

10 GATE STREET, LONDON

Plant Noise Assessment

REPORT 5579/PNA Prepared: 12 July 2013 Revision Number: 0

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Revision	Comment	Date	Prepared By	Approved By
0	First issue of report	12 July 2013	Mike Fuller	Russell Richardson

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### 1.0 INTRODUCTION

It is proposed to install a new restaurant kitchen extract fan at 10 Gate Street, London. Camden Council requires consideration be given to atmospheric noise emissions from the proposed equipment at the nearest noise-sensitive windows of the development and for a plant noise impact assessment to be submitted in support of the planning application.

RBA Acoustics have been commissioned to undertake measurements of the prevailing noise conditions at the site and to determine the atmospheric noise emissions in accordance with Camden Council's requirements. This report presents the results of the noise measurements, associated criteria and provides the required assessment.

### 2.0 ENVIRONMENTAL NOISE SURVEY

#### 2.1 General

In accordance with the requirements of the Local Authority, monitoring of the prevailing background noise was undertaken over the following periods:

Wednesday 29 May to Thursday 30 May 2013

During the survey periods the weather conditions were generally appropriate for the noise measurement exercise, it being dry with light winds.

Measurements were made of the  $L_{A90},\ L_{AMax}$  and  $L_{Aeq}$  noise levels over sample periods of 15 minutes duration.

### 2.2 Measurement Locations

#### Position 1

Measurements were undertaken with the microphone positioned 1m outside a fourth floor window on the western façade of the building. The noise climate at this location was considered to be representative of the windows of the new flats on the floors above, there being the closest residential windows to the proposed plant discharge location at roof level. The prevailing noise climate was noted to be affected predominantly by road traffic noise from the Kingsway and High Holborn thoroughfares and noise from the existing plant of the surrounding buildings.

The measurement position is also illustrated on the attached Site Plan 5579/SP1.

#### 2.3 Instrumentation

			Table 5579/T1	– Equipment Details	
Manufacturer	Madal Tura		Calibration		
Manufacturer	Model Type	Serial No.	Certificate No.	Expiry Date	
01dB A&V Type 1 Sound Level Meter	Black Solo 01	60610	CE-DTE-T-12-	7 December 2014	
01dB A&V Pre Amplifier	PRE 21 S	13676	PVE-64835	7 December 2014	
Gras ½" Microphone	MCE 212	84948			
01dB-Stell Calibrator	Cal 21	50441910	U12030	13 September 2014	

The following equipment was used for the measurements.

The sound level meter was calibrated both prior to and on completion of the survey with no calibration drift observed.

### 3.0 OPERATING HOURS

We understand the restaurant's opening hours are to be the same as existing, the longest of which are 12:00 to 23:30 hours, Monday to Saturday and the plant will be operating during these hours only. Therefore these hours have been used in our assessment.

### 4.0 RESULTS

The noise levels at the measurement positions are shown as time-histories on the attached charts 5579/G1 and 5579/G2

In order to ensure a worst-case assessment the lowest background LA90 noise levels measured have been used in our analyses. The lowest LA90 and the period averaged LAeq dB noise levels measured are summarised below.

Measurement Period	Position 1				
	L90 (dBA)	L <sub>eq</sub> (dBA)			
Daytime (07:00 – 23:00)	57	62			
Night-time (23:00 – 07:00)	54	59			
Operating Hours (12:00 – 23:30)	56	62			

### 5.0 CRITERIA

#### 5.1 Camden Council LDF

There are no specific numerical criteria within the pre-application advice document (Ref: SJH/JGP/DP3030 dated 20/12/12). From previous experience, the requirements of Camden Council are set out in their Local Development Framework (LDF) in Table E of DP28. Noise levels from new plant and machinery are confirmed as follows.

Table 557	9/T3 – Camden	Council Noise	Thresholds

Noise description and Location of measurement	Period	Time	Noise Level
Noise at 1 metre external to a sensitive façade	Day, evening and night	00:00-24:00	5dB(A) <lago< td=""></lago<>
Noise that has a distinguishable discrete continuous note (whine, hiss, screech, hum) at 1 metre external to a sensitive façade	Day, evening and night	00:00-24:00	10dB(A) <lago< td=""></lago<>
Noise that has distinct impulses (bangs, clicks, clatters, thumps) at 1 metre external to a sensitive façade	Day, evening and night	00:00-24:00	10dB(A) <lago< td=""></lago<>
Noise at 1 metre external to sensitive façade where LA90 >60dB	Day, evening and night	00:00-24:00	55dB LAeq

A comparison to the results shown in Table 5579/T2 and the Camden Council requirements in Table 5579/T3 indicates a plant noise emission limit of 5dB below the lowest measured LA90 level is applied.

In line with the above requirements we would propose items of mechanical services be designed so that cumulative atmospheric noise emissions from the plant discharge and breakout noise from the ducts do not exceed the following levels when assessed at the nearest noise sensitive location:

Operating Hours (12:00 - 23:30)
LAeq 51 dB

In line with the requirements of the Local Authority and BS 4142, should the proposed plant be identified as having intermittent or tonal characteristics, a further 5dB should be subtracted from any of the above proposed noise emission limits.

### 6.0 ASSESSMENT OF ATMOSPHERIC NOISE

Our assessment has been based upon the following information:

#### 6.1 Proposed Air Conditioning Unit

1No. Elta SLC 450/2-1AC Axial Fan

#### 6.2 Position of Units/Duct Dimensions

The equipment is to be located within the extract canopy of the restaurant kitchen and ducted externally, discharging at roof level. The duct is to comprise a 450mm diameter round duct, which is to run horizontally for approximately 3m internally before turning vertically and running externally adjacent to the stair-core up the building, to roof level.

#### 6.3 Noise Levels

Octave band sound power data for the proposed extract fan is not available from the manufacturer; however, duty information has been supplied, given below:

- Volume Flow Rate: 2.62 m<sup>3</sup>/s
- Static Pressure: 171 Pa

This duty information has been used to calculate empirical in-duct sound power levels for use in the assessment, as shown in Table 5579/T4:

					Table 55	79/T4 – N	lanufactu	ırer's Noi	se Levels
Unit	Daramatar	Sound Power Level (dB) at Octave Band Centre Frequency (Hz)							
Onit	Parameter	63	125	250	500	<u>1k</u>	<u>2k</u>	<u>4k</u>	<u>8k</u>
Elta SLC 450/2-1AC	Empir. Induct L <sub>w</sub>	80	81	83	82	81	78	75	70

Review of the octave band data indicates there are no tonal characteristics associated with the proposed plant. Comparison of the empirical noise levels to manufacturer's data of similar type fans indicates this spectrum is typical.

#### 6.4 Location of Nearest Residential Windows

The worst-affected residential windows to the plant are considered to belong to the fifth and sixth floor of the development on the western façade (shown on the attached Figures 5579/FP1 & 5579/FP2 and Elevation 5579/E), the closest of which is approximately 2.7m below the discharge location.

#### 6.5 Calculation of Noise Levels at Nearest Residential Window

Our calculation method for predicting noise levels from the proposed restaurant extract unit at the nearest residential window, based on the information stated above, is summarised below.

- Source Term In-duct SWL
- Duct Losses
- Grille End Reflections
- 20LogR Distance Attenuation
- Directivity
- Reflections
- Noise Control Measures

Screening via the building has not been included in this calculation in order to account for a worst-case assessment. Calculation sheets are attached for further information in Appendix B.

The results of the calculations indicate the following noise levels at the worst affected residential windows:

Table 5579/T5 – Measured Levels

Operating Derived	Fifth Floor Windows			
Operating Period	Prediction	Criterion		
Operating Hours (12:00 – 23:30)	62	51		

Noise from the unattenuated kitchen extract fan unit is above the target criterion. Therefore additional noise mitigation measures are required.

#### 6.6 Mitigation

We recommend that the kitchen extract fan is fitted with an attenuator within the building before the ductwork rises externally up the building (to also reduce any potential breakout noise to the flat windows assessed in further in Section 7.0). The attenuator should be capable of achieving the performance levels detailed in the Table 5579/T6 below. An example attenuator capable of achieving this performance level is the manufacturer's (Elta's) 1D-EP model.

Table 5579/T6 – Required Attenuator Insertion Loss

Insertion Loss (dB) at Octave Band Centre Frequency (Hz)							
63	125	250	500	1k	2k	4k	8k
-4	-6	-8	-11	-18	-19	-17	-14

Adoption of an attenuator achieving the above insertion loss values would ensure that noise levels at the closest residential windows (of the fifth floor flat) are within the criterion. Noise levels will also therefore be acceptable at the closest residential windows not part of this development. Furthermore, the inevitable screening to the windows of the western façade will likely further reduce noise levels.

### 7.0 ASSESSMENT OF BREAK-OUT NOISE TO FLATS

Our assessment of noise break-out from the ductwork to the new flats has been based upon the information detailed in Section 6.0 above and the following further information:

#### 7.1 Proposed Duct and Other Constructions

The duct is to be of galvanised steel and round (450mm in diameter). The duct is to be concealed behind a perforated metal grid, the transmission loss of which is considered to be negligible

#### 7.2 Noise Levels

Extract fan noise levels are as detailed in Section 6.3.

#### 7.3 Location of Nearest Residential Windows

The closest noise-sensitive residential windows of the flats on the western façade of the same building are approximately 2m horizontally from the ductwork, shown on the attached Figures 5579/FP1 & 5579/FP2.

#### 7.4 Breakout Noise Emissions Criterion

In order to ensure the cumulative plant noise level does not exceed the criterion of 51dBA L<sub>eq</sub> at the worst affected residential windows (the fifth floor windows), breakout noise should not exceed 43dBA L<sub>eq</sub> at this location, if an attenuator is fitted achieving the performance outlined in Section 6.6.

#### 7.5 Calculation of Noise Levels at Nearest Residential Window

Our calculation method for predicting noise levels at the residential windows due to breakout noise from the proposed restaurant extract ductwork, based on the information stated above, is summarised below.

- Source Term in-duct SWL
- Attenuator insertion loss meeting performance requirements detailed in Section 6.6
- Duct Losses
- Transmission Loss of Duct
- 10log(S/A) duct radiation area correction
- 10log(Q/S) Line Source Attenuation (where Q =2 for hemispherical radiation)
- Screening via the building

Calculation sheets are attached for further information in Appendix B.

The results of the calculations indicate the following noise levels at the windows of the worst affected bedrooms:

Table 5579/T7 – Measured Levels

Operating Desired	Fifth Floor Windows				
Operating Period	Prediction	Criterion			
Operating Hours (12:00 – 23:30)	39 dBA	43 dBA			

Break-out noise from the ductwork to the flats meets the target criterion, ensuring cumulative plant noise emissions do not exceed 51dBA at any noise-sensitive windows, providing an attenuator achieving the outlined performance in Section 6.6 is fitted before the duct rises externally up the building façade, to the atmospheric side of the extract fan. Doing so will ensure breakout noise levels from the plant ductwork are within the proposed criteria at any of the windows of the western façade of the same building.

### 8.0 VIBRATION CONTROL

In addition to the control of airborne noise transfer, it is also important to consider the transfer of noise as vibration to flats above the kitchen extract location in the same building.

We would typically advise that the extract fan be isolated from the supporting structure by means of either steel spring isolators or rubber footings. For particularly sensitive locations, or when on lightweight structures the mounts should ideally be caged and be of the restrained type.

It is important the isolation is not "short-circuited" by associated pipework or conduits. To this end, any conduits should be looped and flexible connectors should be introduced between the condenser and any associated pipework. Pipework should be supported by brackets containing neoprene inserts.

### 9.0 CONCLUSION

Measurements of the existing background noise levels at 10 Gate Street, London have been undertaken. The results of the measurements have been used in order to determine the required criteria for atmospheric noise emissions from the future plant installations.

The results of the assessment indicate atmospheric plant noise emissions and atmospheric break-out noise from the plant and ductwork are within the proposed criterion.

As such, noise emissions from the proposed plant installations should be considered acceptable and, subject to the inclusion of attenuation to the kitchen extract fan, will be in compliance with the guidelines set out under policy DP28 for noise emissions.

### Appendix A - Acoustic Terminology

dB	Decibel - Used as a measurement of sound pressure level. It is the logarithmic ratio of
	the noise being assessed to a standard reference level.

- dB(A) The human ear is more susceptible to mid-frequency noise than the high and low frequencies. To take account of this when measuring noise, the 'A' weighting scale is used so that the measured noise corresponds roughly to the overall level of noise that is discerned by the average human. It is also possible to calculate the 'A' weighted noise level by applying certain corrections to an un-weighted spectrum. The measured or calculated 'A' weighted noise level is known as the dB(A) level. Because of being a logarithmic scale noise levels in dB(A) do not have a linear relationship to each other. For similar noises, a change in noise level of 10dB(A) represents a doubling or halving of subjective loudness. A change of 3dB(A) is just perceptible.
- Leq Leq is defined as a notional steady sound level which, over a stated period of time, would contain the same amount of acoustical energy as the actual, fluctuating sound measured over that period (1 hour).
- LAeq The level of notional steady sound which, over a stated period of time, would have the same A-weighted acoustic energy as the A-weighted fluctuating noise measured over that period.
- LAn (e.g LA10, LA90) If a non-steady noise is to be described it is necessary to know both its level and the degree of fluctuation. The Ln indices are used for this purpose, and the term refers to the level exceeded for n% of the time, hence L10 is the level exceeded for 10% of the time and as such can be regarded as the 'average maximum level'. Similarly, L90 is the average minimum level and is often used to describe the background noise.
- Lmax,T The instantaneous maximum sound pressure level which occurred during the measurement period, T. It is commonly used to measure the effect of very short duration bursts of noise, such as for example sudden bangs, shouts, car horns, emergency sirens etc. which audibly stand out from the general level of, say, traffic noise, but because of their very short duration, maybe only a very small fraction of a second, may not have any effect on the Leq value.

### Appendix B – Plant calculations

Received Atmospheric Noise Levels Summary at Fifth Floor Windows											
Factor	63	125	250	500	1k	2k	4k	8k	dBA		
Elta SLC 450/2-1AC (Empir. In-duct L <sub>w</sub> )	80	81	83	82	81	78	75	70			
Duct Losses	-1	-1	-1	-1	-2	-2	-2	-2			
Grille End Reflection	-9	-5	-2	0	0	0	0	0			
Distance Loss (20logR, where R=2.7)	-9	-9	-9	-9	-9	-9	-9	-9			
Directivity	0	-1	-1	-3	-6	-9	-8	-8			
Hemispherical Radiation -11	-8	-8	-8	-8	-8	-8	-8	-8			
Total Received level without attenuator	53	57	62	62	56	51	48	43	62		
Required Attenuator Insertion Loss	-4	-6	-8	-11	-18	-19	-17	-14			
Total Received Level with Example attenuator (dB)*	49	51	54	51	38	32	31	29	50		

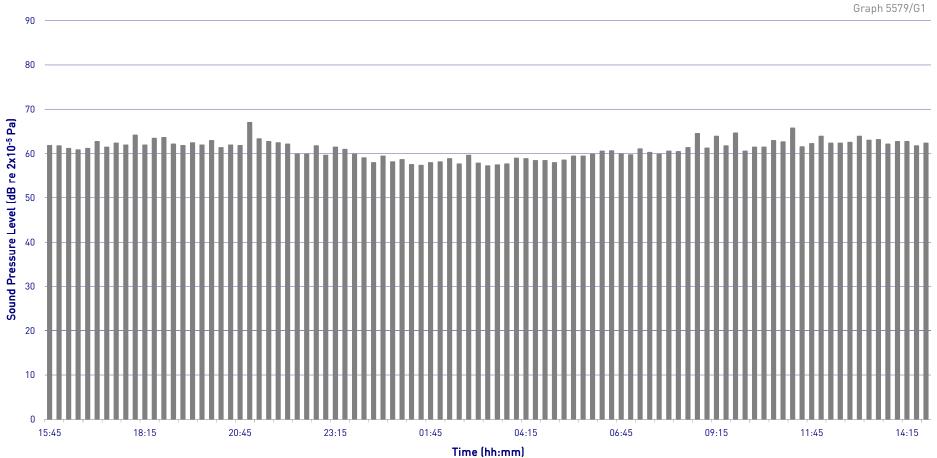
### Received Atmospheric Noise Levels Summary at Fifth Floor Windows

Please note:- No rounding has been applied in the calculation until the final received noise level. Rounded noise levels are given here for clarity only.

	Wed Breakout Noise Levets Summary at Finth Floor Windows								
Factor	63	125	250	500	1k	2k	4k	8k	dBA
Elta SLC 450/2-1AC (Empir. In-duct L <sub>w</sub> )	81	78	85	82	85	83	80	76	
Duct Losses	-1	-1	-1	-1	-2	-2	-2	-2	
Required Attenuator Insertion Loss for Atmospheric Noise	-4	-6	-8	-11	-18	-19	-17	-14	
Duct Transmission Loss (450mm round long seam duct)	-47	-53	-37	-33	-33	-27	-25	-23	
10Log(S/A)	16	16	16	16	16	16	16	16	
Radiated Lw from ductwork is therefore:	45	34	55	52	48	51	52	53	
10Log(Q/S) Attenuation (where Q=2, r=2m)	-14	-14	-14	-14	-14	-14	-14	-14	
Line of sight screening	-5	-5	-5	-5	-5	-5	-5	-5	
Total Received Level (dB)*	26	15	36	33	29	32	33	34	39

#### Received Breakout Noise Levels Summary at Fifth Floor Windows

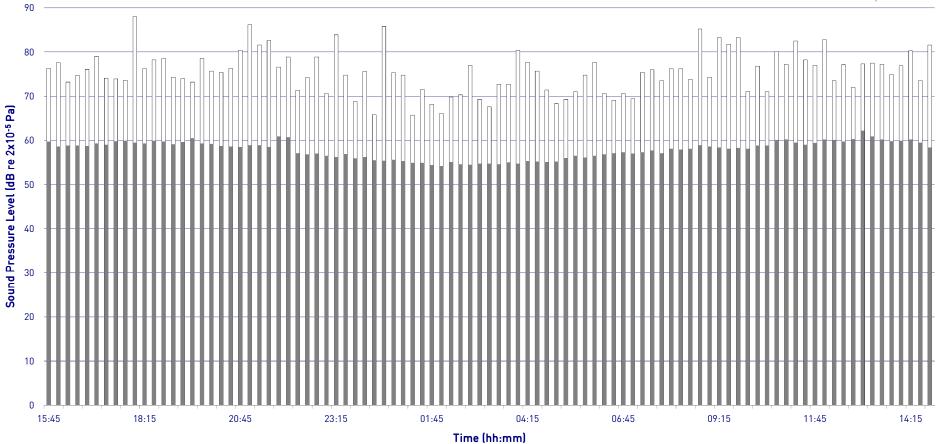
Please note:- No rounding has been applied in the calculation until the final received noise level. Rounded noise levels are given here for clarity only. 10 Gate Street, London WC2A L<sub>Aeq</sub> Time History - Position 1 Monday 29 April to Tuesday 30 April 2013



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LAeq

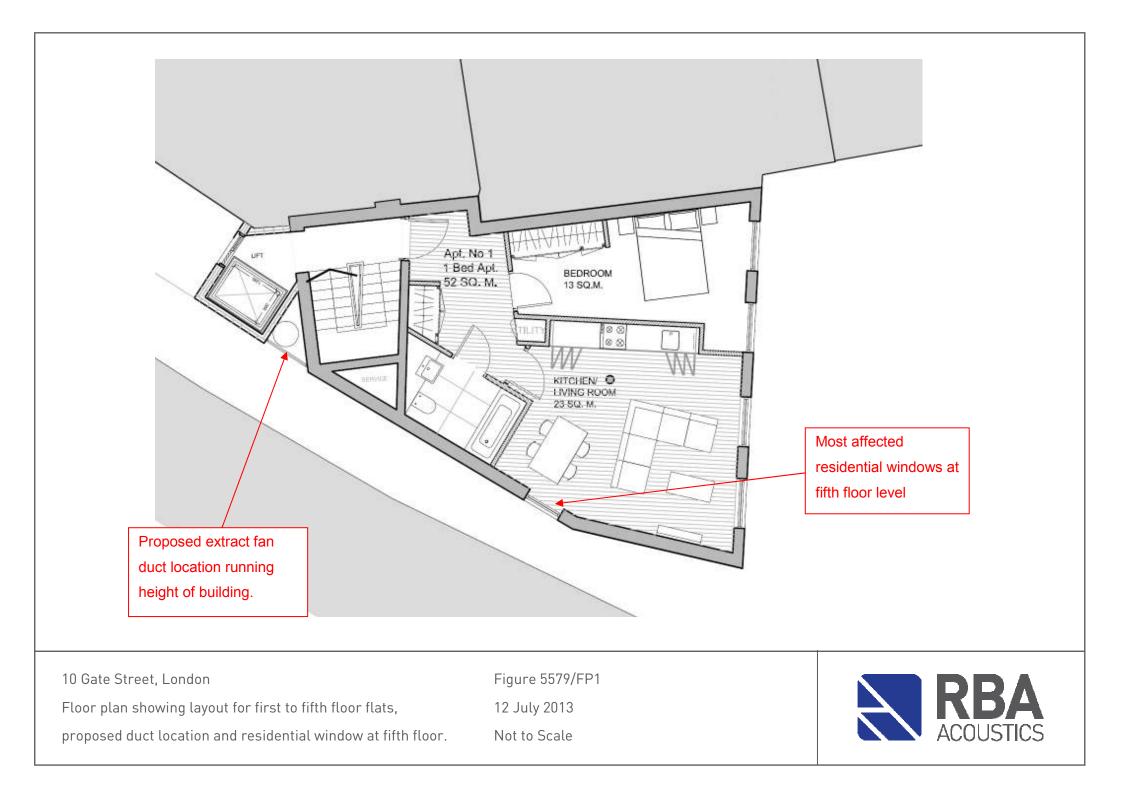
10 Gate Street, London WC2A L<sub>A90</sub> and L<sub>Amax</sub> Time History - Position 1 Monday 29 April to Tuesday 30 April 2013

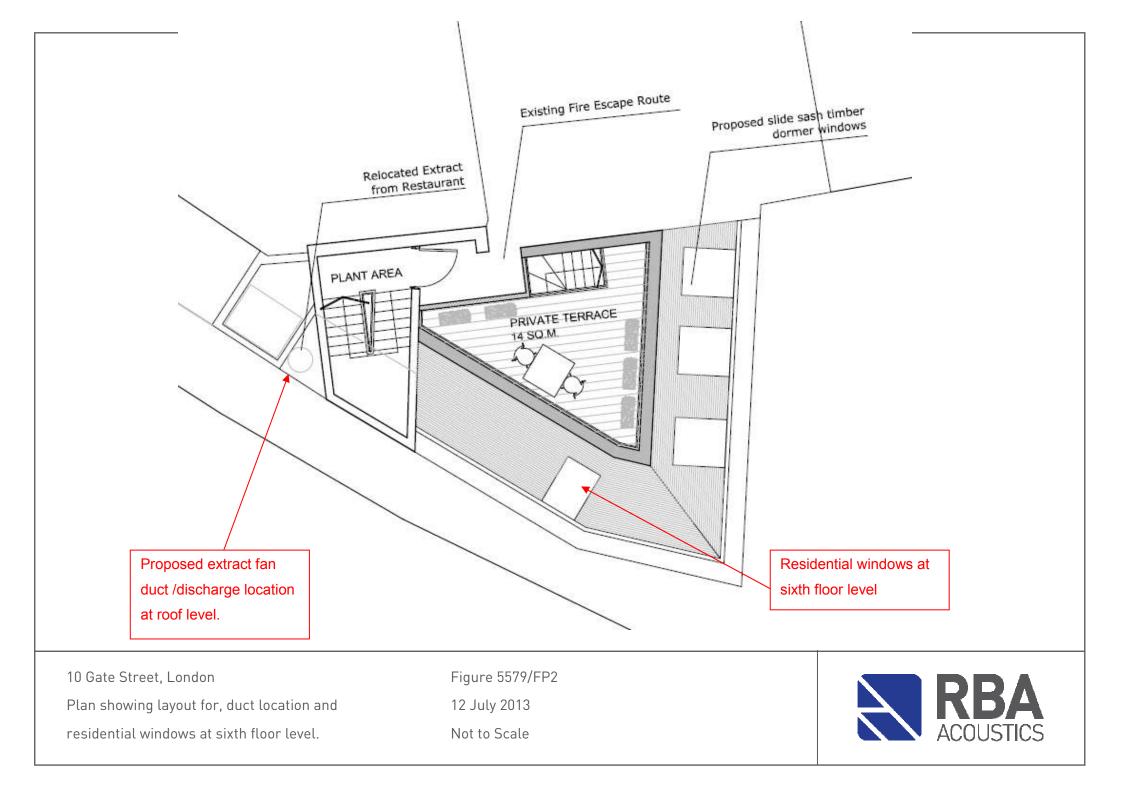


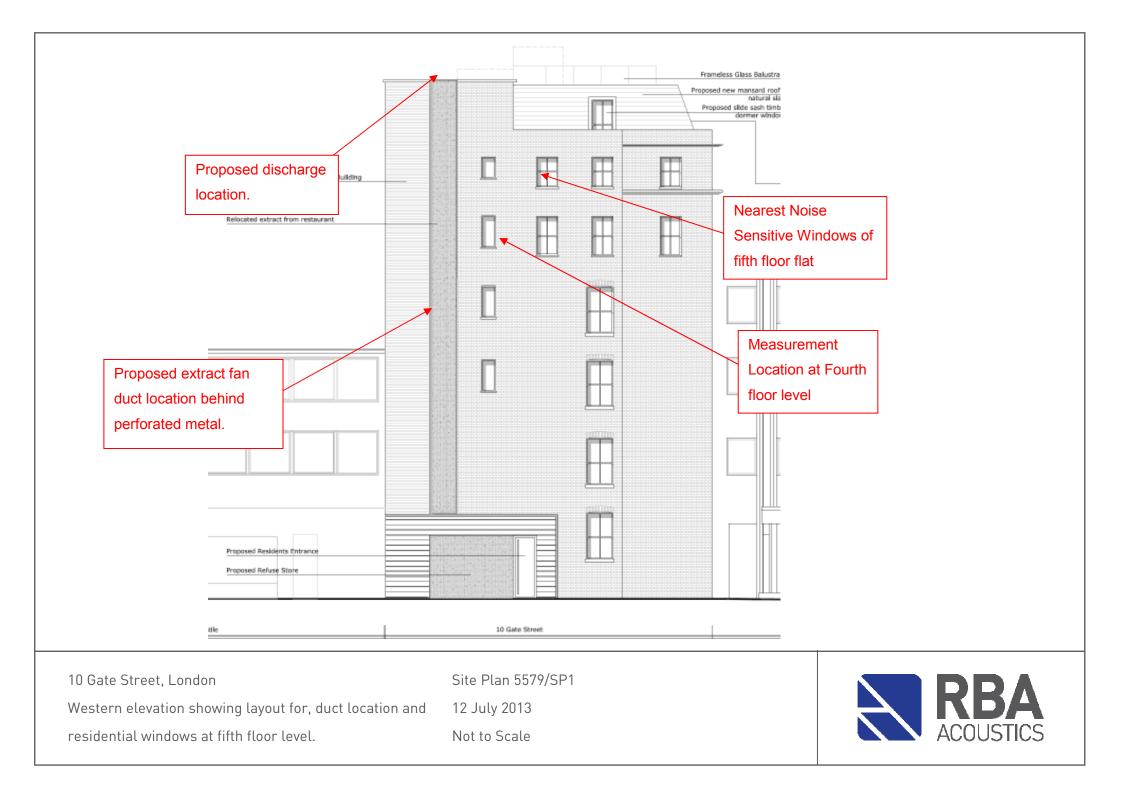


Graph 5579/G2

□LAmax ■LA90







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