399.27	121.13	7270	
		Total>	197.75	52.50m	420.70	89.25	16165	
22	73.20	Total>	203.34	54.00m	430.16	101.17	16447	
23	73.00	Total>	207.06	55.00m	436.46	109.32	16634	
24	72.50	Total>	216.37	57.50m	452.21	130.19	17102	
25	72.00	Total>	225.68	60.00m	467.96	151.34	17571	
26	71.20	Total>	240.57	64.00m	493.15	184.99	18320	
27	70.60	Total>	251.74	67.00m	512.05	210.39	18882	
28	70.00	Total>	262.91	70.00m	530.95	236.39	19445	

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	
16	76.75	0.00	0.00	0.00	0.00	0.00	0.00	

(continued)

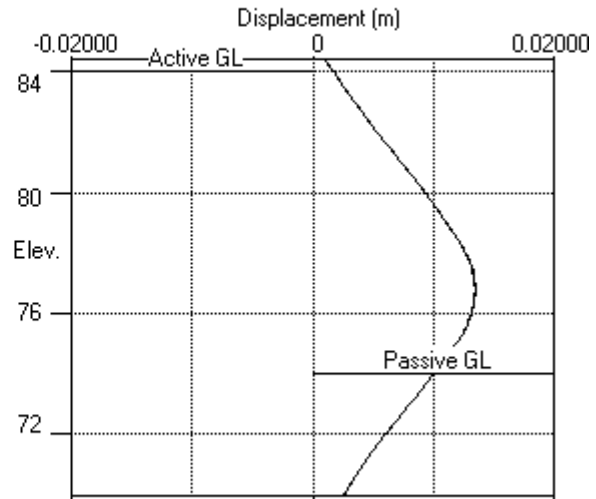
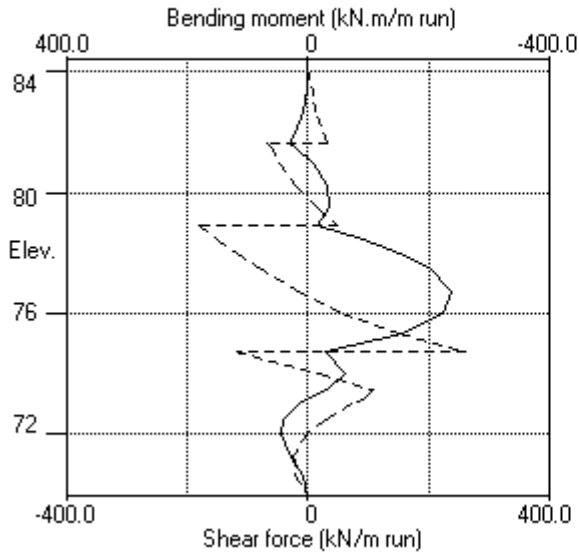
Stage No.24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
17	76.00	0.00	0.00	0.00	0.00	0.00	0.0	
18	75.38	0.00	0.00	0.00	0.00	0.00	0.0	
19	74.75	0.00	0.00	0.00	0.00	0.00	0.0	
20	74.00	0.00	0.00	0.00	0.00	0.00	0.0	
		0.00	0.00	0.00	0.00	0.00	7178	
21	73.50	0.00	9.01	3.16	29.30	29.30	7426	
		Total>	9.01	2.50m	231.93	147.31	16498	
22	73.20	Total>	14.74	4.00m	241.53	144.31	16785	
		Total>	84.74	4.00m	311.54	211.57	16785	
23	73.00	Total>	88.56	5.00m	317.95	209.50	16976	
24	72.50	Total>	98.08	7.50m	333.91	205.10	17454	
25	72.00	Total>	107.31	10.00m	349.58	201.40	17932	
26	71.20	Total>	121.23	14.00m	373.81	194.73	18697	
27	70.60	Total>	131.10	17.00m	391.40	188.92	19271	
28	70.00	Total>	140.73	20.00m	408.76	182.19	19844	

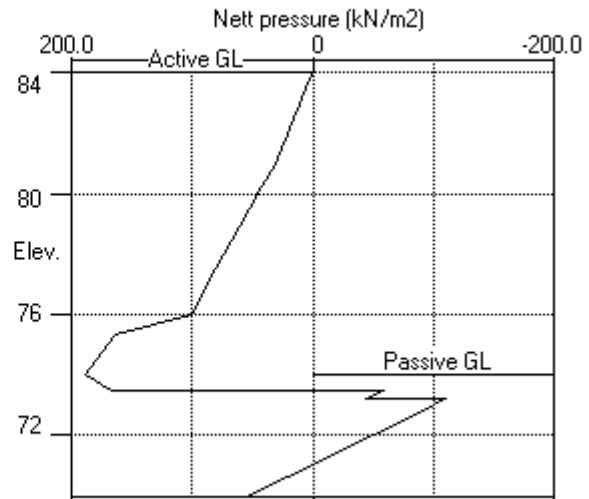
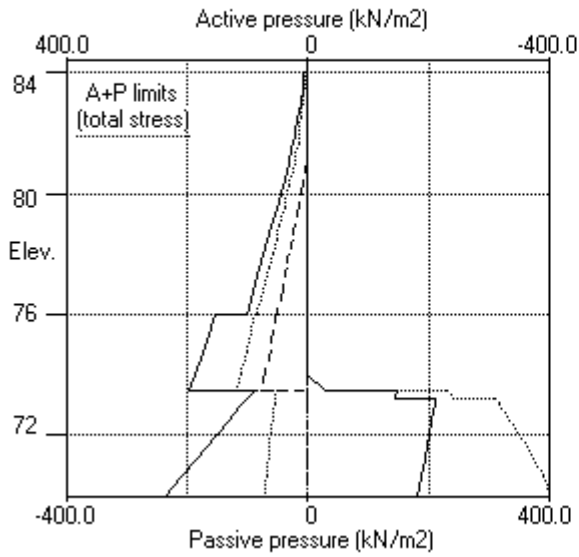
Note: 12.34a Soil pressure at active limit  
 29.30p Soil pressure at passive limit

Units: kN,m

Stage No.24 Change soil type 2 to soil type 5

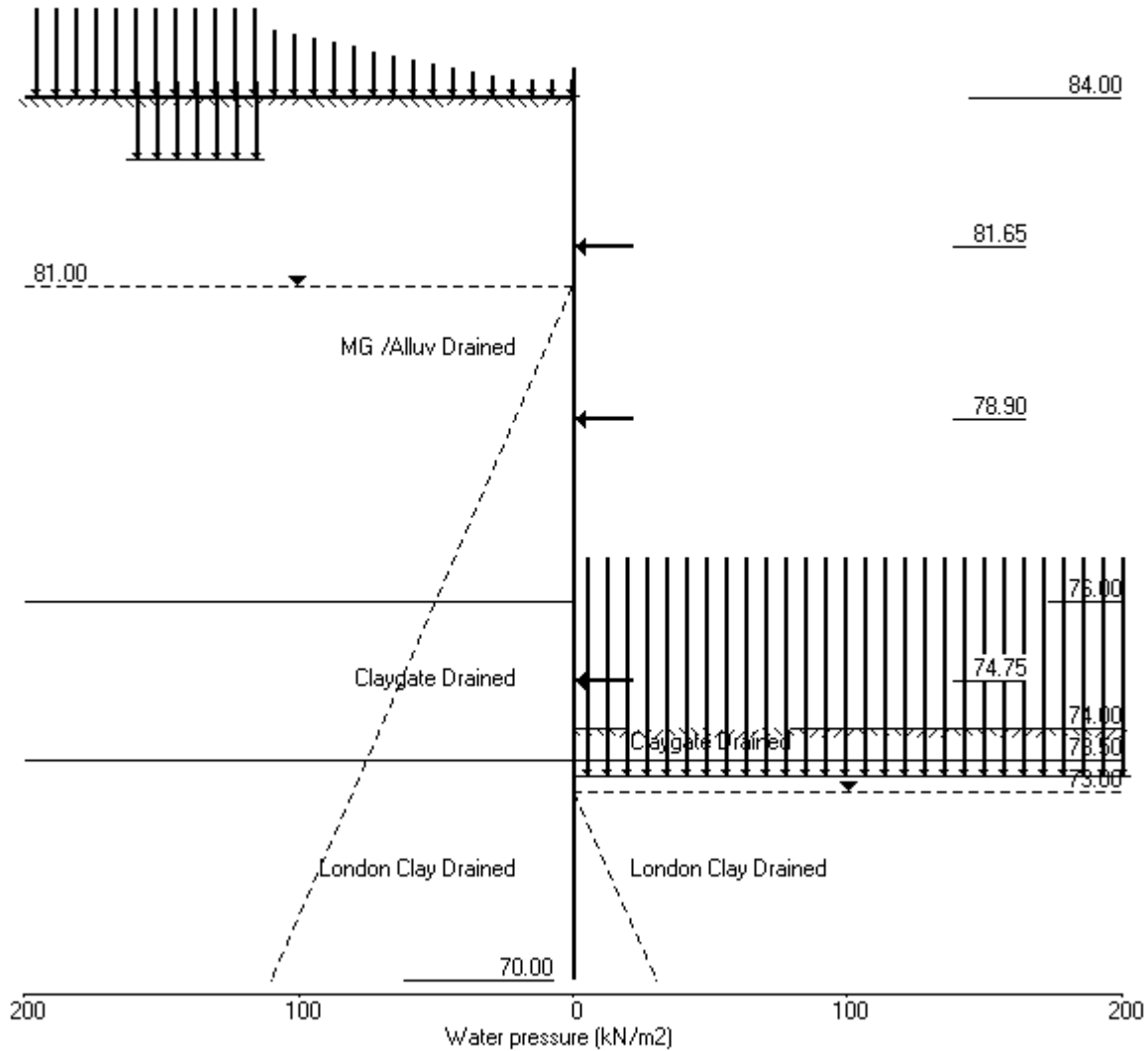


Stage No.24 Change soil type 2 to soil type 5



Units: kN,m

Stage No.25 Change soil type 3 to soil type 6



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 25 Change properties of soil type 3 to soil type 6  
 Ko pressures will be reset

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor  
 of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.001	-1.89E-03	0.0	-0.0	
2	84.00	0.00	0.002	-1.89E-03	0.0	-0.0	
		8.23	0.002	-1.89E-03	0.0	-0.0	
3	83.50	7.27	0.002	-1.90E-03	3.9	1.3	
4	83.00	12.00	0.003	-1.90E-03	8.7	4.3	
5	82.50	16.81	0.004	-1.92E-03	15.9	10.4	
6	82.00	21.62	0.005	-1.96E-03	25.5	20.6	
7	81.65	24.96	0.006	-2.01E-03	33.7	31.2	112.4
		24.96	0.006	-2.01E-03	-78.7	31.2	
8	81.50	26.38	0.006	-2.03E-03	-74.9	19.6	
9	81.00	31.07	0.007	-2.03E-03	-60.5	-14.2	
10	80.25	41.80	0.009	-1.91E-03	-33.2	-49.5	
11	79.50	52.55	0.010	-1.70E-03	2.2	-61.4	
12	78.90	61.20	0.011	-1.53E-03	36.3	-50.1	180.6
		61.20	0.011	-1.53E-03	-144.3	-50.1	
13	78.45	67.68	0.012	-1.35E-03	-115.3	-108.6	
14	78.00	74.16	0.012	-1.05E-03	-83.4	-153.5	
15	77.50	81.37	0.013	-6.31E-04	-44.5	-185.7	
16	76.75	92.10	0.013	9.10E-05	20.6	-195.6	
17	76.00	102.62	0.013	7.52E-04	93.6	-153.8	
		156.43	0.013	7.52E-04	93.6	-153.8	
18	75.38	166.77	0.012	1.09E-03	194.6	-64.8	
19	74.75	175.39	0.011	1.05E-03	301.5	89.7	518.6
		175.39	0.011	1.05E-03	-217.1	89.7	
20	74.00	182.63	0.011	9.27E-04	-82.9	-20.5	
21	73.50	157.22	0.010	1.00E-03	2.1	-40.9	
22	73.20	140.32	0.010	1.06E-03	46.7	-33.7	
		-32.87	0.010	1.06E-03	46.7	-33.7	
23	73.00	-30.67	0.010	1.09E-03	40.4	-25.0	
24	72.50	-25.62	0.009	1.13E-03	26.3	-9.1	
25	72.00	-20.65	0.009	1.14E-03	14.7	0.3	
26	71.20	-10.75	0.008	1.13E-03	2.2	3.6	
27	70.60	-2.02	0.007	1.12E-03	-1.7	2.2	
28	70.00	7.57	0.006	1.12E-03	0.0	0.0	
Strut force at elev.			81.65 =	112.36 kN/m run =	112.36 kN/strut		
Strut force at elev.			78.90 =	180.61 kN/m run =	180.61 kN/strut		
Strut force at elev.			74.75 =	518.62 kN/m run =	518.62 kN/strut		





(continued)

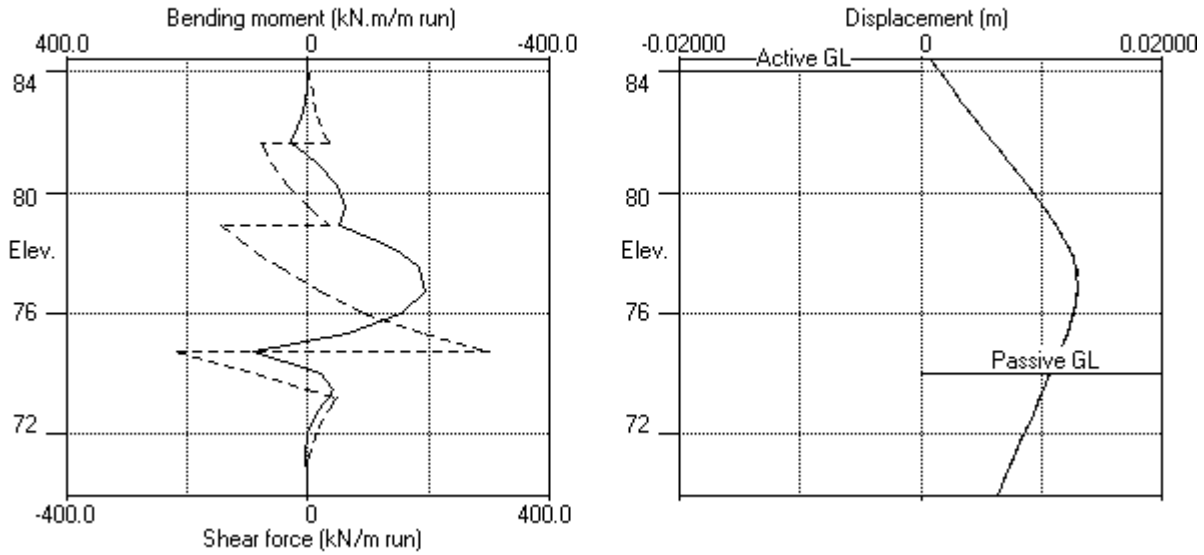
Stage No.25 Change properties of soil type 3 to soil type 6  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
17	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	0.00	0.00	0.00	0.00	0.00	7893
21	73.50	0.00	9.01	3.16	29.30	29.30	29.30p	8165
		0.00	9.01	3.16	30.99	30.99	30.99p	8165
22	73.20	0.00	14.74	5.18	50.70	50.70	50.70p	8307
		0.00	84.74	29.77	291.49	223.89	223.89	8307
23	73.00	0.00	88.56	31.11	304.66	223.62	223.62	8402
24	72.50	5.00	93.08	32.70	320.20	218.55	223.55	8639
25	72.00	10.00	97.31	34.18	334.75	213.86	223.86	8875
26	71.20	18.00	103.23	36.26	355.12	205.03	223.03	9254
27	70.60	24.00	107.10	37.62	368.41	197.34	221.34	9538
28	70.00	30.00	110.73	38.90	380.91	188.77	218.77	9822

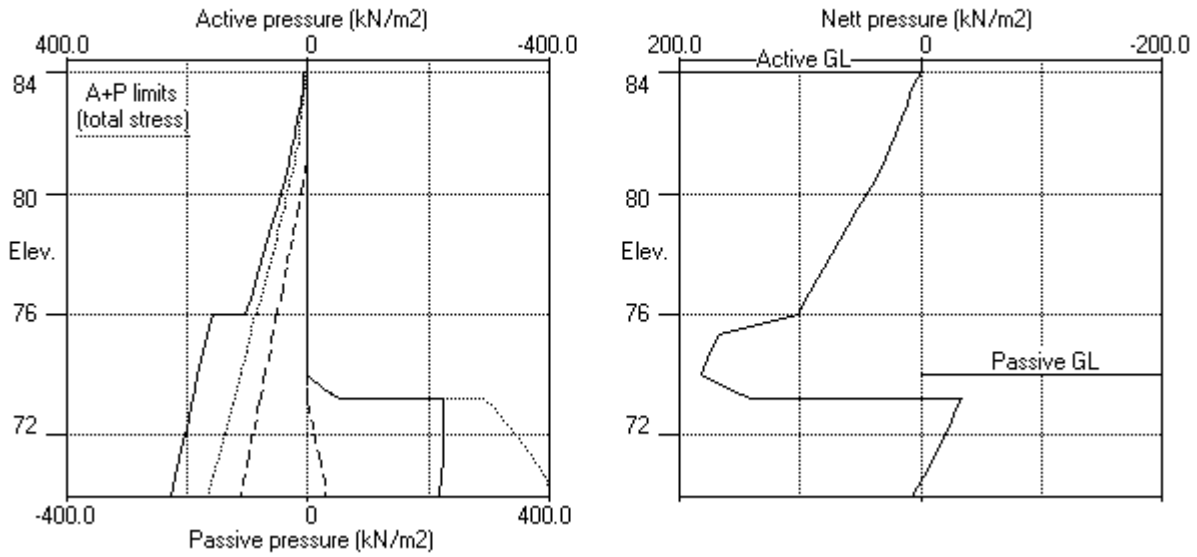
Note: 12.34a Soil pressure at active limit  
 50.70p Soil pressure at passive limit

Units: kN,m

Stage No.25 Change soil type 3 to soil type 6



Stage No.25 Change soil type 3 to soil type 6



Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		---- Bending moment ----				----- Shear force -----			
		max.	min.	Calculated		Factored		Calculated		Factored	
				m	m	max.	min.	max.	min.	max.	min.
				kN.m/m		kN.m/m		kN/m		kN/m	
1	84.40	0.001	0.000	0	-0	0	-0	0	-26	0	-36
2	84.00	0.002	0.000	0	-11	0	-14	0	-26	0	-36
3	83.50	0.003	0.000	1	-24	2	-32	4	-26	5	-35
4	83.00	0.004	0.000	4	-36	6	-49	9	-24	12	-32
5	82.50	0.005	0.000	10	-48	14	-64	16	-21	21	-28
6	82.00	0.006	0.000	21	-57	28	-77	26	-81	34	-110
7	81.65	0.007	0.000	31	-62	42	-83	34	-79	45	-106
8	81.50	0.007	0.000	20	-64	28	-86	0	-76	0	-102
9	81.00	0.008	0.000	0	-69	0	-93	0	-69	0	-93
10	80.25	0.009	0.000	0	-111	0	-150	1	-56	2	-76
11	79.50	0.010	0.000	0	-147	0	-199	18	-131	25	-177
12	78.90	0.011	0.000	0	-167	0	-226	49	-179	66	-242
13	78.45	0.012	0.000	0	-175	0	-236	27	-150	36	-203
14	78.00	0.013	0.000	0	-174	0	-235	46	-123	63	-167
15	77.50	0.013	0.000	0	-201	0	-272	37	-97	50	-132
16	76.75	0.013	0.000	1	-238	1	-321	67	-51	90	-68
17	76.00	0.013	0.000	2	-223	3	-302	104	0	140	0
18	75.38	0.012	0.000	18	-171	25	-231	195	0	263	0
19	74.75	0.011	0.000	90	-139	121	-187	302	-217	407	-293
20	74.00	0.011	0.000	55	-72	75	-97	111	-83	150	-112
21	73.50	0.010	0.000	58	-41	78	-55	109	-6	147	-8
22	73.20	0.010	0.000	56	-34	76	-45	94	-9	127	-12
23	73.00	0.010	0.000	54	-25	73	-34	73	-13	98	-18
24	72.50	0.009	0.000	57	-9	77	-12	29	-20	39	-27
25	72.00	0.009	0.000	56	0	75	0	15	-23	20	-30
26	71.20	0.008	0.000	31	0	42	0	2	-33	3	-44
27	70.60	0.007	0.000	11	0	14	0	0	-26	0	-35
28	70.00	0.006	0.000	0	-0	0	-0	0	-0	0	-0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment						Shear force					
	Calculated				Factored		Calculated				Factored	
	max. elev.	min. elev.	max. elev.	min. elev.	max.	min.	max. elev.	min. elev.	max. elev.	min. elev.	max.	min.
	kN.m/m	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m			kN/m	kN/m	kN/m	kN/m
1	4	74.75	-1	79.50	5	-2	3	76.00	-1	72.50	3	-2
2	No calculation at this stage											
3	No calculation at this stage											
4	No calculation at this stage											
5	7	74.00	-10	78.90	9	-13	9	76.00	-3	81.50	12	-4
6	No calculation at this stage											
7	36	74.00	-79	79.50	48	-107	51	76.00	-26	84.40	69	-36
8	No calculation at this stage											
9	35	74.00	-79	79.50	47	-106	50	76.00	-26	84.40	68	-36
10	58	73.50	-175	78.45	78	-236	104	76.00	-81	82.00	140	-110
11	No calculation at this stage											
12	57	73.50	-174	78.45	77	-234	103	76.00	-81	82.00	139	-109
13	32	72.00	-165	76.00	43	-223	100	74.00	-119	78.00	135	-160
14	No calculation at this stage											
15	46	72.00	-181	76.00	62	-244	108	74.00	-123	78.00	146	-167
16	No calculation at this stage											
17	57	72.50	-222	76.75	77	-300	107	74.00	-131	79.50	145	-177
18	No calculation at this stage											
19	55	72.50	-211	76.75	75	-284	111	74.00	-127	78.90	150	-171
20	No calculation at this stage											
21	56	72.50	-212	76.75	75	-286	111	74.00	-125	78.90	149	-169
22	56	72.50	-212	76.75	75	-286	111	74.00	-125	78.90	149	-169
23	56	72.50	-231	76.75	75	-312	126	74.75	-174	78.90	170	-235
24	45	72.00	-238	76.75	61	-321	262	74.75	-179	78.90	354	-242
25	90	74.75	-196	76.75	121	-264	302	74.75	-217	74.75	407	-293

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum	elev.	minimum	elev.	
	m		m		
1	0.001	84.40	0.000	84.40	Apply surcharge no.1 at elev. 84.00
2	No calculation at this stage				Apply surcharge no.2 at elev. 84.00
3	No calculation at this stage				Apply surcharge no.3 at elev. 84.00
4	No calculation at this stage				Apply surcharge no.6 at elev. 84.00
5	0.001	80.25	0.000	84.40	Apply surcharge no.7 at elev. 83.00
6	No calculation at this stage				Install strut no.1 at elev. 84.40
7	0.006	78.90	0.000	84.40	Excav. to elev. 81.50 on PASSIVE side
8	No calculation at this stage				Install strut no.2 at elev. 82.00
9	0.006	78.90	0.000	84.40	Apply water pressure profile no.1
10	0.011	78.00	0.000	84.40	Excav. to elev. 77.50 on PASSIVE side
11	No calculation at this stage				Install strut no.3 at elev. 78.00
12	0.011	78.00	0.000	84.40	Apply water pressure profile no.3
13	0.012	76.75	0.000	84.40	Excav. to elev. 74.00 on PASSIVE side
14	No calculation at this stage				Install strut no.4 at elev. 74.75
15	0.012	76.75	0.000	84.40	Apply surcharge no.4 at elev. 73.20
16	No calculation at this stage				Install strut no.5 at elev. 79.50
17	0.013	76.75	0.000	84.40	Remove strut no.3 at elev. 78.00
18	No calculation at this stage				Install strut no.6 at elev. 78.90
19	0.013	76.75	0.000	84.40	Remove strut no.5 at elev. 79.50
20	No calculation at this stage				Install strut no.7 at elev. 81.65
21	0.013	76.75	0.000	84.40	Remove strut no.2 at elev. 82.00
22	0.013	76.75	0.000	84.40	Remove strut no.1 at elev. 84.40
23	0.013	76.75	0.000	84.40	Change soil type 1 to soil type 4
24	0.013	76.75	0.000	84.40	Change soil type 2 to soil type 5
25	0.013	76.75	0.000	84.40	Change soil type 3 to soil type 6

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Strut forces at each stage (horizontal components)**

Stage no.	----- Strut no. 1 ----- at elev. 84.40			----- Strut no. 2 ----- at elev. 82.00			----- Strut no. 3 ----- at elev. 78.00		
	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut
7	26	159	215	---	---	---	---	---	---
9	26	158	214	0	0	0	---	---	---
10	slack	slack	slack	93	560	756	---	---	---
12	slack	slack	slack	93	559	754	1	6	8
13	slack	slack	slack	67	404	545	165	990	1337
15	slack	slack	slack	69	412	556	168	1007	1359
17	slack	slack	slack	47	282	380	---	---	---
19	slack	slack	slack	61	367	496	---	---	---
21	slack	slack	slack	---	---	---	---	---	---

Stage no.	----- Strut no. 4 ----- at elev. 74.75			----- Strut no. 5 ----- at elev. 79.50			----- Strut no. 6 ----- at elev. 78.90		
	--Calculated-- kN per m run	--Factored-- kN per strut	Factor kN per strut	--Calculated-- kN per m run	--Factored-- kN per strut	Factor kN per strut	--Calculated-- kN per m run	--Factored-- kN per strut	Factor kN per strut
15	slack	slack	slack	---	---	---	---	---	---
17	36	36	48	150	898	1213	---	---	---
19	22	22	30	---	---	---	143	143	193
21	24	24	32	---	---	---	134	134	181
22	24	24	32	---	---	---	134	134	181
23	72	72	98	---	---	---	222	222	299
24	378	378	511	---	---	---	228	228	308
25	519	519	700	---	---	---	181	181	244



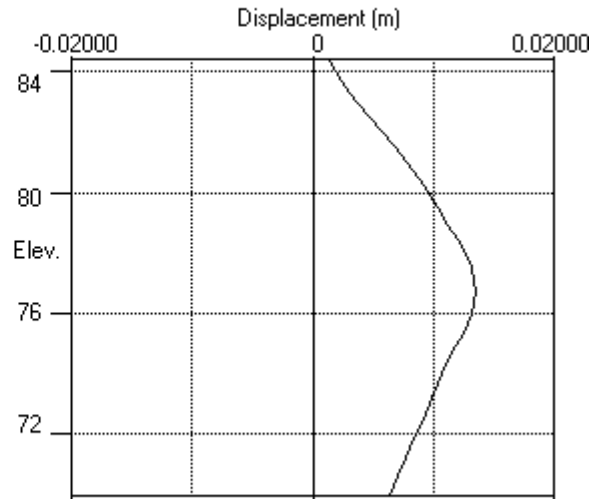
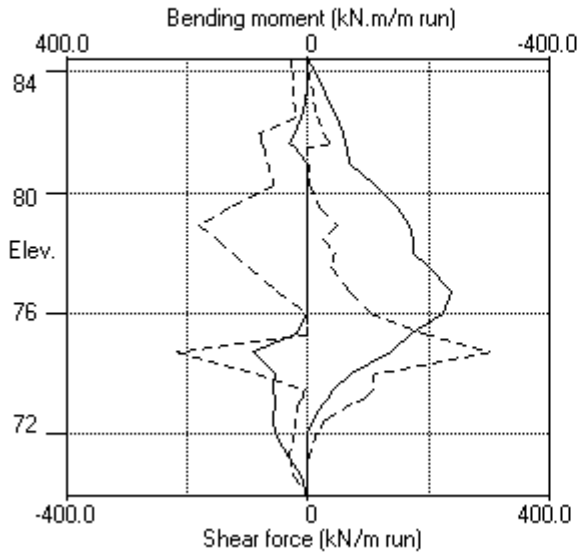
Stage no.	----- Strut no. 7 ----- at elev. 81.65		
	--Calculated--		Factored
	kN per m run	kN per strut	kN per strut
21	67	67	91
22	67	67	91
23	101	101	136
24	99	99	134
25	112	112	152

Temporary license on loan from Geosolve | Sheet No.  
Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
Licensed from GEOSOLVE | Made by : MC  
Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS1  
59 Maresfield Gardens | Date: 6-12-2012  
East Wall | Checked :

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Units: kN,m

Bending moment, shear force, displacement envelopes



Temporary license on loan from Geosolve | Sheet No.  
 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	84.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES (Unfactored SLS soil strengths)**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.390)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (2.476)	1.000 (2.477)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.253 (4.831)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.500	0.00
3 London Clay	0.00	0.670	0.00	0.00	0.670	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.500	0.00
6 London Clay Drained	25.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile		Active side			Passive side			
Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	73.00	73.00	0.0 MC
4	1	82.00	82.00	0.0	1	73.20	73.20	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.80 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 7.0700E-03 m4/m run  
 E.I = 197960 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	84.40	6.00	0.010000	2.000E+08	5.00	0.00	0	No
2	82.00	6.00	0.010000	2.000E+08	5.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	1.00	0.00	0	No
4	74.75	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5	79.50	6.00	0.100000	2.000E+08	5.00	0.00	0	No
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	3.000E+07	1.00	0.00	0	No
8	76.30	6.00	0.010000	2.000E+08	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- kN/m2 ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	84.00	0.00(A)	8.00	20.00	5.00	=	N/A	1.30 Var
2	84.00	5.00(A)	8.00	15.00	5.00	=	N/A	1.30 Var
3	84.00	1.00(A)	8.00	4.00	0.00	17.00	N/A	1.00 P/U
4	73.20	-0.00(P)	8.00	10.00	70.00	=	N/A	1.00 -
5	74.00	-0.00(P)	10.00	10.00	70.00	=	N/A	1.00 -
6	84.00	5.00(A)	10.00	15.00	17.00	=	N/A	1.00 P/U
7	83.00	5.00(A)	2.00	2.00	25.00	=	N/A	1.00 P/U

Note: A = Active side, P = Passive side

A trapezoidal surcharge is defined by two values:

N = at edge near to wall, F = at edge far from wall

Limit State Categories P/U = Permanent Unfavourable

P/F = Permanent Favourable

Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 84.00 No analysis at this stage
2	Apply surcharge no.2 at elevation 84.00 No analysis at this stage
3	Apply surcharge no.3 at elevation 84.00 No analysis at this stage
4	Apply surcharge no.6 at elevation 84.00 No analysis at this stage
5	Apply surcharge no.7 at elevation 83.00 No analysis at this stage
6	Install strut or anchor no.1 at elevation 84.40
7	Excavate to elevation 81.50 on PASSIVE side
8	Install strut or anchor no.2 at elevation 82.00
9	Apply water pressure profile no.2 ( Worst Cred. )
10	Excavate to elevation 77.50 on PASSIVE side
11	Install strut or anchor no.3 at elevation 78.00
12	Apply water pressure profile no.4 ( Worst Cred. )
13	Excavate to elevation 74.00 on PASSIVE side
14	Install strut or anchor no.4 at elevation 74.75
15	Apply surcharge no.4 at elevation 73.20
16	Install strut or anchor no.5 at elevation 79.50
17	Remove strut or anchor no.3 at elevation 78.00
18	Install strut or anchor no.6 at elevation 78.90
19	Remove strut or anchor no.5 at elevation 79.50
20	Install strut or anchor no.7 at elevation 81.65
21	Remove strut or anchor no.2 at elevation 82.00
22	Remove strut or anchor no.1 at elevation 84.40
23	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
24	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
25	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: ULS DA1 Combination 2

Water pressures : Worst Credible

Partial factor on C' = 1.250

Partial factor on Phi' = 1.250

Partial factor on Cu = 1.400

Partial factor on Soil Modulus = 1.000

Partial factor on Permanent Unfavourable loads = 1.000

Partial factor on Permanent Favourable loads = 1.000

Partial factor on Permanent Variable loads = 1.300

Stability analysis:

Method of analysis - Strength Factor method

Overall factor on soil strength for calculating wall depth = 1.00

Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>

Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients

Open Tension Crack analysis? - No

Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:

Length of wall (normal to plane of analysis) = 6.00 m

Width of excavation on active side of wall = 20.00 m

Width of excavation on passive side of wall = 10.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

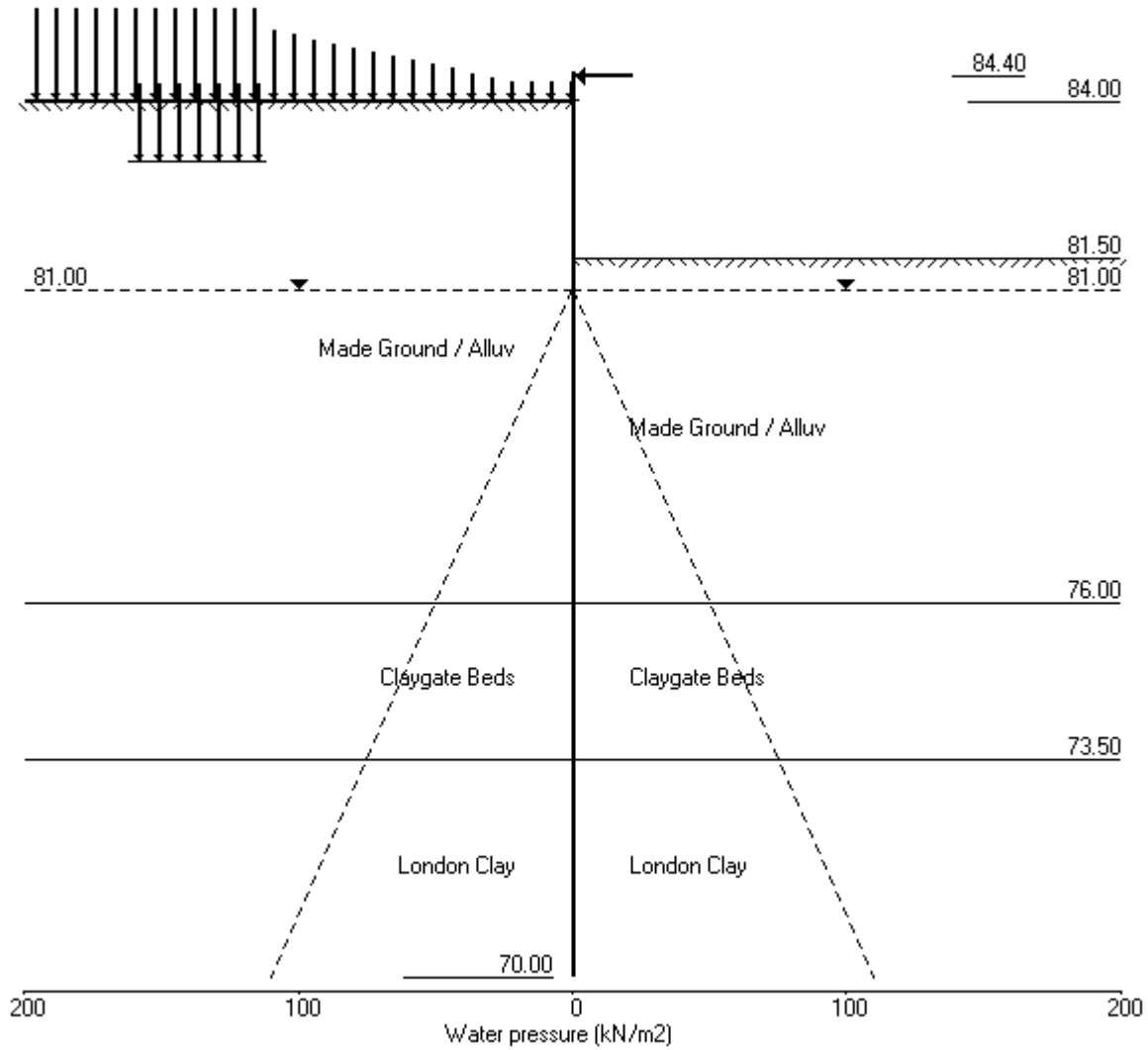
**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 84.00	No	No	No
2	Apply surcharge no.2 at elev. 84.00	No	No	No
3	Apply surcharge no.3 at elev. 84.00	No	No	No
4	Apply surcharge no.6 at elev. 84.00	No	No	No
5	Apply surcharge no.7 at elev. 83.00	No	No	No
6	Install strut no.1 at elev. 84.40	No	No	No
7	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
8	Install strut no.2 at elev. 82.00	No	No	No
9	Apply water pressure profile no.2	No	No	No
10	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
11	Install strut no.3 at elev. 78.00	No	No	No
12	Apply water pressure profile no.4	No	No	No
13	Excav. to elev. 74.00 on PASSIVE side	Yes	No	Yes
14	Install strut no.4 at elev. 74.75	No	No	No
15	Apply surcharge no.4 at elev. 73.20	No	No	No
16	Install strut no.5 at elev. 79.50	No	No	No
17	Remove strut no.3 at elev. 78.00	No	No	No
18	Install strut no.6 at elev. 78.90	No	No	No
19	Remove strut no.5 at elev. 79.50	No	No	No
20	Install strut no.7 at elev. 81.65	No	No	No
21	Remove strut no.2 at elev. 82.00	No	No	No
22	Remove strut no.1 at elev. 84.40	No	No	No
23	Change soil type 1 to soil type 4	No	No	No
24	Change soil type 2 to soil type 5	No	No	No
25	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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Units: kN,m

Stage No.7 Excav. to elev. 81.50 on PASSIVE side



Temporary license on loan from Geosolve | Sheet No.  
 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 7 Excavate to elevation 81.50 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

		Overall					
		FoS for toe		Toe elev. for			
		elev. = 70.00		FoS = 1.000			
		-----		-----			
Stage	--- G.L. ---	Strut	Factor	Moment	Toe	Wall	
No.	Act.	Pass.	Elev.	of	equilib.	Penetr	
				Safety	at elev.	-ation	
7	84.00	81.50	84.40	5.125	n/a	81.22	0.28

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.002	-1.57E-03	-28.4	-0.0	28.4
2	84.00	0.00	0.002	-1.56E-03	-28.4	-11.4	
3	83.50	2.50	0.003	-1.51E-03	-27.8	-25.5	
4	83.00	5.00	0.004	-1.43E-03	-25.9	-38.9	
5	82.50	7.50	0.004	-1.32E-03	-22.8	-51.2	
6	82.00	10.00	0.005	-1.17E-03	-18.4	-61.5	
7	81.65	11.75	0.005	-1.06E-03	-14.6	-67.3	
8	81.50	12.50	0.006	-1.01E-03	-12.8	-69.4	
		-2.40	0.006	-1.01E-03	-12.8	-69.4	
9	81.00	-1.46	0.006	-8.30E-04	-13.8	-76.0	
10	80.25	3.23	0.007	-5.23E-04	-13.1	-86.1	
11	79.50	11.62	0.007	-1.81E-04	-7.5	-94.2	
12	78.90	15.94	0.007	1.06E-04	0.7	-96.3	
13	78.45	17.77	0.007	3.23E-04	8.3	-94.4	
14	78.00	19.83	0.007	5.31E-04	16.8	-88.8	
15	77.50	22.39	0.006	7.42E-04	27.3	-77.9	
16	77.00	25.17	0.006	9.18E-04	39.2	-61.3	
17	76.50	28.13	0.005	1.04E-03	52.5	-38.5	
18	76.00	31.16	0.005	1.10E-03	67.4	-8.7	
		-48.24	0.005	1.10E-03	67.4	-8.7	
19	75.38	-39.20	0.004	1.07E-03	40.0	23.9	
20	74.75	-29.79	0.003	9.77E-04	18.5	41.2	
21	74.00	-19.30	0.003	8.10E-04	0.1	46.6	
22	73.50	-13.19	0.002	6.96E-04	-8.0	44.2	
23	73.20	-9.76	0.002	6.31E-04	-11.5	41.2	
24	72.60	-3.81	0.002	5.19E-04	-15.6	32.5	
25	72.00	1.15	0.002	4.36E-04	-16.4	22.4	
26	71.20	6.84	0.001	3.72E-04	-13.2	9.5	
27	70.60	10.92	0.001	3.53E-04	-7.8	2.8	
28	70.00	15.19	0.001	3.49E-04	0.0	0.0	
Strut force at elev.			84.40 =	28.42 kN/m	run =	170.54 kN/strut	



(continued)

Stage No.7 Excavate to elevation 81.50 on PASSIVE side

Node no.	Y coord	----- ACTIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	6.50	0.00	52.42	0.00	0.00a	3299
3	83.50	Total>	15.09	2.50m	61.00	2.50	2.50a	3299
4	83.00	Total>	23.98	5.00m	69.90	5.00	5.00a	3299
5	82.50	Total>	33.08	7.50m	79.00	7.50	7.50a	3299
6	82.00	Total>	42.21	10.00m	88.13	10.00	10.00a	3299
7	81.65	Total>	48.57	11.75m	94.50	11.75	11.75a	3299
8	81.50	Total>	51.29	12.50m	97.21	12.50	12.50a	3299
9	81.00	Total>	60.28	15.00m	106.21	15.00	15.00a	3299
10	80.25	Total>	73.61	27.70	119.54	27.70	27.70a	3299
11	79.50	Total>	86.75	40.83	132.68	40.83	40.83a	3299
12	78.90	Total>	97.14	51.22	143.07	51.22	51.22a	3299
13	78.45	Total>	104.86	58.94	150.80	58.94	58.94a	3299
14	78.00	Total>	112.54	66.62	158.47	66.62	66.62a	3299
15	77.50	Total>	121.02	75.10	166.96	75.10	75.10a	3299
16	77.00	Total>	129.46	83.54	175.40	83.54	83.54a	3299
17	76.50	Total>	137.87	91.94	183.80	91.94	91.94a	3299
18	76.00	Total>	146.24	100.32	192.18	100.32	100.32a	3299
		Total>	146.24	40.00m	274.30	55.44	55.44	9898
19	75.38	Total>	157.30	44.79	291.76	68.83	68.83	10392
20	74.75	Total>	168.34	50.47	309.20	82.40	82.40	10887
21	74.00	Total>	181.55	57.26	330.10	98.32	98.32	11481
22	73.50	Total>	190.35	61.77	344.02	108.51	108.51	11877
		Total>	190.35	52.50m	349.61	161.51	161.51	11877
23	73.20	Total>	195.93	54.00m	357.95	169.01	169.01	12084
24	72.60	Total>	207.08	57.00m	374.62	183.57	183.57	12497
25	72.00	Total>	218.23	60.00m	391.29	197.66	197.66	12910
26	71.20	Total>	233.10	64.00m	413.52	215.99	215.99	13460
27	70.60	Total>	244.25	67.00m	430.19	229.64	229.64	13873
28	70.00	Total>	255.40	70.00m	446.87	243.39	243.39	14286

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
1	84.40	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	84.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	83.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	83.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	45.91	14.90	14.90	3470
9	81.00	Total>	8.50	2.50m	54.42	16.46	16.46	3470
10	80.25	Total>	21.28	6.25m	67.20	24.47	24.47	3470
11	79.50	Total>	34.14	10.00m	80.06	29.21	29.21	3470
12	78.90	Total>	44.49	13.00m	90.41	35.27	35.27	3470
13	78.45	Total>	52.31	15.25m	98.23	41.17	41.17	3470
14	78.00	Total>	60.17	17.50m	106.09	46.78	46.78	3470
15	77.50	Total>	68.97	23.06	114.89	52.71	52.71	3470
16	77.00	Total>	77.82	31.91	123.74	58.37	58.37	3470

(continued)

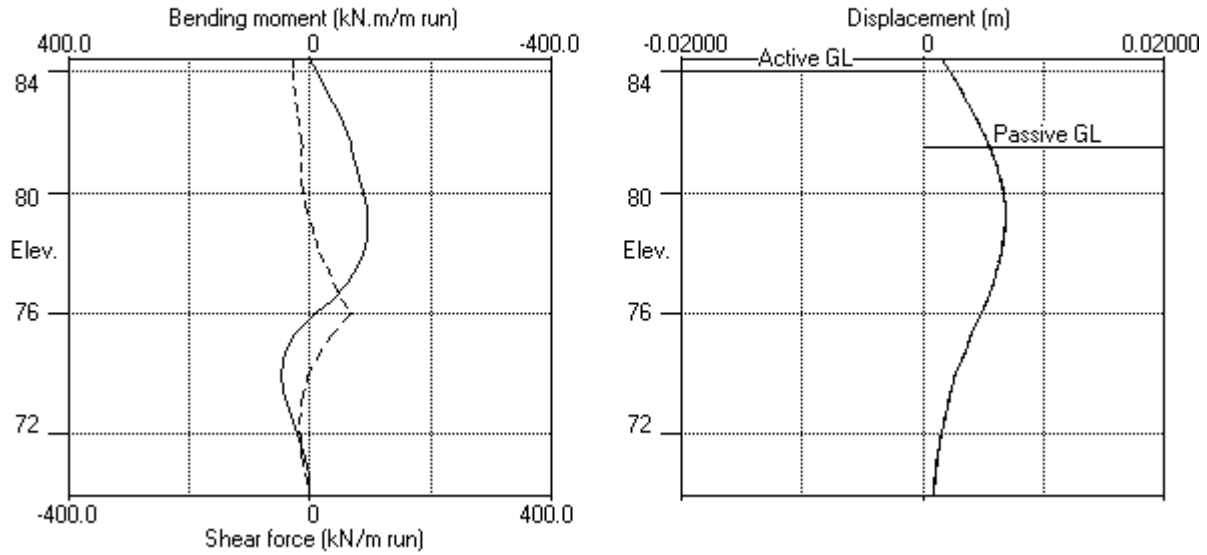
Stage No.7 Excavate to elevation 81.50 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure	Soil stiffness
		Water press.	Vertical	Effective Active limit	Effective Passive limit	Earth pressure		
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3	
17	76.50	Total>	86.72	40.81	132.65	63.82	3470	
18	76.00	Total>	95.68	49.77	141.61	69.15	3470	
		Total>	95.68	27.50m	223.72	103.68	10411	
19	75.38	Total>	107.57	30.63m	242.01	108.02	10932	
20	74.75	Total>	119.52	33.75m	260.37	112.19	11452	
21	74.00	Total>	133.92	37.50m	282.46	117.62	12077	
22	73.50	Total>	143.56	40.00m	297.21	121.70	12494	
		Total>	143.56	40.00m	302.81	174.70	12494	
23	73.20	Total>	149.65	41.50m	311.66	178.77	12711	
24	72.60	Total>	161.84	44.50m	329.37	187.39	13145	
25	72.00	Total>	174.05	47.50m	347.10	196.51	13580	
26	71.20	Total>	190.33	51.50m	370.74	209.15	14159	
27	70.60	Total>	202.54	54.50m	388.47	218.72	14593	
28	70.00	Total>	214.74	57.50m	406.19	228.20	15028	

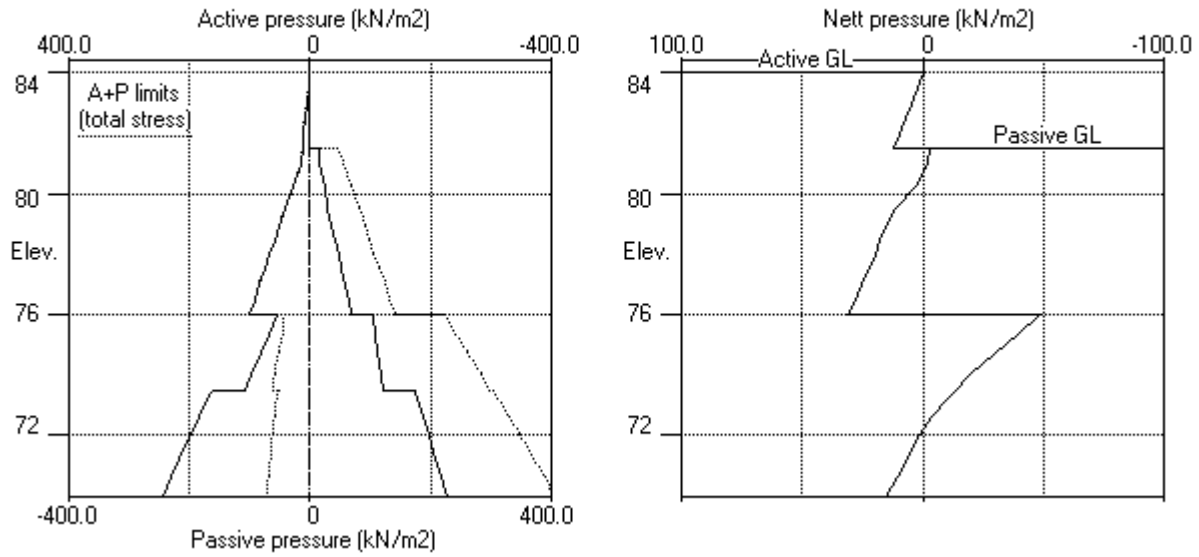
Note: 100.32a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.7 Excav. to elev. 81.50 on PASSIVE side

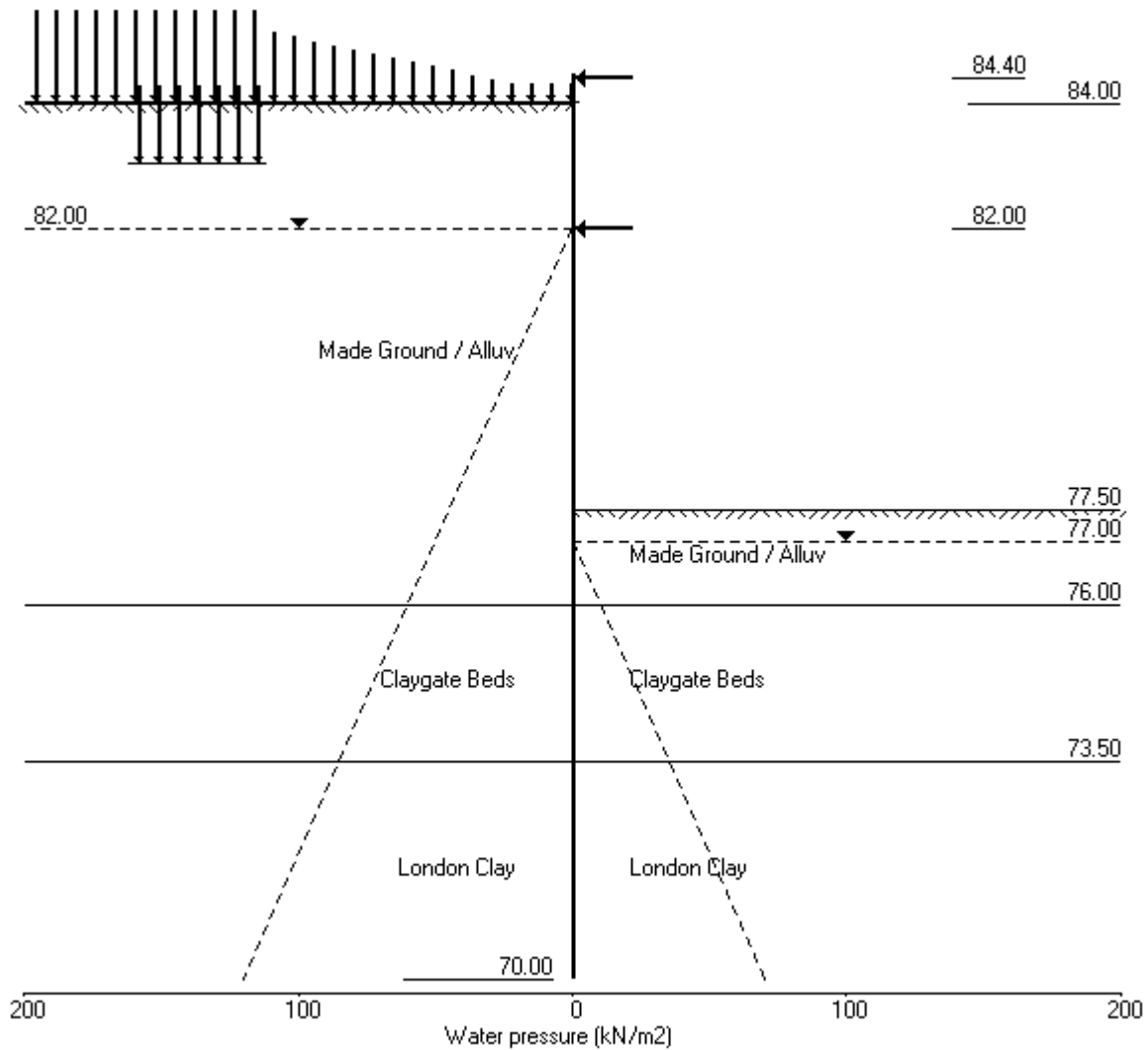


Stage No.7 Excav. to elev. 81.50 on PASSIVE side



Units: kN,m

Stage No.10 Excav. to elev. 77.50 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 10 Excavate to elevation 77.50 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

				Overall		
				FoS for toe	Toe elev. for	
				elev. = 70.00	FoS = 1.000	
				-----	-----	
Stage	--- G.L. ---		Strut	Factor	Moment	Toe Wall
No.	Act. Pass.	Elev.	Elev.	of	equilib.	elev. Penetr
				Safety	at elev.	-ation
10	84.00 77.50			More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.000	-2.70E-03	0.0	-0.0	-0.0
2	84.00	0.00	0.001	-2.70E-03	0.0	-0.0	
		15.16	0.001	-2.70E-03	0.0	-0.0	
3	83.50	5.54	0.003	-2.70E-03	5.2	2.0	
4	83.00	5.00	0.004	-2.71E-03	7.8	5.4	
5	82.50	7.50	0.006	-2.73E-03	10.9	10.0	
6	82.00	10.00	0.007	-2.77E-03	15.3	16.5	126.1
		10.00	0.007	-2.77E-03	-110.8	16.5	
7	81.65	11.75	0.008	-2.76E-03	-107.0	-21.6	
8	81.50	12.50	0.008	-2.74E-03	-105.2	-37.5	
9	81.00	15.00	0.010	-2.58E-03	-98.3	-88.3	
10	80.25	27.70	0.011	-2.12E-03	-82.3	-156.5	
11	79.50	40.83	0.013	-1.42E-03	-56.6	-209.1	
12	78.90	51.22	0.013	-7.54E-04	-29.0	-235.1	
13	78.45	58.94	0.014	-2.11E-04	-4.2	-242.7	
14	78.00	66.62	0.014	3.34E-04	24.1	-238.4	
15	77.50	75.10	0.013	9.11E-04	59.5	-217.7	
		45.15	0.013	9.11E-04	59.5	-217.7	
16	77.00	54.34	0.013	1.41E-03	84.4	-182.1	
17	76.50	59.13	0.012	1.81E-03	112.7	-133.0	
18	76.00	66.89	0.011	2.06E-03	144.2	-69.1	
		-73.25	0.011	2.06E-03	144.2	-69.1	
19	75.38	-67.63	0.010	2.16E-03	100.2	6.2	
20	74.75	-59.72	0.008	2.07E-03	60.4	55.0	
21	74.00	-50.25	0.007	1.81E-03	19.2	82.6	
22	73.50	-40.48	0.006	1.59E-03	-3.5	87.6	
23	73.20	-31.60	0.005	1.46E-03	-14.3	84.7	
24	72.60	-15.81	0.005	1.23E-03	-28.5	70.3	
25	72.00	-2.31	0.004	1.04E-03	-34.0	50.2	
26	71.20	13.35	0.003	9.02E-04	-29.6	22.1	
27	70.60	24.54	0.003	8.58E-04	-18.2	6.6	



(continued)

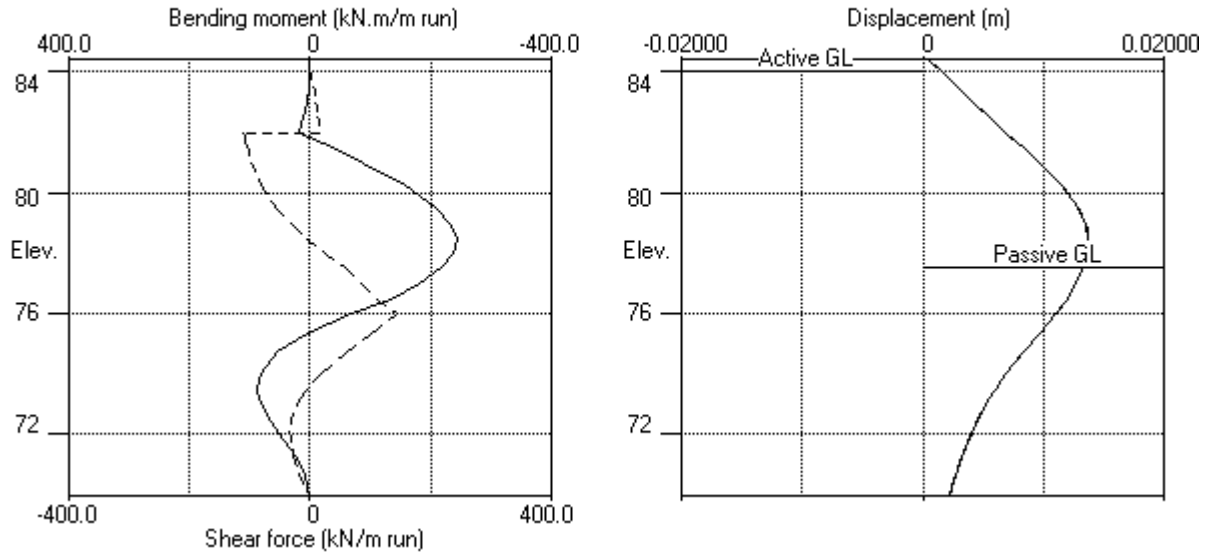
Stage No.10 Excavate to elevation 77.50 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	
		Total>	0.00	0.00	45.91	29.95	4263	
16	77.00	Total>	8.51	2.50m	54.42	29.20	4263	
17	76.50	Total>	17.05	5.00m	62.96	32.81	4263	
18	76.00	Total>	25.65	7.50m	71.57	33.42	4263	
		Total>	25.65	7.50m	153.69	113.25	12788	
19	75.38	Total>	37.18	10.63m	171.62	112.43	13427	
20	74.75	Total>	48.89	13.75m	189.74	110.19	14066	
21	74.00	Total>	63.25	17.50m	211.78	107.51	14834	
22	73.50	Total>	73.01	20.00m	226.66	106.44	15345	
		Total>	73.01	20.00m	232.25	159.44	15345	
23	73.20	Total>	79.24	21.50m	241.24	160.53	15612	
24	72.60	Total>	91.85	24.50m	259.38	163.82	16145	
25	72.00	Total>	104.67	27.50m	277.71	168.43	16679	
26	71.20	Total>	122.02	31.50m	302.43	175.95	17390	
27	70.60	Total>	135.20	34.50m	321.13	181.97	17924	
28	70.00	Total>	148.50	37.50m	339.95	187.83	18458	

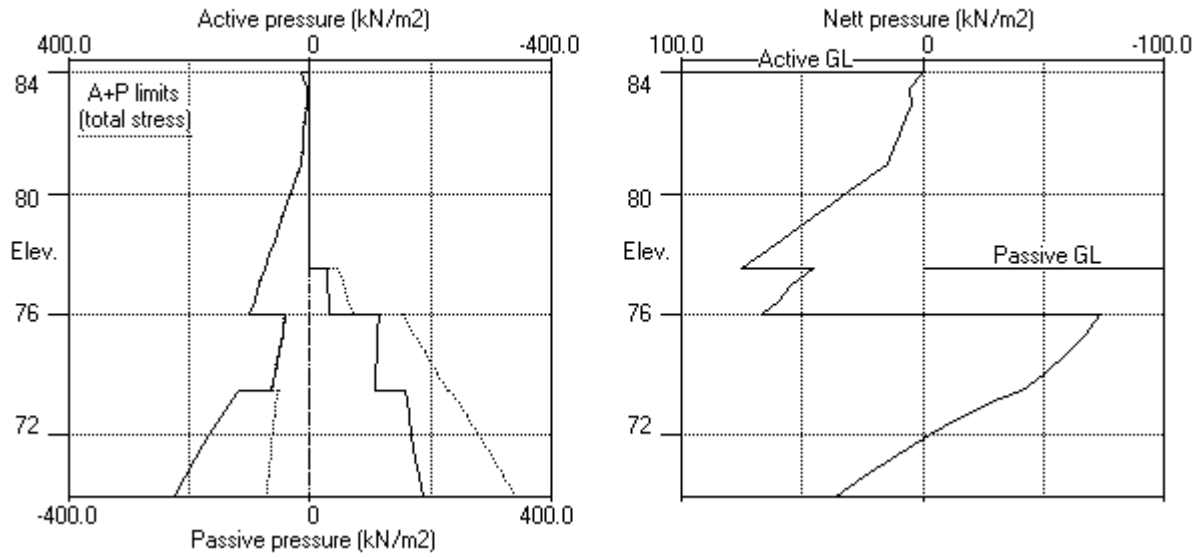
Note: 57.26a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.10 Excav. to elev. 77.50 on PASSIVE side



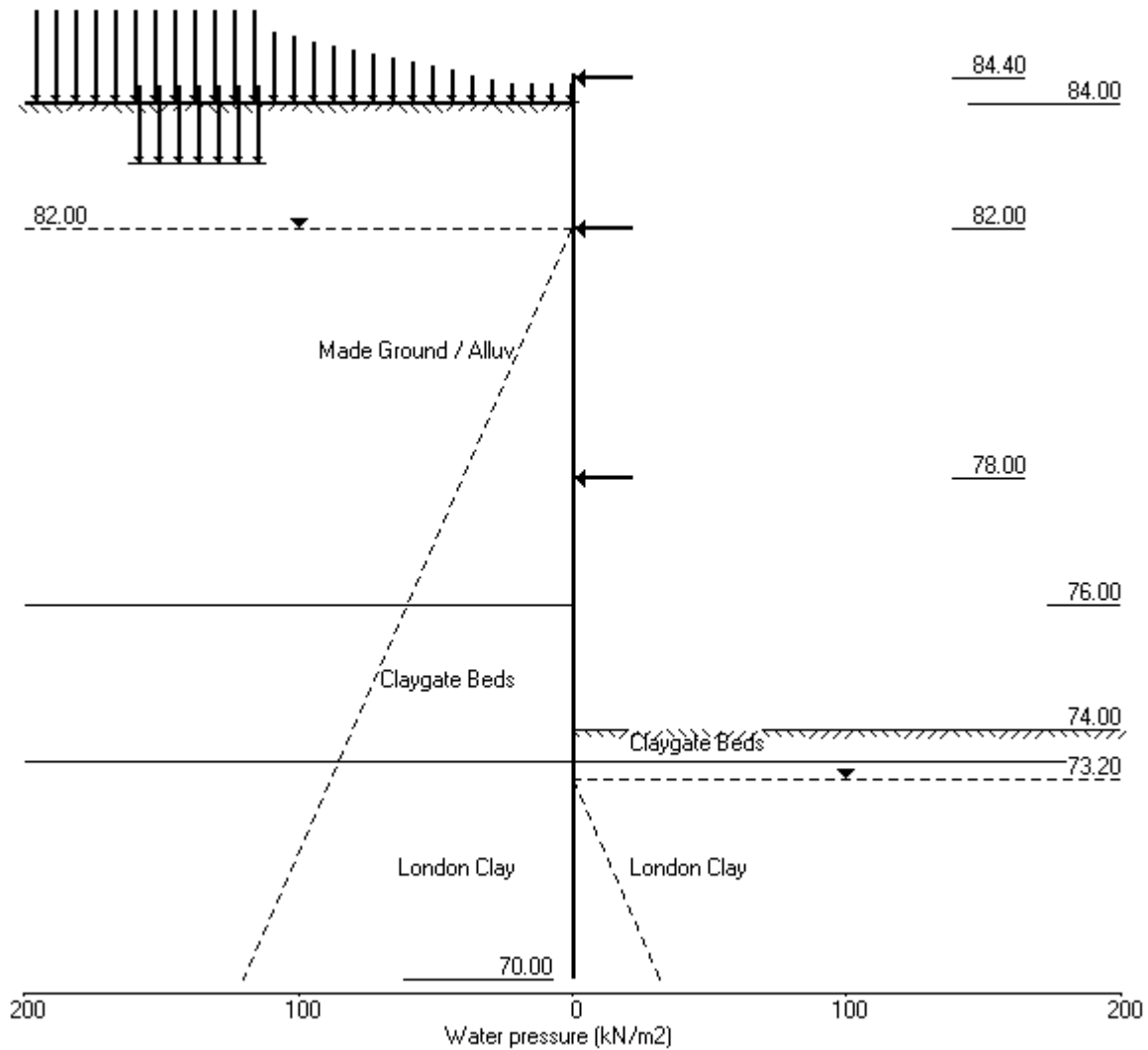
Stage No.10 Excav. to elev. 77.50 on PASSIVE side





Units: kN,m

Stage No.13 Excav. to elev. 74.00 on PASSIVE side



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 13 Excavate to elevation 74.00 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

				Overall		
				FoS for toe	Toe elev. for	
				elev. = 70.00	FoS = 1.000	
				-----	-----	
Stage	--- G.L. ---		Strut	Factor	Moment	Toe Wall
No.	Act. Pass.	Elev.	Elev.	of	equilib.	elev. Penetr
				Safety	at elev.	-ation
13	84.00 74.00			More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.000	-2.47E-03	0.0	-0.0	-0.0
2	84.00	0.00	0.001	-2.47E-03	0.0	-0.0	
		15.16	0.001	-2.47E-03	0.0	-0.0	
3	83.50	6.08	0.003	-2.47E-03	5.3	2.0	
4	83.00	6.05	0.004	-2.48E-03	8.3	5.5	
5	82.50	9.07	0.005	-2.50E-03	12.1	10.6	
6	82.00	12.09	0.006	-2.54E-03	17.4	17.9	95.6
		12.09	0.006	-2.54E-03	-78.1	17.9	
7	81.65	14.19	0.007	-2.55E-03	-73.5	-8.7	
8	81.50	15.08	0.008	-2.54E-03	-71.3	-19.6	
9	81.00	17.97	0.009	-2.45E-03	-63.1	-53.2	
10	80.25	30.83	0.011	-2.17E-03	-44.8	-94.1	
11	79.50	43.33	0.012	-1.77E-03	-17.0	-117.7	
12	78.90	52.36	0.013	-1.41E-03	11.7	-119.5	
13	78.45	58.94	0.014	-1.15E-03	36.8	-108.7	
14	78.00	66.62	0.014	-9.31E-04	65.0	-85.9	200.4
		66.62	0.014	-9.31E-04	-135.3	-85.9	
15	77.50	75.10	0.015	-6.39E-04	-99.9	-144.9	
16	77.00	83.54	0.015	-2.22E-04	-60.2	-185.3	
17	76.50	91.94	0.015	2.69E-04	-16.4	-204.7	
18	76.00	100.32	0.015	7.82E-04	31.7	-201.2	
		40.00	0.015	7.82E-04	31.7	-201.2	
19	75.38	44.80	0.014	1.37E-03	58.2	-174.2	
20	74.75	50.47	0.013	1.85E-03	88.0	-129.8	
21	74.00	57.26	0.011	2.19E-03	128.4	-50.8	
		-66.46	0.011	2.19E-03	128.4	-50.8	
22	73.50	-57.89	0.010	2.25E-03	97.3	6.6	
		-105.83	0.010	2.25E-03	97.3	6.6	
23	73.20	-96.32	0.010	2.22E-03	67.0	32.1	
24	72.60	-67.79	0.008	2.09E-03	17.7	54.9	
25	72.00	-39.36	0.007	1.92E-03	-14.4	53.3	



(continued)

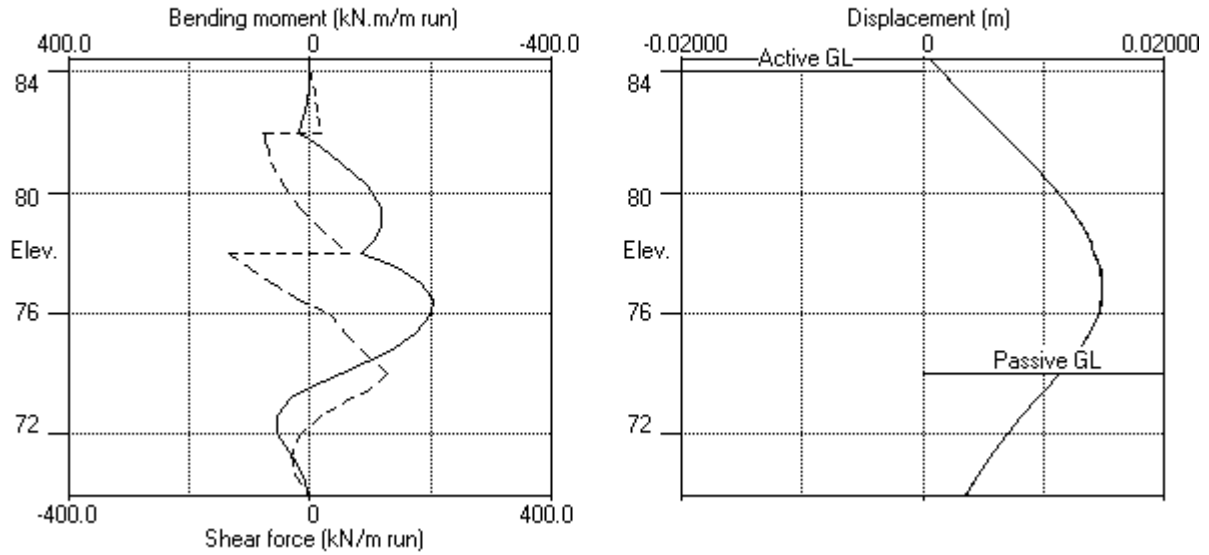
Stage No.13 Excavate to elevation 74.00 on PASSIVE side

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective Active limit kN/m2	Effective Passive limit kN/m2	Earth pressure kN/m2		
8	81.50	0.00	0.00	0.00	0.00	0.00	0.0	
9	81.00	0.00	0.00	0.00	0.00	0.00	0.0	
10	80.25	0.00	0.00	0.00	0.00	0.00	0.0	
11	79.50	0.00	0.00	0.00	0.00	0.00	0.0	
12	78.90	0.00	0.00	0.00	0.00	0.00	0.0	
13	78.45	0.00	0.00	0.00	0.00	0.00	0.0	
14	78.00	0.00	0.00	0.00	0.00	0.00	0.0	
15	77.50	0.00	0.00	0.00	0.00	0.00	0.0	
16	77.00	0.00	0.00	0.00	0.00	0.00	0.0	
17	76.50	0.00	0.00	0.00	0.00	0.00	0.0	
18	76.00	0.00	0.00	0.00	0.00	0.00	0.0	
19	75.38	0.00	0.00	0.00	0.00	0.00	0.0	
20	74.75	0.00	0.00	0.00	0.00	0.00	0.0	
21	74.00	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	148.52	123.72	17286	
22	73.50	Total>	9.01	2.50m	162.65	119.66	17882	
		Total>	9.01	2.50m	168.24	168.24	17882	
23	73.20	Total>	14.74	4.00m	176.73	170.58	18193	
24	72.60	Total>	26.30	7.00m	193.81	166.12	18815	
25	72.00	Total>	38.06	10.00m	211.09	161.72	19436	
26	71.20	Total>	54.16	14.00m	234.56	156.42	20266	
27	70.60	Total>	66.62	17.00m	252.54	152.53	20887	
28	70.00	Total>	79.41	20.00m	270.85	148.19	21509	

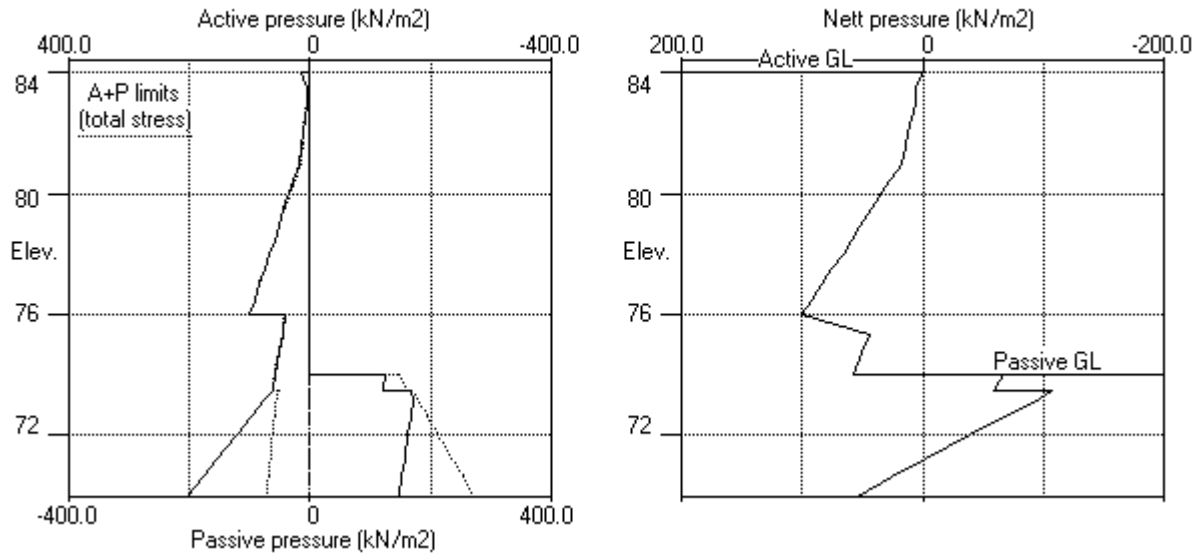
Note: 61.77a Soil pressure at active limit  
 168.24p Soil pressure at passive limit

Units: kN,m

Stage No.13 Excav. to elev. 74.00 on PASSIVE side

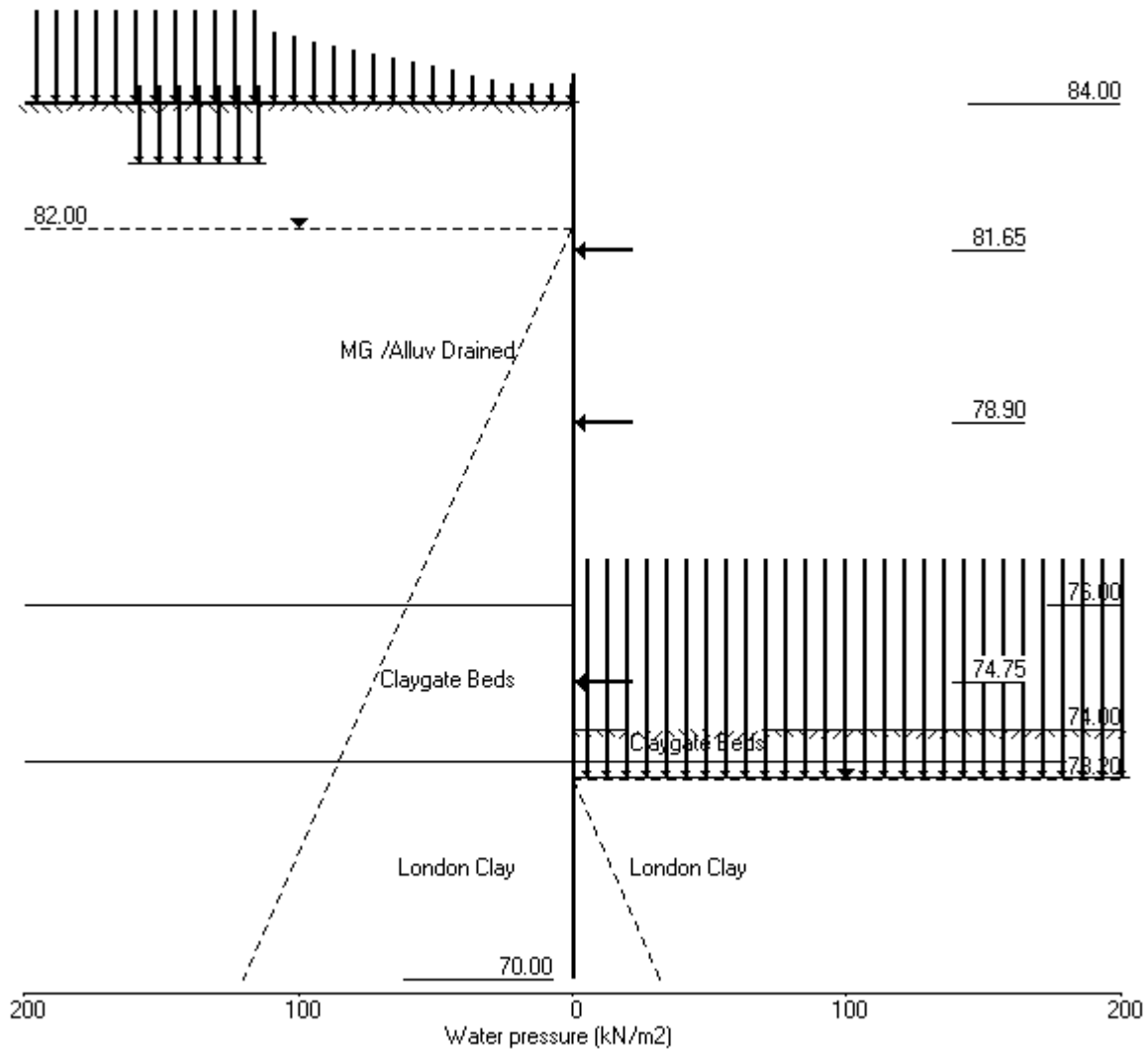


Stage No.13 Excav. to elev. 74.00 on PASSIVE side



Units: kN,m

Stage No.23 Change soil type 1 to soil type 4



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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

		Overall			
		FoS for toe	Toe elev. for		
		elev. = 70.00	FoS = 1.000		
-----					
Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	Factor of Safety	Moment of equil. at elev.	Toe elev. Penetr- ation
23	84.00 74.00		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.000	-2.47E-03	0.0	-0.0	
2	84.00	0.00	0.001	-2.47E-03	0.0	-0.0	
		14.74	0.001	-2.47E-03	0.0	-0.0	
3	83.50	7.63	0.003	-2.47E-03	5.6	2.0	
4	83.00	12.38	0.004	-2.48E-03	10.6	6.1	
5	82.50	17.23	0.005	-2.51E-03	18.0	13.1	
6	82.00	22.08	0.006	-2.55E-03	27.8	24.4	
7	81.65	27.20	0.007	-2.61E-03	36.4	35.6	134.6
		27.20	0.007	-2.61E-03	-98.2	35.6	
8	81.50	29.38	0.008	-2.63E-03	-93.9	21.2	
9	81.00	36.62	0.009	-2.63E-03	-77.4	-21.7	
10	80.25	47.40	0.011	-2.46E-03	-45.9	-68.3	
11	79.50	58.10	0.013	-2.16E-03	-6.4	-88.1	
12	78.90	66.60	0.014	-1.90E-03	31.1	-81.0	203.2
		66.60	0.014	-1.90E-03	-172.2	-81.0	
13	78.45	72.92	0.015	-1.64E-03	-140.8	-151.5	
14	78.00	79.20	0.015	-1.23E-03	-106.5	-207.3	
15	77.50	86.17	0.016	-6.58E-04	-65.2	-250.5	
16	77.00	93.13	0.016	1.78E-06	-20.4	-272.1	
17	76.50	100.09	0.016	6.87E-04	27.9	-270.5	
18	76.00	107.06	0.015	1.33E-03	79.7	-243.9	
		48.62	0.015	1.33E-03	79.7	-243.9	
19	75.38	52.99	0.014	2.01E-03	111.5	-185.3	
20	74.75	58.47	0.013	2.47E-03	146.3	-105.7	69.6
		58.47	0.013	2.47E-03	76.7	-105.7	
21	74.00	72.01	0.011	2.73E-03	125.6	-32.9	
		-53.21	0.011	2.73E-03	125.6	-32.9	
22	73.50	-30.71	0.010	2.74E-03	104.6	24.8	
		-78.66	0.010	2.74E-03	104.6	24.8	
23	73.20	-61.61	0.009	2.68E-03	83.6	53.7	
		-128.87	0.009	2.68E-03	83.6	53.7	





(continued)

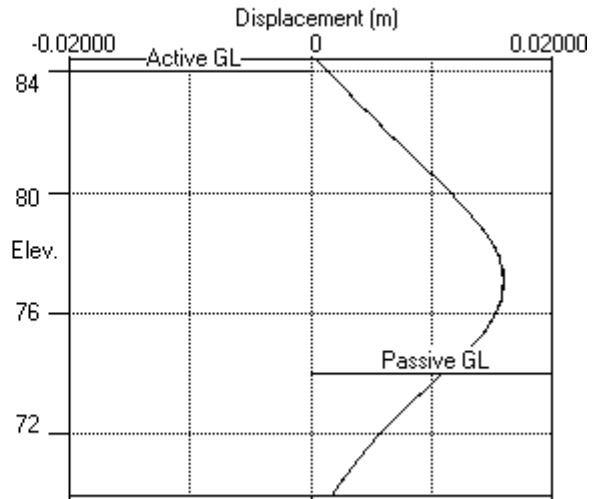
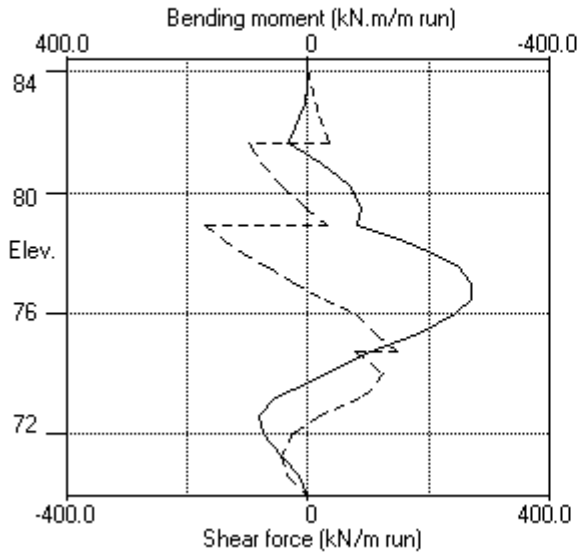
Stage No.23 Change properties of soil type 1 to soil type 4  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
16	77.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
17	76.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
21	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		Total>	0.00	0.00	148.52	125.22	125.22	18696
22	73.50	Total>	9.01	2.50m	162.65	111.66	111.66	19341
		Total>	9.01	2.50m	168.24	160.24	160.24	19341
23	73.20	Total>	14.74	4.00m	176.73	157.62	157.62	19677
		Total>	84.74	4.00m	246.75	224.88	224.88	19677
24	72.60	Total>	96.19	7.00m	263.73	214.16	214.16	20350
25	72.00	Total>	107.31	10.00m	280.37	204.57	204.57	21022
26	71.20	Total>	121.23	14.00m	301.65	191.88	191.88	21919
27	70.60	Total>	131.10	17.00m	317.03	181.84	181.84	22592
28	70.00	Total>	140.73	20.00m	332.19	170.80	170.80	23264

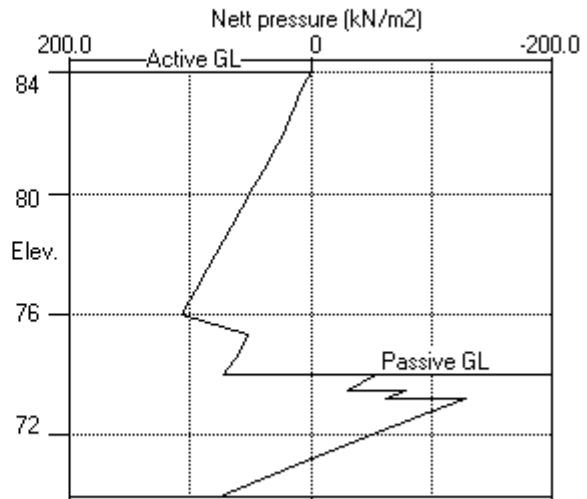
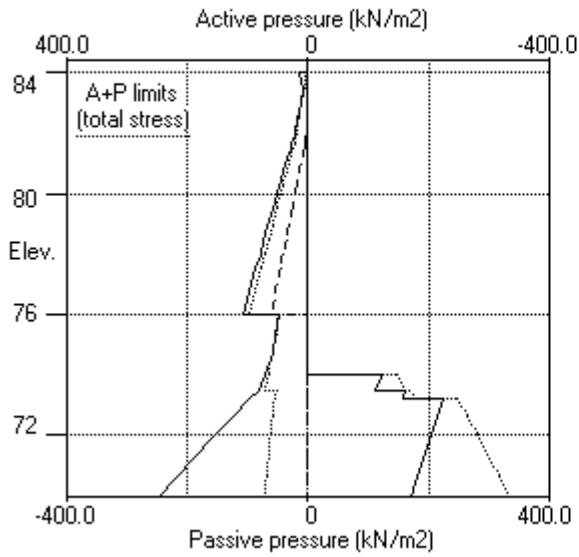
Note: 58.47a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.23 Change soil type 1 to soil type 4

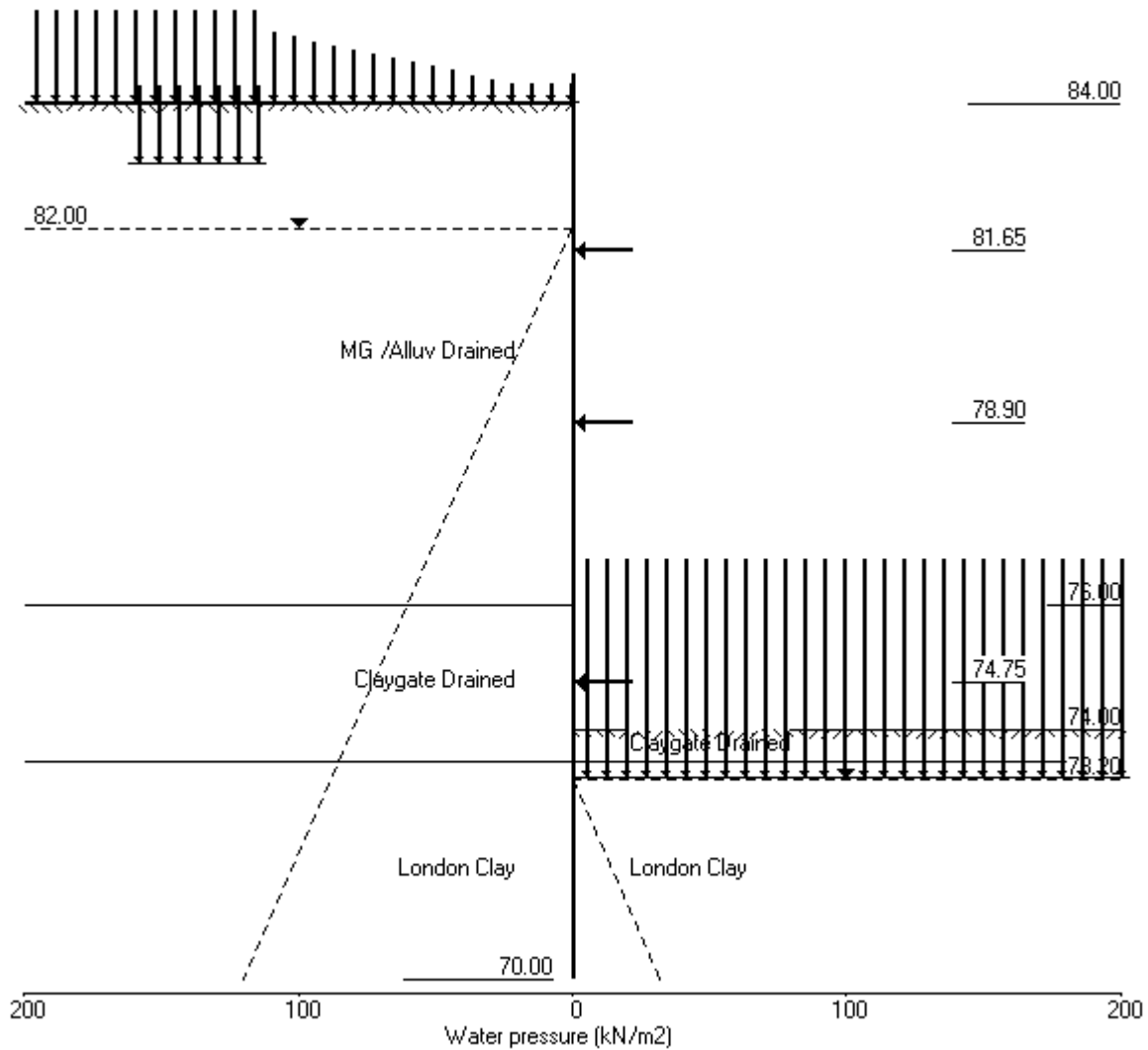


Stage No.23 Change soil type 1 to soil type 4



Units: kN,m

Stage No.24 Change soil type 2 to soil type 5



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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

		Overall			
		FoS for toe	Toe elev. for		
		elev. = 70.00	FoS = 1.000		
-----					
Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	Factor of Safety	Moment of equil. at elev.	Toe elev. Penetr-ation
24	84.00 74.00		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.000	-2.46E-03	0.0	-0.0	
2	84.00	0.00	0.001	-2.46E-03	0.0	-0.0	
		14.68	0.001	-2.46E-03	0.0	-0.0	
3	83.50	7.59	0.003	-2.46E-03	5.6	2.0	
4	83.00	12.35	0.004	-2.47E-03	10.6	6.0	
5	82.50	17.20	0.005	-2.50E-03	17.9	13.0	
6	82.00	22.07	0.006	-2.55E-03	27.8	24.3	
7	81.65	27.20	0.007	-2.60E-03	36.4	35.5	133.3
		27.20	0.007	-2.60E-03	-96.9	35.5	
8	81.50	29.38	0.008	-2.62E-03	-92.7	21.3	
9	81.00	36.63	0.009	-2.62E-03	-76.2	-21.0	
10	80.25	47.42	0.011	-2.45E-03	-44.7	-66.6	
11	79.50	58.12	0.013	-2.17E-03	-5.1	-85.6	
12	78.90	66.60	0.014	-1.92E-03	32.3	-77.7	208.6
		66.60	0.014	-1.92E-03	-176.3	-77.7	
13	78.45	72.90	0.015	-1.66E-03	-144.9	-150.0	
14	78.00	79.16	0.015	-1.25E-03	-110.7	-207.7	
15	77.50	86.11	0.016	-6.76E-04	-69.4	-252.9	
16	77.00	93.05	0.016	-8.00E-06	-24.6	-276.7	
17	76.50	100.01	0.016	6.91E-04	23.7	-277.2	
18	76.00	106.99	0.015	1.36E-03	75.4	-252.7	
		154.05	0.015	1.36E-03	75.4	-252.7	
19	75.38	165.21	0.014	2.03E-03	175.2	-175.8	
20	74.75	176.14	0.013	2.36E-03	281.9	-34.1	378.3
		176.14	0.013	2.36E-03	-96.5	-34.1	
21	74.00	188.39	0.011	2.54E-03	40.2	-58.1	
22	73.50	173.64	0.010	2.63E-03	130.7	-14.4	
		-86.59	0.010	2.63E-03	130.7	-14.4	
23	73.20	-70.52	0.009	2.62E-03	107.2	22.0	
		-137.78	0.009	2.62E-03	107.2	22.0	



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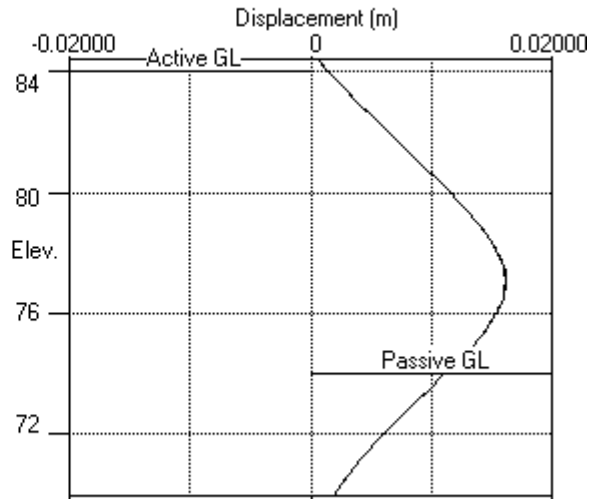
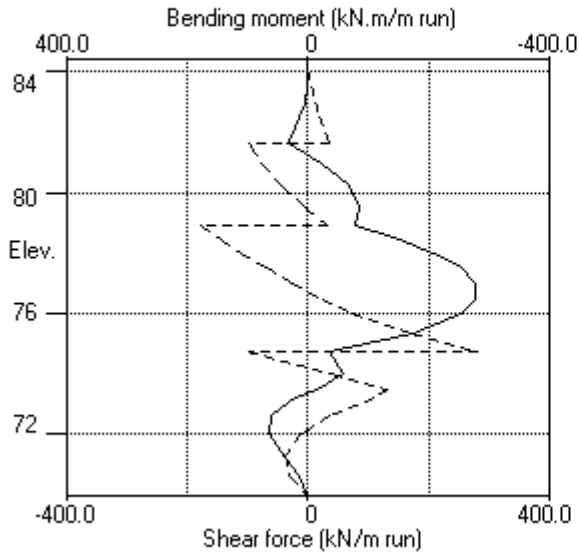
Stage No.24 Change properties of soil type 2 to soil type 5  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
16	77.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
17	76.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
21	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	0.00	0.00	0.00	0.00	0.00	7192
22	73.50	0.00	9.01	3.83	22.95	22.95	22.95p	7440
		Total>	9.01	2.50m	168.24	164.25	164.25	16527
23	73.20	Total>	14.74	4.00m	176.73	162.12	162.12	16815
		Total>	84.74	4.00m	246.75	229.38	229.38	16815
24	72.60	Total>	96.19	7.00m	263.73	218.99	218.99	17389
25	72.00	Total>	107.31	10.00m	280.37	209.09	209.09	17964
26	71.20	Total>	121.23	14.00m	301.65	195.43	195.43	18730
27	70.60	Total>	131.10	17.00m	317.03	184.42	184.42	19305
28	70.00	Total>	140.73	20.00m	332.19	172.33	172.33	19880

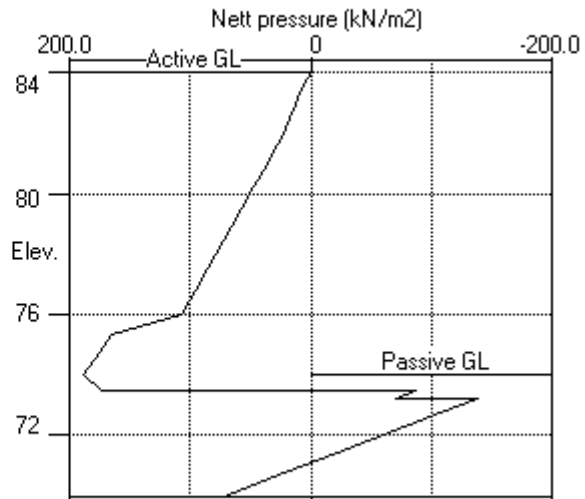
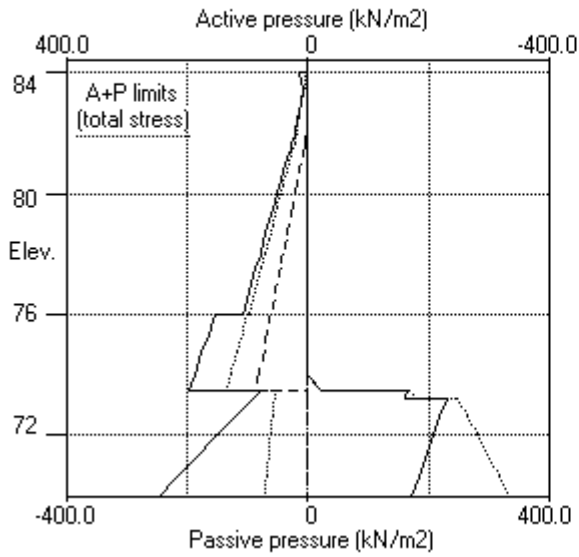
Note: 12.34a Soil pressure at active limit  
 22.95p Soil pressure at passive limit

Units: kN,m

Stage No.24 Change soil type 2 to soil type 5

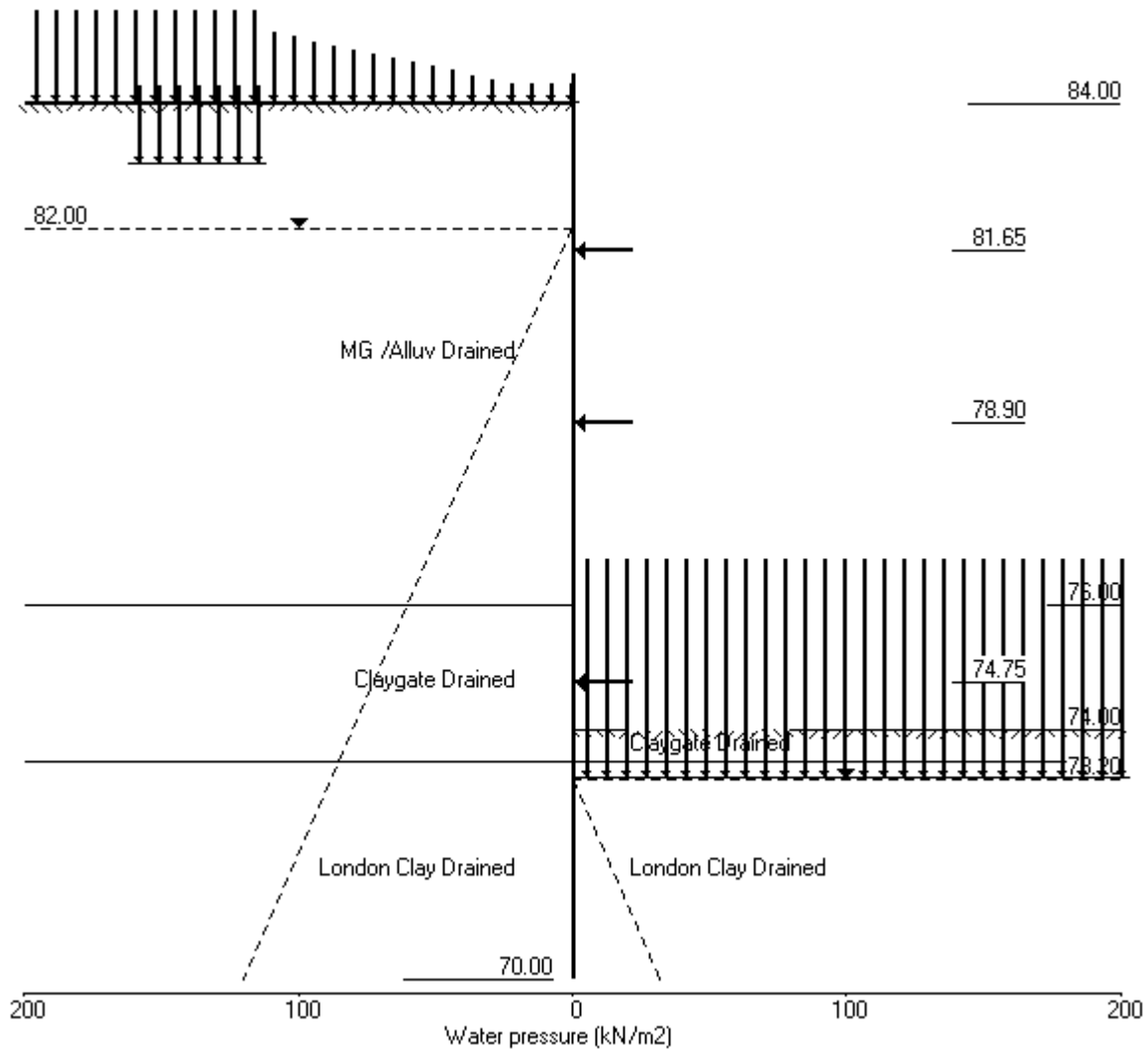


Stage No.24 Change soil type 2 to soil type 5



Units: kN,m

Stage No.25 Change soil type 3 to soil type 6





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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns East Wall Final\_ULS2  
 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

Stage No. 25 Change properties of soil type 3 to soil type 6  
 Ko pressures will be reset

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

		Overall			
		FoS for toe	Toe elev. for		
		elev. = 70.00	FoS = 1.000		
-----					
Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	Factor of Safety	Moment of equilib. at elev.	Toe elev. Penetr-ation
25	84.00 74.00		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	84.40	0.00	0.000	-2.53E-03	0.0	-0.0	
2	84.00	0.00	0.001	-2.53E-03	0.0	-0.0	
		15.32	0.001	-2.53E-03	0.0	-0.0	
3	83.50	8.09	0.003	-2.53E-03	5.9	2.1	
4	83.00	12.72	0.004	-2.54E-03	11.1	6.3	
5	82.50	17.44	0.005	-2.57E-03	18.6	13.6	
6	82.00	22.16	0.006	-2.62E-03	28.5	25.3	
7	81.65	27.19	0.007	-2.67E-03	37.1	36.7	147.6
		27.19	0.007	-2.67E-03	-110.4	36.7	
8	81.50	29.35	0.008	-2.70E-03	-106.2	20.5	
9	81.00	36.49	0.009	-2.69E-03	-89.7	-28.6	
10	80.25	47.18	0.011	-2.47E-03	-58.4	-84.4	
11	79.50	57.93	0.013	-2.10E-03	-19.0	-113.7	
12	78.90	66.62	0.014	-1.75E-03	18.4	-114.2	156.8
		66.62	0.014	-1.75E-03	-138.4	-114.2	
13	78.45	73.14	0.015	-1.43E-03	-107.0	-169.5	
14	78.00	79.67	0.015	-1.00E-03	-72.6	-210.0	
15	77.50	86.92	0.016	-4.38E-04	-30.9	-236.1	
16	77.00	94.12	0.016	1.63E-04	14.3	-240.6	
17	76.50	101.22	0.015	7.47E-04	63.2	-221.5	
18	76.00	108.17	0.015	1.25E-03	115.5	-177.1	
		157.49	0.015	1.25E-03	115.5	-177.1	
19	75.38	167.70	0.014	1.64E-03	217.1	-74.5	
20	74.75	176.03	0.013	1.61E-03	324.6	93.9	538.2
		176.03	0.013	1.61E-03	-213.6	93.9	
21	74.00	182.83	0.012	1.47E-03	-79.1	-18.0	
22	73.50	163.50	0.011	1.54E-03	7.5	-34.7	
		164.27	0.011	1.54E-03	7.5	-34.7	
23	73.20	151.83	0.011	1.58E-03	54.9	-24.4	
		-34.22	0.011	1.58E-03	54.9	-24.4	



(continued)

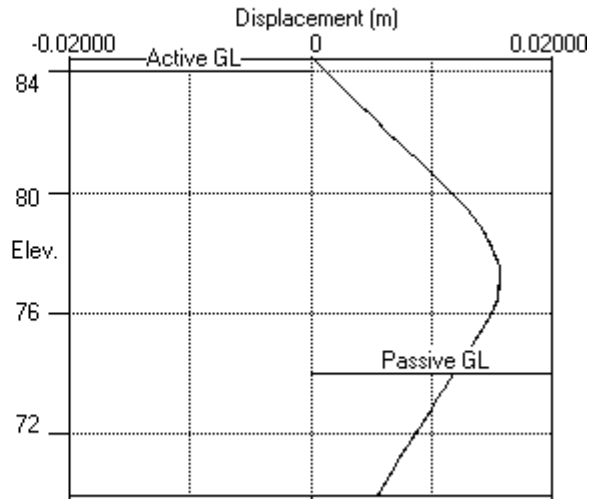
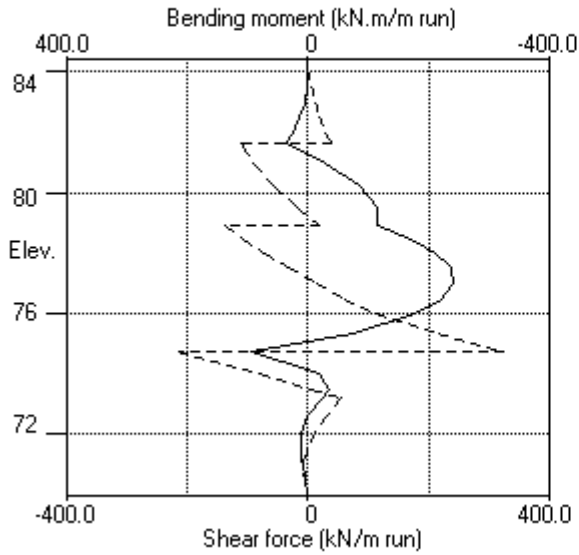
Stage No.25 Change properties of soil type 3 to soil type 6  
 Ko pressures will be reset

Node no.	Y coord	----- PASSIVE side -----					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertical kN/m2	Effective stresses Active limit kN/m2	Effective stresses Passive limit kN/m2	Earth pressure kN/m2		
5	82.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	82.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	81.65	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	81.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	81.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	80.25	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	79.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
12	78.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0
13	78.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0
14	78.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
15	77.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
16	77.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
17	76.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0
18	76.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
19	75.38	0.00	0.00	0.00	0.00	0.00	0.00	0.0
20	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.0
21	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		0.00	0.00	0.00	0.00	0.00	0.00	7739
22	73.50	0.00	9.01	3.83	22.95	22.95	22.95p	8006
		0.00	9.01	3.83	23.94	23.94	23.94p	8006
23	73.20	0.00	14.74	6.26	39.17	39.17	39.17p	8145
		0.00	84.74	36.02	225.22	225.22	225.22p	8145
24	72.60	6.00	90.19	38.34	239.72	231.24	237.24	8423
25	72.00	12.00	95.31	40.52	253.33	220.10	232.10	8702
26	71.20	20.00	101.23	43.04	269.07	203.91	223.91	9073
27	70.60	26.00	105.10	44.68	279.33	190.67	216.67	9351
28	70.00	32.00	108.73	46.22	288.99	176.34	208.34	9630

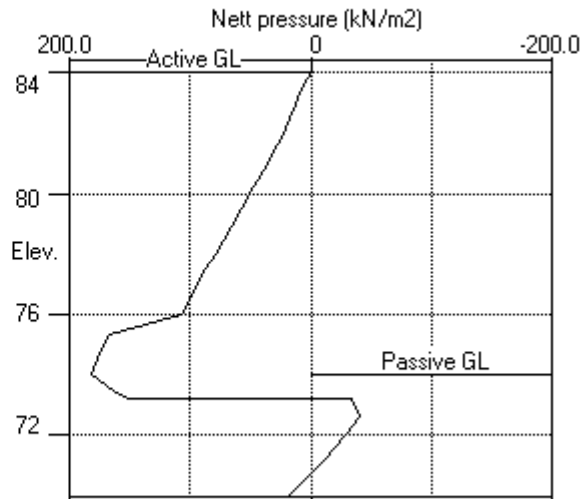
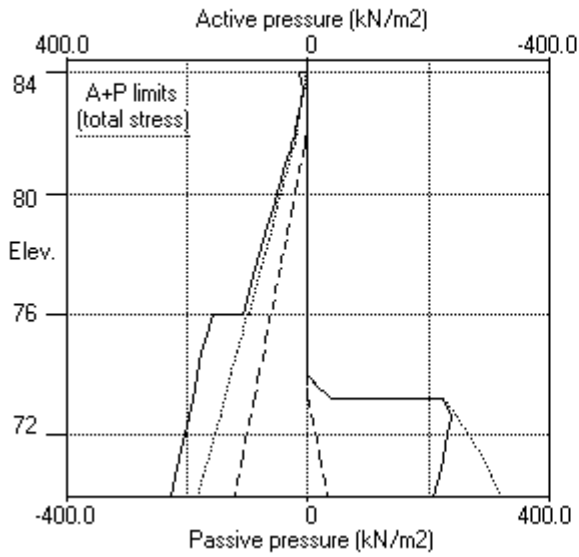
Note: 12.34a Soil pressure at active limit  
 225.22p Soil pressure at passive limit

Units: kN,m

Stage No.25 Change soil type 3 to soil type 6



Stage No.25 Change soil type 3 to soil type 6



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 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: ULS DA1 Combination 2  
 Water pressures : Worst Credible  
 Partial factor on C' = 1.250  
 Partial factor on Phi' = 1.250  
 Partial factor on Cu = 1.400  
 Partial factor on Soil Modulus = 1.000  
 Partial factor on Permanent Unfavourable loads = 1.000  
 Partial factor on Permanent Favourable loads = 1.000  
 Partial factor on Permanent Variable loads = 1.300

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

Stage No.	G.L.		Strut Elev.	Overall		Toe elev. for	
	Act.	Pass.		Factor	Moment	Toe elev.	Wall Penetr
				elev. = 70.00		FoS = 1.000	
				Safety at elev.		-ation	
1	84.00	84.00	Cant.	Conditions not suitable for FoS calc.			
2	84.00	84.00		No analysis at this stage			
3	84.00	84.00		No analysis at this stage			
4	84.00	84.00		No analysis at this stage			
5	84.00	84.00	Cant.	Conditions not suitable for FoS calc.			
6	84.00	84.00		No analysis at this stage			
7	84.00	81.50	84.40	5.125	n/a	81.22	0.28
8	84.00	81.50		No analysis at this stage			
All remaining stages have more than one strut - FoS calculation n/a							

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 59 Maresfield Gardens | Date: 6-12-2012  
 East Wall | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	84.40	0.002	-0.000	0.0	-0.0	0.0	-28.4
2	84.00	0.002	0.000	0.0	-11.4	0.0	-28.4
3	83.50	0.003	0.000	2.3	-25.5	6.5	-27.8
4	83.00	0.004	0.000	6.7	-38.9	11.1	-25.9
5	82.50	0.006	0.000	13.6	-51.2	18.6	-22.8
6	82.00	0.007	0.000	25.3	-61.5	28.5	-110.8
7	81.65	0.008	0.000	36.7	-67.3	37.1	-110.4
8	81.50	0.008	0.000	21.3	-69.4	0.0	-106.2
9	81.00	0.010	0.000	0.0	-88.3	0.0	-98.3
10	80.25	0.011	0.000	0.0	-156.5	0.0	-82.3
11	79.50	0.013	0.000	0.0	-209.1	12.9	-165.8
12	78.90	0.014	0.000	0.0	-235.1	32.3	-176.3
13	78.45	0.015	0.000	0.0	-242.7	36.8	-144.9
14	78.00	0.015	0.000	0.0	-238.4	65.0	-140.0
15	77.50	0.016	0.000	0.0	-265.0	59.5	-104.6
16	77.00	0.016	0.000	0.5	-280.0	84.4	-64.8
17	76.50	0.016	0.000	1.5	-277.2	112.7	-20.7
18	76.00	0.015	0.000	2.8	-252.7	144.2	0.0
19	75.38	0.014	0.000	23.9	-191.9	217.1	0.0
20	74.75	0.013	0.000	93.9	-147.8	324.6	-213.6
21	74.00	0.012	0.000	82.6	-65.7	136.7	-79.1
22	73.50	0.011	0.000	87.6	-34.7	130.7	-8.0
23	73.20	0.011	0.000	84.7	-24.4	107.2	-14.3
24	72.60	0.010	0.000	84.2	0.0	36.3	-28.5
25	72.00	0.009	0.000	78.4	0.0	11.7	-34.0
26	71.20	0.007	0.000	41.8	0.0	0.0	-46.2
27	70.60	0.006	0.000	14.0	0.0	0.0	-35.0
28	70.00	0.006	0.000	0.0	-0.0	0.0	-0.0

**Summary of results (continued)**

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev.	minimum kN.m/m	elev.	maximum kN/m	elev.	minimum kN/m	elev.
1	4.5	74.75	-1.5	79.50	3.0	76.00	-1.4	72.60
2	No calculation at this stage							
3	No calculation at this stage							
4	No calculation at this stage							
5	7.2	74.00	-10.4	78.90	9.1	76.00	-3.0	81.50
6	No calculation at this stage							
7	46.6	74.00	-96.3	78.90	67.4	76.00	-28.4	84.40
8	No calculation at this stage							
9	45.8	74.00	-96.0	78.90	66.8	76.00	-28.2	84.40
10	87.6	73.50	-242.7	78.45	144.2	76.00	-110.8	82.00
11	No calculation at this stage							
12	86.8	73.50	-241.8	78.45	143.6	76.00	-110.6	82.00
13	54.9	72.60	-204.7	76.50	128.4	74.00	-135.3	78.00
14	No calculation at this stage							
15	67.4	72.00	-218.3	76.50	136.7	74.00	-140.0	78.00
16	No calculation at this stage							
17	84.2	72.60	-280.0	77.00	138.6	74.75	-165.8	79.50
18	No calculation at this stage							
19	81.8	72.60	-263.9	76.50	135.2	74.00	-151.9	78.90
20	No calculation at this stage							
21	82.1	72.60	-265.4	77.00	134.7	74.00	-150.2	78.90
22	82.1	72.60	-265.4	77.00	134.7	74.00	-150.2	78.90
23	80.6	72.60	-272.1	77.00	146.3	74.75	-172.2	78.90
24	65.5	72.00	-277.2	76.50	281.9	74.75	-176.3	78.90
25	93.9	74.75	-240.6	77.00	324.6	74.75	-213.6	74.75

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum m	elev.	minimum m	elev.	
1	0.001	84.40	0.000	84.40	Apply surcharge no.1 at elev. 84.00
2	No calculation at this stage				Apply surcharge no.2 at elev. 84.00
3	No calculation at this stage				Apply surcharge no.3 at elev. 84.00
4	No calculation at this stage				Apply surcharge no.6 at elev. 84.00
5	0.001	80.25	0.000	84.40	Apply surcharge no.7 at elev. 83.00
6	No calculation at this stage				Install strut no.1 at elev. 84.40
7	0.007	78.90	0.000	84.40	Excav. to elev. 81.50 on PASSIVE side
8	No calculation at this stage				Install strut no.2 at elev. 82.00
9	0.007	78.90	0.000	84.40	Apply water pressure profile no.2
10	0.014	78.45	0.000	84.40	Excav. to elev. 77.50 on PASSIVE side
11	No calculation at this stage				Install strut no.3 at elev. 78.00
12	0.014	78.45	0.000	84.40	Apply water pressure profile no.4
13	0.015	77.00	0.000	84.40	Excav. to elev. 74.00 on PASSIVE side
14	No calculation at this stage				Install strut no.4 at elev. 74.75
15	0.015	77.00	0.000	84.40	Apply surcharge no.4 at elev. 73.20
16	No calculation at this stage				Install strut no.5 at elev. 79.50
17	0.016	77.00	-0.000	84.40	Remove strut no.3 at elev. 78.00
18	No calculation at this stage				Install strut no.6 at elev. 78.90
19	0.016	77.00	-0.000	84.40	Remove strut no.5 at elev. 79.50
20	No calculation at this stage				Install strut no.7 at elev. 81.65
21	0.016	77.00	0.000	84.40	Remove strut no.2 at elev. 82.00
22	0.016	77.00	0.000	84.40	Remove strut no.1 at elev. 84.40
23	0.016	77.00	0.000	84.40	Change soil type 1 to soil type 4
24	0.016	77.00	0.000	84.40	Change soil type 2 to soil type 5
25	0.016	77.00	0.000	84.40	Change soil type 3 to soil type 6

-----  
**Summary of results (continued)**

**Strut forces at each stage (horizontal components)**

Stage no.	--- Strut no. 1 --- at elev. 84.40		--- Strut no. 2 --- at elev. 82.00		--- Strut no. 3 --- at elev. 78.00	
	kN/m run	kN/strut	kN/m run	kN/strut	kN/m run	kN/strut
7	28.42	170.54	---	---	---	---
9	28.23	169.39	0.21	1.29	---	---
10	slack	slack	126.11	756.67	---	---
12	slack	slack	125.90	755.39	0.84	5.04
13	slack	slack	95.55	573.32	200.35	1202.11
15	slack	slack	96.95	581.69	203.11	1218.64
17	slack	slack	71.46	428.79	---	---
19	slack	slack	88.47	530.84	---	---
21	slack	slack	---	---	---	---



---

Stage no.	--- Strut no. 4 --- at elev. 74.75		--- Strut no. 5 --- at elev. 79.50		--- Strut no. 6 --- at elev. 78.90	
	kN/m run	kN/strut	kN/m run	kN/strut	kN/m run	kN/strut
15	slack	slack	---	---	---	---
17	51.11	51.11	178.71	1072.26	---	---
19	35.40	35.40	---	---	170.93	170.93
21	37.31	37.31	---	---	158.02	158.02
22	37.31	37.31	---	---	158.02	158.02
23	69.63	69.63	---	---	203.21	203.21
24	378.35	378.35	---	---	208.62	208.62
25	538.20	538.20	---	---	156.81	156.81

Run ID. 59 Maresfield Gdns East Wall Final\_ULS2  
59 Maresfield Gardens  
East Wall

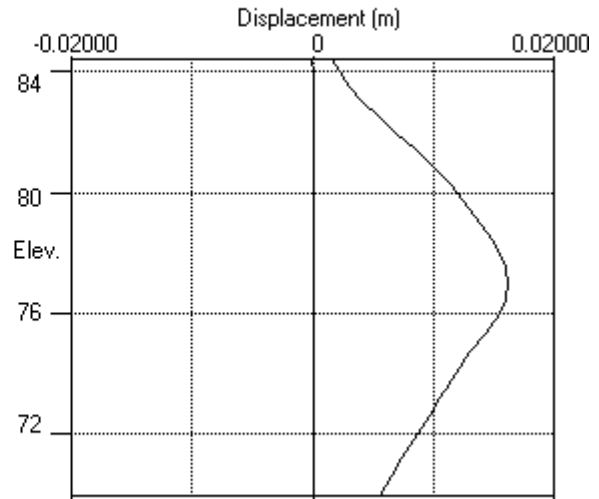
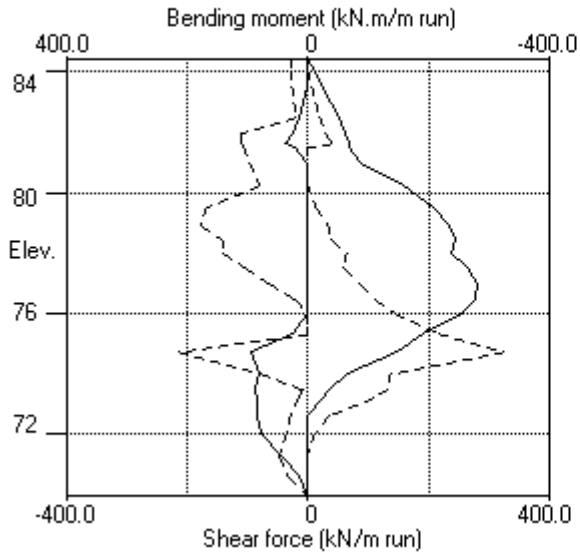
| Sheet No.  
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| Checked :

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Stage	--- Strut no. 7 ---	
no.	at elev. 81.65	
	kN/m run	kN/strut
21	97.12	97.12
22	97.12	97.12
23	134.62	134.62
24	133.31	133.31
25	147.57	147.57

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: 59 Maresfield Gdns South Wall\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 West Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	82.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	( Nu ) ( NC/OC )	( Kac ) ( Ka )	( Kpc ) ( Kp )	( dc/dy ) ( kN/m2 )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000 )	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.000)	75.00u ( 6.000 )
3 London Clay ( 73.50 )	19.00	45000 ( 2608 )	1.000	OC (0.490)	1.000 (1.000)	1.000 (1.000)	90.00u ( 5.200 )
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800 )	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565 )	1.000	OC (0.200)	0.337 (1.360)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.000	0.00
3 London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.670	0.00
6 London Clay Drained	26.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile no.	Active side				Passive side			
	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	76.00	76.00	0.0 MC
4	1	82.00	82.00	0.0	1	75.00	75.00	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m<sup>2</sup>  
 Moment of inertia of wall I = 7.0700E-03 m<sup>4</sup>/m run  
 E.I = 197960 kN.m<sup>2</sup>/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1		Not defined						
2	82.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
4	76.25	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5		Not defined						
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	2.000E+08	1.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	81.50	1.30(A)	0.50	20.00	100.00	=	N/A	1.00 P/U
2	81.50	0.80(A)	20.00	0.50	80.00	=	N/A	1.00 P/U
3	82.00	0.00(A)	20.00	20.00	5.00	=	N/A	1.00 P/U
4	76.00	-0.00(P)	8.00	10.00	50.00	=	N/A	1.00 -

Note: A = Active side, P = Passive side  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 81.50 No analysis at this stage
2	Apply surcharge no.2 at elevation 81.50 No analysis at this stage
3	Apply surcharge no.3 at elevation 82.00 No analysis at this stage
4	Excavate to elevation 81.50 on PASSIVE side
5	Install strut or anchor no.2 at elevation 82.00
6	Apply water pressure profile no.1 ( Mod. Conserv. )
7	Excavate to elevation 77.50 on PASSIVE side
8	Install strut or anchor no.3 at elevation 78.00
9	Apply water pressure profile no.3 ( Mod. Conserv. )
10	Excavate to elevation 76.00 on PASSIVE side
11	Apply surcharge no.4 at elevation 76.00
12	Install strut or anchor no.4 at elevation 76.25
13	Install strut or anchor no.6 at elevation 78.90
14	Remove strut or anchor no.3 at elevation 78.00
15	Install strut or anchor no.7 at elevation 81.65
16	Remove strut or anchor no.2 at elevation 82.00
17	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
18	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
19	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

## FACTORS OF SAFETY and ANALYSIS OPTIONS

Limit State options: Serviceability Limit State  
All loads and soil strengths are unfactored

Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:

Length of wall (normal to plane of analysis) = 6.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

## OUTPUT OPTIONS

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 81.50	No	No	No
2	Apply surcharge no.2 at elev. 81.50	No	No	No
3	Apply surcharge no.3 at elev. 82.00	No	No	No
4	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
5	Install strut no.2 at elev. 82.00	No	No	No
6	Apply water pressure profile no.1	No	No	No
7	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
8	Install strut no.3 at elev. 78.00	No	No	No
9	Apply water pressure profile no.3	No	No	No
10	Excav. to elev. 76.00 on PASSIVE side	No	No	No
11	Apply surcharge no.4 at elev. 76.00	No	No	No
12	Install strut no.4 at elev. 76.25	No	No	No
13	Install strut no.6 at elev. 78.90	No	No	No
14	Remove strut no.3 at elev. 78.00	No	No	No
15	Install strut no.7 at elev. 81.65	No	No	No
16	Remove strut no.2 at elev. 82.00	No	No	No
17	Change soil type 1 to soil type 4	No	No	No
18	Change soil type 2 to soil type 5	No	No	No
19	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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 Data filename/Run ID: 59 Maresfield Gdns South Wall\_SLS |  
 59 Maresfield Gardens | Date: 6-12-2012  
 West Wall | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		---- Bending moment ----				----- Shear force -----			
		max.	min.	Calculated		Factored		Calculated		Factored	
				max.	min.	max.	min.	max.	min.	max.	min.
		m	m	kN.m/m		kN.m/m		kN/m		kN/m	
1	82.00	0.005	0.000	0	0	0	0	0	-57	0	-77
2	81.65	0.006	0.000	0	-20	0	-27	2	-84	2	-113
3	81.50	0.006	0.000	0	-29	0	-38	1	-83	1	-112
4	81.00	0.007	0.000	0	-56	0	-76	0	-78	0	-105
5	80.40	0.007	0.000	0	-94	0	-127	0	-65	0	-88
6	79.80	0.008	0.000	0	-128	0	-172	0	-48	0	-65
7	79.35	0.008	0.000	0	-144	0	-195	0	-38	0	-51
8	78.90	0.009	0.000	0	-152	0	-205	1	-50	2	-68
9	78.45	0.009	0.000	0	-152	0	-205	22	-26	30	-35
10	78.00	0.009	0.000	0	-156	0	-210	49	-18	66	-25
11	77.50	0.009	0.000	0	-148	0	-199	82	0	111	0
12	77.19	0.009	0.000	0	-134	0	-181	104	0	140	0
13	76.88	0.009	0.000	0	-114	0	-154	127	0	172	0
14	76.56	0.008	0.000	19	-94	26	-127	152	0	205	0
15	76.25	0.008	0.000	71	-76	96	-102	178	-69	240	-94
16	76.00	0.008	0.000	56	-56	76	-76	112	-48	151	-65
17	75.50	0.007	0.000	36	-16	49	-22	81	-39	109	-52
18	75.00	0.007	0.000	45	-3	61	-4	52	-28	70	-38
19	74.40	0.006	0.000	65	-7	87	-9	24	-15	33	-20
20	73.95	0.006	0.000	70	-2	94	-3	20	-4	27	-5
21	73.50	0.006	0.000	68	0	91	0	39	-11	53	-14
22	73.05	0.005	0.000	61	0	82	0	19	-19	26	-25
23	72.60	0.005	0.000	51	0	69	0	4	-24	5	-33
24	72.00	0.005	0.000	35	0	47	0	0	-26	0	-35
25	71.40	0.005	0.000	19	0	26	0	0	-23	0	-31
26	70.80	0.004	0.000	7	0	10	0	0	-16	0	-22
27	70.40	0.004	0.000	2	0	3	0	0	-9	0	-12
28	70.00	0.004	0.000	0	-0	0	-0	0	-0	0	-0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment						Shear force					
	Calculated			Factored			Calculated			Factored		
	max.	elev.	min.	max.	min.	max.	elev.	min.	elev.	max.	min.	
	kN.m/m		kN.m/m			kN/m			kN/m			
1	2	73.95	-6	78.45	3	-8	4	76.00	-3	80.40	5	-4
2	No calculation at this stage											
3	No calculation at this stage											
4	24	74.40	-15	78.45	32	-21	22	76.00	-9	80.40	29	-12
5	No calculation at this stage											
6	23	74.40	-15	78.45	31	-21	21	76.00	-9	80.40	28	-12
7	52	73.95	-139	78.45	70	-188	88	76.00	-56	82.00	119	-75
8	No calculation at this stage											
9	52	73.95	-139	78.45	70	-187	88	76.00	-56	82.00	119	-75
10	42	73.50	-120	78.45	57	-162	86	76.00	-50	82.00	116	-68
11	69	73.95	-146	78.45	94	-197	112	76.00	-57	82.00	151	-77
12	No calculation at this stage											
13	No calculation at this stage											
14	70	73.95	-149	78.00	94	-201	111	76.00	-57	82.00	150	-77
15	No calculation at this stage											
16	70	73.95	-150	78.00	94	-203	111	76.00	-65	81.65	150	-87
17	68	73.95	-156	78.00	92	-210	128	76.25	-77	81.65	173	-103
18	35	76.25	-152	78.90	47	-205	167	76.25	-84	81.65	226	-113
19	71	76.25	-142	78.90	96	-192	178	76.25	-80	81.65	240	-108

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum	elev.	minimum	elev.	
	m		m		
1	0.000	78.90	0.000	82.00	Apply surcharge no.1 at elev. 81.50
2	No calculation at this stage				Apply surcharge no.2 at elev. 81.50
3	No calculation at this stage				Apply surcharge no.3 at elev. 82.00
4	0.004	82.00	0.000	82.00	Excav. to elev. 81.50 on PASSIVE side
5	No calculation at this stage				Install strut no.2 at elev. 82.00
6	0.004	82.00	0.000	82.00	Apply water pressure profile no.1
7	0.009	78.45	0.000	82.00	Excav. to elev. 77.50 on PASSIVE side
8	No calculation at this stage				Install strut no.3 at elev. 78.00
9	0.009	78.45	0.000	82.00	Apply water pressure profile no.3
10	0.009	78.00	0.000	82.00	Excav. to elev. 76.00 on PASSIVE side
11	0.009	78.45	0.000	82.00	Apply surcharge no.4 at elev. 76.00
12	No calculation at this stage				Install strut no.4 at elev. 76.25
13	No calculation at this stage				Install strut no.6 at elev. 78.90
14	0.009	78.45	0.000	82.00	Remove strut no.3 at elev. 78.00
15	No calculation at this stage				Install strut no.7 at elev. 81.65
16	0.009	78.45	0.000	82.00	Remove strut no.2 at elev. 82.00
17	0.009	78.45	0.000	82.00	Change soil type 1 to soil type 4
18	0.009	78.45	0.000	82.00	Change soil type 2 to soil type 5
19	0.008	78.45	0.000	82.00	Change soil type 3 to soil type 6

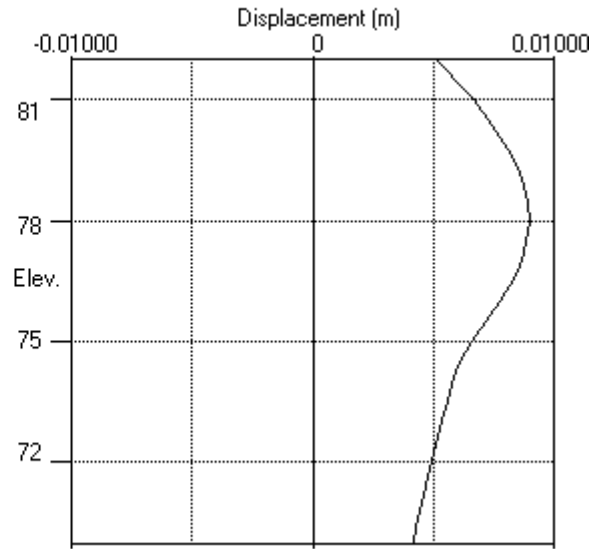
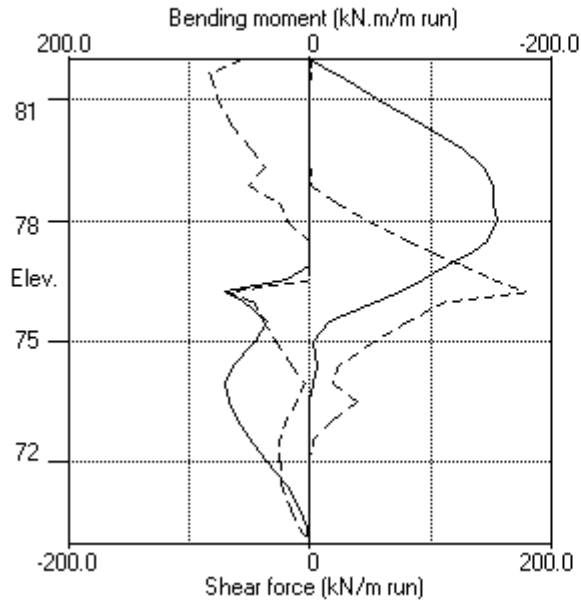


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59 Maresfield Gardens  
West Wall

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| Date: 6-12-2012  
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Units: kN,m

Bending moment, shear force, displacement envelopes



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 59 Maresfield Gardens | Date:12-12-2012  
 South Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	82.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES (Unfactored SLS soil strengths)**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.000)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (1.000)	1.000 (1.000)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.337 (1.360)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction	Wall adhesion	Back-fill	Soil friction	Wall adhesion	Back-fill
No. Description	angle	coeff.	angle	angle	coeff.	angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.000	0.00
3 London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.670	0.00
6 London Clay Drained	26.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile		Active side			Passive side			
Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	76.00	76.00	0.0 MC
4	1	82.00	82.00	0.0	1	75.00	75.00	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m<sup>2</sup>  
 Moment of inertia of wall I = 7.0700E-03 m<sup>4</sup>/m run  
 E.I = 197960 kN.m<sup>2</sup>/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1		Not defined						
2	82.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
4	76.25	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5		Not defined						
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	2.000E+08	1.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	81.50	1.30(A)	0.50	20.00	100.00	=	N/A	1.00 P/U
2	81.50	0.80(A)	20.00	0.50	80.00	=	N/A	1.00 P/U
3	82.00	0.00(A)	20.00	20.00	5.00	=	N/A	1.00 P/U
4	75.44	-0.00(P)	8.00	10.00	50.00	=	N/A	1.00 -

Note: A = Active side, P = Passive side

Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 81.50 No analysis at this stage
2	Apply surcharge no.2 at elevation 81.50 No analysis at this stage
3	Apply surcharge no.3 at elevation 82.00 No analysis at this stage
4	Excavate to elevation 81.50 on PASSIVE side
5	Install strut or anchor no.2 at elevation 82.00
6	Apply water pressure profile no.1 ( Mod. Conserv. )
7	Excavate to elevation 77.50 on PASSIVE side
8	Install strut or anchor no.3 at elevation 78.00
9	Apply water pressure profile no.3 ( Mod. Conserv. )
10	Excavate to elevation 75.44 on PASSIVE side
11	Apply surcharge no.4 at elevation 75.44
12	Install strut or anchor no.4 at elevation 76.25
13	Install strut or anchor no.6 at elevation 78.90
14	Remove strut or anchor no.3 at elevation 78.00
15	Install strut or anchor no.7 at elevation 81.65
16	Remove strut or anchor no.2 at elevation 82.00
17	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
18	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
19	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: ULS DA1 Combination 1  
Water pressures : Moderately Conservative  
Partial factor on C' = 1.000  
Partial factor on Phi' = 1.000  
Partial factor on Cu = 1.000  
Partial factor on Soil Modulus = 1.000  
Partial factor on Permanent Unfavourable loads = 1.000  
Partial factor on Permanent Favourable loads = 1.000  
Partial factor on Permanent Variable loads = 1.100  
Design factor on calculated Bending Moments = 1.350

Parameters for undrained strata:  
Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:  
Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:  
Length of wall (normal to plane of analysis) = 6.00 m  
  
Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m  
  
Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 81.50	No	No	No
2	Apply surcharge no.2 at elev. 81.50	No	No	No
3	Apply surcharge no.3 at elev. 82.00	No	No	No
4	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
5	Install strut no.2 at elev. 82.00	No	No	No
6	Apply water pressure profile no.1	No	No	No
7	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
8	Install strut no.3 at elev. 78.00	No	No	No
9	Apply water pressure profile no.3	No	No	No
10	Excav. to elev. 75.44 on PASSIVE side	No	No	No
11	Apply surcharge no.4 at elev. 75.44	No	No	No
12	Install strut no.4 at elev. 76.25	No	No	No
13	Install strut no.6 at elev. 78.90	No	No	No
14	Remove strut no.3 at elev. 78.00	No	No	No
15	Install strut no.7 at elev. 81.65	No	No	No
16	Remove strut no.2 at elev. 82.00	No	No	No
17	Change soil type 1 to soil type 4	No	No	No
18	Change soil type 2 to soil type 5	No	No	No
19	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment				Shear force			
		max.	min.	Calculated max.	Calculated min.	Factored max.	Factored min.	Calculated max.	Calculated min.	Factored max.	Factored min.
		m	m	kN.m/m		kN.m/m		kN/m		kN/m	
1	82.00	0.005	0.000	0	0	0	0	0	-56	0	-75
2	81.65	0.006	0.000	0	-19	0	-26	2	-81	2	-110
3	81.50	0.006	0.000	0	-28	0	-37	1	-80	1	-108
4	81.00	0.007	0.000	0	-55	0	-74	0	-75	0	-101
5	80.40	0.007	0.000	0	-91	0	-123	0	-63	0	-85
6	79.80	0.008	0.000	0	-123	0	-166	0	-43	0	-59
7	79.35	0.009	0.000	0	-139	0	-187	0	-32	0	-44
8	78.90	0.009	0.000	0	-145	0	-196	8	-67	11	-91
9	78.45	0.009	0.000	0	-141	0	-191	21	-43	28	-59
10	78.00	0.009	0.000	0	-153	0	-206	47	-36	64	-48
11	77.50	0.009	0.000	0	-153	0	-207	80	-15	108	-21
12	77.19	0.009	0.000	0	-145	0	-196	102	-1	138	-1
13	76.88	0.009	0.000	0	-130	0	-175	125	0	169	0
14	76.56	0.009	0.000	12	-114	16	-154	150	0	203	0
15	76.25	0.009	0.000	63	-97	85	-130	176	-112	237	-152
16	76.00	0.008	0.000	37	-82	51	-111	88	-91	119	-123
17	75.44	0.008	0.000	19	-39	25	-53	105	-21	141	-29
18	74.92	0.007	0.000	36	-30	49	-40	71	-13	97	-18
19	74.40	0.007	0.000	52	-24	70	-32	41	-4	55	-5
20	73.95	0.006	0.000	64	-12	87	-16	34	-4	45	-5
21	73.50	0.006	0.000	67	-1	91	-2	51	-7	69	-10
22	73.05	0.006	0.000	63	0	85	0	27	-14	36	-19
23	72.60	0.006	0.000	55	0	74	0	8	-22	10	-30
24	72.00	0.005	0.000	39	0	53	0	0	-27	0	-37
25	71.40	0.005	0.000	22	0	30	0	0	-26	0	-35
26	70.80	0.005	0.000	8	0	11	0	0	-18	0	-25
27	70.40	0.004	0.000	3	0	3	0	0	-10	0	-14
28	70.00	0.004	0.000	0	-0	0	-0	0	0	0	0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment						Shear force					
	Calculated		Factored		Calculated		Factored		Calculated		Factored	
	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.
	kN.m/m		kN.m/m		kN.m/m		kN/m		kN/m		kN/m	
1	2	73.95	-6	78.45	3	-8	4	76.00	-3	80.40	5	-4
2	No calculation at this stage											
3	No calculation at this stage											
4	24	74.40	-15	78.45	32	-21	22	76.00	-9	80.40	29	-12
5	No calculation at this stage											
6	23	74.40	-15	78.45	31	-21	21	76.00	-9	80.40	28	-12
7	52	73.95	-139	78.45	70	-188	88	76.00	-56	82.00	119	-75
8	No calculation at this stage											
9	52	73.95	-139	78.45	70	-188	88	76.00	-56	82.00	118	-75
10	41	73.50	-119	77.19	55	-160	82	75.44	-48	82.00	110	-64
11	67	73.50	-134	77.50	90	-182	105	75.44	-53	82.00	141	-72
12	No calculation at this stage											
13	No calculation at this stage											
14	67	73.50	-145	78.00	91	-196	102	75.44	-51	82.00	138	-69
15	No calculation at this stage											
16	67	73.50	-148	78.00	91	-200	102	75.44	-59	81.65	138	-80
17	65	73.50	-153	77.50	87	-207	111	76.25	-70	81.65	149	-94
18	31	72.60	-141	78.45	42	-190	152	76.25	-96	76.25	206	-130
19	63	76.25	-145	78.90	85	-196	176	76.25	-112	76.25	237	-152

**Maximum and minimum displacement at each stage**

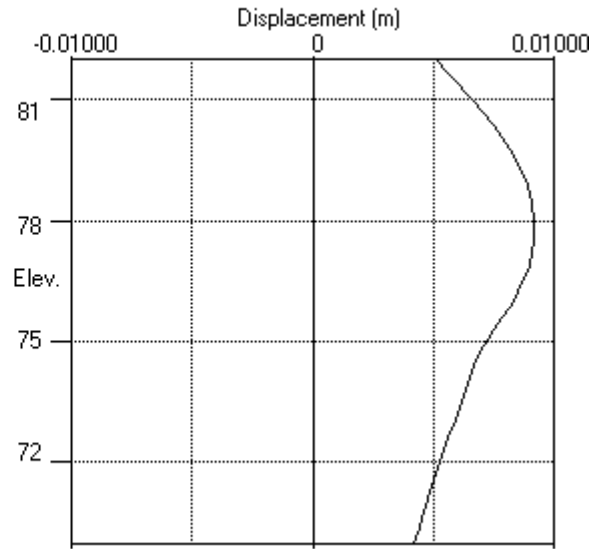
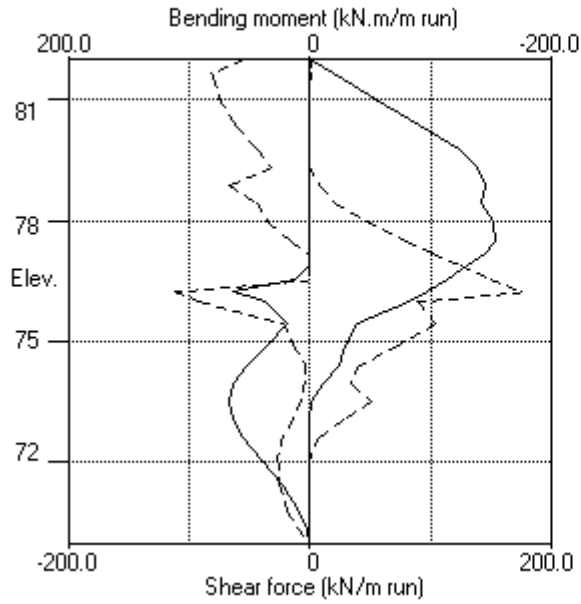
Stage no.	Displacement				Stage description
	maximum elev.	minimum elev.	maximum elev.	minimum elev.	
	m		m		
1	0.000	78.90	0.000	82.00	Apply surcharge no.1 at elev. 81.50
2	No calculation at this stage				Apply surcharge no.2 at elev. 81.50
3	No calculation at this stage				Apply surcharge no.3 at elev. 82.00
4	0.004	82.00	0.000	82.00	Excav. to elev. 81.50 on PASSIVE side
5	No calculation at this stage				Install strut no.2 at elev. 82.00
6	0.004	82.00	0.000	82.00	Apply water pressure profile no.1
7	0.009	78.45	0.000	82.00	Excav. to elev. 77.50 on PASSIVE side
8	No calculation at this stage				Install strut no.3 at elev. 78.00
9	0.009	78.45	0.000	82.00	Apply water pressure profile no.3
10	0.009	78.00	0.000	82.00	Excav. to elev. 75.44 on PASSIVE side
11	0.009	78.00	0.000	82.00	Apply surcharge no.4 at elev. 75.44
12	No calculation at this stage				Install strut no.4 at elev. 76.25
13	No calculation at this stage				Install strut no.6 at elev. 78.90
14	0.009	78.00	0.000	82.00	Remove strut no.3 at elev. 78.00
15	No calculation at this stage				Install strut no.7 at elev. 81.65
16	0.009	78.00	0.000	82.00	Remove strut no.2 at elev. 82.00
17	0.009	78.00	0.000	82.00	Change soil type 1 to soil type 4
18	0.009	78.45	0.000	82.00	Change soil type 2 to soil type 5
19	0.009	78.45	0.000	82.00	Change soil type 3 to soil type 6

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59 Maresfield Gardens  
South Wall

| Sheet No.  
| Job No. J11251  
| Made by : MC  
| Date:12-12-2012  
| Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: 59 Maresfield Gdns South Wall\_ULS2 |  
 59 Maresfield Gardens | Date:12-12-2012  
 South Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	82.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES (Unfactored SLS soil strengths)**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.000)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (1.000)	1.000 (1.000)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.337 (1.360)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.000	0.00
3 London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.670	0.00
6 London Clay Drained	26.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile no.	Active side				Passive side			
	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	76.00	76.00	0.0 MC
4	1	82.00	82.00	0.0	1	75.00	75.00	0.0 WC



**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m<sup>2</sup>  
 Moment of inertia of wall I = 7.0700E-03 m<sup>4</sup>/m run  
 E.I = 197960 kN.m<sup>2</sup>/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1		Not defined						
2	82.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
4	76.25	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5		Not defined						
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	2.000E+08	1.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- kN/m <sup>2</sup> ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	81.50	1.30(A)	0.50	20.00	100.00	=	N/A	1.00 P/U
2	81.50	0.80(A)	20.00	0.50	80.00	=	N/A	1.00 P/U
3	82.00	0.00(A)	20.00	20.00	5.00	=	N/A	1.00 P/U
4	75.44	-0.00(P)	8.00	10.00	50.00	=	N/A	1.00 -

Note: A = Active side, P = Passive side  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 81.50 No analysis at this stage
2	Apply surcharge no.2 at elevation 81.50 No analysis at this stage
3	Apply surcharge no.3 at elevation 82.00 No analysis at this stage
4	Excavate to elevation 81.50 on PASSIVE side
5	Install strut or anchor no.2 at elevation 82.00
6	Apply water pressure profile no.2 ( Worst Cred. )
7	Excavate to elevation 77.50 on PASSIVE side
8	Install strut or anchor no.3 at elevation 78.00
9	Apply water pressure profile no.4 ( Worst Cred. )
10	Excavate to elevation 75.44 on PASSIVE side
11	Apply surcharge no.4 at elevation 75.44
12	Install strut or anchor no.4 at elevation 76.25
13	Install strut or anchor no.6 at elevation 78.90
14	Remove strut or anchor no.3 at elevation 78.00
15	Install strut or anchor no.7 at elevation 81.65
16	Remove strut or anchor no.2 at elevation 82.00
17	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
18	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
19	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

## FACTORS OF SAFETY and ANALYSIS OPTIONS

Limit State options: ULS DA1 Combination 2  
Water pressures : Worst Credible  
Partial factor on C' = 1.250  
Partial factor on Phi' = 1.250  
Partial factor on Cu = 1.400  
Partial factor on Soil Modulus = 1.000  
Partial factor on Permanent Unfavourable loads = 1.000  
Partial factor on Permanent Favourable loads = 1.000  
Partial factor on Permanent Variable loads = 1.300

### Stability analysis:

Method of analysis - Strength Factor method  
Overall factor on soil strength for calculating wall depth = 1.00

### Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 0.00 m

### Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

### Boundary conditions:

Length of wall (normal to plane of analysis) = 6.00 m  
  
Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m  
  
Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

## OUTPUT OPTIONS

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 81.50	No	No	No
2	Apply surcharge no.2 at elev. 81.50	No	No	No
3	Apply surcharge no.3 at elev. 82.00	No	No	No
4	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
5	Install strut no.2 at elev. 82.00	No	No	No
6	Apply water pressure profile no.2	No	No	No
7	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
8	Install strut no.3 at elev. 78.00	No	No	No
9	Apply water pressure profile no.4	No	No	No
10	Excav. to elev. 75.44 on PASSIVE side	No	No	No
11	Apply surcharge no.4 at elev. 75.44	No	No	No
12	Install strut no.4 at elev. 76.25	No	No	No
13	Install strut no.6 at elev. 78.90	No	No	No
14	Remove strut no.3 at elev. 78.00	No	No	No
15	Install strut no.7 at elev. 81.65	No	No	No
16	Remove strut no.2 at elev. 82.00	No	No	No
17	Change soil type 1 to soil type 4	No	No	No
18	Change soil type 2 to soil type 5	No	No	No
19	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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 59 Maresfield Gardens | Date:12-12-2012  
 South Wall | Checked :

Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: ULS DA1 Combination 2  
 Water pressures : Worst Credible  
 Partial factor on C' = 1.250  
 Partial factor on Phi' = 1.250  
 Partial factor on Cu = 1.400  
 Partial factor on Soil Modulus = 1.000  
 Partial factor on Permanent Unfavourable loads = 1.000  
 Partial factor on Permanent Favourable loads = 1.000  
 Partial factor on Permanent Variable loads = 1.300

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

Stage No.	--- G.L. --- Act. Pass.	Strut Elev.	Overall		Toe elev. for		
			Factor of Safety	Moment of equilib. at elev.	elev. = 70.00	FoS = 1.000	
1	82.00 82.00	Cant.	Conditions not suitable for FoS calc.				
2	82.00 82.00		No analysis at this stage				
3	82.00 82.00		No analysis at this stage				
4	82.00 81.50	Cant.	Conditions not suitable for FoS calc.				
5	82.00 81.50		No analysis at this stage				
6	82.00 81.50	82.00	7.066	n/a	81.49	0.01	
7	82.00 77.50	82.00	1.737	n/a	75.53	1.97	
8	82.00 77.50		No analysis at this stage				

All remaining stages have more than one strut - FoS calculation n/a

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 59 Maresfield Gardens | Date:12-12-2012  
 South Wall | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	82.00	0.005	0.000	0.0	0.0	0.0	-56.9
2	81.65	0.006	0.000	0.3	-19.9	1.8	-85.6
3	81.50	0.006	0.000	0.1	-28.3	0.7	-84.3
4	81.00	0.007	0.000	0.0	-56.1	0.0	-77.4
5	80.40	0.008	0.000	0.0	-93.8	0.0	-62.1
6	79.80	0.008	0.000	0.0	-124.5	0.0	-41.3
7	79.35	0.009	0.000	0.0	-137.8	0.0	-31.4
8	78.90	0.009	0.000	0.0	-141.7	17.1	-79.7
9	78.45	0.009	0.000	0.0	-145.7	13.7	-53.5
10	78.00	0.010	0.000	0.0	-155.8	42.7	-48.8
11	77.50	0.010	0.000	0.0	-159.7	78.0	-25.2
12	77.00	0.010	0.000	0.0	-145.3	116.5	0.0
13	76.63	0.009	0.000	0.0	-126.9	147.4	0.0
14	76.25	0.009	0.000	59.8	-107.2	180.0	-114.9
15	76.00	0.009	0.000	33.9	-92.6	94.0	-92.2
16	75.44	0.008	0.000	18.9	-50.3	108.1	-21.2
17	75.00	0.008	0.000	35.1	-38.2	78.9	-15.6
18	74.40	0.007	0.000	51.3	-32.7	41.7	-7.1
19	73.95	0.007	0.000	57.2	-21.4	30.6	-3.7
20	73.50	0.007	0.000	58.2	-11.9	46.6	-8.1
21	73.05	0.007	0.000	53.5	-8.1	30.1	-14.6
22	72.60	0.006	0.000	47.4	-3.4	14.0	-18.8
23	72.00	0.006	0.000	34.9	0.0	4.9	-22.4
24	71.40	0.005	0.000	21.8	0.0	0.6	-23.3
25	70.80	0.005	0.000	8.4	0.0	0.0	-17.9
26	70.40	0.005	0.000	2.6	0.0	0.0	-10.5
27	70.00	0.005	0.000	0.0	-0.0	0.0	0.0

**Summary of results (continued)**

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev.	minimum kN.m/m	elev.	maximum kN/m	elev.	minimum kN/m	elev.
1	2.5	73.95	-5.9	78.45	4.0	76.00	-2.7	80.40
2	No calculation at this stage							
3	No calculation at this stage							
4	23.8	74.40	-15.5	78.45	21.6	76.00	-8.9	80.40
5	No calculation at this stage							
6	22.9	74.40	-15.2	78.45	20.9	76.00	-8.8	80.40
7	55.2	73.95	-145.7	78.45	94.0	76.00	-56.9	82.00
8	No calculation at this stage							
9	54.8	73.95	-145.2	78.45	93.6	76.00	-56.8	82.00
10	31.4	73.50	-126.0	77.00	85.1	75.44	-48.8	78.00
11	57.3	73.50	-138.4	77.50	108.1	75.44	-52.8	82.00
12	No calculation at this stage							
13	No calculation at this stage							
14	58.1	73.50	-153.2	77.50	105.2	75.44	-51.2	78.90
15	No calculation at this stage							
16	58.2	73.50	-154.8	77.50	104.8	75.44	-57.4	81.65
17	55.5	73.50	-159.7	77.50	111.6	76.25	-79.7	78.90
18	24.5	72.00	-140.1	78.45	154.3	76.25	-98.1	76.25
19	59.8	76.25	-141.7	78.90	180.0	76.25	-114.9	76.25

**Maximum and minimum displacement at each stage**

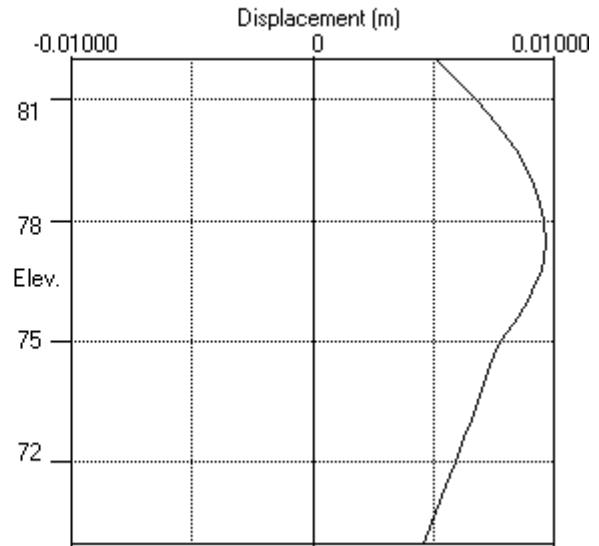
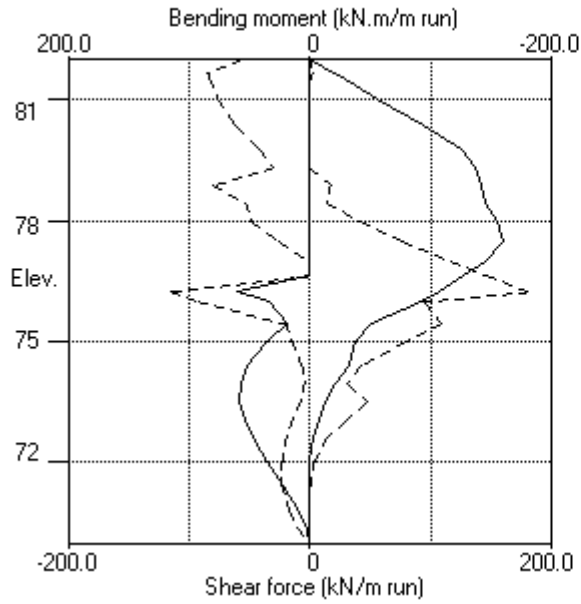
Stage no.	Displacement				Stage description
	maximum m	elev.	minimum m	elev.	
1	0.000	78.90	0.000	82.00	Apply surcharge no.1 at elev. 81.50
2	No calculation at this stage				Apply surcharge no.2 at elev. 81.50
3	No calculation at this stage				Apply surcharge no.3 at elev. 82.00
4	0.004	82.00	0.000	82.00	Excav. to elev. 81.50 on PASSIVE side
5	No calculation at this stage				Install strut no.2 at elev. 82.00
6	0.004	82.00	0.000	82.00	Apply water pressure profile no.2
7	0.009	78.45	0.000	82.00	Excav. to elev. 77.50 on PASSIVE side
8	No calculation at this stage				Install strut no.3 at elev. 78.00
9	0.009	78.45	0.000	82.00	Apply water pressure profile no.4
10	0.010	77.50	0.000	82.00	Excav. to elev. 75.44 on PASSIVE side
11	0.009	78.00	0.000	82.00	Apply surcharge no.4 at elev. 75.44
12	No calculation at this stage				Install strut no.4 at elev. 76.25
13	No calculation at this stage				Install strut no.6 at elev. 78.90
14	0.009	78.00	0.000	82.00	Remove strut no.3 at elev. 78.00
15	No calculation at this stage				Install strut no.7 at elev. 81.65
16	0.009	78.00	0.000	82.00	Remove strut no.2 at elev. 82.00
17	0.009	78.00	0.000	82.00	Change soil type 1 to soil type 4
18	0.009	78.00	0.000	82.00	Change soil type 2 to soil type 5
19	0.009	78.00	0.000	82.00	Change soil type 3 to soil type 6

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59 Maresfield Gardens  
South Wall

| Sheet No.  
| Job No. J11251  
| Made by : MC  
| Date:12-12-2012  
| Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: 59 Maresfield Gdns West Wall\_SLS |  
 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	82.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh,kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.000)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (1.000)	1.000 (1.000)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.337 (1.360)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

----- Soil type -----	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
No. Description						
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.000	0.00
3 London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.670	0.00
6 London Clay Drained	26.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

Initial water table elevation      Active side      Passive side  
 81.00      81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile	Active side				Passive side			
	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	76.00	76.00	0.0 MC
4	1	82.00	82.00	0.0	1	75.00	75.00	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m<sup>2</sup>  
 Moment of inertia of wall I = 7.0700E-03 m<sup>4</sup>/m run  
 E.I = 197960 kN.m<sup>2</sup>/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1		Not defined						
2	82.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
4	76.25	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5		Not defined						
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	2.000E+08	1.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	81.50	1.30(A)	0.50	20.00	100.00	=	N/A	1.00 P/U
2	81.50	0.80(A)	20.00	0.50	80.00	=	N/A	1.00 P/U
3	82.00	0.00(A)	20.00	20.00	5.00	=	N/A	1.00 P/U
4	75.44	-0.00(P)	8.00	10.00	50.00	=	N/A	1.00 -

Note: A = Active side, P = Passive side  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.3 at elevation 82.00 No analysis at this stage
2	Excavate to elevation 81.50 on PASSIVE side
3	Install strut or anchor no.2 at elevation 82.00
4	Apply water pressure profile no.1 ( Mod. Conserv. )
5	Excavate to elevation 77.50 on PASSIVE side
6	Install strut or anchor no.3 at elevation 78.00
7	Apply water pressure profile no.3 ( Mod. Conserv. )
8	Excavate to elevation 75.44 on PASSIVE side
9	Apply surcharge no.4 at elevation 75.44
10	Install strut or anchor no.4 at elevation 76.25
11	Install strut or anchor no.6 at elevation 78.90
12	Remove strut or anchor no.3 at elevation 78.00
13	Install strut or anchor no.7 at elevation 81.65
14	Remove strut or anchor no.2 at elevation 82.00
15	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
16	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
17	Change properties of soil type 3 to soil type 6 Ko pressures will be reset



**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: Serviceability Limit State  
All loads and soil strengths are unfactored

Stability analysis:  
Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

Parameters for undrained strata:  
Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:  
Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:  
Length of wall (normal to plane of analysis) = 6.00 m  
  
Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m  
  
Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement	Active, Passive pressures	Graph. output
1	Apply surcharge no.3 at elev. 82.00	No	No	No
2	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
3	Install strut no.2 at elev. 82.00	No	No	No
4	Apply water pressure profile no.1	No	No	No
5	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
6	Install strut no.3 at elev. 78.00	No	No	No
7	Apply water pressure profile no.3	No	No	No
8	Excav. to elev. 75.44 on PASSIVE side	No	No	No
9	Apply surcharge no.4 at elev. 75.44	No	No	No
10	Install strut no.4 at elev. 76.25	No	No	No
11	Install strut no.6 at elev. 78.90	No	No	No
12	Remove strut no.3 at elev. 78.00	No	No	No
13	Install strut no.7 at elev. 81.65	No	No	No
14	Remove strut no.2 at elev. 82.00	No	No	No
15	Change soil type 1 to soil type 4	No	No	No
16	Change soil type 2 to soil type 5	No	No	No
17	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: Serviceability Limit State  
 All loads and soil strengths are unfactored

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	G.L.		Strut Elev.	FoS for toe elev. = 70.00		Toe elev. for FoS = 1.000	
	Act.	Pass.		Factor of Safety at elev.	Moment of equilib.	Toe elev.	Wall Penetration
1	82.00	82.00	Cant.	Conditions not suitable for FoS calc.			
2	82.00	81.50	Cant.	Conditions not suitable for FoS calc.			
3	82.00	81.50		No analysis at this stage			
4	82.00	81.50	82.00	18.221	n/a	81.50	0.00
5	82.00	77.50	82.00	2.754	n/a	76.81	0.69
6	82.00	77.50		No analysis at this stage			

All remaining stages have more than one strut - FoS calculation n/a

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 West Wall | Checked :

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**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		---- Bending moment ----				----- Shear force -----			
		max.	min.	Calculated		Factored		Calculated		Factored	
				max.	min.	max.	min.	max.	min.	max.	min.
		m	m	kN.m/m		kN.m/m		kN/m		kN/m	
1	82.00	0.003	0.000	0	0	0	0	0	-42	0	-57
2	81.65	0.003	0.000	0	-15	0	-20	2	-64	2	-87
3	81.50	0.003	0.000	0	-21	0	-28	1	-63	1	-85
4	81.00	0.004	0.000	0	-41	0	-56	0	-59	0	-79
5	80.40	0.005	0.000	0	-72	0	-98	0	-49	0	-67
6	79.80	0.006	0.000	0	-98	0	-132	0	-35	0	-47
7	79.35	0.006	0.000	0	-110	0	-149	0	-27	0	-37
8	78.90	0.007	0.000	0	-116	0	-156	7	-65	9	-87
9	78.45	0.007	0.000	0	-115	0	-155	13	-45	17	-61
10	78.00	0.007	0.000	0	-127	0	-171	35	-39	48	-53
11	77.50	0.007	0.000	0	-131	0	-177	64	-23	87	-30
12	77.19	0.007	0.000	0	-126	0	-170	84	-11	113	-14
13	76.88	0.007	0.000	0	-115	0	-155	105	0	142	0
14	76.56	0.007	0.000	10	-104	13	-140	128	0	172	0
15	76.25	0.007	0.000	53	-91	72	-123	151	-109	204	-148
16	76.00	0.007	0.000	28	-81	38	-109	66	-90	89	-121
17	75.44	0.007	0.000	9	-48	12	-65	86	-27	116	-36
18	74.92	0.006	0.000	16	-40	21	-54	61	-16	82	-21
19	74.40	0.006	0.000	32	-36	43	-48	37	-4	50	-6
20	73.95	0.006	0.000	44	-25	59	-33	32	-2	43	-3
21	73.50	0.005	0.000	48	-13	64	-17	49	-3	67	-4
22	73.05	0.005	0.000	46	-6	62	-8	29	-8	39	-11
23	72.60	0.005	0.000	40	-2	55	-2	12	-15	16	-21
24	72.00	0.005	0.000	29	0	40	0	3	-20	4	-27
25	71.40	0.005	0.000	17	0	23	0	0	-19	0	-26
26	70.80	0.004	0.000	6	0	9	0	0	-14	0	-19
27	70.40	0.004	0.000	2	0	3	0	0	-8	0	-11
28	70.00	0.004	0.000	0	-0	0	-0	0	0	0	0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment						Shear force					
	Calculated				Factored		Calculated				Factored	
	max.	elev.	min.	elev.	max.	min.	max.	elev.	min.	elev.	max.	min.
	kN.m/m		kN.m/m		kN.m/m		kN/m		kN/m		kN/m	
1	4	74.40	-2	78.45	5	-3	3	76.00	-1	72.60	5	-2
2	11	74.40	-3	78.00	14	-4	9	76.00	-3	72.60	12	-5
3	No calculation at this stage											
4	10	74.40	-3	78.00	13	-4	9	76.00	-3	72.60	12	-4
5	32	73.50	-110	78.45	43	-149	66	76.00	-42	82.00	89	-57
6	No calculation at this stage											
7	31	73.50	-110	78.45	42	-149	66	76.00	-42	82.00	89	-57
8	23	73.05	-102	76.88	31	-138	63	75.44	-39	78.00	85	-53
9	47	73.50	-115	77.19	63	-155	86	75.44	-41	82.00	116	-56
10	No calculation at this stage											
11	No calculation at this stage											
12	48	73.50	-123	77.50	64	-166	84	75.44	-39	82.00	114	-53
13	No calculation at this stage											
14	48	73.50	-124	77.50	64	-167	84	75.44	-45	81.65	113	-61
15	45	73.50	-131	77.50	61	-177	93	76.25	-65	78.90	125	-87
16	20	72.00	-113	78.45	27	-153	130	76.25	-96	76.25	175	-129
17	53	76.25	-116	78.90	72	-156	151	76.25	-109	76.25	204	-148

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum	elev.	minimum	elev.	
	m		m		
1	0.001	82.00	0.000	82.00	Apply surcharge no.3 at elev. 82.00
2	0.002	82.00	0.000	82.00	Excav. to elev. 81.50 on PASSIVE side
3	No calculation at this stage				Install strut no.2 at elev. 82.00
4	0.002	82.00	0.000	82.00	Apply water pressure profile no.1
5	0.006	78.00	0.000	82.00	Excav. to elev. 77.50 on PASSIVE side
6	No calculation at this stage				Install strut no.3 at elev. 78.00
7	0.006	78.00	0.000	82.00	Apply water pressure profile no.3
8	0.007	77.19	0.000	82.00	Excav. to elev. 75.44 on PASSIVE side
9	0.007	77.50	0.000	82.00	Apply surcharge no.4 at elev. 75.44
10	No calculation at this stage				Install strut no.4 at elev. 76.25
11	No calculation at this stage				Install strut no.6 at elev. 78.90
12	0.007	77.50	0.000	82.00	Remove strut no.3 at elev. 78.00
13	No calculation at this stage				Install strut no.7 at elev. 81.65
14	0.007	77.50	0.000	82.00	Remove strut no.2 at elev. 82.00
15	0.007	77.50	0.000	82.00	Change soil type 1 to soil type 4
16	0.007	78.00	0.000	82.00	Change soil type 2 to soil type 5
17	0.007	78.00	0.000	82.00	Change soil type 3 to soil type 6

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Strut forces at each stage (horizontal components)**

Stage no.	----- Strut no. 2 ----- at elev. 82.00			----- Strut no. 3 ----- at elev. 78.00			----- Strut no. 4 ----- at elev. 76.25		
	--Calculated-- kN per m run	Factored kN per strut	Factored kN per slack	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut
4				---	---	---	---	---	---
5	42	254	343	---	---	---	---	---	---
7	42	254	343	0	2	3	---	---	---
8	35	211	284	52	314	423	---	---	---
9	41	247	333	33	199	269	---	---	---
12	39	237	320	---	---	---	12	12	17
14	---	---	---	---	---	---	14	14	19
15	---	---	---	---	---	---	62	62	83
16	---	---	---	---	---	---	225	225	304
17	---	---	---	---	---	---	261	261	352

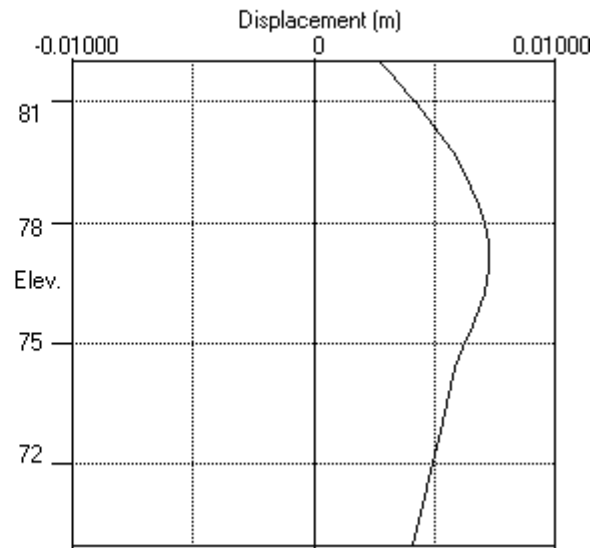
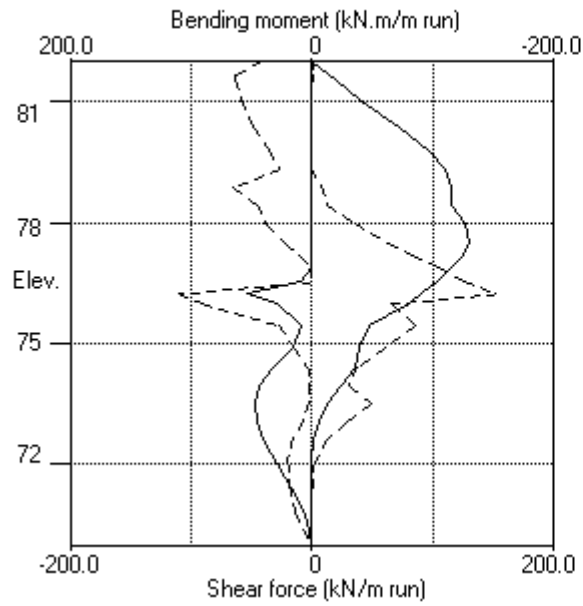
Stage no.	----- Strut no. 6 ----- at elev. 78.90			----- Strut no. 7 ----- at elev. 81.65		
	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut
12	24	24	33	---	---	---
14	16	16	22	46	46	62
15	71	71	96	55	55	74
16	28	28	38	62	62	83
17	3	3	4	66	66	89

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59 Maresfield Gardens  
West Wall

| Sheet No.  
| Job No. J11251  
| Made by : MC  
| Date:12-12-2012  
| Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: 59 Maresfield Gdns West Wall\_ULS1 |  
 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	82.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES (Unfactored SLS soil strengths)**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.000)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (1.000)	1.000 (1.000)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.337 (1.360)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.000	0.00
3 London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.670	0.00
6 London Clay Drained	26.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile		Active side			Passive side			
Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	76.00	76.00	0.0 MC
4	1	82.00	82.00	0.0	1	75.00	75.00	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m<sup>2</sup>  
 Moment of inertia of wall I = 7.0700E-03 m<sup>4</sup>/m run  
 E.I = 197960 kN.m<sup>2</sup>/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1		Not defined						
2	82.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
4	76.25	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5		Not defined						
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	2.000E+08	1.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	81.50	1.30(A)	0.50	20.00	100.00	=	N/A	1.00 P/U
2	81.50	0.80(A)	20.00	0.50	80.00	=	N/A	1.00 P/U
3	82.00	0.00(A)	20.00	20.00	5.00	=	N/A	1.00 P/U
4	75.44	-0.00(P)	8.00	10.00	50.00	=	N/A	1.00 -

Note: A = Active side, P = Passive side  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.3 at elevation 82.00 No analysis at this stage
2	Excavate to elevation 81.50 on PASSIVE side
3	Install strut or anchor no.2 at elevation 82.00
4	Apply water pressure profile no.1 ( Mod. Conserv. )
5	Excavate to elevation 77.50 on PASSIVE side
6	Install strut or anchor no.3 at elevation 78.00
7	Apply water pressure profile no.3 ( Mod. Conserv. )
8	Excavate to elevation 75.44 on PASSIVE side
9	Apply surcharge no.4 at elevation 75.44
10	Install strut or anchor no.4 at elevation 76.25
11	Install strut or anchor no.6 at elevation 78.90
12	Remove strut or anchor no.3 at elevation 78.00
13	Install strut or anchor no.7 at elevation 81.65
14	Remove strut or anchor no.2 at elevation 82.00
15	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
16	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
17	Change properties of soil type 3 to soil type 6 Ko pressures will be reset



**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: ULS DA1 Combination 1  
Water pressures : Moderately Conservative  
Partial factor on C' = 1.000  
Partial factor on Phi' = 1.000  
Partial factor on Cu = 1.000  
Partial factor on Soil Modulus = 1.000  
Partial factor on Permanent Unfavourable loads = 1.000  
Partial factor on Permanent Favourable loads = 1.000  
Partial factor on Permanent Variable loads = 1.100  
Design factor on calculated Bending Moments = 1.350

Parameters for undrained strata:  
Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:  
Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:  
Length of wall (normal to plane of analysis) = 6.00 m  
  
Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m  
  
Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.3 at elev. 82.00	No	No	No
2	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
3	Install strut no.2 at elev. 82.00	No	No	No
4	Apply water pressure profile no.1	No	No	No
5	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
6	Install strut no.3 at elev. 78.00	No	No	No
7	Apply water pressure profile no.3	No	No	No
8	Excav. to elev. 75.44 on PASSIVE side	No	No	No
9	Apply surcharge no.4 at elev. 75.44	No	No	No
10	Install strut no.4 at elev. 76.25	No	No	No
11	Install strut no.6 at elev. 78.90	No	No	No
12	Remove strut no.3 at elev. 78.00	No	No	No
13	Install strut no.7 at elev. 81.65	No	No	No
14	Remove strut no.2 at elev. 82.00	No	No	No
15	Change soil type 1 to soil type 4	No	No	No
16	Change soil type 2 to soil type 5	No	No	No
17	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes

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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
 Licensed from GEOSOLVE | Made by : MC  
 Data filename/Run ID: 59 Maresfield Gdns West Wall\_ULS1 |  
 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 1**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment				Shear force			
		m		Calculated		Factored		Calculated		Factored	
		max.	min.	max.	min.	max.	min.	max.	min.	max.	min.
1	82.00	0.003	0.000	0	0	0	0	0	-42	0	-57
2	81.65	0.003	0.000	0	-15	0	-20	2	-64	2	-87
3	81.50	0.003	0.000	0	-21	0	-28	1	-63	1	-85
4	81.00	0.004	0.000	0	-41	0	-56	0	-59	0	-79
5	80.40	0.005	0.000	0	-72	0	-98	0	-49	0	-67
6	79.80	0.006	0.000	0	-98	0	-132	0	-35	0	-47
7	79.35	0.006	0.000	0	-110	0	-149	0	-27	0	-37
8	78.90	0.007	0.000	0	-116	0	-156	7	-65	9	-87
9	78.45	0.007	0.000	0	-115	0	-155	13	-45	17	-61
10	78.00	0.007	0.000	0	-127	0	-171	35	-39	48	-53
11	77.50	0.007	0.000	0	-131	0	-177	64	-23	87	-30
12	77.19	0.007	0.000	0	-126	0	-170	84	-11	113	-14
13	76.88	0.007	0.000	0	-115	0	-155	105	0	142	0
14	76.56	0.007	0.000	10	-104	13	-140	128	0	172	0
15	76.25	0.007	0.000	53	-91	72	-123	151	-109	204	-148
16	76.00	0.007	0.000	28	-81	38	-109	66	-90	89	-121
17	75.44	0.007	0.000	9	-48	12	-65	86	-27	116	-36
18	74.92	0.006	0.000	16	-40	21	-54	61	-16	82	-21
19	74.40	0.006	0.000	32	-36	43	-48	37	-4	50	-6
20	73.95	0.006	0.000	44	-25	59	-33	32	-2	43	-3
21	73.50	0.005	0.000	48	-13	64	-17	49	-3	67	-4
22	73.05	0.005	0.000	46	-6	62	-8	29	-8	39	-11
23	72.60	0.005	0.000	40	-2	55	-2	12	-15	16	-21
24	72.00	0.005	0.000	29	0	40	0	3	-20	4	-27
25	71.40	0.005	0.000	17	0	23	0	0	-19	0	-26
26	70.80	0.004	0.000	6	0	9	0	0	-14	0	-19
27	70.40	0.004	0.000	2	0	3	0	0	-8	0	-11
28	70.00	0.004	0.000	0	-0	0	-0	0	0	0	0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment						Shear force					
	Calculated				Factored		Calculated				Factored	
	max.	elev.	min.	elev.	max.	min.	max.	elev.	min.	elev.	max.	min.
1	4	74.40	-2	78.45	5	-3	3	76.00	-1	72.60	5	-2
2	11	74.40	-3	78.00	14	-4	9	76.00	-3	72.60	12	-5
3	No calculation at this stage											
4	10	74.40	-3	78.00	13	-4	9	76.00	-3	72.60	12	-4
5	32	73.50	-110	78.45	43	-149	66	76.00	-42	82.00	89	-57
6	No calculation at this stage											
7	31	73.50	-110	78.45	42	-149	66	76.00	-42	82.00	89	-57
8	23	73.05	-102	76.88	31	-138	63	75.44	-39	78.00	85	-53
9	47	73.50	-115	77.19	63	-155	86	75.44	-41	82.00	116	-56
10	No calculation at this stage											
11	No calculation at this stage											
12	48	73.50	-123	77.50	64	-166	84	75.44	-39	82.00	114	-53
13	No calculation at this stage											
14	48	73.50	-124	77.50	64	-167	84	75.44	-45	81.65	113	-61
15	45	73.50	-131	77.50	61	-177	93	76.25	-65	78.90	125	-87
16	20	72.00	-113	78.45	27	-153	130	76.25	-96	76.25	175	-129
17	53	76.25	-116	78.90	72	-156	151	76.25	-109	76.25	204	-148

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum	elev.	minimum	elev.	
	m		m		
1	0.001	82.00	0.000	82.00	Apply surcharge no.3 at elev. 82.00
2	0.002	82.00	0.000	82.00	Excav. to elev. 81.50 on PASSIVE side
3	No calculation at this stage				Install strut no.2 at elev. 82.00
4	0.002	82.00	0.000	82.00	Apply water pressure profile no.1
5	0.006	78.00	0.000	82.00	Excav. to elev. 77.50 on PASSIVE side
6	No calculation at this stage				Install strut no.3 at elev. 78.00
7	0.006	78.00	0.000	82.00	Apply water pressure profile no.3
8	0.007	77.19	0.000	82.00	Excav. to elev. 75.44 on PASSIVE side
9	0.007	77.50	0.000	82.00	Apply surcharge no.4 at elev. 75.44
10	No calculation at this stage				Install strut no.4 at elev. 76.25
11	No calculation at this stage				Install strut no.6 at elev. 78.90
12	0.007	77.50	0.000	82.00	Remove strut no.3 at elev. 78.00
13	No calculation at this stage				Install strut no.7 at elev. 81.65
14	0.007	77.50	0.000	82.00	Remove strut no.2 at elev. 82.00
15	0.007	77.50	0.000	82.00	Change soil type 1 to soil type 4
16	0.007	78.00	0.000	82.00	Change soil type 2 to soil type 5
17	0.007	78.00	0.000	82.00	Change soil type 3 to soil type 6

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Strut forces at each stage (horizontal components)**

Stage no.	----- Strut no. 2 ----- at elev. 82.00			----- Strut no. 3 ----- at elev. 78.00			----- Strut no. 4 ----- at elev. 76.25		
	--Calculated-- kN per m run	Factored kN per strut	Factored kN per slack	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut
4				---	---	---	---	---	---
5	42	254	343	---	---	---	---	---	---
7	42	254	343	0	2	3	---	---	---
8	35	211	284	52	314	423	---	---	---
9	41	247	333	33	199	269	---	---	---
12	39	237	320	---	---	---	12	12	17
14	---	---	---	---	---	---	14	14	19
15	---	---	---	---	---	---	62	62	83
16	---	---	---	---	---	---	225	225	304
17	---	---	---	---	---	---	261	261	352

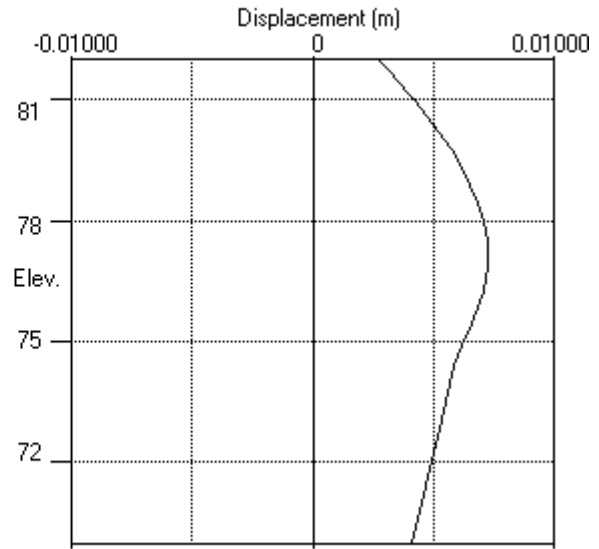
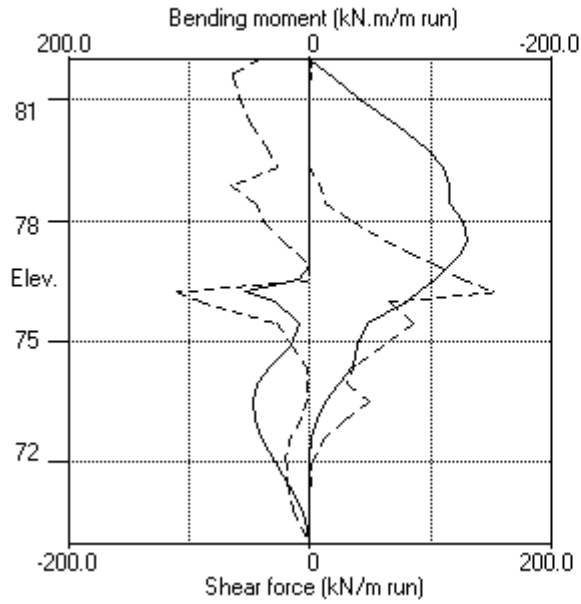
Stage no.	----- Strut no. 6 ----- at elev. 78.90			----- Strut no. 7 ----- at elev. 81.65		
	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut	--Calculated-- kN per m run	Factored kN per strut	Factored kN per strut
12	24	24	33	---	---	---
14	16	16	22	46	46	62
15	71	71	96	55	55	74
16	28	28	38	62	62	83
17	3	3	4	66	66	89

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59 Maresfield Gardens  
West Wall

| Sheet No.  
| Job No. J11251  
| Made by : MC  
| Date:12-12-2012  
| Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: 59 Maresfield Gdns West Wall\_ULS2 |  
 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	82.00	1 Made Ground / Alluv	1 Made Ground / Alluv
2	76.00	2 Claygate Beds	2 Claygate Beds
3	73.50	3 London Clay	3 London Clay

**SOIL PROPERTIES (Unfactored SLS soil strengths)**

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC ( Nu )	Ka ( Kac )	Kp ( Kpc )	kN/m2 ( dc/dy )
1 Made Ground / Alluv	17.00	12500	0.500	NC (0.490)	1.000 (2.570)	1.000 (2.571)	25.00u
2 Claygate .. ( 76.00 )	18.00	37500 ( 3000)	0.500	OC (0.490)	1.000 (2.000)	1.000 (2.000)	75.00u ( 6.000)
3 London Clay ( 73.50 )	19.00	45000 ( 2608)	1.000	OC (0.490)	1.000 (1.000)	1.000 (1.000)	90.00u ( 5.200)
4 MG /Alluv Drained	18.00	7500	0.500	NC (0.250)	0.324 (1.327)	3.601 (5.104)	0.0d
5 Claygate .. ( 76.00 )	18.00	22500 ( 1800)	1.000	OC (0.200)	0.351 (1.391)	3.440 (5.233)	0.0d
6 London Cl.. ( 73.50 )	19.00	27000 ( 1565)	1.000	OC (0.200)	0.337 (1.360)	3.440 (5.233)	0.0d

**Additional soil parameters associated with Ka and Kp**

Soil type	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction	Wall adhesion	Back-fill	Soil friction	Wall adhesion	Back-fill
No. Description	angle	coeff.	angle	angle	coeff.	angle
1 Made Ground / Alluv	0.00	1.000	0.00	0.00	1.000	0.00
2 Claygate Beds	0.00	0.000	0.00	0.00	0.000	0.00
3 London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4 MG /Alluv Drained	27.00	0.641	0.00	27.00	0.471	0.00
5 Claygate Drained	25.00	0.670	0.00	25.00	0.670	0.00
6 London Clay Drained	26.00	0.670	0.00	25.00	0.670	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	81.00	81.00

Automatic water pressure balancing at toe of wall : No

Water press. profile	Active side				Passive side			
	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	81.00	81.00	0.0	1	77.50	77.50	0.0 MC
2	1	82.00	82.00	0.0	1	77.00	77.00	0.0 WC
3	1	81.00	81.00	0.0	1	76.00	76.00	0.0 MC
4	1	82.00	82.00	0.0	1	75.00	75.00	0.0 WC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 70.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 7.0700E-03 m4/m run  
 E.I = 197960 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1		Not defined						
2	82.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
3	78.00	6.00	0.010000	2.000E+08	4.00	0.00	0	No
4	76.25	1.00	0.350000	3.000E+07	1.00	0.00	0	No
5		Not defined						
6	78.90	1.00	0.250000	3.000E+07	1.00	0.00	0	No
7	81.65	1.00	0.250000	2.000E+08	1.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge ----- Near edge Far edge		Equiv. soil type	Partial factor/ Category
1	81.50	1.30(A)	0.50	20.00	100.00	=	N/A	1.00 P/U
2	81.50	0.80(A)	20.00	0.50	80.00	=	N/A	1.00 P/U
3	82.00	0.00(A)	20.00	20.00	5.00	=	N/A	1.00 P/U
4	75.44	-0.00(P)	8.00	10.00	50.00	=	N/A	1.00 -

Note: A = Active side, P = Passive side

Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.3 at elevation 82.00 No analysis at this stage
2	Excavate to elevation 81.50 on PASSIVE side
3	Install strut or anchor no.2 at elevation 82.00
4	Apply water pressure profile no.2 ( Worst Cred. )
5	Excavate to elevation 77.50 on PASSIVE side
6	Install strut or anchor no.3 at elevation 78.00
7	Apply water pressure profile no.4 ( Worst Cred. )
8	Excavate to elevation 75.44 on PASSIVE side
9	Apply surcharge no.4 at elevation 75.44
10	Install strut or anchor no.4 at elevation 76.25
11	Install strut or anchor no.6 at elevation 78.90
12	Remove strut or anchor no.3 at elevation 78.00
13	Install strut or anchor no.7 at elevation 81.65
14	Remove strut or anchor no.2 at elevation 82.00
15	Change properties of soil type 1 to soil type 4 Ko pressures will be reset
16	Change properties of soil type 2 to soil type 5 Ko pressures will be reset
17	Change properties of soil type 3 to soil type 6 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: ULS DA1 Combination 2  
Water pressures : Worst Credible  
Partial factor on C' = 1.250  
Partial factor on Phi' = 1.250  
Partial factor on Cu = 1.400  
Partial factor on Soil Modulus = 1.000  
Partial factor on Permanent Unfavourable loads = 1.000  
Partial factor on Permanent Favourable loads = 1.000  
Partial factor on Permanent Variable loads = 1.300

Stability analysis:  
Method of analysis - Strength Factor method  
Overall factor on soil strength for calculating wall depth = 1.00

Parameters for undrained strata:  
Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:  
Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 20.00 m

Boundary conditions:  
Length of wall (normal to plane of analysis) = 6.00 m  
  
Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 10.00 m  
  
Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement	Active, Passive pressures	Graph. output
		Bending mom.		
		Shear force		
1	Apply surcharge no.3 at elev. 82.00	No	No	No
2	Excav. to elev. 81.50 on PASSIVE side	Yes	No	Yes
3	Install strut no.2 at elev. 82.00	No	No	No
4	Apply water pressure profile no.2	No	No	No
5	Excav. to elev. 77.50 on PASSIVE side	Yes	No	Yes
6	Install strut no.3 at elev. 78.00	No	No	No
7	Apply water pressure profile no.4	No	No	No
8	Excav. to elev. 75.44 on PASSIVE side	No	No	No
9	Apply surcharge no.4 at elev. 75.44	No	No	No
10	Install strut no.4 at elev. 76.25	No	No	No
11	Install strut no.6 at elev. 78.90	No	No	No
12	Remove strut no.3 at elev. 78.00	No	No	No
13	Install strut no.7 at elev. 81.65	No	No	No
14	Remove strut no.2 at elev. 82.00	No	No	No
15	Change soil type 1 to soil type 4	No	No	No
16	Change soil type 2 to soil type 5	No	No	No
17	Change soil type 3 to soil type 6	No	No	No
*	Summary output	Yes	-	Yes



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 Program: WALLAP Version 6.05 Revision A42.B57.R48 | Job No. J11251  
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 Data filename/Run ID: 59 Maresfield Gdns West Wall\_ULS2 |  
 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: ULS DA1 Combination 2  
 Water pressures : Worst Credible  
 Partial factor on C' = 1.250  
 Partial factor on Phi' = 1.250  
 Partial factor on Cu = 1.400  
 Partial factor on Soil Modulus = 1.000  
 Partial factor on Permanent Unfavourable loads = 1.000  
 Partial factor on Permanent Favourable loads = 1.000  
 Partial factor on Permanent Variable loads = 1.300

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

Stage No.	G.L.		Strut Elev.	Overall		Toe elev. for FoS = 1.000	Wall Penetration
	Act.	Pass.		Factor of Safety	Moment of equilib. at elev.		
1	82.00	82.00	Cant.	Conditions not suitable for FoS calc.			
2	82.00	81.50	Cant.	Conditions not suitable for FoS calc.			
3	82.00	81.50		No analysis at this stage			
4	82.00	81.50	82.00	13.014	n/a	81.49	0.01
5	82.00	77.50	82.00	1.967	n/a	75.86	1.64
6	82.00	77.50		No analysis at this stage			
All remaining stages have more than one strut - FoS calculation n/a							

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 59 Maresfield Gardens | Date:12-12-2012  
 West Wall | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 6.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: ULS DA1 Combination 2**

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	82.00	0.003	0.000	0.0	-0.0	0.0	-42.5
2	81.65	0.003	0.000	0.3	-14.8	1.8	-67.0
3	81.50	0.003	0.000	0.1	-21.2	0.7	-65.8
4	81.00	0.004	0.000	0.4	-41.5	0.0	-59.3
5	80.40	0.005	0.000	0.0	-73.1	0.0	-47.0
6	79.80	0.006	0.000	0.0	-96.4	0.0	-31.0
7	79.35	0.006	0.000	0.0	-105.7	0.0	-25.2
8	78.90	0.007	0.000	0.0	-107.5	16.9	-75.6
9	78.45	0.007	0.000	0.0	-111.0	6.2	-53.6
10	78.00	0.007	0.000	0.0	-125.2	31.3	-44.3
11	77.50	0.007	0.000	0.0	-132.0	62.5	-28.1
12	77.00	0.007	0.000	0.0	-122.6	97.3	-8.2
13	76.63	0.007	0.000	3.1	-108.0	125.6	0.0
14	76.25	0.007	0.000	55.7	-95.0	155.7	-116.3
15	76.00	0.007	0.000	29.2	-85.8	66.8	-95.3
16	75.44	0.007	0.000	8.8	-54.2	84.7	-30.7
17	75.00	0.007	0.000	13.2	-45.8	64.1	-20.7
18	74.40	0.006	0.000	26.7	-42.9	37.2	-7.0
19	73.95	0.006	0.000	37.3	-32.2	30.9	-1.9
20	73.50	0.006	0.000	41.2	-20.1	49.1	-2.8
21	73.05	0.006	0.000	40.6	-13.1	31.2	-7.2
22	72.60	0.006	0.000	36.2	-7.8	15.2	-12.4
23	72.00	0.005	0.000	27.9	-1.7	6.1	-17.7
24	71.40	0.005	0.000	16.5	0.0	2.3	-18.2
25	70.80	0.005	0.000	6.3	0.0	0.2	-13.7
26	70.40	0.005	0.000	2.0	0.0	0.0	-7.9
27	70.00	0.005	0.000	0.0	-0.0	0.0	-0.0

**Summary of results (continued)**

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev.	minimum kN.m/m	elev.	maximum kN/m	elev.	minimum kN/m	elev.
1	3.8	74.40	-1.9	78.45	3.5	76.00	-1.2	72.60
2	10.6	74.40	-3.3	78.00	9.0	76.00	-3.4	72.60
3	No calculation at this stage							
4	9.7	74.40	-3.1	78.00	8.3	76.00	-3.1	72.60
5	31.8	73.50	-111.0	78.45	66.8	76.00	-42.5	82.00
6	No calculation at this stage							
7	31.4	73.50	-110.6	78.45	66.4	76.00	-42.4	82.00
8	17.9	72.60	-102.3	77.00	61.7	75.44	-44.3	78.00
9	40.5	73.50	-113.7	77.00	84.7	75.44	-39.8	82.00
10	No calculation at this stage							
11	No calculation at this stage							
12	41.1	73.50	-121.9	77.50	82.6	75.44	-40.3	78.90
13	No calculation at this stage							
14	41.2	73.50	-123.1	77.50	82.3	75.44	-43.4	81.65
15	38.8	73.50	-132.0	77.50	94.9	76.25	-75.6	78.90
16	18.6	72.00	-110.4	78.00	132.5	76.25	-101.6	76.25
17	55.7	76.25	-109.8	78.45	155.7	76.25	-116.3	76.25

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum m	elev.	minimum m	elev.	
1	0.001	82.00	0.000	82.00	Apply surcharge no.3 at elev. 82.00
2	0.002	82.00	0.000	82.00	Excav. to elev. 81.50 on PASSIVE side
3	No calculation at this stage				Install strut no.2 at elev. 82.00
4	0.002	82.00	0.000	82.00	Apply water pressure profile no.2
5	0.006	78.00	0.000	82.00	Excav. to elev. 77.50 on PASSIVE side
6	No calculation at this stage				Install strut no.3 at elev. 78.00
7	0.006	78.00	0.000	82.00	Apply water pressure profile no.4
8	0.007	77.00	0.000	82.00	Excav. to elev. 75.44 on PASSIVE side
9	0.007	77.50	0.000	82.00	Apply surcharge no.4 at elev. 75.44
10	No calculation at this stage				Install strut no.4 at elev. 76.25
11	No calculation at this stage				Install strut no.6 at elev. 78.90
12	0.007	77.50	0.000	82.00	Remove strut no.3 at elev. 78.00
13	No calculation at this stage				Install strut no.7 at elev. 81.65
14	0.007	77.50	0.000	82.00	Remove strut no.2 at elev. 82.00
15	0.007	77.50	0.000	82.00	Change soil type 1 to soil type 4
16	0.007	77.50	0.000	82.00	Change soil type 2 to soil type 5
17	0.007	78.00	0.000	82.00	Change soil type 3 to soil type 6

**Summary of results (continued)**

**Strut forces at each stage (horizontal components)**

Stage no.	--- Strut no. 2 --- at elev. 82.00		--- Strut no. 3 --- at elev. 78.00		--- Strut no. 4 --- at elev. 76.25	
	kN/m run	kN/strut	kN/m run	kN/strut	kN/m run	kN/strut
4	slack	slack	---	---	---	---
5	42.52	255.10	---	---	---	---
7	42.41	254.47	0.35	2.10	---	---
8	33.89	203.36	58.61	351.64	---	---
9	39.84	239.02	39.49	236.93	---	---
12	37.88	227.27	---	---	14.87	14.87
14	---	---	---	---	16.64	16.64
15	---	---	---	---	68.92	68.92
16	---	---	---	---	234.18	234.18
17	---	---	---	---	272.08	272.08

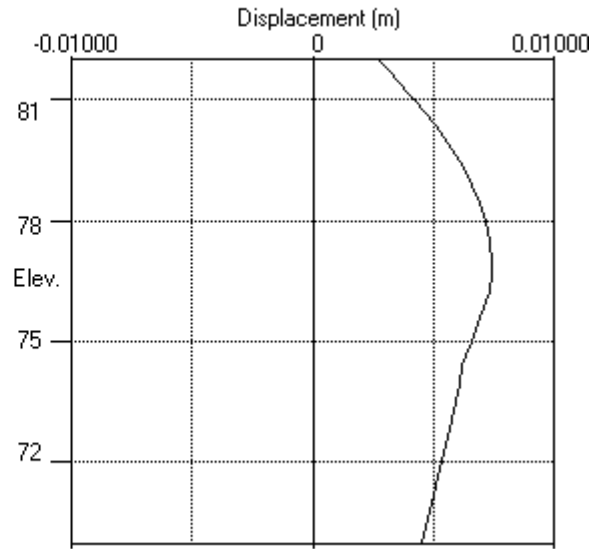
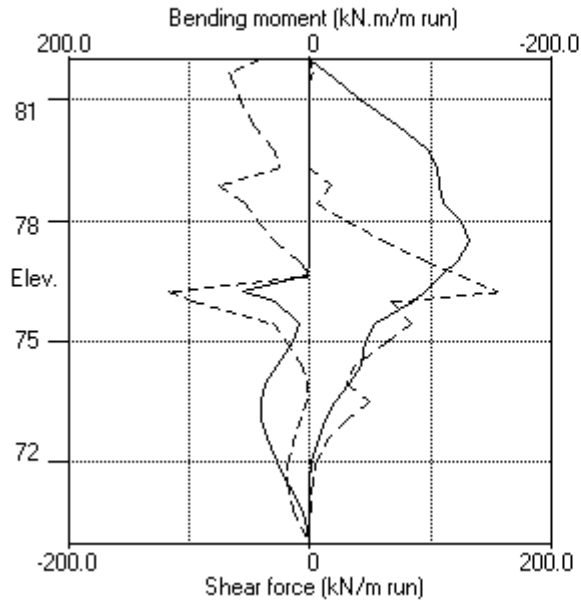
Stage no.	--- Strut no. 6 --- at elev. 78.90		--- Strut no. 7 --- at elev. 81.65	
	kN/m run	kN/strut	kN/m run	kN/strut
12	28.70	28.70	---	---
14	21.24	21.24	43.92	43.92
15	92.54	92.54	58.01	58.01
16	48.70	48.70	64.68	64.68
17	21.65	21.65	68.86	68.86

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59 Maresfield Gardens  
West Wall

| Sheet No.  
| Job No. J11251  
| Made by : MC  
| Date:12-12-2012  
| Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



## APPENDIX 5

### Soil Displacement Model Results



Maresfield Gardens  
 Final Run  
 MC

**Drng. Ref.**

**Made by** **Date** **Checked**  
**MP** **11-Dec-2012**

**Problem Type**

Problem Type : Tunnelling and Embedded Wall Excavations

**Displacement Data**

Type	Name	Direction of extrusion	Point/Line/Line for extrusion			No. of intervals across extrusion/line	Extrusion depth	No. of intervals along extrusion	Calculate	Surface type for tunnels			
			First point	Second point									
			X	Y	Z (level)	X	Y	Z (level)					
			[m]	[m]	[m]	[m]	[m]	[m]					
Line	Line 1	-	20.50000	20.00000	82.00000	37.00000	20.00000	82.00000	50	-	Yes	Sub-surface	
Grid	Grid 1	Global X	0.00000	0.00000	82.00000	-	40.00000	82.00000	50	60.00000	50	Yes	Sub-surface
Grid	Grid 2	Global Y	20.00000	20.00000	82.00000	37.00000	-	82.00000	10	3.00000	10	Yes	Sub-surface
Line	Line 2	-	25.00000	20.00000	82.00000	25.00000	10.00000	82.00000	10	-	-	Yes	Sub-surface
Line	Line 3	-	33.00000	20.00000	82.00000	33.00000	10.00000	82.00000	10	-	-	Yes	Sub-surface

**Vertical Ground Movement Curves**

**Curve Name:** Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))

**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (%) ]  
 [0.000,0.000,0.039][0.100,0.000,0.049][0.200,0.000,0.056][0.300,0.000,0.062]  
 [0.400,0.000,0.067][0.500,0.000,0.070][0.600,0.000,0.072][0.700,0.000,0.073]  
 [0.800,0.000,0.073][0.900,0.000,0.072][1.000,0.000,0.070][1.100,0.000,0.068]  
 [1.200,0.000,0.065][1.300,0.000,0.061][1.400,0.000,0.058][1.500,0.000,0.054]  
 [1.600,0.000,0.050][1.700,0.000,0.046][1.800,0.000,0.042][1.900,0.000,0.038]  
 [2.000,0.000,0.034][2.100,0.000,0.030][2.200,0.000,0.027][2.300,0.000,0.023]  
 [2.400,0.000,0.020][2.500,0.000,0.017][2.600,0.000,0.014][2.700,0.000,0.012]  
 [2.800,0.000,0.010][2.900,0.000,0.008][3.000,0.000,0.007][3.100,0.000,0.005]  
 [3.200,0.000,0.004][3.300,0.000,0.004][3.400,0.000,0.003][3.500,0.000,0.002]  
 [3.600,0.000,0.002][3.700,0.000,0.002][3.800,0.000,0.001][3.900,0.000,0.001]  
 [4.000,0.000,0.000]

**Curve Fitting:** Polynomial

**Method:**

**x Order:** 4

**y Order:** 0

**Polynomial:** z = -2.6455E-3x<sup>4</sup> + 2.8495E-2x<sup>3</sup> - 1.0051E-1x<sup>2</sup> + 1.0569E-1x + 3.8990E-2

**Coeff. of:** 9.9991E-1

**Determination:**

**Horizontal Ground Movement Curves**

**Curve Name:** Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))

**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (%) ]  
 [0.000,0.000,0.150][4.000,0.000,0.000]

**Curve Fitting:** Polynomial

**Method:**

**x Order:** 1

**y Order:** 0

**Polynomial:** z = -3.75E-2x + 1.50E-1

**Coeff. of:** 1.00

**Determination:**

**Polygonal Excavations**

**Excavation Name:** General Excavation

**Surface level [m]:** 82.000

**Contribution:** Positive

Corner	x	y	Base Level	Stiffened	Previous Side		Next Side	
					d	p1 p2*	d	p1 p2*
	[m]	[m]	[m]		[m]	[%]	[m]	[%]
1	20.500	20.500	76.000	No	-	-	-	-
2	20.500	27.500	76.000	No	-	-	-	-
3	37.000	27.500	76.000	No	-	-	-	-
4	37.000	20.500	76.000	No	-	-	-	-

Side	Corner 1		Corner 2		Vertical		Horizontal	
	x	y	x	y	d	p1 p2*	d	p1 p2*
	[m]	[m]	[m]	[m]	[m]	[%]	[m]	[%]
1	20.500	20.500	20.500	27.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
2	20.500	27.500	37.000	27.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
3	37.000	27.500	37.000	20.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
4	37.000	20.500	20.500	20.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	

**Excavation Name:** Pool Excavation

**Surface level [m]:** 84.000

**Contribution:** Positive

Corner	x	y	Base Level	Stiffened	Previous Side		Next Side	
					d	p1 p2*	d	p1 p2*
	[m]	[m]	[m]		[m]	[%]	[m]	[%]
1	31.500	20.500	74.000	No	-	-	-	-
2	31.500	27.500	74.000	No	-	-	-	-
3	37.000	27.500	74.000	No	-	-	-	-
4	37.000	20.500	74.000	No	-	-	-	-

Side	Corner 1		Corner 2		Vertical		Horizontal	
	x	y	x	y	d	p1 p2*	d	p1 p2*
	[m]	[m]	[m]	[m]	[m]	[%]	[m]	[%]
1	31.500	20.500	31.500	27.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
2	31.500	27.500	37.000	27.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
3	37.000	27.500	37.000	20.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
4	37.000	20.500	31.500	20.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	

**Excavation Name:** Upper Pool Excavation

**Surface level [m]:** 84.000

**Contribution:** Negative

Corner	x	y	Base Level	Stiffened	Previous Side		Next Side	
					d	p1 p2*	d	p1 p2*
	[m]	[m]	[m]		[m]	[%]	[m]	[%]
1	31.500	20.500	76.000	No	-	-	-	-
2	31.500	27.500	76.000	No	-	-	-	-



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**Maresfield Gardens**  
**Final Run**  
**MC**

**Dr. Ref.**

**Made by** **Date** **Checked**  
**MP** **11-Dec-2012**

Corner	x	y	Base Level	Stiffened	Previous Side	Next Side
	[m]	[m]	[m]		d	d
					p1	p1
					p2*	p2*
					[m]	[m]
					[%]	[%]
3	37.000	27.500	76.000	No	-	-
4	37.000	20.500	76.000	No	-	-

Side	Corner 1		Corner 2		Vertical		Horizontal	
	x	y	x	y	d	p1	d	p1
	[m]	[m]	[m]	[m]	[m]	[%]	[m]	[%]
1	31.500	20.500	31.500	27.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
2	31.500	27.500	37.000	27.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
3	37.000	27.500	37.000	20.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	
4	37.000	20.500	31.500	20.500	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))		Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))	

**Damage Category Strains**

Name	0 (Negligible)	1 (Very Slight)	2 (Slight)	3 (Moderate)
	to	to	to	to
	1 (Very Slight)	2 (Slight)	3 (Moderate)	4 (Severe)
Burland Strain Limits	0.0	500.00E-6	750.00E-6	0.0015000

**Specific Structures - Geometry**

Structure Name	Sub-Structure Name	Displacement Line	Start Distance Along Line	End Distance Along Line	Vertical Offsets from Line for Vertical Movement	Vertical Displacement Limit	Damage Category Strains	Poisson's Ratio	E/G
57 Maresfield	North Elevation	Line 1	4.50000	13.00000	0	0.10000	Burland Strain Limits	0.20000	2.6000
57 Maresfield	West Wall	Line 2	0.10000	9.00000	0	0.10000	Burland Strain Limits	0.20000	2.6000
57 Maresfield	East Wall	Line 3	0.10000	9.00000	0	0.10000	Burland Strain Limits	0.20000	2.6000

**Specific Structures - Bending Parameters**

Structure Name	Sub-Structure Name	Height	Default Properties	Hogging			Sagging		
				2nd Moment of Area (per unit width)	Distance of Bending from N.A.	Distance of N.A. from Edge of Beam in Tension	2nd Moment of Area (per unit width)	Distance of Bending from N.A.	Distance of N.A. from Edge of Beam in Tension
		[m]		[m <sup>3</sup> ]	[m]	[m]	[m <sup>3</sup> ]	[m]	[m]
57 Maresfield	North Elevation	10.000	Yes	333.33	10.000	10.000	83.333	5.0000	5.0000
57 Maresfield	West Wall	10.000	Yes	333.33	10.000	10.000	83.333	5.0000	5.0000
57 Maresfield	East Wall	10.000	Yes	333.33	10.000	10.000	83.333	5.0000	5.0000

**Building Segment Combinations**

Structure Name	Sub-Structure Name	Vertical Offsets from Line for Vertical Movement	Segment	Start	Length	Curvature	Combined Segment
		Calculations		[m]	[m]	[m]	
No structures have segments combined.							

**Warnings**

- Multiple excavations have been specified. The displacements resulting from these excavations are calculated by summing the displacements resulting from each individual excavation. No account has been taken of the interactions between excavations (e.g. overlapping zones of influence or 'shielding' of one excavation by another).
- Embedded Wall Excavation PE1 : General Excavation intersects PE2 : Pool Excavation, and PE3 : Upper Pool Excavation.
- Embedded Wall Excavation PE2 : Pool Excavation intersects PE1 : General Excavation.
- Embedded Wall Excavation PE3 : Upper Pool Excavation intersects PE1 : General Excavation.

**Displacement and Strain Results**

Type/No.	Coordinates			Displacements			Angle of Line		
Name	Dist.	x	y	z	x	y	z	Along the Perpendicular to Line	
	[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	to Line	
					[mm]	[mm]	[mm]	[°]	
Line 1	Line 1	20.50000	20.00000	82.00000	2.9969	8.9487	4.8841	2.9969	8.9487
		0.33000	20.83000	20.00000	82.00000	2.9967	8.9529	4.8485	2.9967
		0.66000	21.16000	20.00000	82.00000	2.9965	8.9574	4.8109	2.9965
		0.99000	21.49000	20.00000	82.00000	2.9963	8.9622	4.7715	2.9963
		1.32000	21.82000	20.00000	82.00000	2.9960	8.9673	4.7304	2.9960
		1.65000	22.15000	20.00000	82.00000	2.9957	8.9727	4.6877	2.9957
		1.98000	22.48000	20.00000	82.00000	2.9954	8.9785	4.6436	2.9954
		2.31000	22.81000	20.00000	82.00000	2.9950	8.9848	4.5982	2.9950
		2.64000	23.14000	20.00000	82.00000	2.9946	8.9916	4.5517	2.9946
		2.97000	23.47000	20.00000	82.00000	2.9942	8.9989	4.5041	2.9942
		3.30000	23.80000	20.00000	82.00000	2.9937	9.0069	4.4558	2.9937
		3.63000	24.13000	20.00000	82.00000	2.9931	9.0156	4.4069	2.9931
		3.96000	24.46000	20.00000	82.00000	2.9925	9.0250	4.3574	2.9925
		4.29000	24.79000	20.00000	82.00000	2.9917	9.0354	4.3078	2.9917
		4.62000	25.12000	20.00000	82.00000	2.9908	9.0469	4.2580	2.9908
		4.95000	25.45000	20.00000	82.00000	2.9898	9.0596	4.2084	2.9898
		5.28000	25.78000	20.00000	82.00000	2.9886	9.0737	4.1592	2.9886
		5.61000	26.11000	20.00000	82.00000	2.9872	9.0896	4.1105	2.9872
		5.94000	26.44000	20.00000	82.00000	2.9855	9.1075	4.0625	2.9855
		6.27000	26.77000	20.00000	82.00000	2.9834	9.1279	4.0156	2.9834
		6.60000	27.10000	20.00000	82.00000	2.9808	9.1512	3.9700	2.9808
		6.93000	27.43000	20.00000	82.00000	2.9776	9.1783	3.9259	2.9776
		7.26000	27.76000	20.00000	82.00000	2.9735	9.2100	3.8835	2.9735
		7.59000	28.09000	20.00000	82.00000	2.9683	9.2477	3.8432	2.9683
		7.92000	28.42000	20.00000	82.00000	2.9612	9.2932	3.8051	2.9612
		8.25000	28.75000	20.00000	82.00000	2.9516	9.3492	3.7696	2.9516
		8.58000	29.08000	20.00000	82.00000	2.9379	9.4195	3.7370	2.9379
		8.91000	29.41000	20.00000	82.00000	2.9177	9.5105	3.7074	2.9177
		9.24000	29.74000	20.00000	82.00000	2.8858	9.6323	3.6814	2.8858
		9.57000	30.07000	20.00000	82.00000	2.8319	9.8027	3.6590	2.8319
		9.90000	30.40000	20.00000	82.00000	2.7311	10.054	3.6407	2.7311
		10.23000	30.73000	20.00000	82.00000	2.5161	10.446	3.6267	2.5161
		10.56000	31.06000	20.00000	82.00000	1.9819	11.065	3.6175	1.9819
		10.89000	31.39000	20.00000	82.00000	0.64459	11.742	3.6132	0.64459
		11.22000	31.72000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		11.55000	32.05000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		11.88000	32.38000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		12.21000	32.71000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		12.54000	33.04000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		12.87000	33.37000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		13.20000	33.70000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		13.53000	34.03000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		13.86000	34.36000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		14.19000	34.69000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		14.52000	35.02000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		14.85000	35.35000	20.00000	82.00000	0.0	11.813	3.6129	0.0
		15.18000	35.68000	20.00000	82.00000	0.0	11.813	3.6129	0.0





GEA LIMITED

(GEOTECHNICAL & ENV ASSOQ) J1251

Maresfield Gardens

Final Run

MC

Job No. Sheet No. Rev.

Drg. Ref.

Made by Date Checked
MP 11-Dec-2012

Table with columns: Type/No., Name, Dist., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line, and various numerical values for grid points.



GEA LIMITED
(GEOTECHNICAL & ENV ASSOQ) J1251

Job No. Sheet No. Rev.

Dr. Ref.

Made by Date Checked
MP 11-Dec-2012

Maresfield Gardens
Final Run
MC

Table with columns: Type/No., Name, Dist., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line (Along the Perpendicular to Line, to x Axis, to Line). Contains 26 rows of data.



















GEA LIMITED
(GEOTECHNICAL & ENV ASSOCIATES)
JOB J1251

Job No. Sheet No. Rev.

Drg. Ref.

Made by Date Checked
MP 11-Dec-2012

Maresfield Gardens
Final Run
MC

Table with columns: Type/No., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line (Along the Perpendicular to x Axis, to Line). Contains numerical data for various points and notes such as 'Point lies within an excavation.'





GEA LIMITED
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Job No. Sheet No. Rev.

Dr. Ref.

Made by Date Checked
MP 11-Dec-2012

Maresfield Gardens
Final Run
MC

Table with columns: Type/No., Name, Dist., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line, and text descriptions of points within excavations.



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Maresfield Gardens
Final Run
MC

Drg. Ref.

Made by
MP

Date
11-Dec-2012

Checked

Table with columns: Type/No., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line (Along the Perpendicular to Line, to Line). Contains multiple rows of numerical data for various points.



GEA LIMITED
(GEOTECHNICAL & ENV ASSOQ) J1251

Job No. Sheet No. Rev.

Dr. Ref.

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MP 11-Dec-2012

Maresfield Gardens
Final Run
MC

Table with columns: Type/No., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line, and Along the Perpendicular to Line. Contains a large list of numerical data points.



GEA LIMITED
(GEOTECHNICAL & ENV ASSO) J11251

Job No. Sheet No. Rev.

Dr. Ref.

Made by MP

Date 11-Dec-2012

Checked

Maresfield Gardens
Final Run
MC

Table with columns: Type/No., Name, Dist., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line, and Along the Perpendicular to Line. It contains a large grid of numerical data points.



GEA LIMITED
(GEOTECHNICAL & ENV ASSO) Q11251

Job No. Sheet No. Rev.

Maresfield Gardens
Final Run
MC

Drq. Ref.

Made by Date Checked
MP 11-Dec-2012

Table with columns: Type/No., Name, Dist., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line, and Along the Perpendicular to Line. Contains numerical data for points 24.00000 to 8.40000.











Maresfield Gardens
Final Run
MC

Dr. Ref.

Made by
MP

Date
11-Dec-2012

Checked

Table with columns: Type/No., Name, Dist., Coordinates (x, y, z), Displacements (x, y, z), Angle of Line, and Perpendicular to Line. Contains data for Line 1 and Line 2.

Specific Building Damage Results - Horizontal Displacements

Table with columns: Dist., Coordinates (x, y, z), Displacements (x, y, z), Perpendicular to Line. Includes sub-headers for 'Structure: 57 Maresfield Sub-structure: North Elevation' and 'Structure: 57 Maresfield Sub-structure: West Wall'.



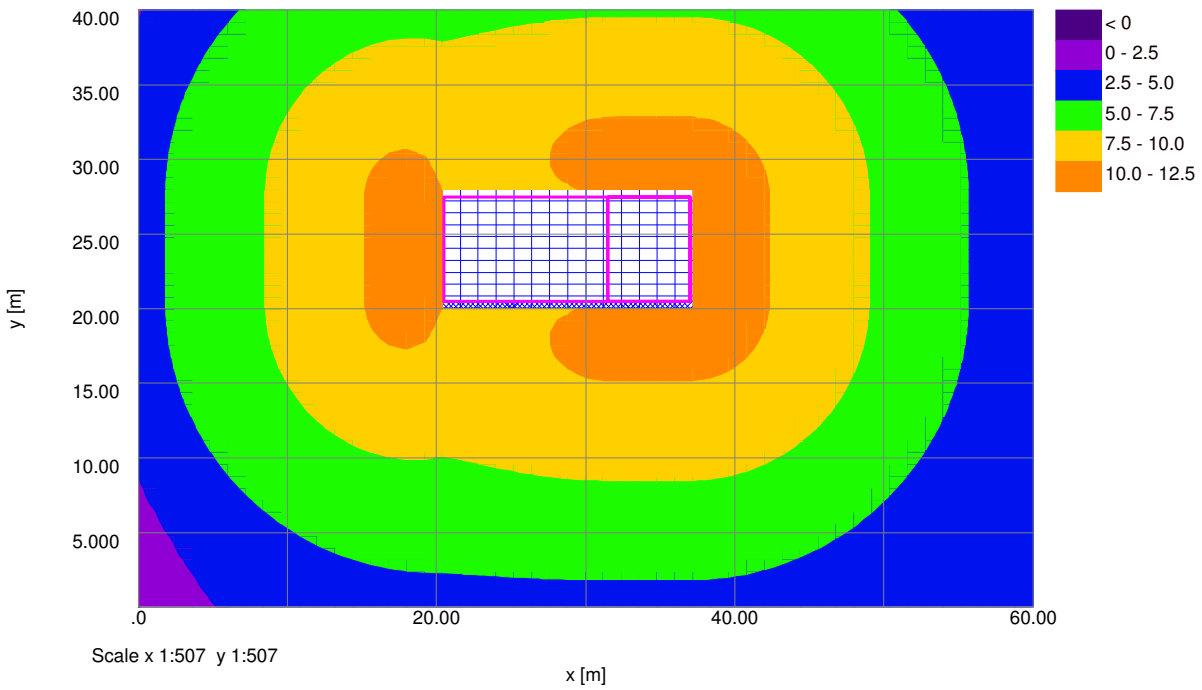
Maresfield Gardens  
 Final Run  
 MC

Structure Name	Sub-Structure Name	Vertical Offsets from Line for Vertical	Deflection Ratio	Average Horizontal Strain	Maximum Slope	Maximum Settlement	Max. Tensile Strain	Maximum Gradient of Horizontal Displacement	Maximum Gradient of Vertical Displacement (Hogging)	Min. Radius of Curvature (Hogging)	Min. Radius of Curvature (Sagging)	Damage Category
57 Maresfield	Maximum Slope	East Wall	1	0.0	8.9000	Sagging	791.88E-6	5.5840	0.054002	-	3945.2	1 (Very Slight)
	Maximum Settlement	West Wall	1	0.0	8.9000	Sagging	769.99E-6	6.0345	0.029688	-	3687.3	0 (Negligible)
	Max. Tensile Strain	East Wall	1	0.0	8.9000	Sagging	791.88E-6	5.5840	0.054002	-	3945.2	1 (Very Slight)
	Min. Radius of Curvature (Hogging)	North Elevation	1	0.0	7.3800	Hogging	150.74E-6	4.2761	0.0082106	23304.	-	0 (Negligible)
	Min. Radius of Curvature (Sagging)	West Wall	1	0.0	8.9000	Sagging	769.99E-6	6.0345	0.029688	-	3687.3	0 (Negligible)

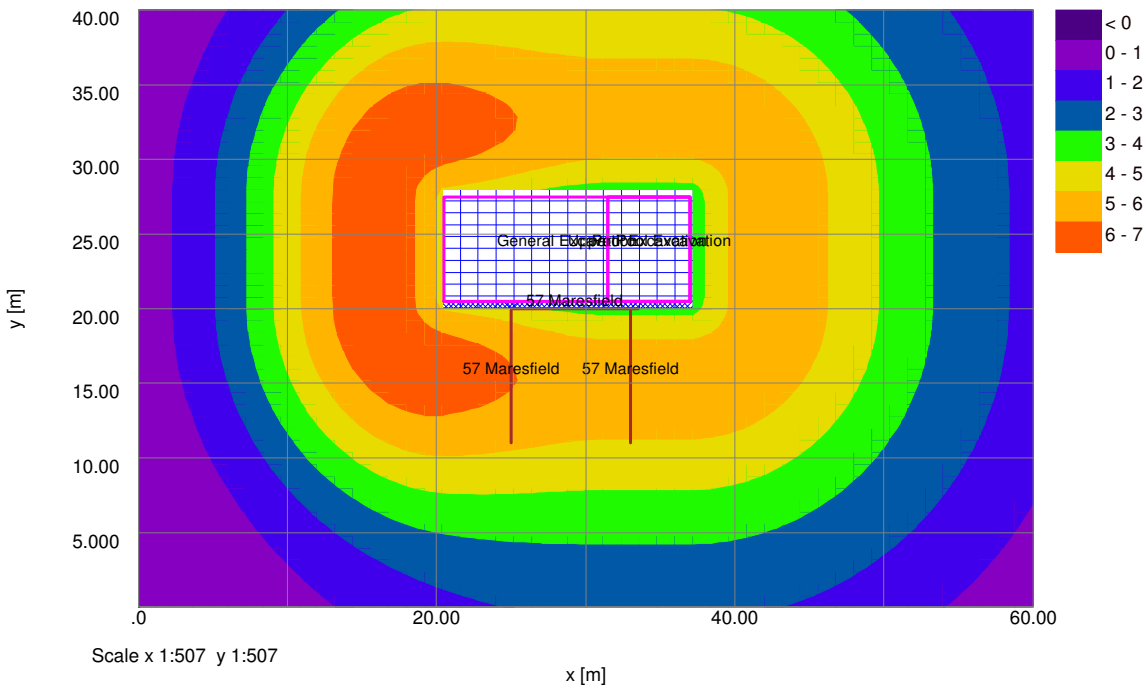
**Specific Building Damage Results - All Combined Segments**

Structure Name	Sub-Structure Name	Vertical Offsets from Line for Vertical Movement Calculations	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max. Tensile Strain	Damage Category
No structures have segments combined.										

Horizontal Displacement Contours: Grid 1 (level 82.000m) Interval 2.5mm



Vertical Settlement Contours: Grid 1 (level 82.000m) (Interval 1mm)





Geotechnical & Environmental Associates (GEA) is an engineer-led and client-focused independent specialist providing a complete range of geotechnical and contaminated land investigation, analytical and consultancy services to the property and construction industries.

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