

# 112 – 116 New Oxford Street



Planning Application Design Document

September 2013



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## 2.0 : Site Location

### Site Description and its Surroundings

2.1 The site is located on New Oxford Street, in Central London and lies within the London Borough of Camden.

2.2 The property is located on the corner junction of Bainbridge Street, and New Oxford Street, with the main frontage being towards the A40 New Oxford Street. The location of the site in relation to the junction is shown on the aerial photograph.

2.3 The site is accessed via both New Oxford Street and Bainbridge Street.

2.4 The property is the first of a terrace. The terrace fronts New Oxford Street, and runs continuously to Fairgate House at Dyott Street. The properties are all constructed of a similar light stone, with grand arched windows. The terrace, excluding the subject site, has additional floors at roof level, which have been constructed from more modern building materials.

2.5 New Oxford Street has a wide range of uses, ground floor uses are predominantly retail creating a vibrant active frontage at this location with predominantly secondary office accommodation to upper levels. The adjoining terrace and immediate environment predominantly comprises retail and office uses. To the east of the site is Holborn and to the west lies the bustling Tottenham Court Road with the Dominion Theatre to the East side.

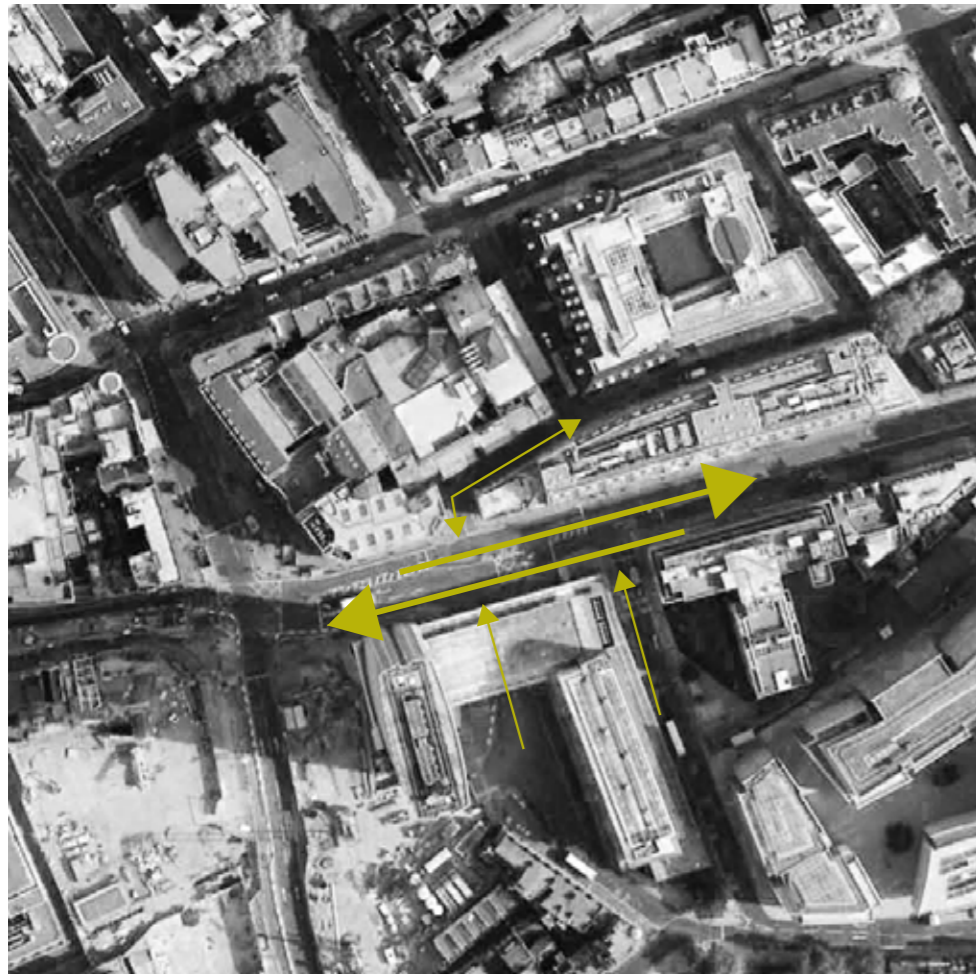
2.6 The surrounding uses are provided in a mix of traditional and contemporary properties, ranging from 4 storeys to the taller buildings located on the opposite side of Great Russell Street to 35 storeys at Centre Point, diagonally opposite the site.

2.7 The site is located in Zone 1 and provides easy access to Tottenham Court Road tube station, which is located approximately 110 metres west of the site, providing access to the Central Line and Northern Line Services connecting to West End destinations including Oxford Circus and Bond Street as well as the City of London. Works are currently being undertaken at Tottenham Court Road for the introduction of the new Crossrail service. Holborn to the east of the site provides good access to the Piccadilly Line.

2.8 Other public transport consists of a range of bus services which run frequently along New Oxford Street; the nearest bus stop is located approximately 20 metres from the site.

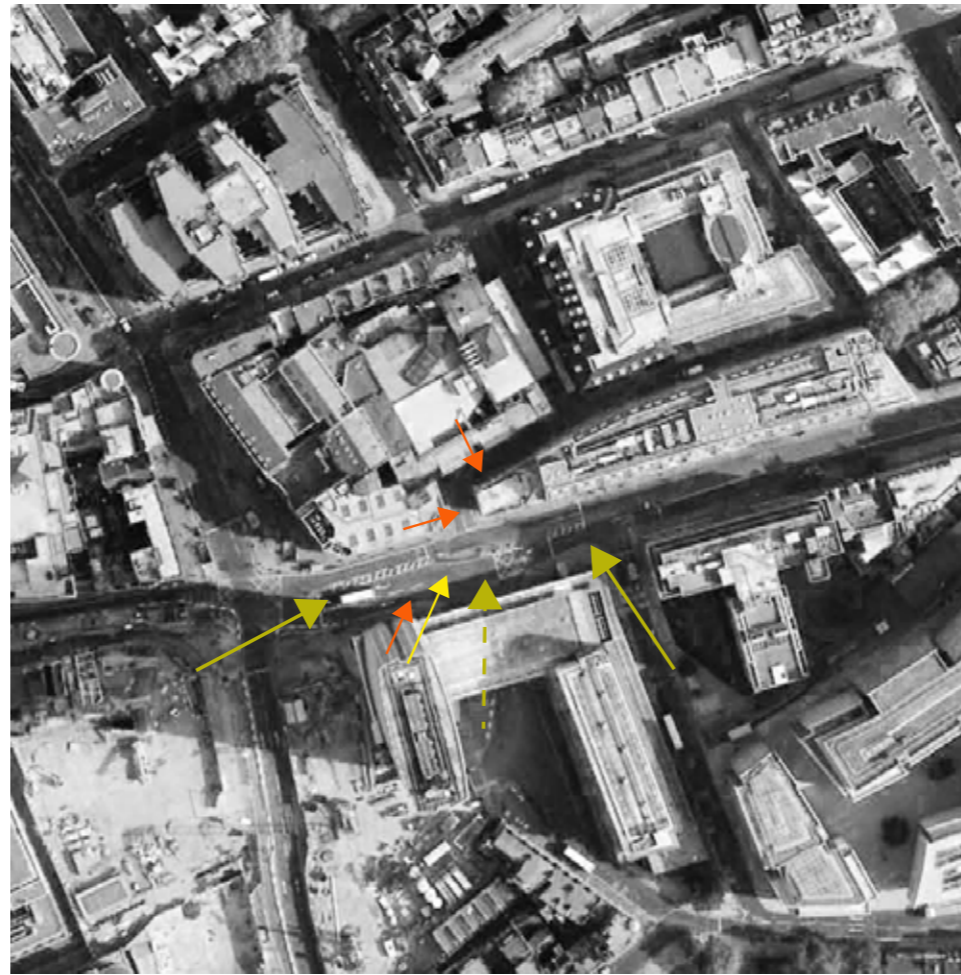
► Aerial Photograph Showing Application Site within Local Urban Street pattern.

## 2.1 : Site Analysis:



Major Road  
Minor Road

► Traffic Flow.



Mid View  
High View  
Ground View

► Views Onto Site From Local Environment.



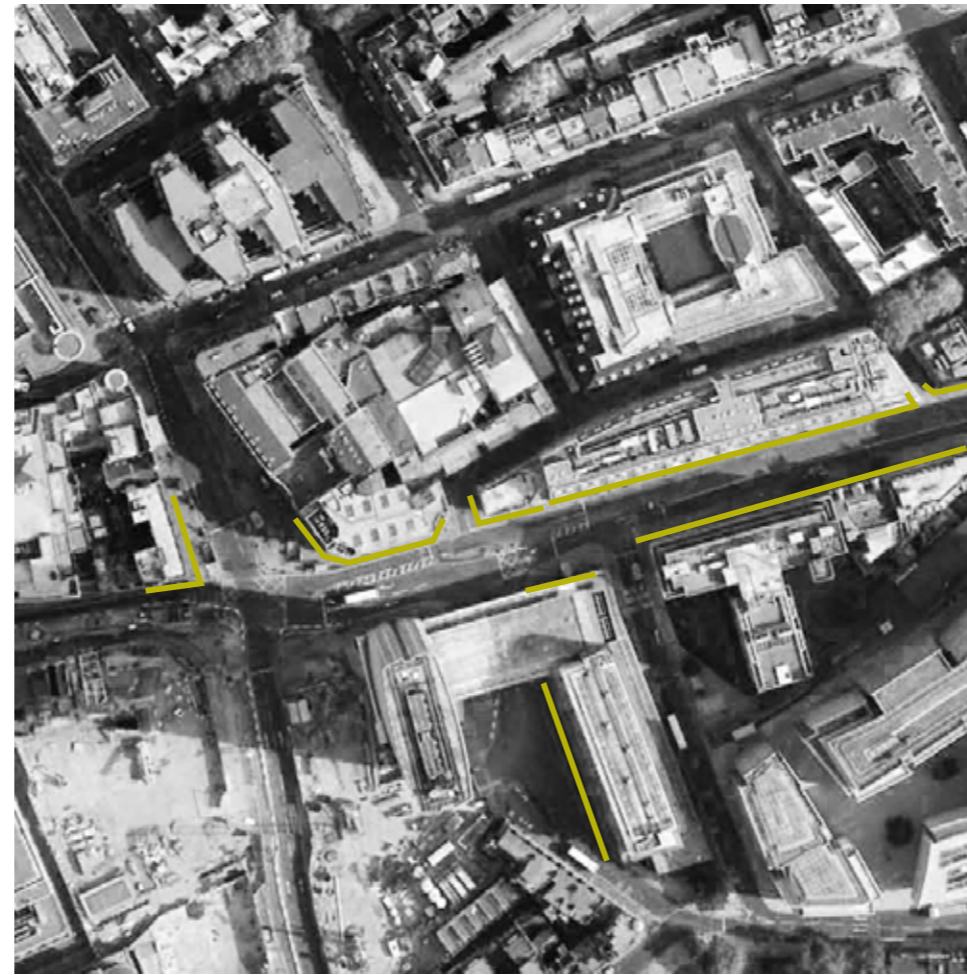
Mid View  
High View

► Views Out of Building and Off The Site.

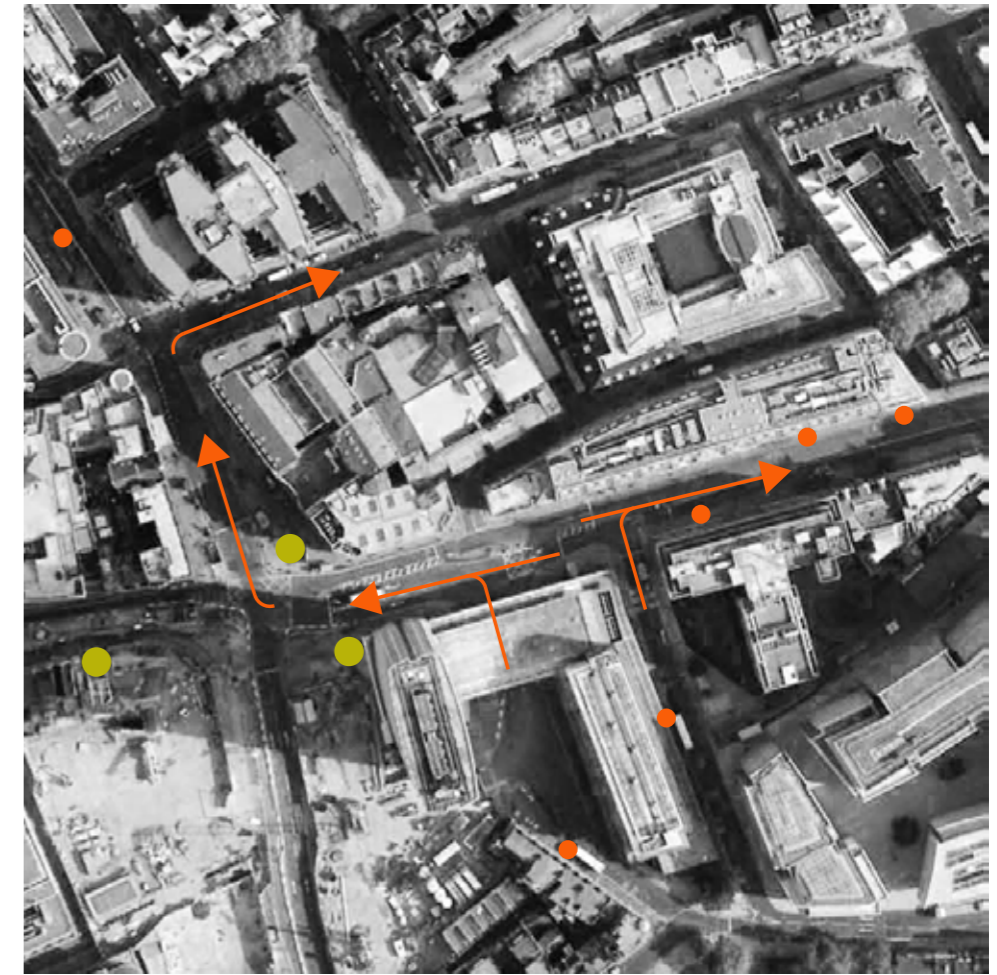
## 2.1 : Site Analysis:



● Building Entry Points



▶ Existing Retail Frontages.



→ Bus Route  
● Bus Stop  
● Underground Entry

▶ Local Public Transport Routes, with Underground Station Entry Points and Bus Stops.

▶ Entry Points Into Building, From New Oxford Street and Bainbridge Street.

### 3.0: Site Photographs: Location of Site Photographs

 Photograph Locations





### 3.1: Site Photographs: Aerial View of Site Within Context



1 View Looking Down from Centre Point, Showing Local Context and Urban Scale of Existing and New Developments.

### 3.2: Site Photographs: New Oxford Street Facade and Building Within Context



2 Corner of Building Where it Turns into Bainbridge Street.



3 View of existing building from Tottenham Court Road and New Oxford Street junction, party wall and stepped height with neighbouring building visible



4 View from New Oxford Street looking up, with narrow entry into Bainbridge Street.

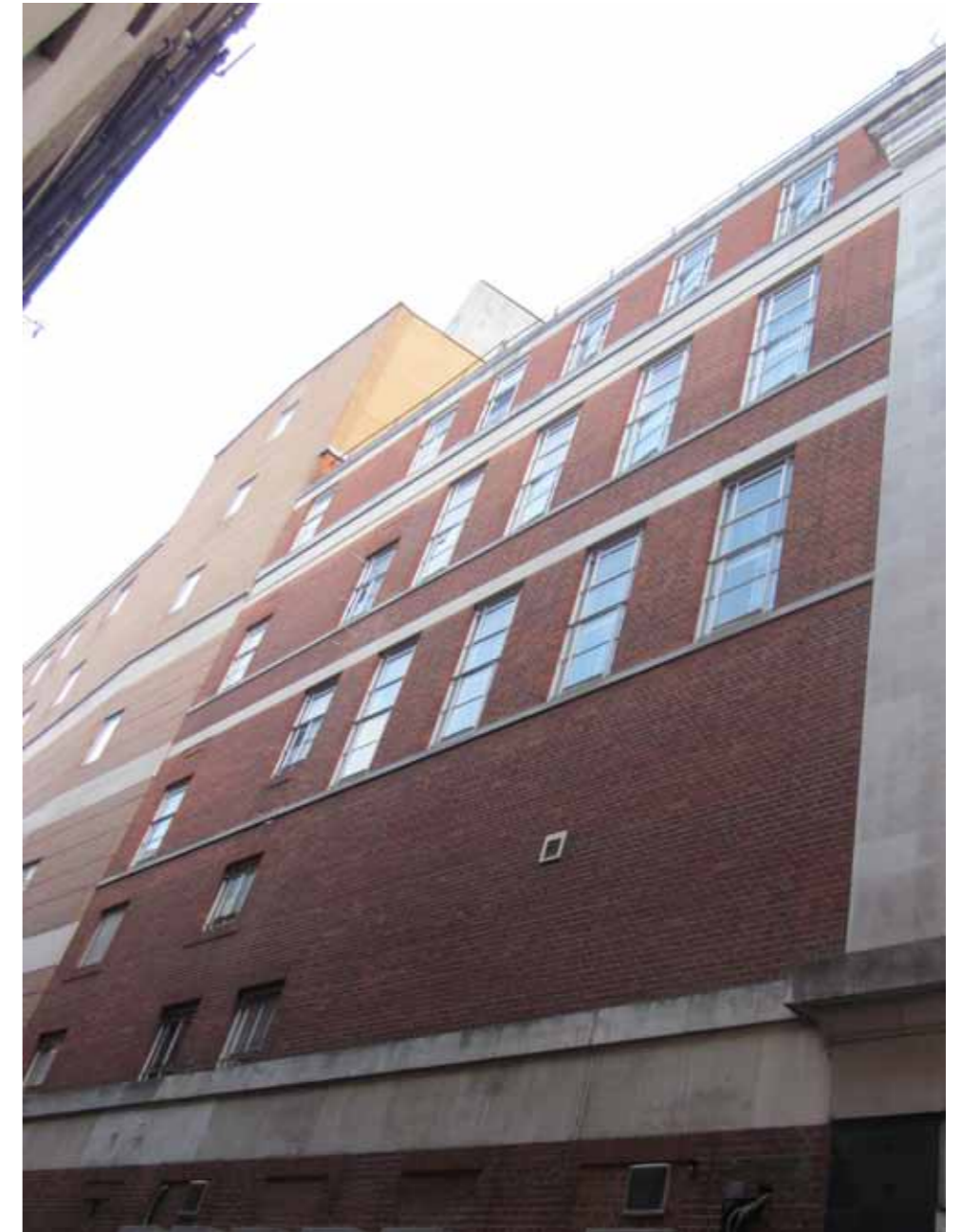
### 3.3: Site Photographs: Bainbridge Street Facade and Building Within Context



5 Bainbridge Street Rear Facade.



6 View of Rear of Theatre and Bainbridge Street



7 Looking up to Bainbridge Street Facade.

### 3.4: Site Photographs: New Oxford Street and Tottenham Court Road Vista



8

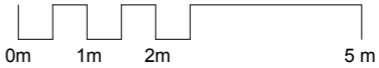
New Oxford Street and Tottenham Court Road Junction Vista.

### 3.5: Site Photographs: New Oxford Street Frontage

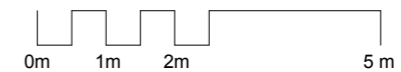


9 New Oxford Street Building Frontage.

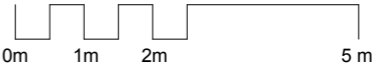
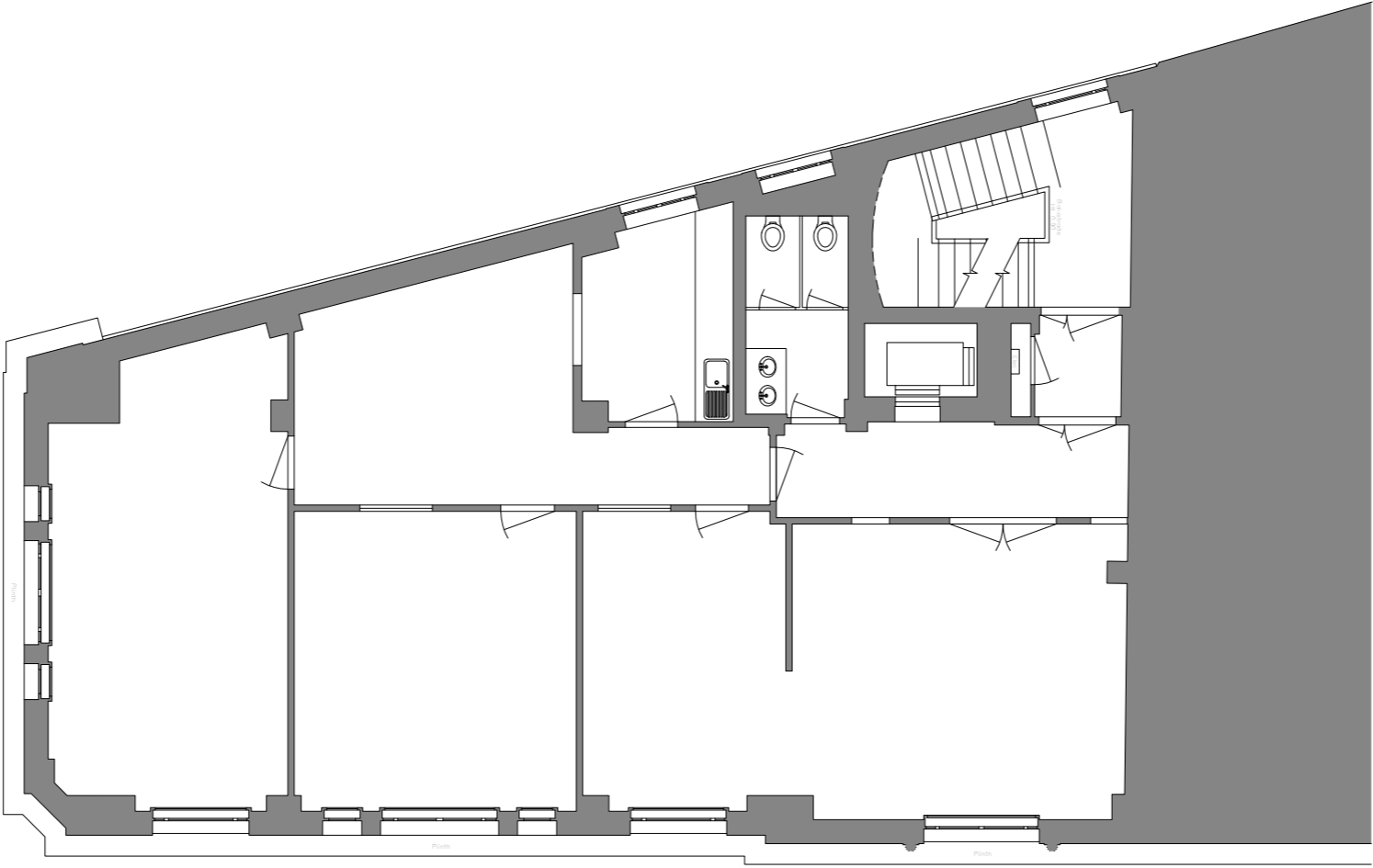
4.0: As Existing Drawings:  
Ground Floor



## 4.1: As Existing Drawings: First Floor

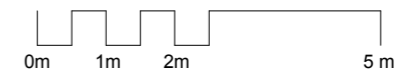
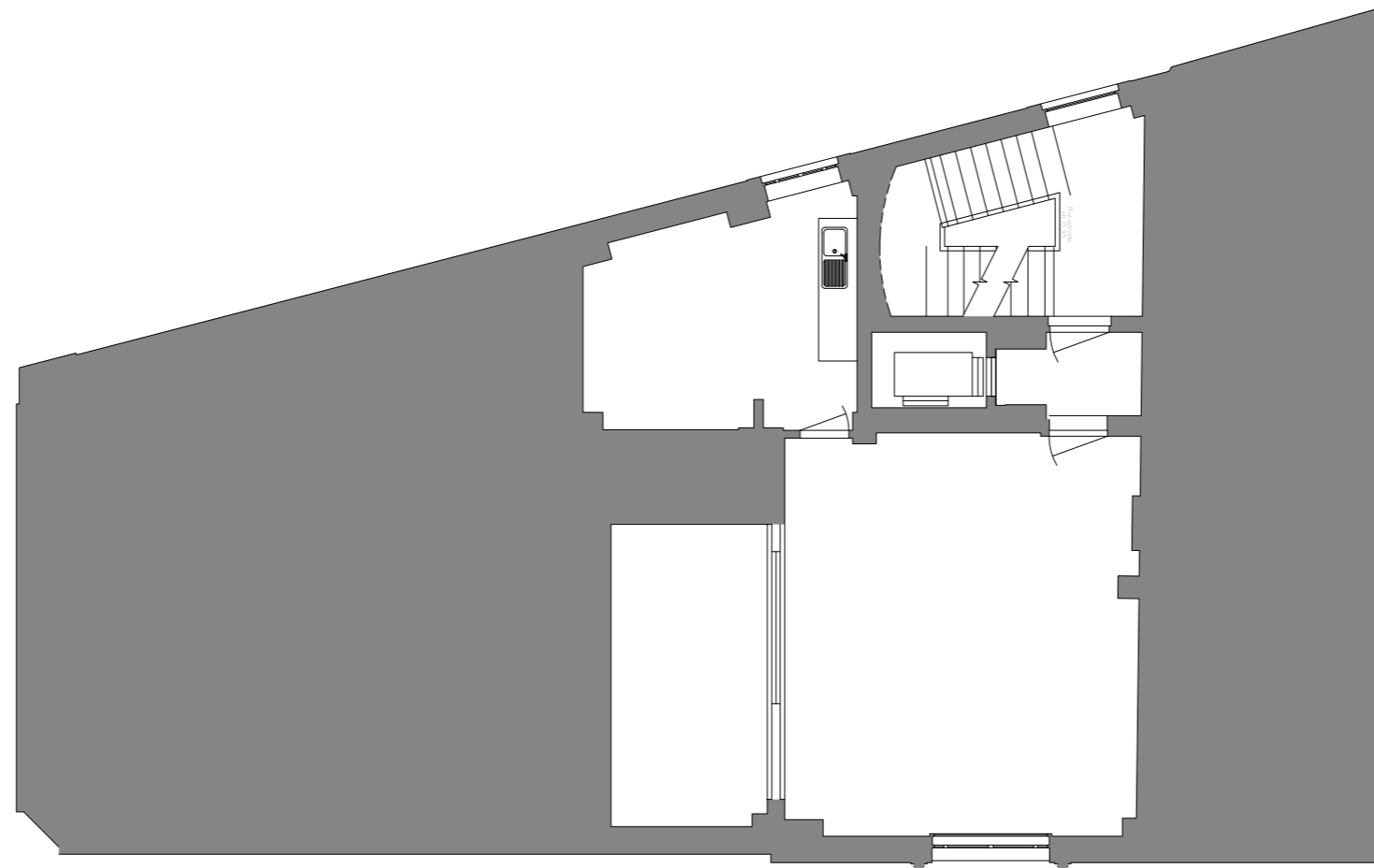


4.2: As Existing Drawings:  
Second Floor

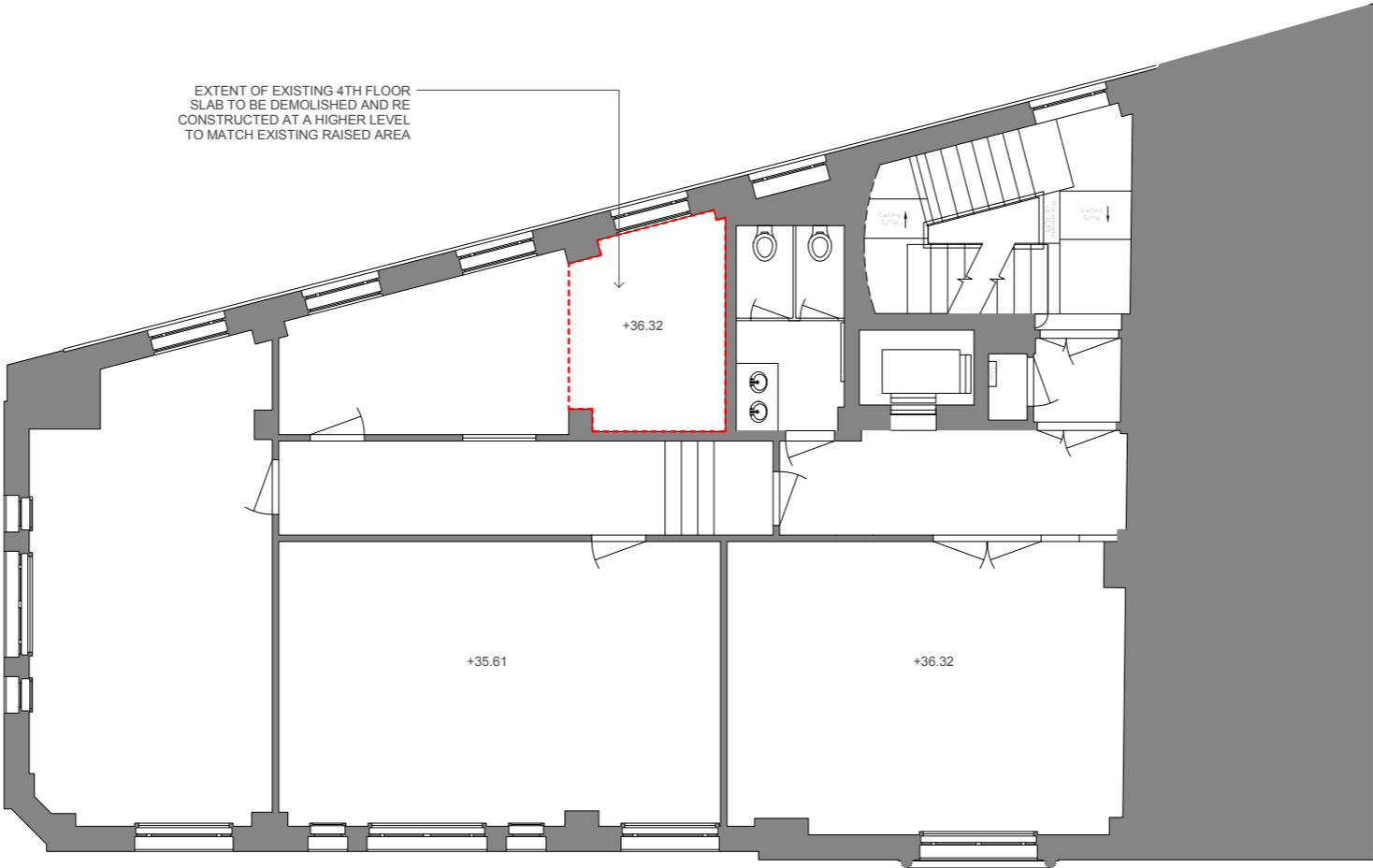




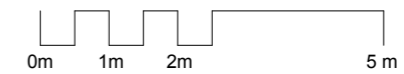
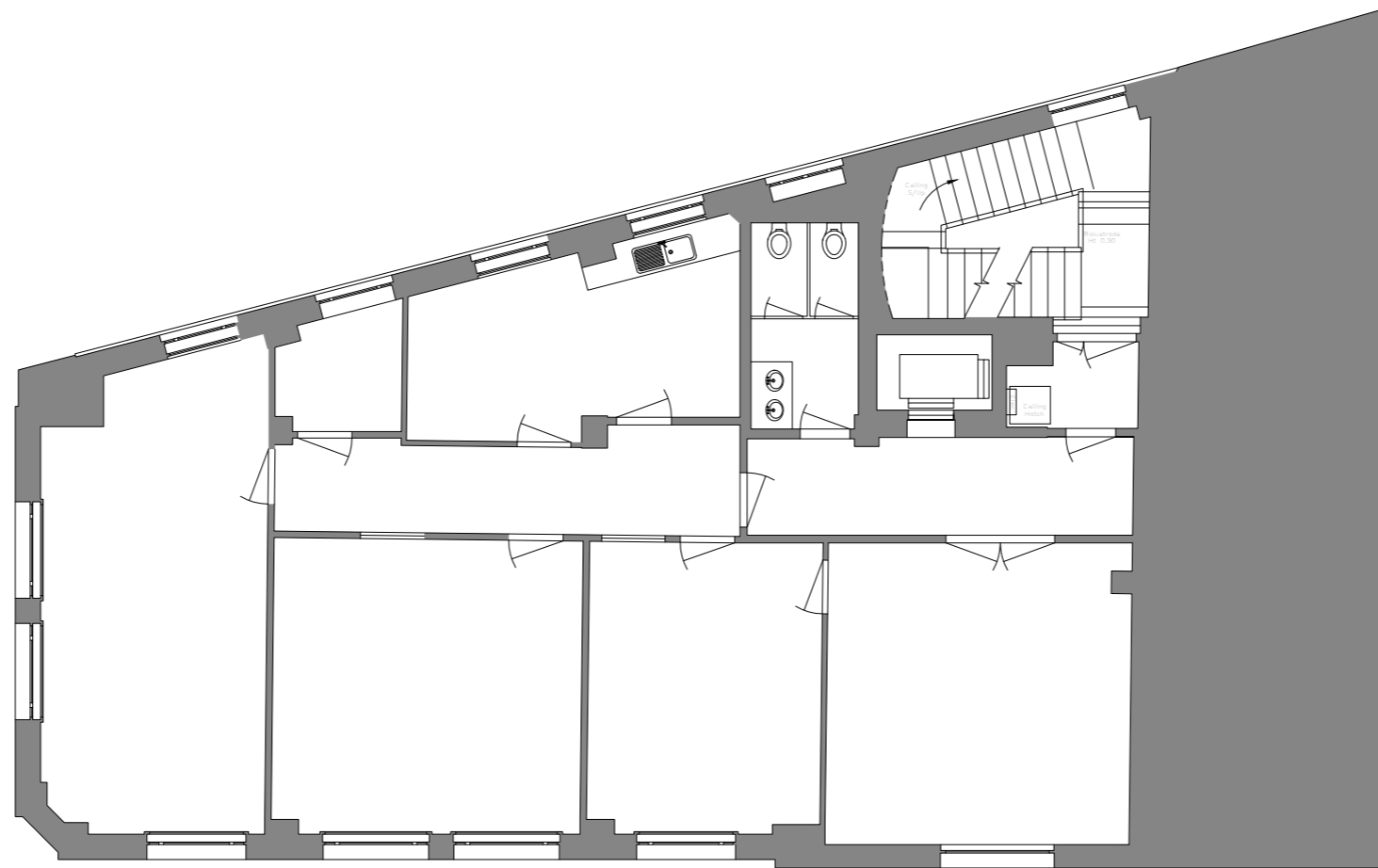
### 4.3: As Existing Drawings: Third Floor



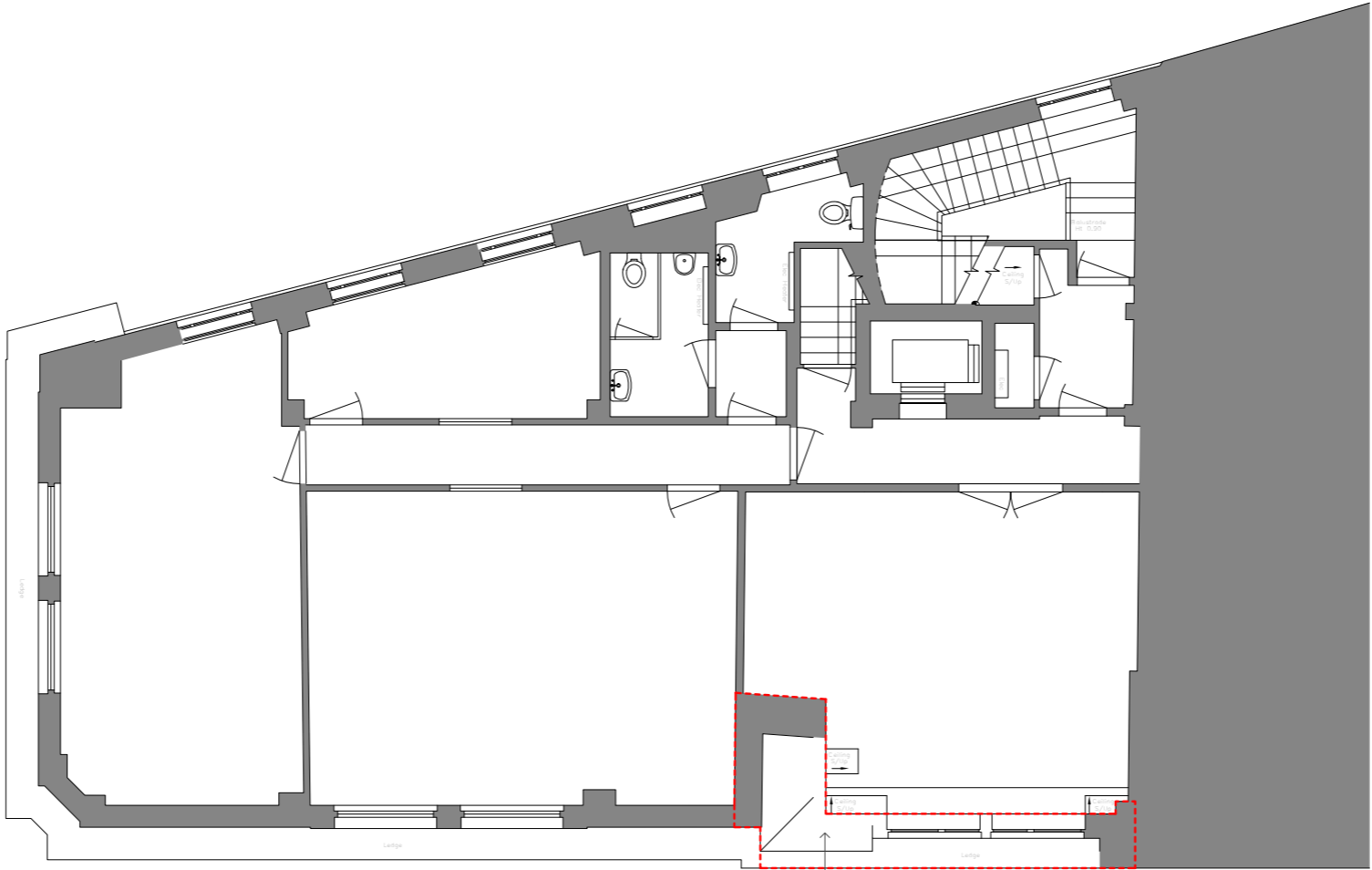
# 4.4: As Existing Drawings: Fourth Floor



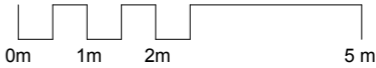
## 4.5: As Existing Drawings: Fifth Floor



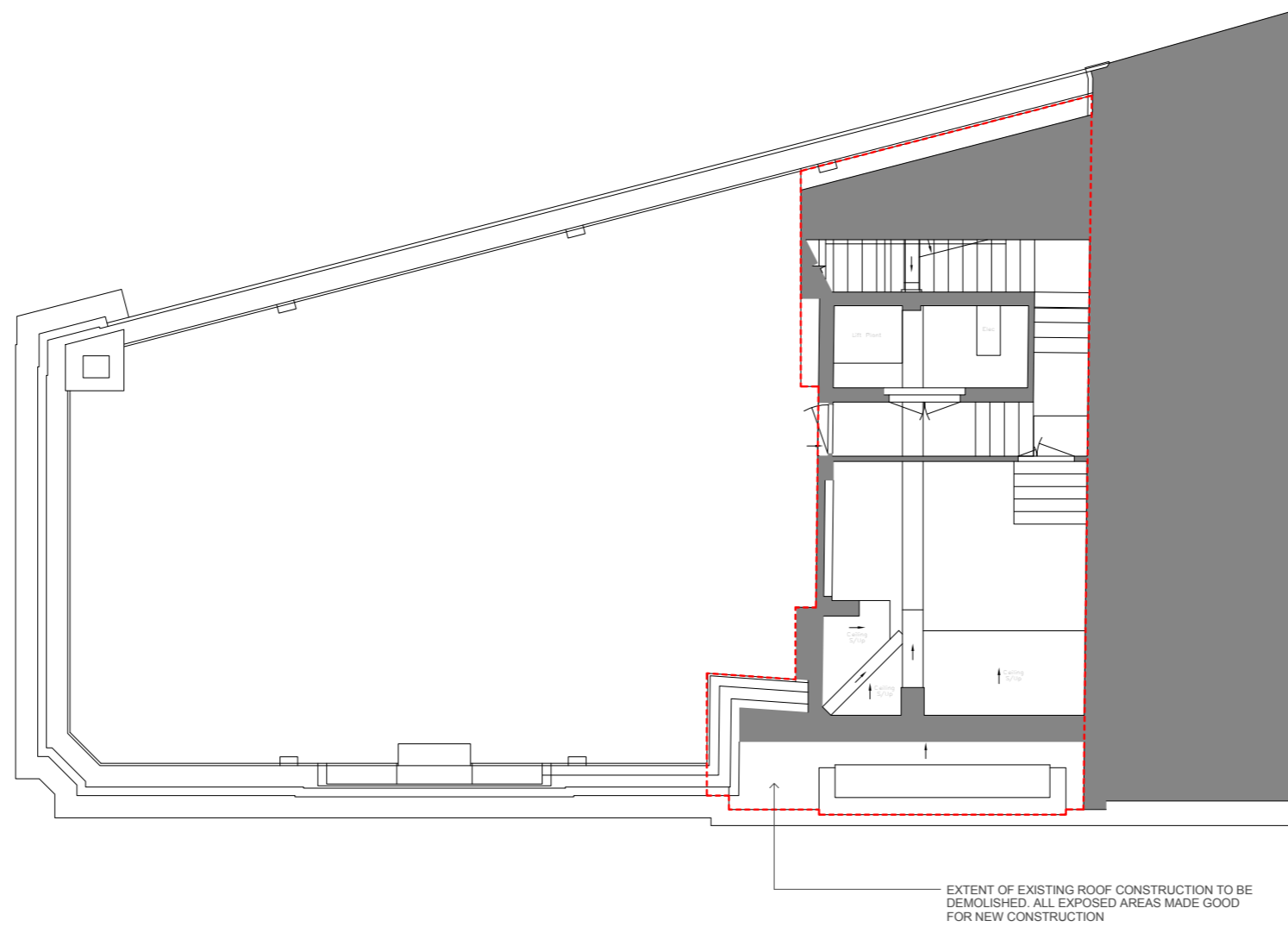
# 4.6: As Existing Drawings: Sixth Floor



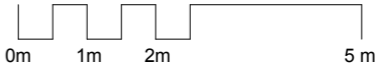
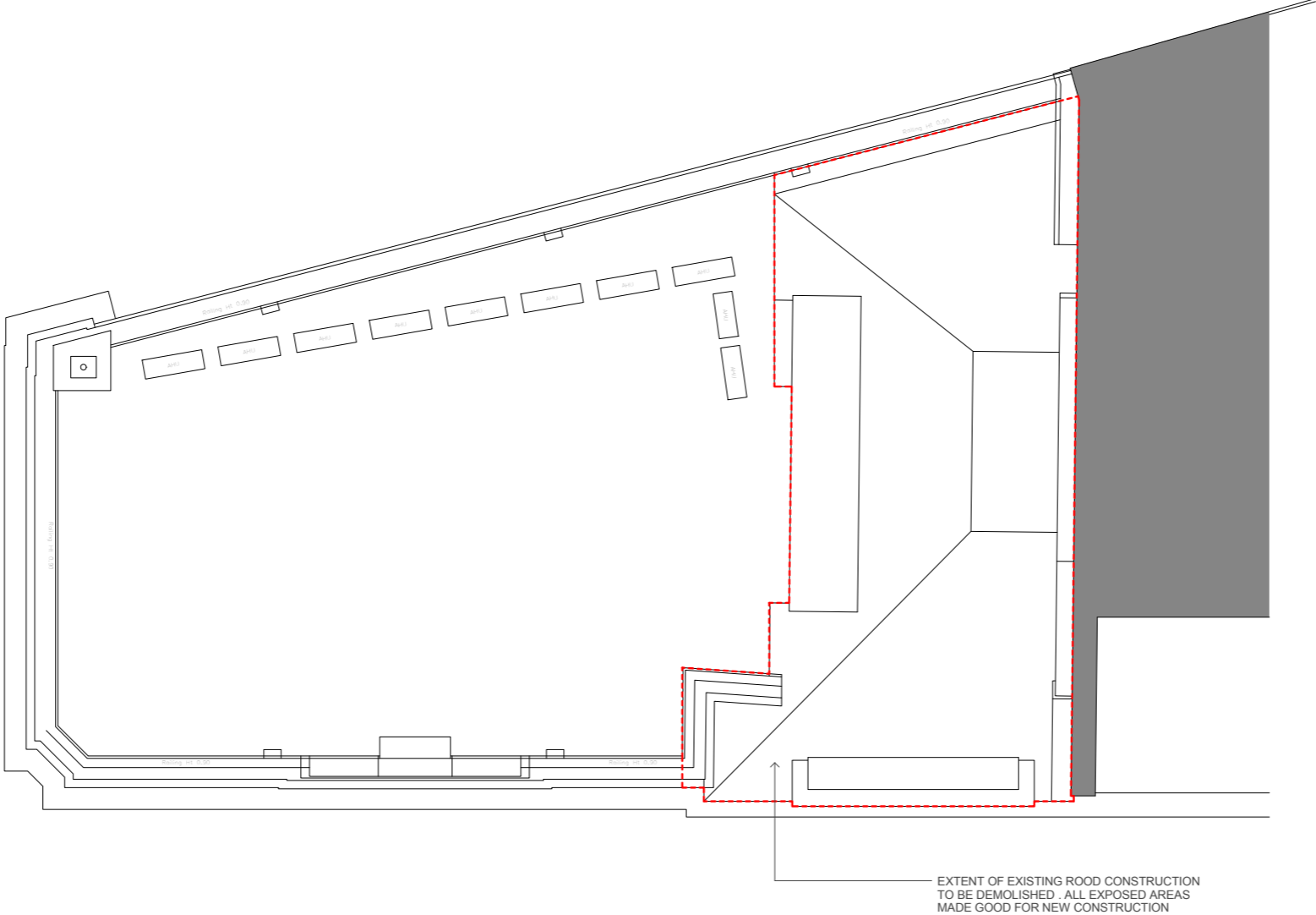
DORMER WINDOWS AND SLOPING ROOF CONSTRUCTION TO BE DEMOLISHED. ALL EXPOSED AREAS MADE GOOD FOR NEW CONSTRUCTION



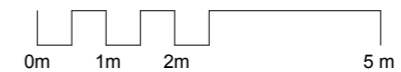
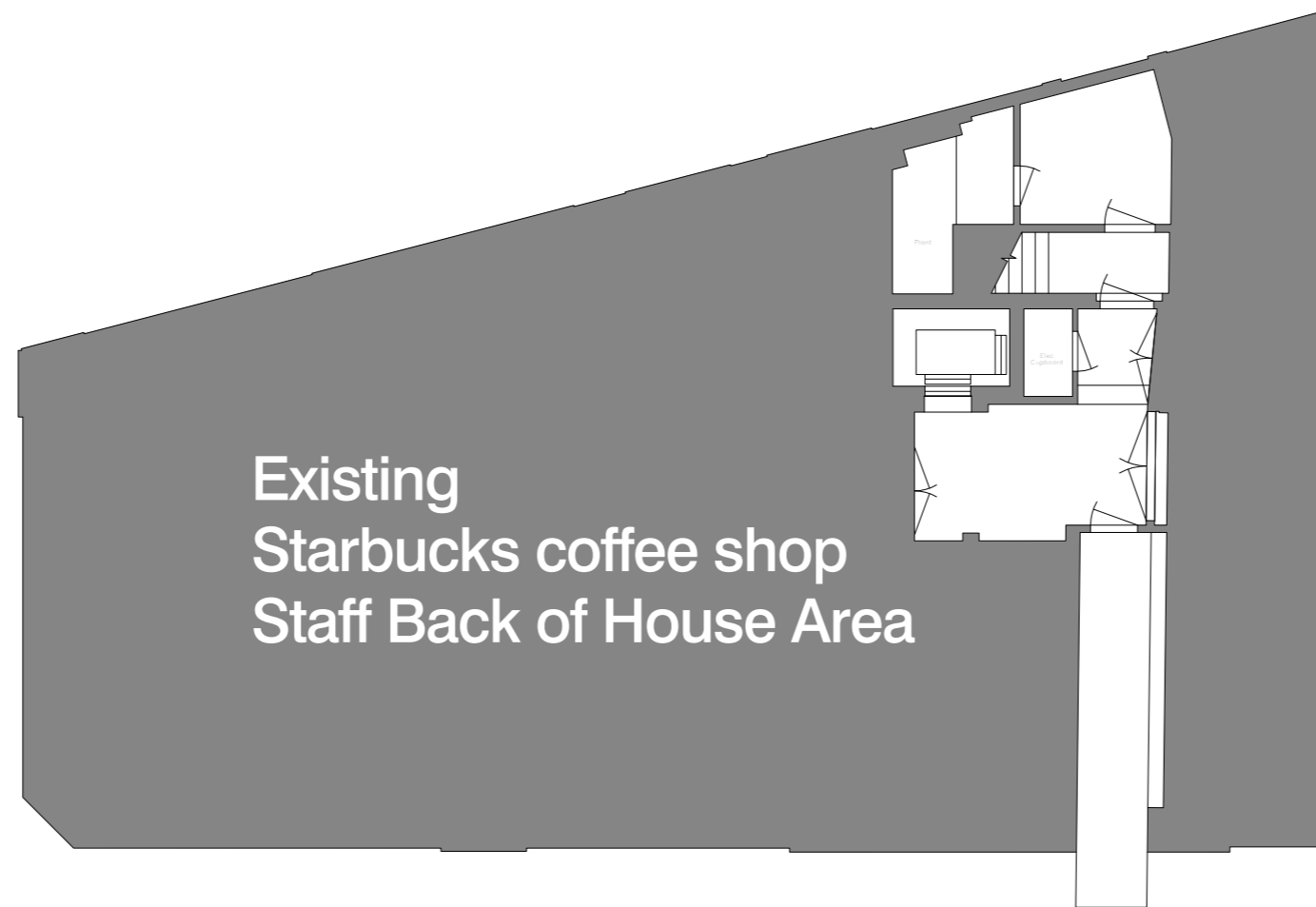
## 4.7: As Existing Drawings: Seventh Floor



# 4.8: As Existing Drawings: Roof Plan



## 4.9: As Existing Drawings: Basement Plan



## 4.10: Site Photographs: Existing Internal Photographs



► View Looking Up The Existing Staircase



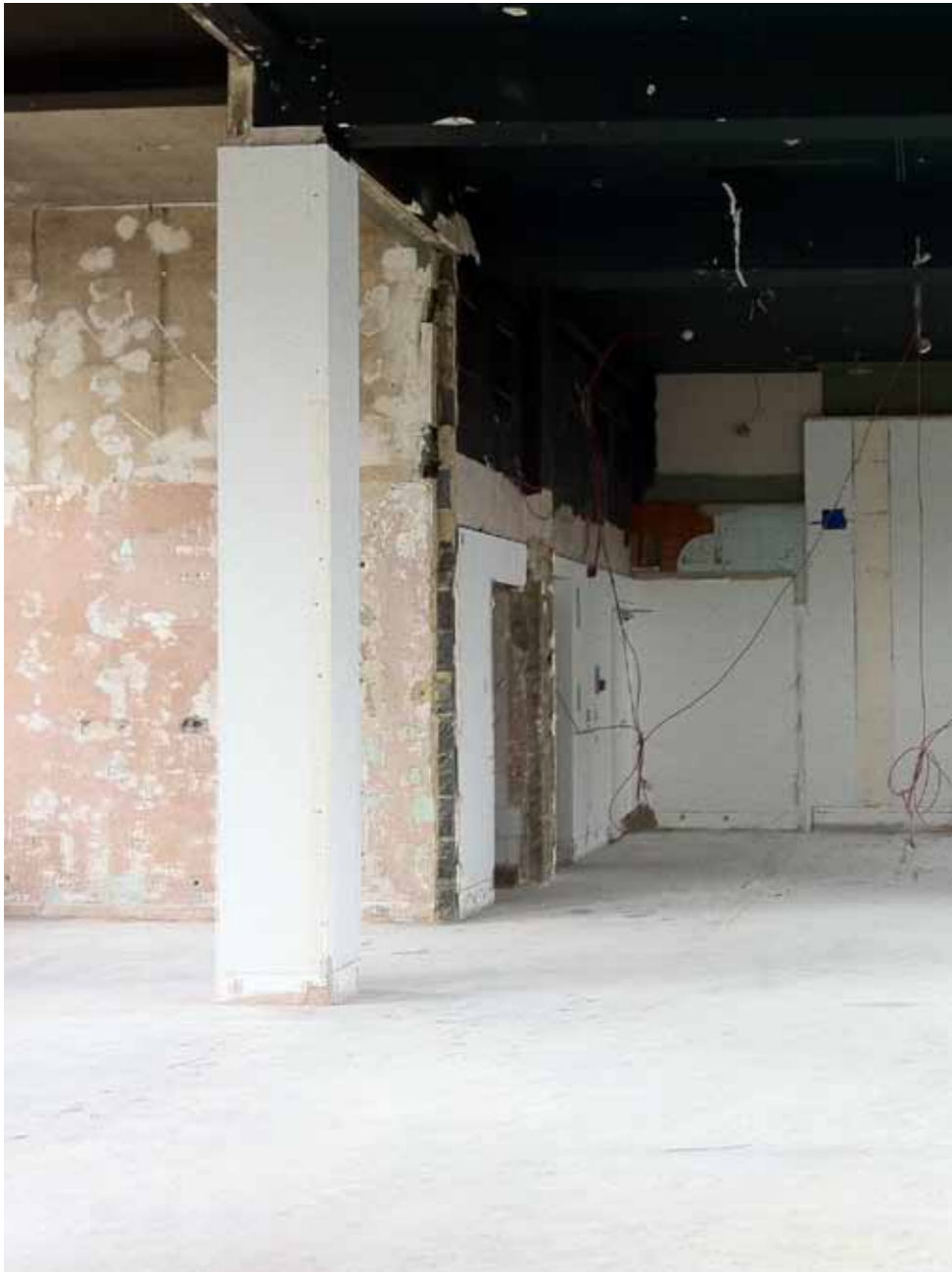
► View of 2nd Floor showing 3rd Floor Mezzanine Floor



► View of 4th Floor



## 4.10: Site Photographs: Existing Internal Photographs



► View of 5th Floor

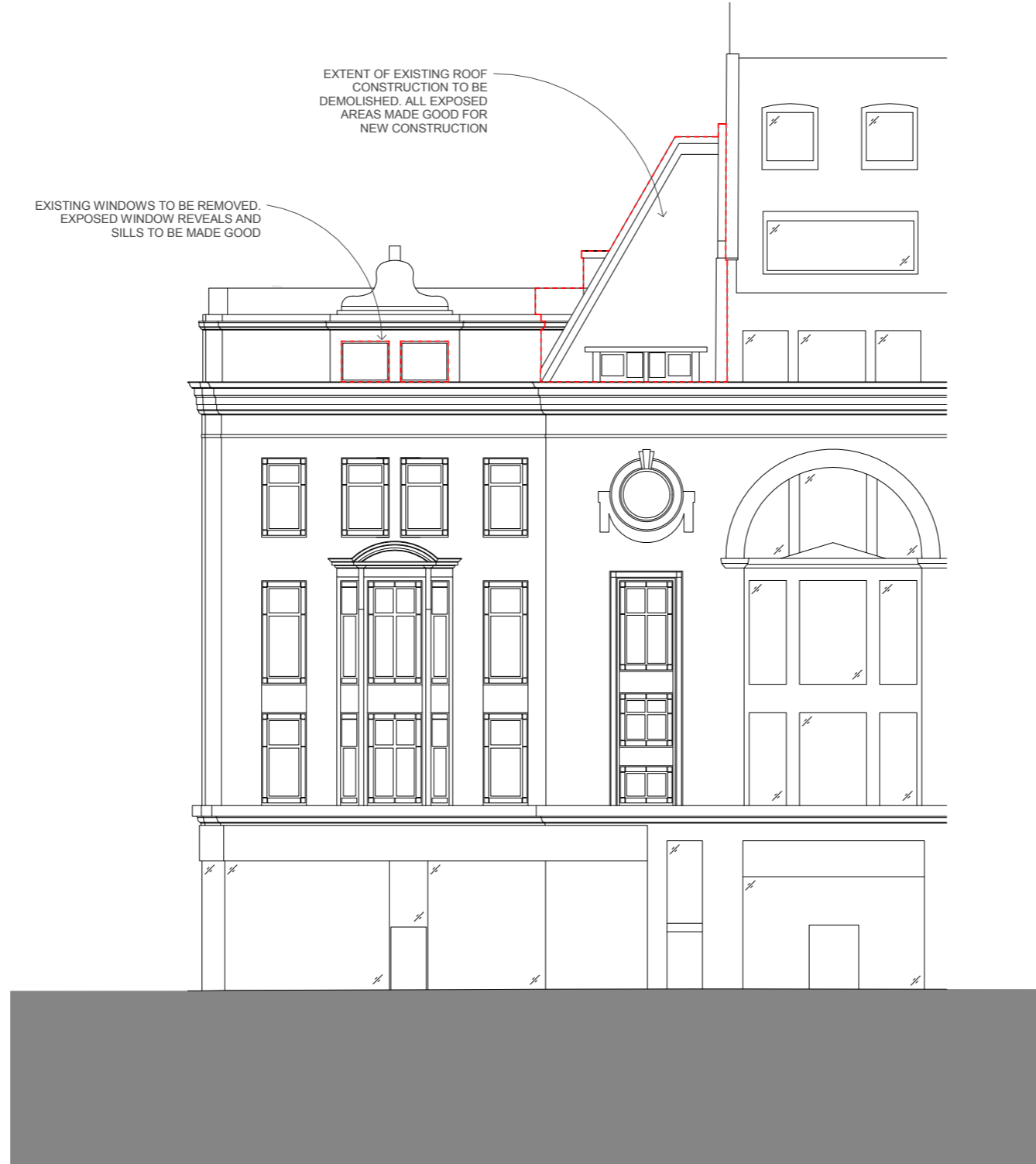


► View of 5th Floor



► View of 6th Floor

## 4.11: As Existing Drawings: New Oxford Street Elevation



1 EXISTING South Elevation  
1:100

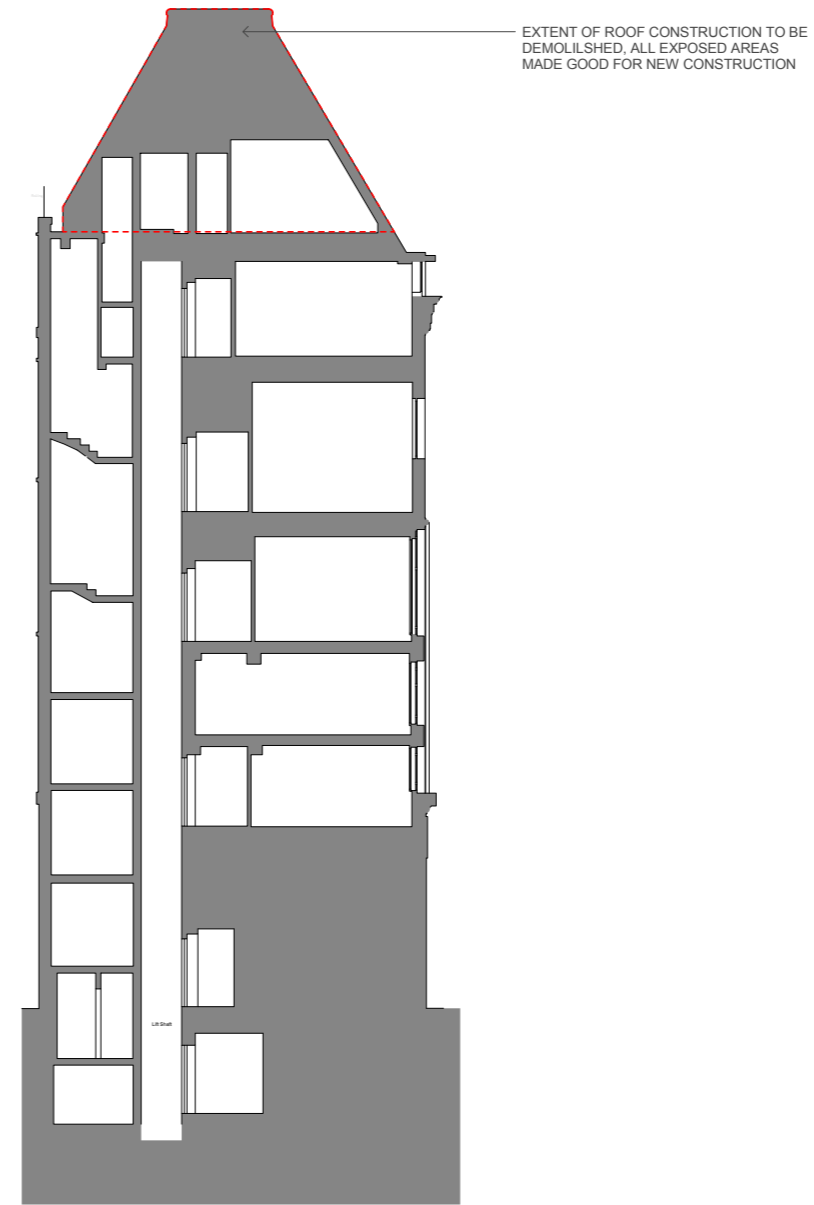
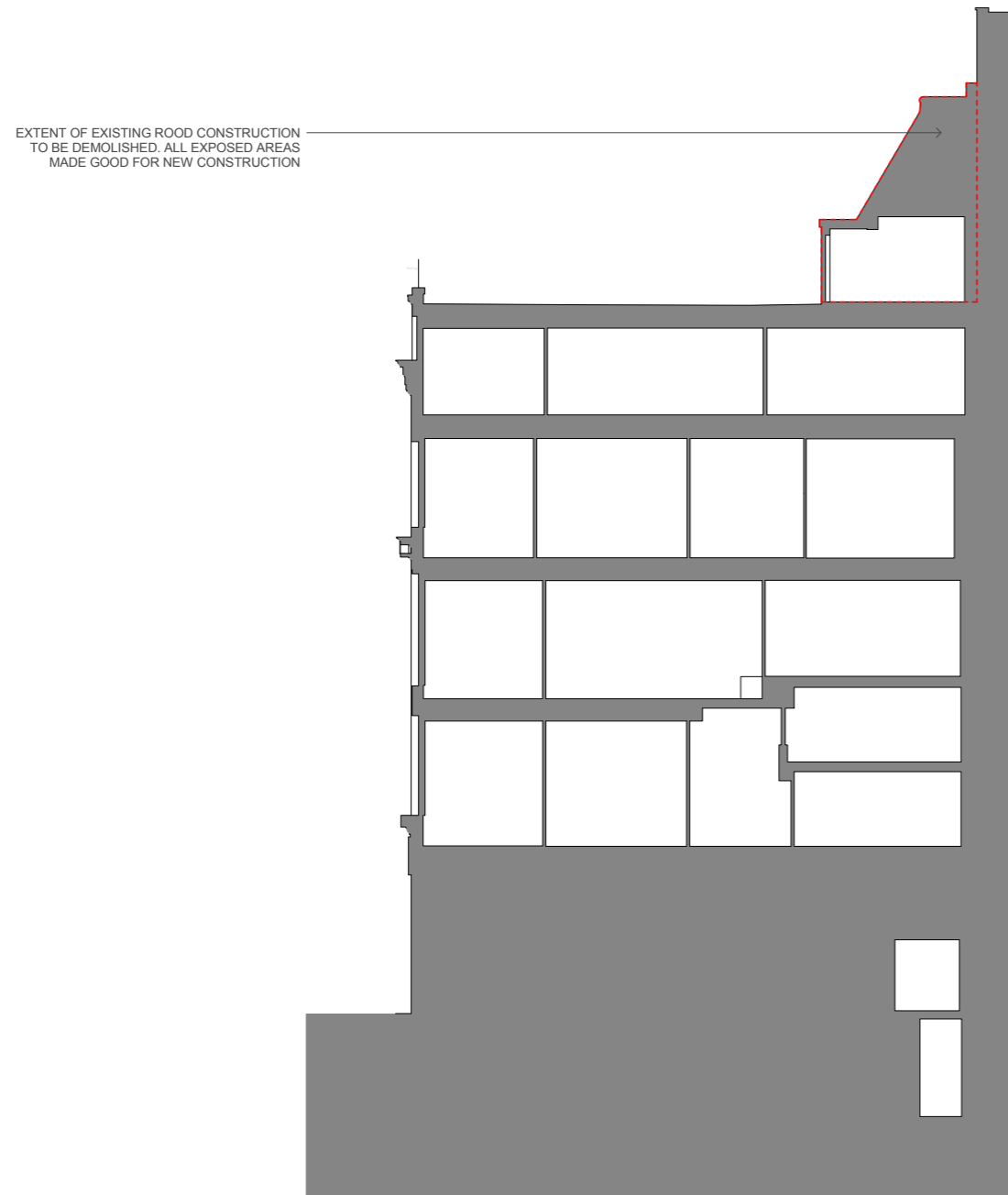
## 4.12: As Existing Drawings: Bainbridge Street Elevations



1 EXISTING West Elevation  
1:100

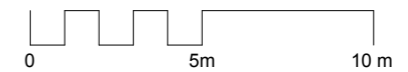
2 EXISTING North Elevation  
1:100

## 4.13: As Existing Drawings: Cross Sections

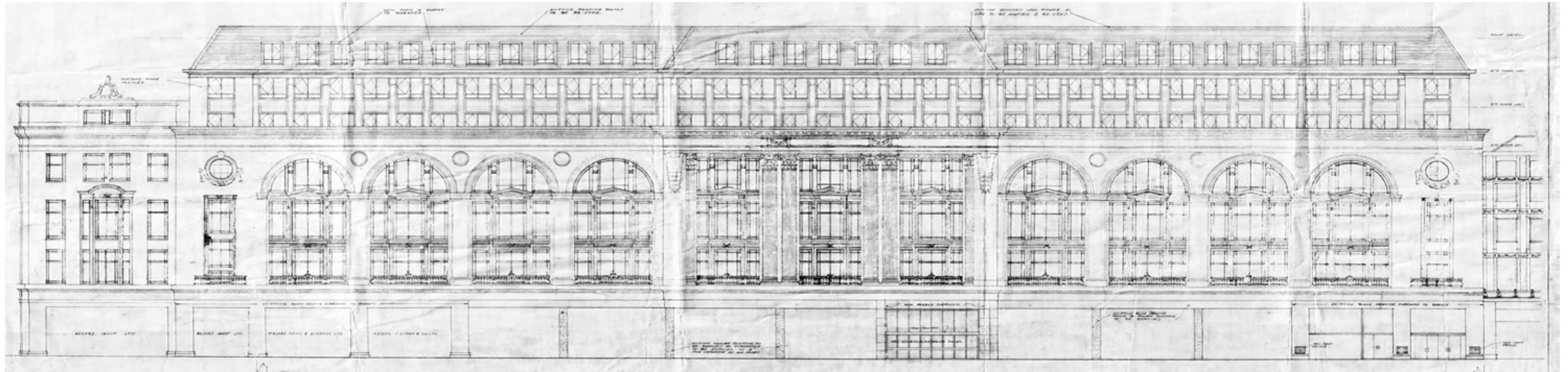


1 EXISTING Section AA  
1:100

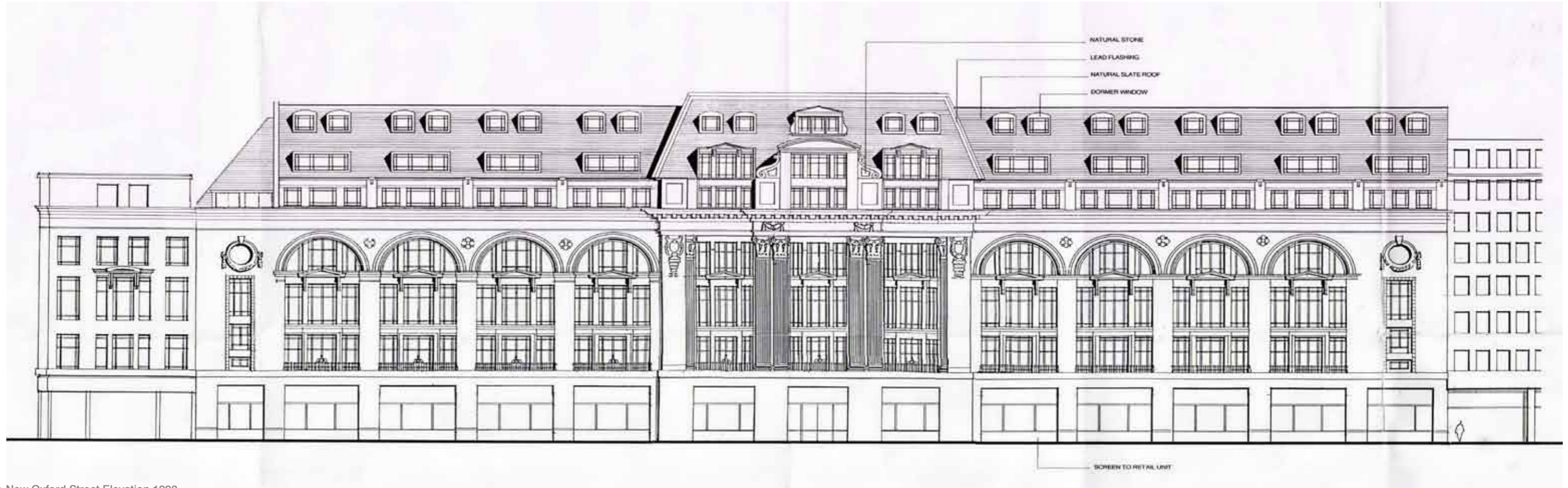
2 EXISTING Section BB  
1:100



## 4.14: As Existing Drawings: New Oxford Street Elevation 1962 and 1993

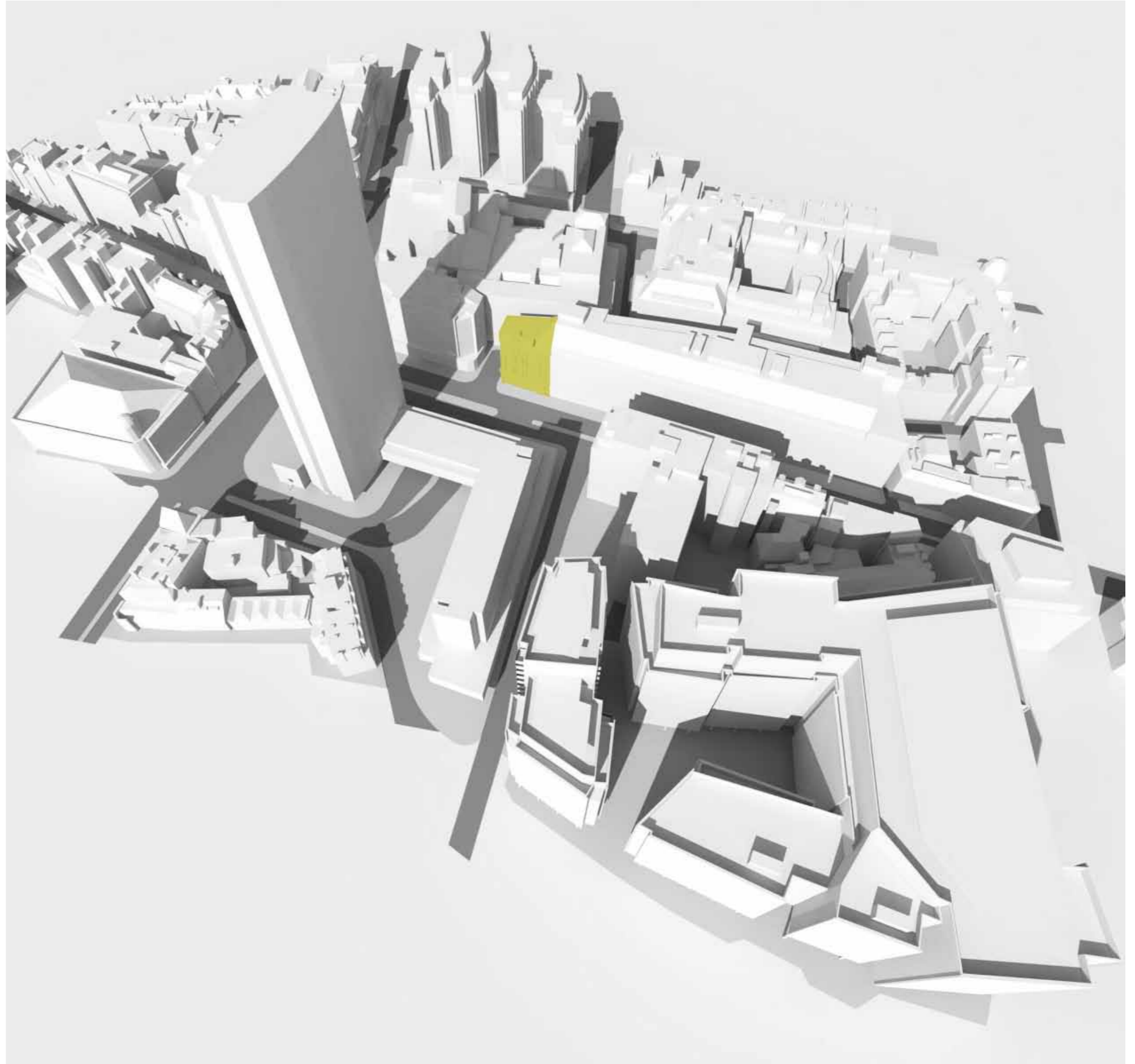


New Oxford Street Elevation 1962



New Oxford Street Elevation 1993

## 5.0: Proposed Development : Description and Floor Plans



## 5.0: Proposed Development : Description and Floor Plans

### EXISTING BUILDING CONDITION:

The existing building currently includes retail (Starbucks shop) at the ground and first floors with staff areas within the basement and vacant secondary office accommodation in the floors above (2 - 6). This office space is generally of poor quality and inefficient in terms of layout.

The site is located on the border of the quieter residential area of Bloomsbury and the much livelier areas of Soho and Covent Garden. It is therefore considered that the site would be entirely appropriate for either residential use or potentially serviced apartments.

The building is sited on a prominent corner of New Oxford Street, this provides great views out onto the junction of Tottenham Court and Oxford Street, this area is currently under going redevelopment with Tottenham Court Road tubestation having the new crossrail extension added and new buildings and plaza at street level.

Given the neighbouring building heights and precedent extensions including the rest of the adjoining terrace (Prospect House), there appears to be scope for additional height, subject to appropriate design. Any roof top feature will be prominent when viewed from the end of Tottenham Court road junction and Earnshaw Street which joins new Oxford Street opposite the Site. The views down from Centre Point Tower are important, the shape of this extension and its materials will be key to making it a 'small jewel' within the city.

Potential extension designs can be informed by adjacent Architectural drivers (neighbouring roof shapes and recent roof top extensions). Sunlight/daylight and Rights to Light issues may also play a part in the massing of any extension.

The materials could be of a traditional 'roof' material metal cladding (of various colour tones), or have elements of stone where it would tie into the existing facade. Using glass or other more reflective materials would enhance the design and add to the potential 'jewel' quality.

The rear facade (Bainbridge Street) is currently of a simple red brick material with simple punched windows, this will remain mostly untouched apart from where new windows will be required for the proposed design.

### PROPOSED DESIGN CONCEPT:

Following our pre-planning application meeting (11th July 2012), the proposed extension was 'revisited' and redesigned to become a 'softer' piece of Architecture, applying rounded corners at all edges and a clearer defined window opening strategy. We believe that this 'revisited' design has a sense of place sitting on top of 112-116 New Oxford Street, and is piece of urban skyline that will blend into the existing surrounding London fabric.

The new roof addition will be 'blended' into the neighbouring roof profile, by taking on board the same slope of the neighbouring roof (Prospect House). With an extra slope along the Bainbridge Road elevation, the overall form has been shaped and considered within the wider context of the neighbouring buildings and long sight lines from the Tottenham Court Road junction.

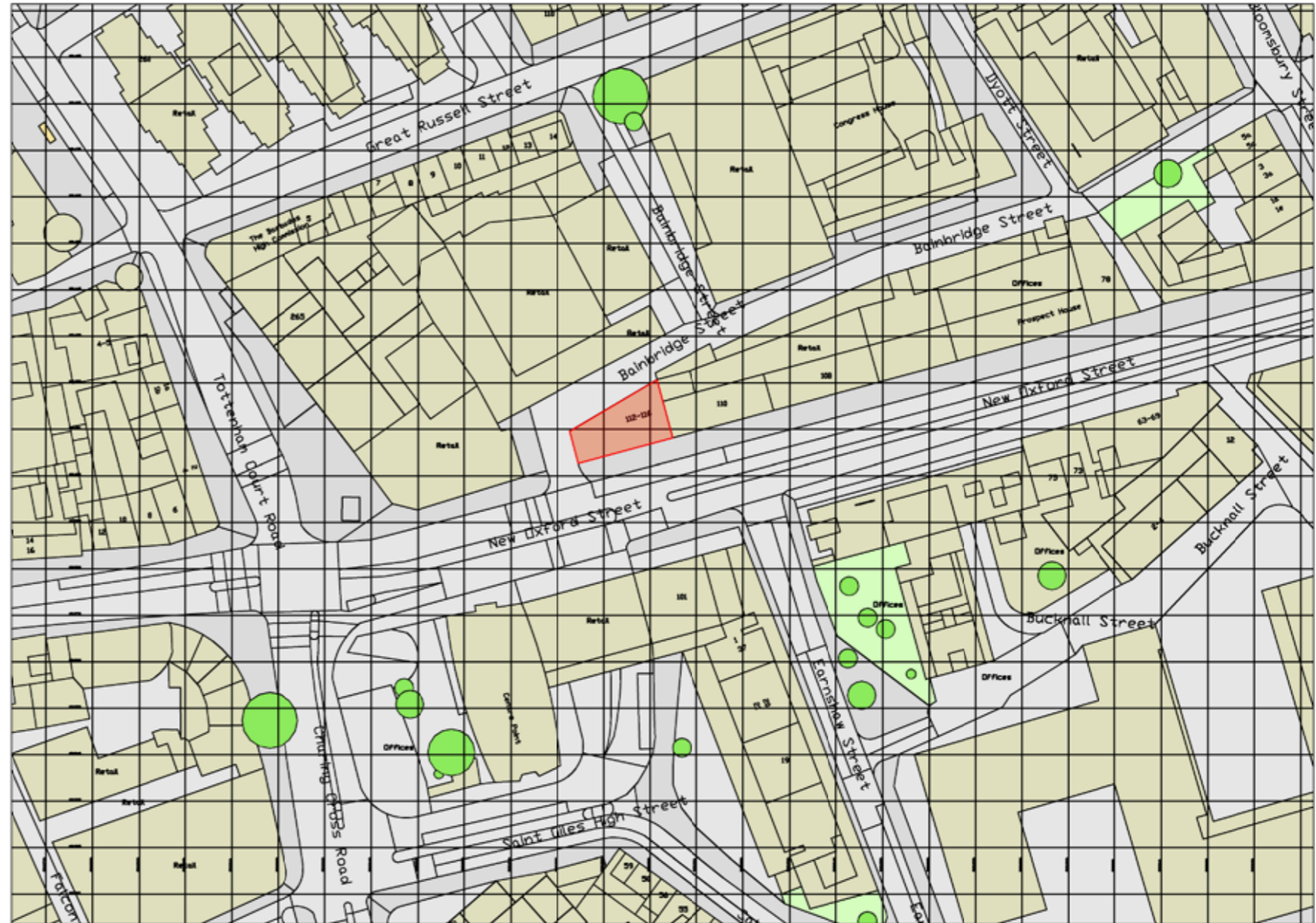
This new extension will appear to rise up from behind the existing stone facade along New Oxford Street and Bainbridge Road, with the sight lines from street level any view of the new extension will be minimal.

The proposed cladding to our extension will also add to the Architectural 'blending' of this new piece of skyline Architecture. Our proposed finish is a modern interpretation of traditional roof finishes that are generally found within the London area. The material will be a copper based product, and the colour choices we are considering are Brass or gold. These colours and the finish will best respond to the stone of the main facade, and fade over time to become more muted.

This cladding proposal shall be made up of small 'diamond' shingles. This cladding 'style' will be best at creating the sloping sides and curves of our design proposal, and again are common within London skyline. Around the Dormer windows the same cladding finish colour will be used, but as a single cladding strip forming a strong clean edge to each dormer.

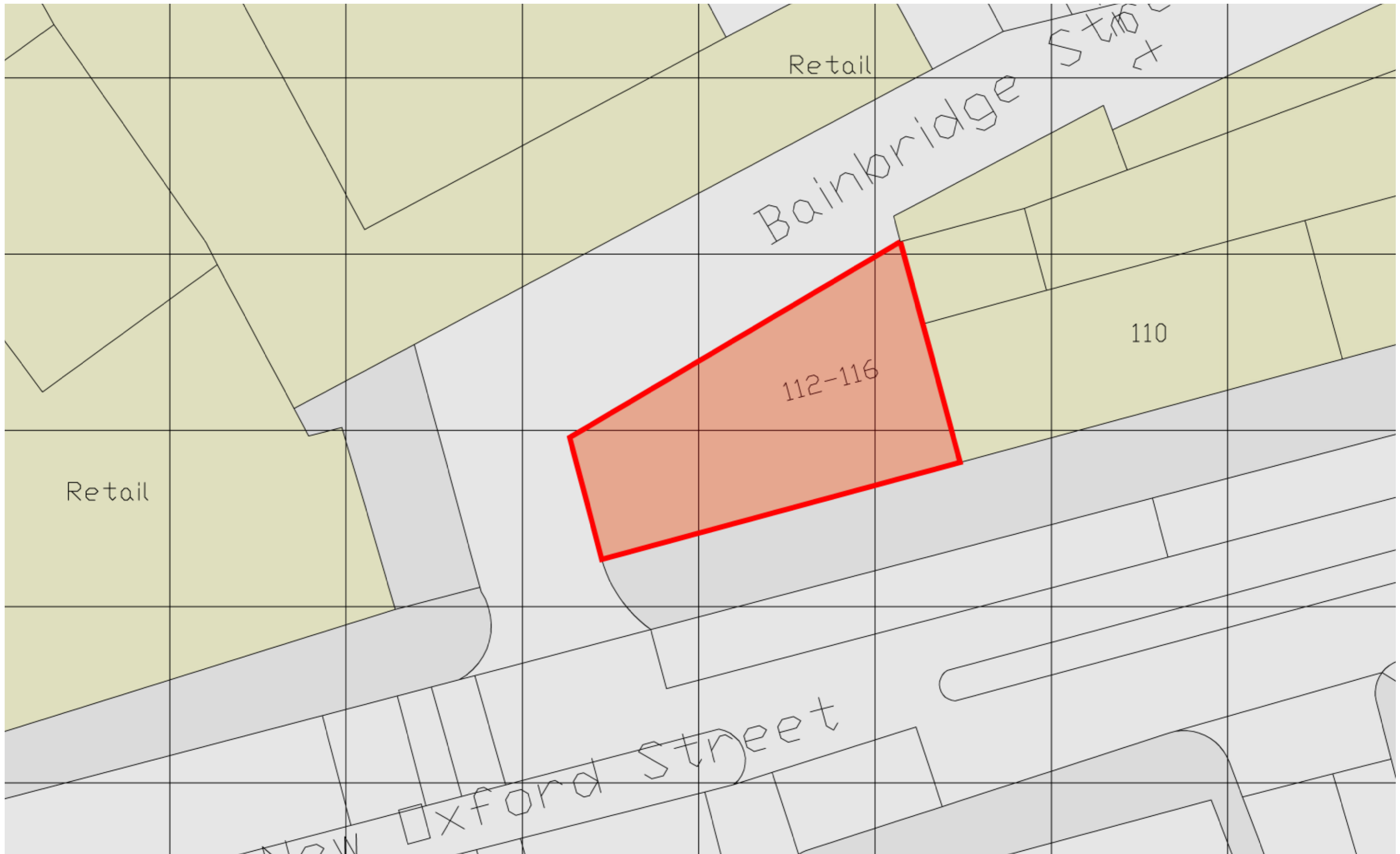
The existing stone parapet which forms the current roof top edge (sixth floor) will be extended along to the neighbouring party wall on Prospect House; this will reinforce its existing strong building line, which at present is broken by the existing sloping roof structure.

## 5.1: Proposed Development : Site Location Plan @ 1:1250

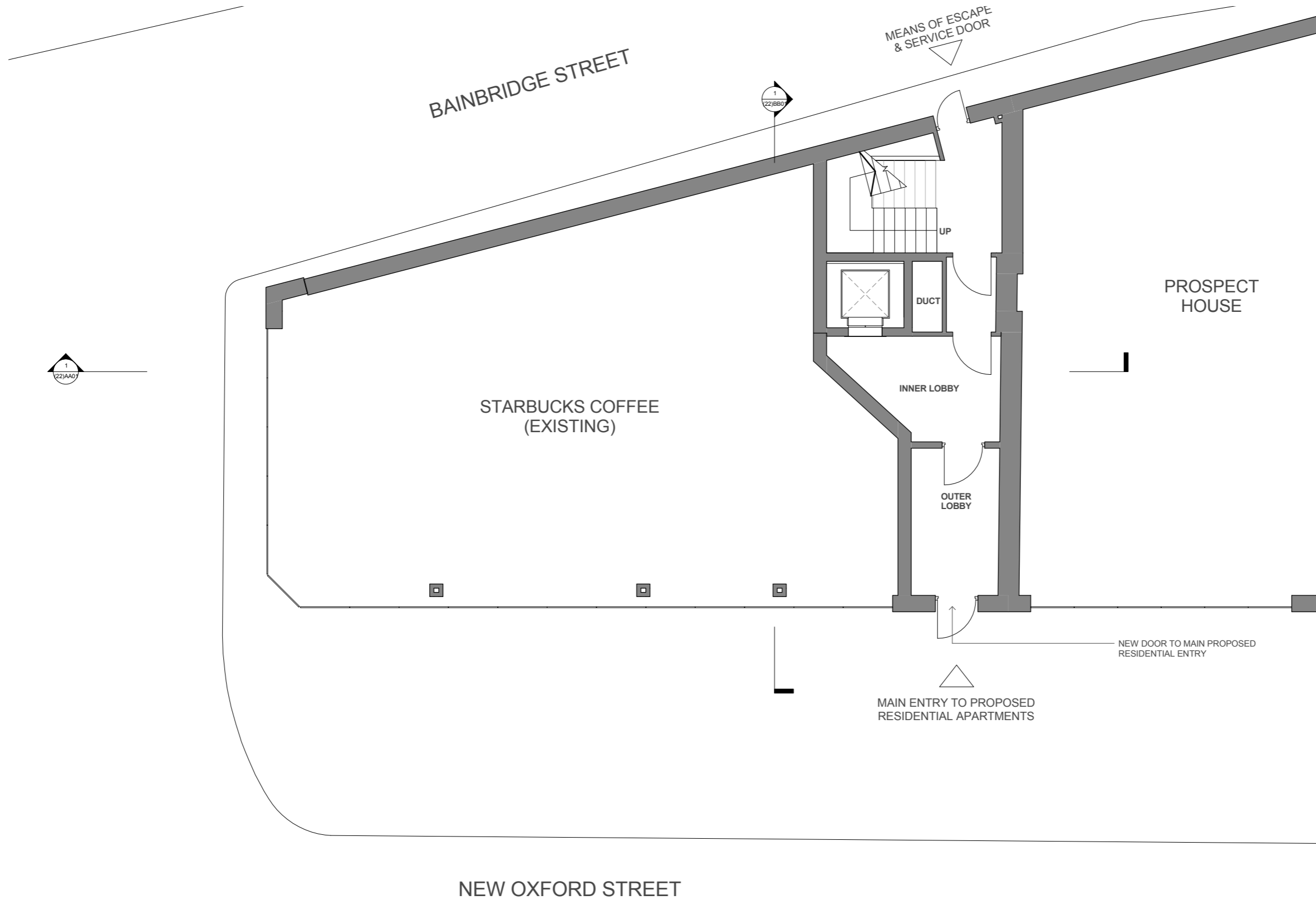




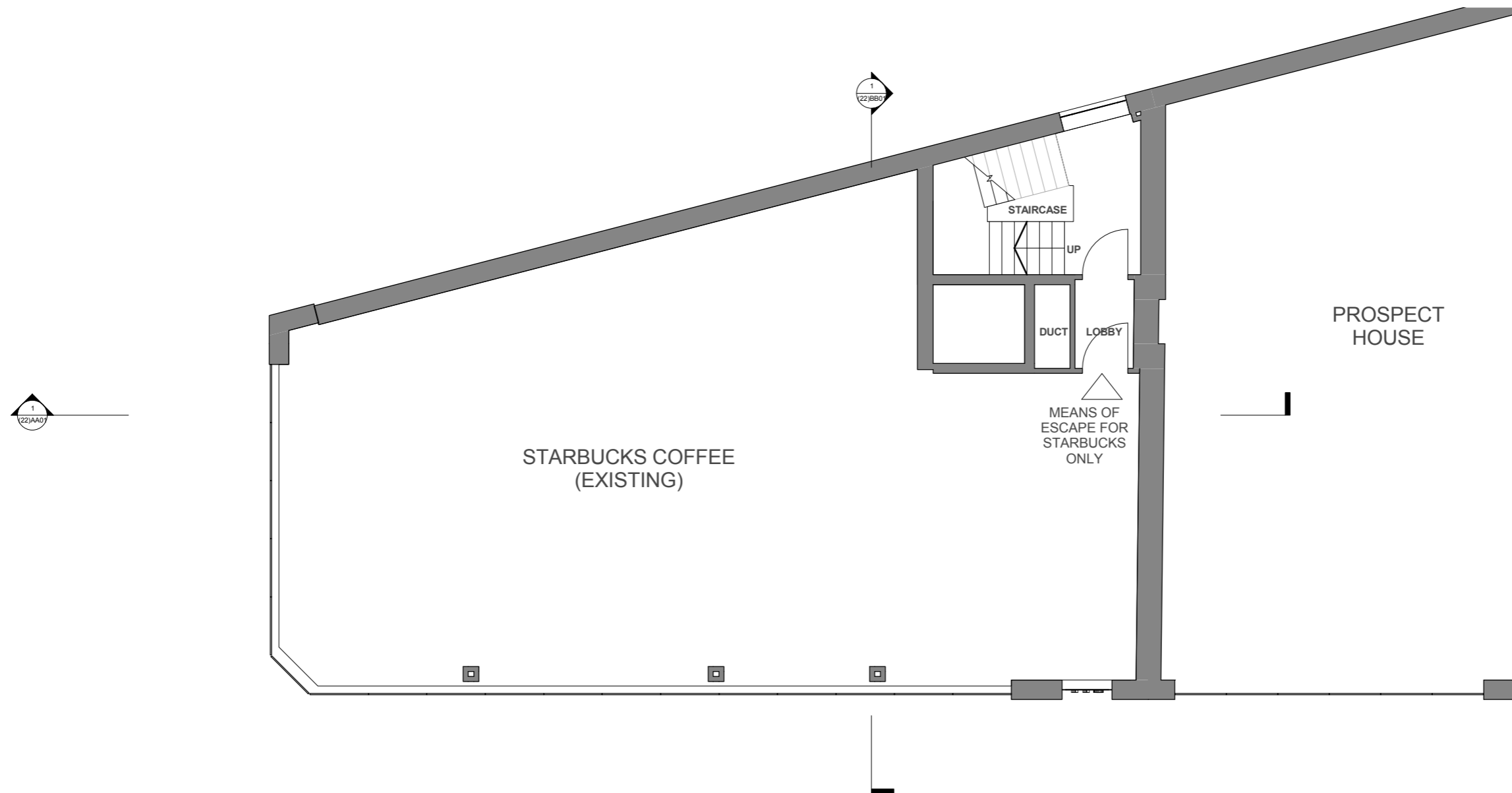
5.2: Proposed Development :  
Site Block Plan @ 1:200



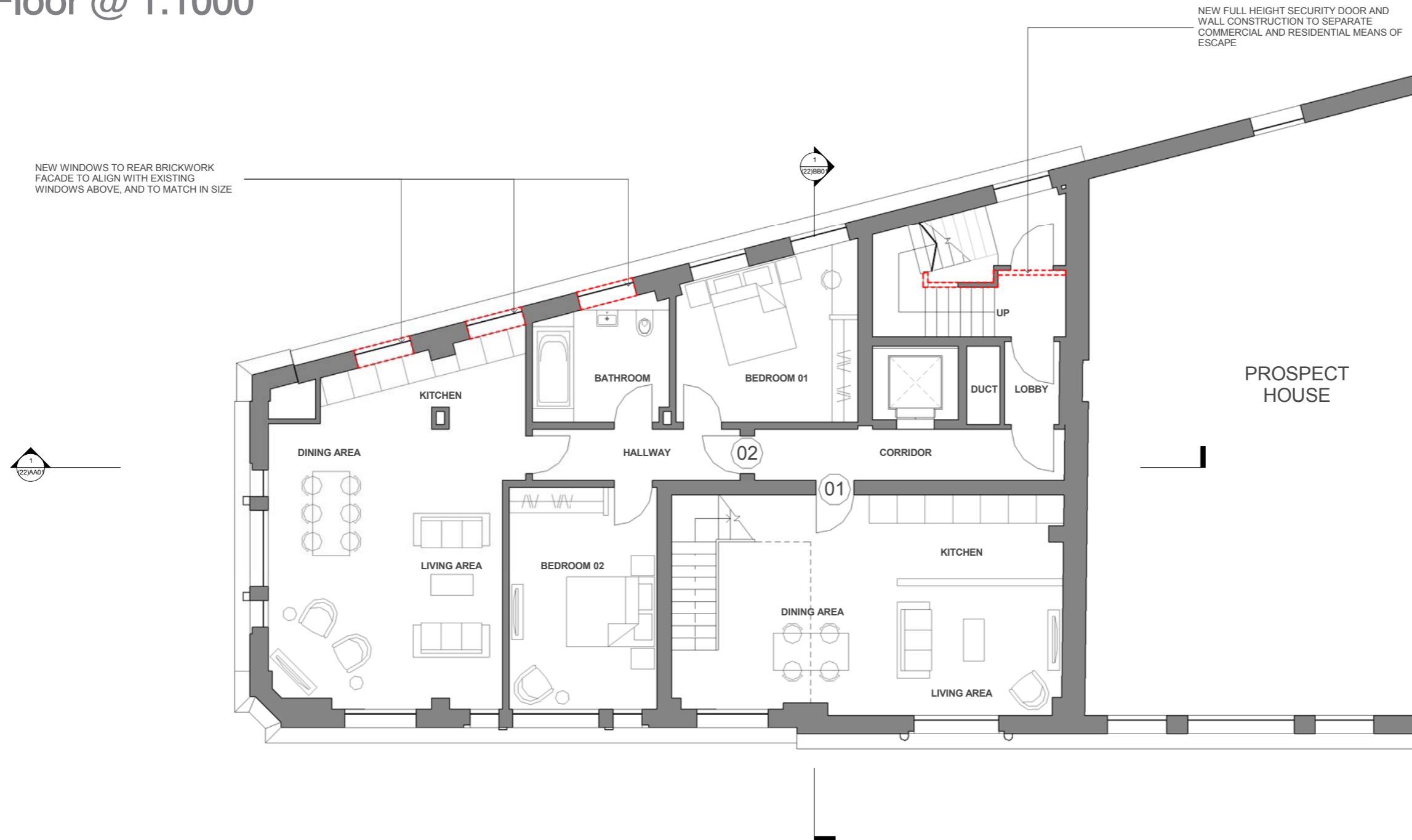
### 5.3: Proposed Development : Ground Floor @ 1:1000



# 5.4: Proposed Development : First Floor @ 1:1000



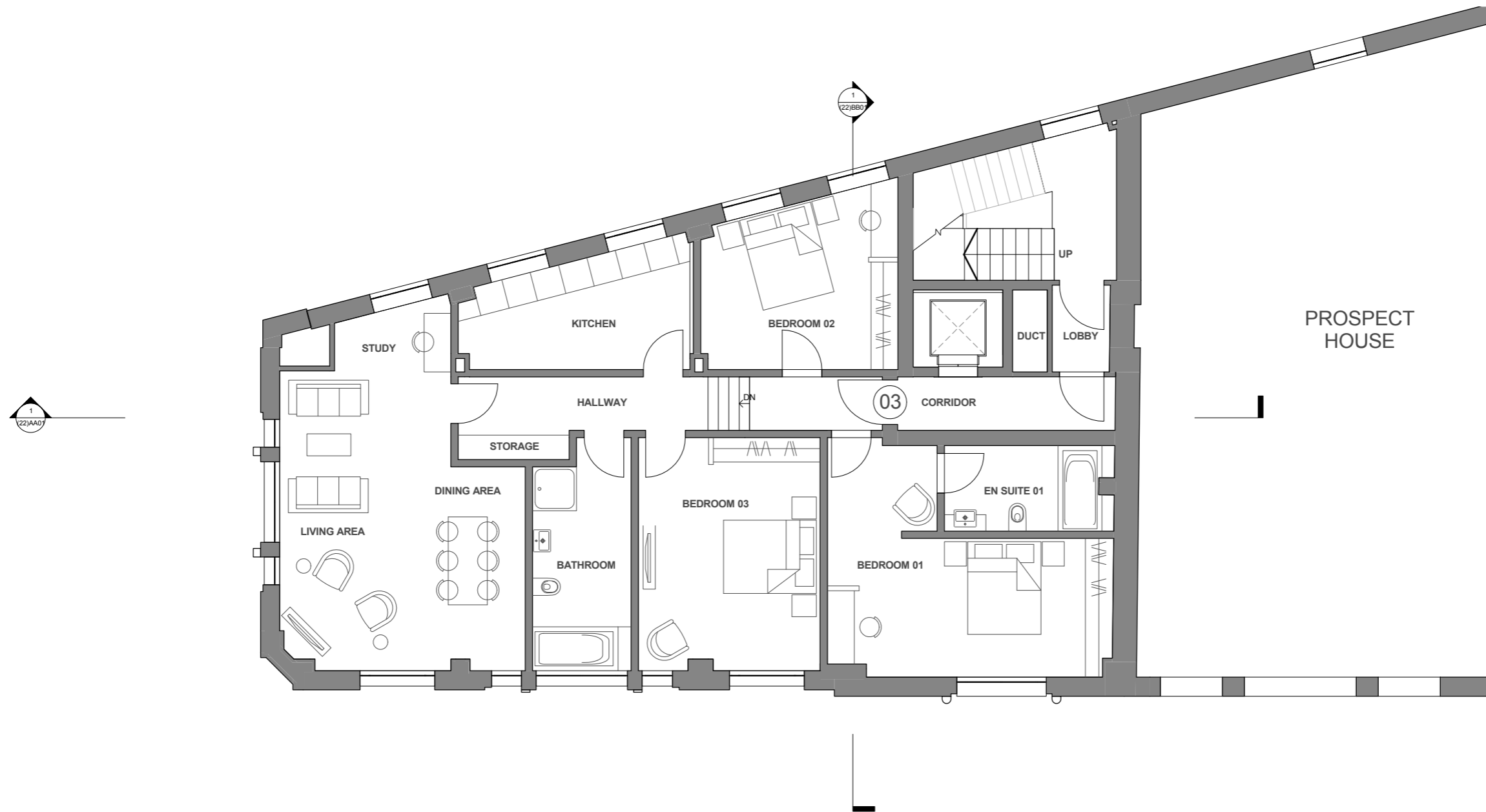
# 5.5: Proposed Development : Second Floor @ 1:1000



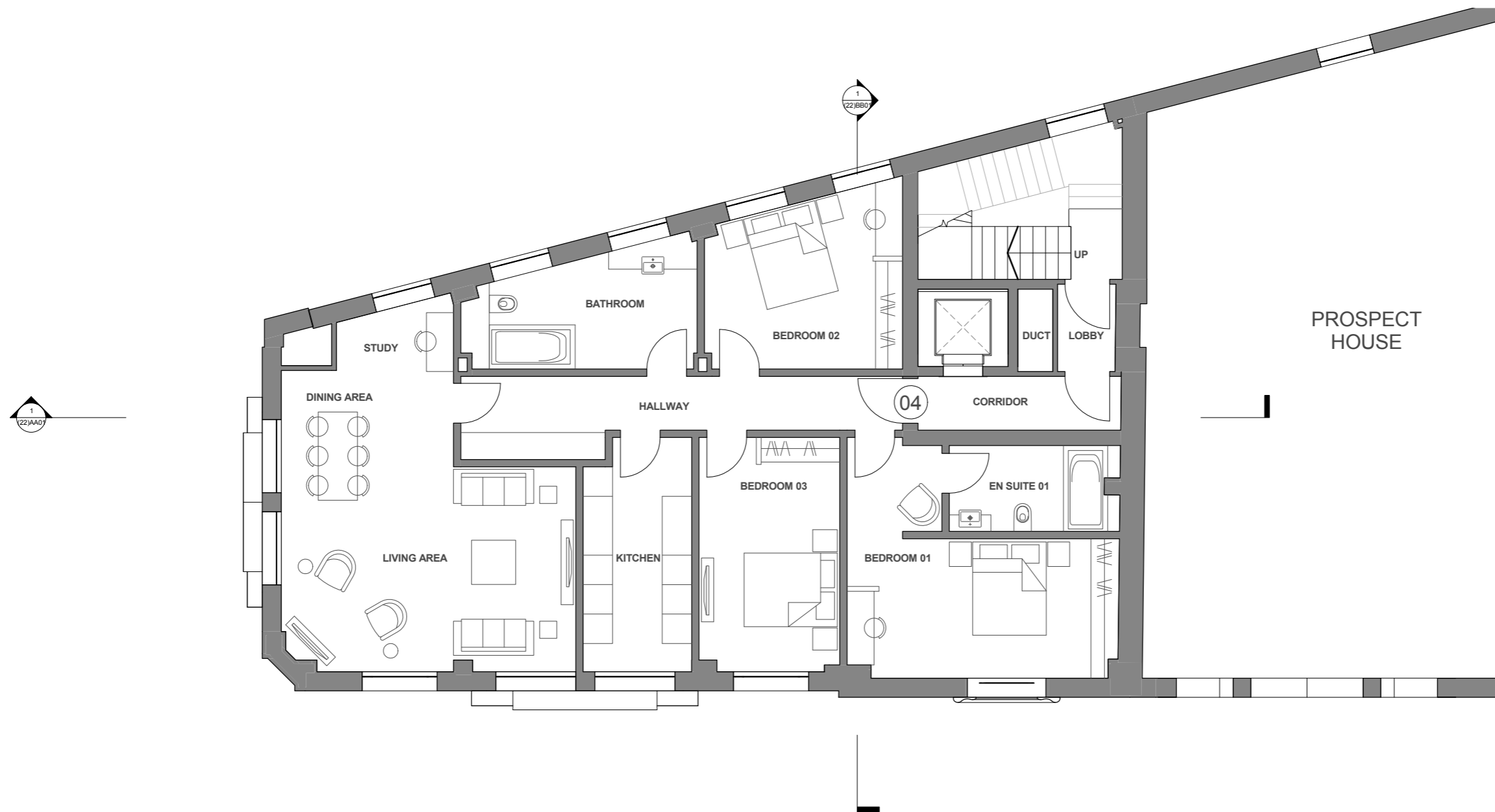
## 5.6: Proposed Development : Third Floor @ 1:1000



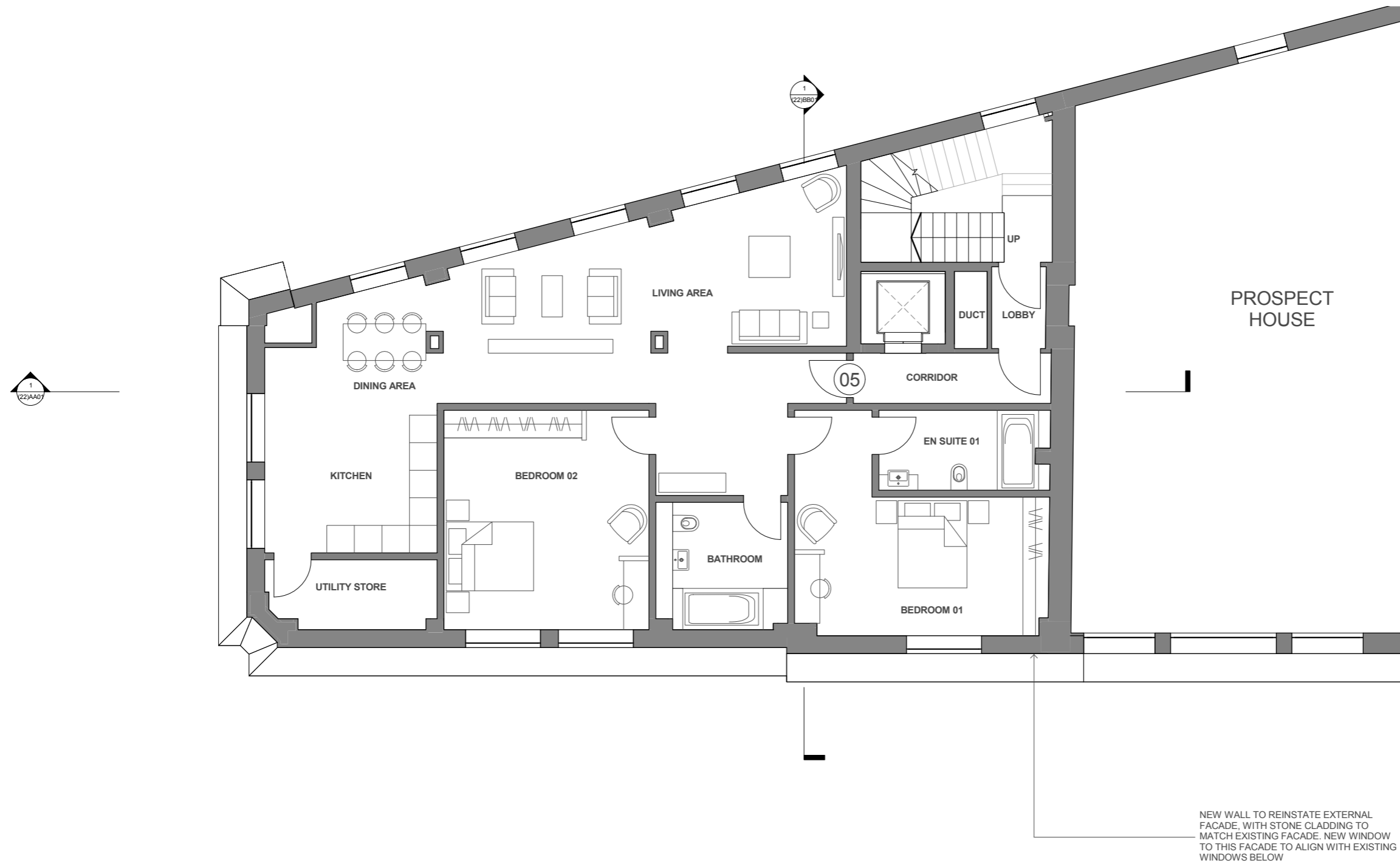
# 5.7: Proposed Development : Fourth Floor @ 1:1000



# 5.8: Proposed Development : Fifth Floor @ 1:1000

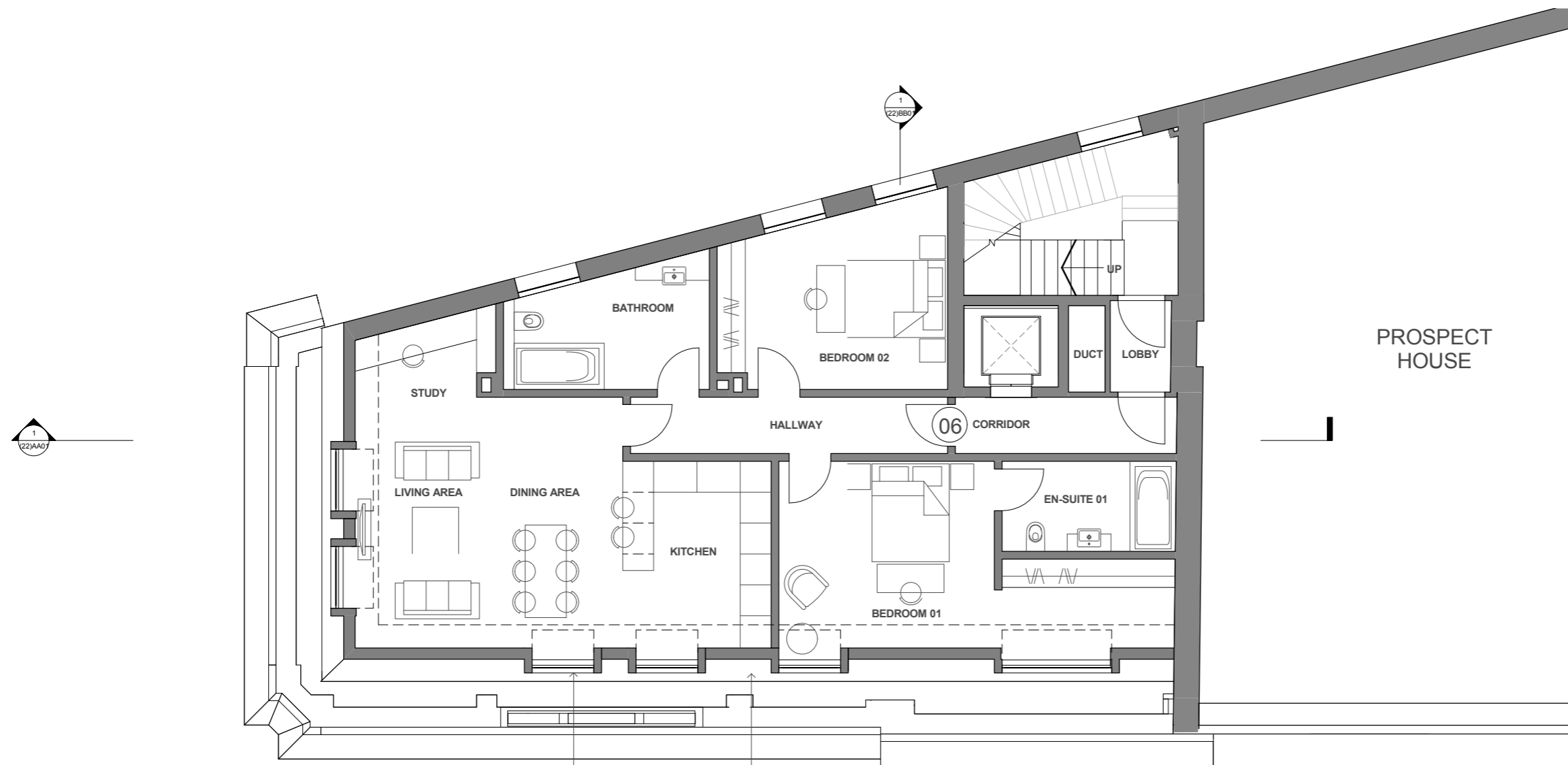


# 5.9: Proposed Development : Sixth Floor @ 1:1000





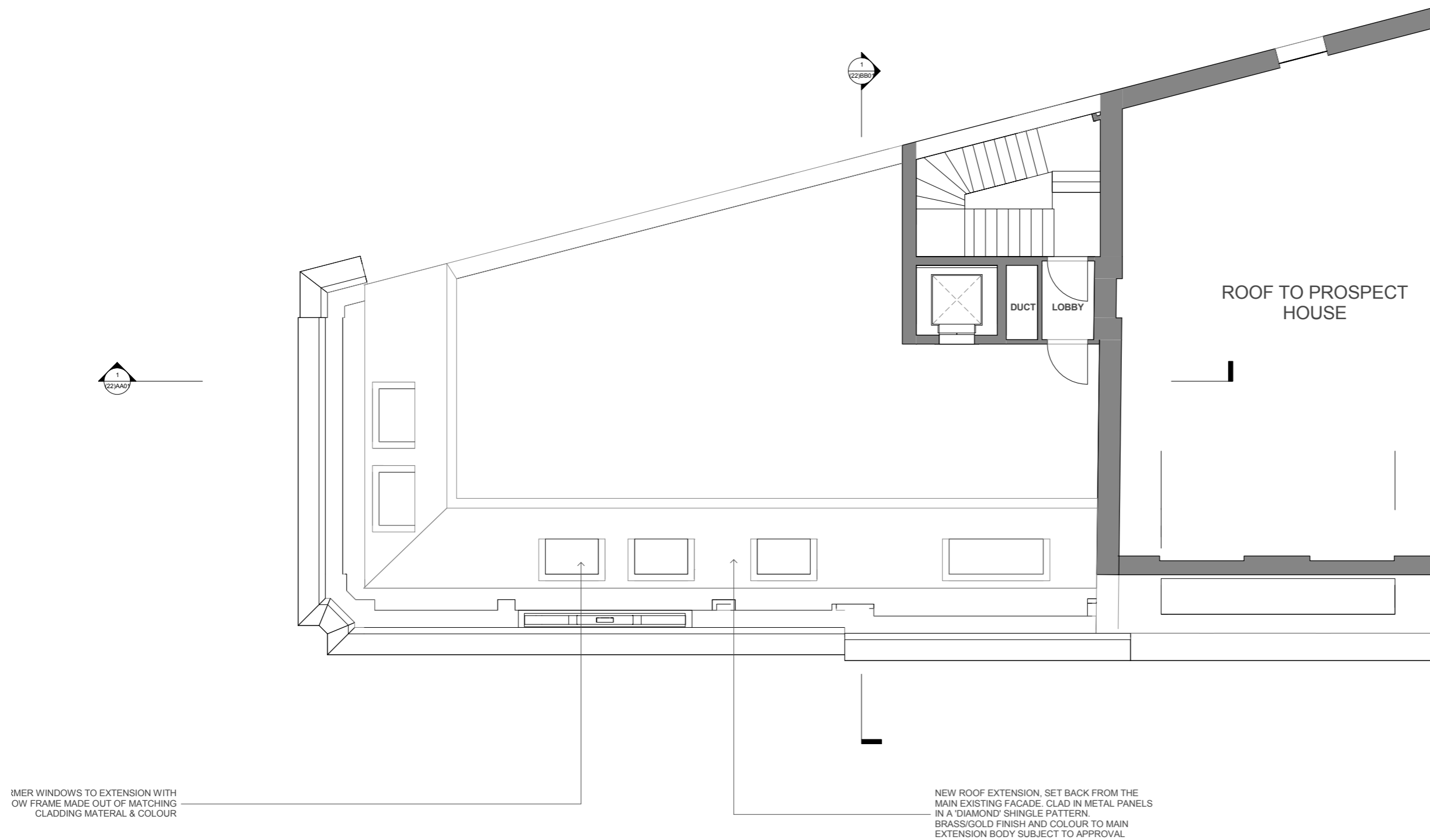
# 5.10: Proposed Development : Seventh Floor @ 1:1000



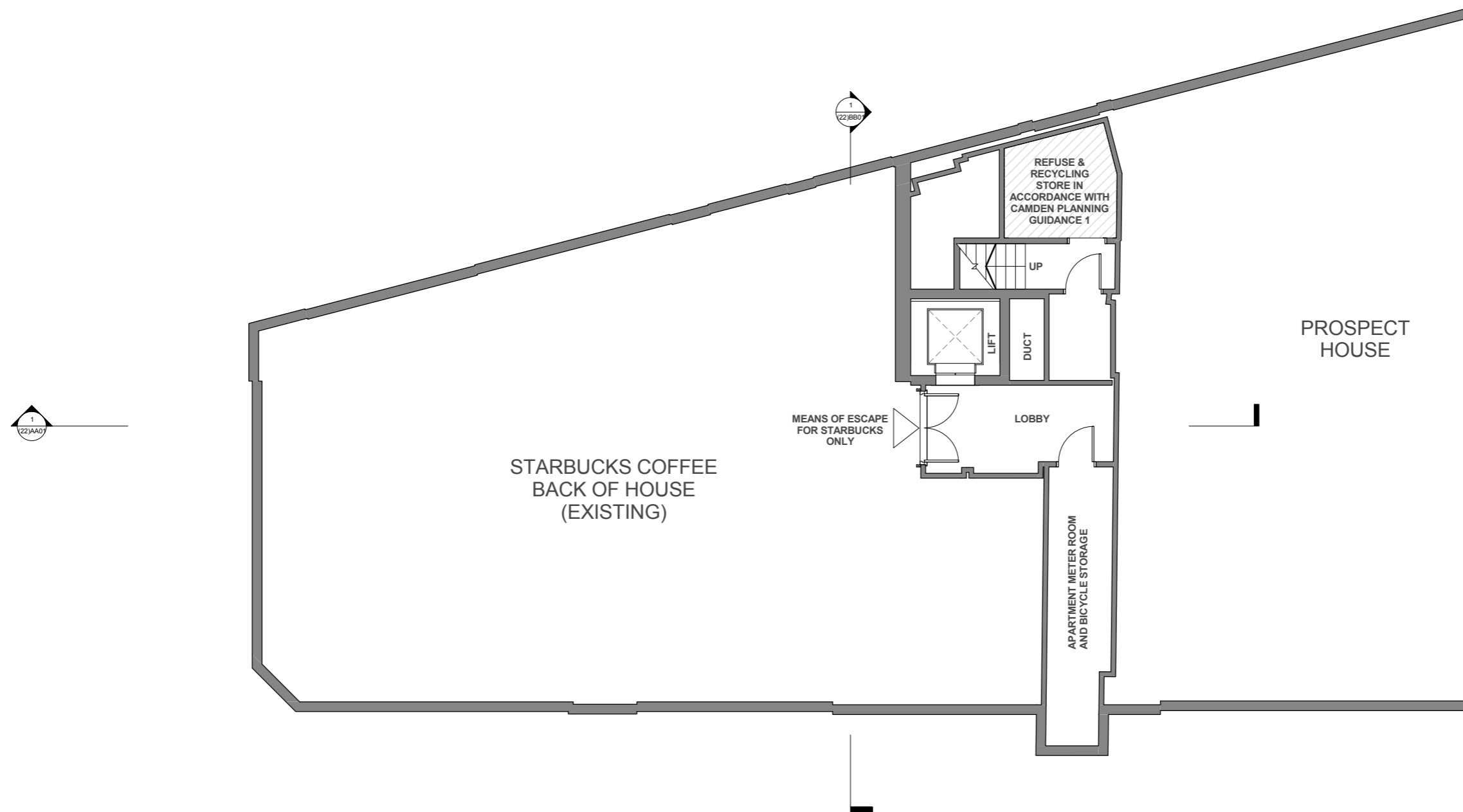
FORMER WINDOWS TO EXTENSION WITH  
DOW FRAME MADE OUT OF MATCHING  
CLADDING MATERIAL & COLOUR

NEW ROOF EXTENSION, SET BACK FROM THE  
MAIN EXISTING FACADE. CLAD IN METAL PANELS  
IN A 'DIAMOND' SHINGLE PATTERN.  
BRASS/GOLD FINISH AND COLOUR TO MAIN  
EXTENSION BODY SUBJECT TO APPROVAL

# 5.11: Proposed Development : Roof Plan @ 1:1000



# 5.13: Proposed Development : Basement Plan @ 1:1000



## 5.14: Proposed Development : Proposed Area Schedule

### Apartment 01

|             |              |                      |                      |
|-------------|--------------|----------------------|----------------------|
| GA Level 03 | Apartment 01 | 8.88 m <sup>2</sup>  | Bathroom             |
| GA Level 03 | Apartment 01 | 32.00 m <sup>2</sup> | Bedroom              |
| GA Level 03 | Apartment 01 | 3.89 m <sup>2</sup>  | Storage              |
| GA Level 02 | Apartment 01 | 7.78 m <sup>2</sup>  | Kitchen              |
| GA Level 02 | Apartment 01 | 11.82 m <sup>2</sup> | Living Area          |
| GA Level 02 | Apartment 01 | 6.80 m <sup>2</sup>  | Dining Room          |
| GA Level 02 | Apartment 01 | 12.62 m <sup>2</sup> | Stairs & Circulation |
| GA Level 03 | Apartment 01 | 3.05 m <sup>2</sup>  | Wardrobe             |
| GA Level 03 | Apartment 01 | 1.10 m <sup>2</sup>  | Storage              |
|             |              | 87.93 m <sup>2</sup> |                      |

### Apartment 02

|             |              |                      |             |
|-------------|--------------|----------------------|-------------|
| GA Level 02 | Apartment 02 | 11.22 m <sup>2</sup> | Kitchen     |
| GA Level 02 | Apartment 02 | 7.25 m <sup>2</sup>  | Bathroom    |
| GA Level 02 | Apartment 02 | 13.35 m <sup>2</sup> | Bedroom 01  |
| GA Level 02 | Apartment 02 | 4.89 m <sup>2</sup>  | Hall        |
| GA Level 02 | Apartment 02 | 15.19 m <sup>2</sup> | Bedroom 02  |
| GA Level 02 | Apartment 02 | 18.10 m <sup>2</sup> | Living Area |
| GA Level 02 | Apartment 02 | 8.37 m <sup>2</sup>  | Dining Area |
|             |              | 78.37 m <sup>2</sup> |             |

### Apartment 03

|             |              |                       |             |
|-------------|--------------|-----------------------|-------------|
| GA Level 04 | Apartment 03 | 5.98 m <sup>2</sup>   | En Suite 01 |
| GA Level 04 | Apartment 03 | 20.67 m <sup>2</sup>  | Bedroom 01  |
| GA Level 04 | Apartment 03 | 17.65 m <sup>2</sup>  | Bedroom 03  |
| GA Level 04 | Apartment 03 | 9.09 m <sup>2</sup>   | Bathroom    |
| GA Level 04 | Apartment 03 | 17.32 m <sup>2</sup>  | Living Area |
| GA Level 04 | Apartment 03 | 10.53 m <sup>2</sup>  | Kitchen     |
| GA Level 04 | Apartment 03 | 13.69 m <sup>2</sup>  | Bedroom 02  |
| GA Level 04 | Apartment 03 | 9.51 m <sup>2</sup>   | Hall        |
| GA Level 04 | Apartment 03 | 10.13 m <sup>2</sup>  | Dining Area |
| GA Level 04 | Apartment 03 | 3.05 m <sup>2</sup>   | Study       |
|             |              | 117.61 m <sup>2</sup> |             |

### Apartment 04

|             |              |                       |             |
|-------------|--------------|-----------------------|-------------|
| GA Level 05 | Apartment 04 | 10.00 m <sup>2</sup>  | Hall        |
| GA Level 05 | Apartment 04 | 13.70 m <sup>2</sup>  | Bedroom 02  |
| GA Level 05 | Apartment 04 | 10.54 m <sup>2</sup>  | Bathroom    |
| GA Level 05 | Apartment 04 | 5.98 m <sup>2</sup>   | En Suite 01 |
| GA Level 05 | Apartment 04 | 19.26 m <sup>2</sup>  | Bedroom 01  |
| GA Level 05 | Apartment 04 | 13.57 m <sup>2</sup>  | Bedroom 03  |
| GA Level 05 | Apartment 04 | 22.74 m <sup>2</sup>  | Living Area |
| GA Level 05 | Apartment 04 | 10.21 m <sup>2</sup>  | Kitchen     |
| GA Level 05 | Apartment 04 | 8.88 m <sup>2</sup>   | Dining Area |
| GA Level 05 | Apartment 04 | 3.06 m <sup>2</sup>   | Study       |
| GA Level 05 | Apartment 04 | 1.62 m <sup>2</sup>   | Storage     |
|             |              | 119.53 m <sup>2</sup> |             |

### Apartment 05

|             |              |                       |             |
|-------------|--------------|-----------------------|-------------|
| GA Level 06 | Apartment 05 | 21.31 m <sup>2</sup>  | Bedroom 02  |
| GA Level 06 | Apartment 05 | 7.82 m <sup>2</sup>   | Bathroom    |
| GA Level 06 | Apartment 05 | 19.68 m <sup>2</sup>  | Bedroom 01  |
| GA Level 06 | Apartment 05 | 25.54 m <sup>2</sup>  | Living Area |
| GA Level 06 | Apartment 05 | 6.37 m <sup>2</sup>   | En Suite 01 |
| GA Level 06 | Apartment 05 | 12.21 m <sup>2</sup>  | Kitchen     |
| GA Level 06 | Apartment 05 | 5.40 m <sup>2</sup>   | Store       |
| GA Level 06 | Apartment 05 | 8.70 m <sup>2</sup>   | Dining Area |
| GA Level 06 | Apartment 05 | 15.20 m <sup>2</sup>  | Hall        |
|             |              | 122.24 m <sup>2</sup> |             |

### Apartment 06

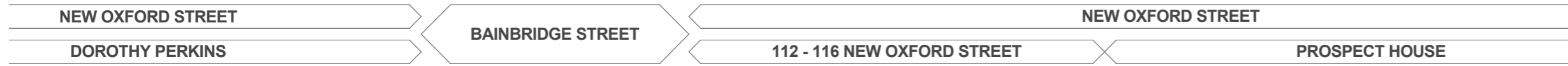
|             |              |                       |             |
|-------------|--------------|-----------------------|-------------|
| GA Level 07 | Apartment 06 | 24.61 m <sup>2</sup>  | Bedroom 01  |
| GA Level 07 | Apartment 06 | 6.75 m <sup>2</sup>   | Hall        |
| GA Level 07 | Apartment 06 | 14.73 m <sup>2</sup>  | Bedroom 02  |
| GA Level 07 | Apartment 06 | 8.79 m <sup>2</sup>   | Bathroom    |
| GA Level 07 | Apartment 06 | 34.32 m <sup>2</sup>  | Living Area |
| GA Level 07 | Apartment 06 | 11.75 m <sup>2</sup>  | Kitchen     |
| GA Level 07 | Apartment 06 | 5.91 m <sup>2</sup>   | En Suite 01 |
|             |              | 106.86 m <sup>2</sup> |             |

### Lobby

|             |       |                      |       |
|-------------|-------|----------------------|-------|
| GA Level 00 | Lobby | 8.57 m <sup>2</sup>  | Inner |
| GA Level 00 | Lobby | 6.81 m <sup>2</sup>  | Outer |
|             |       | 15.38 m <sup>2</sup> |       |

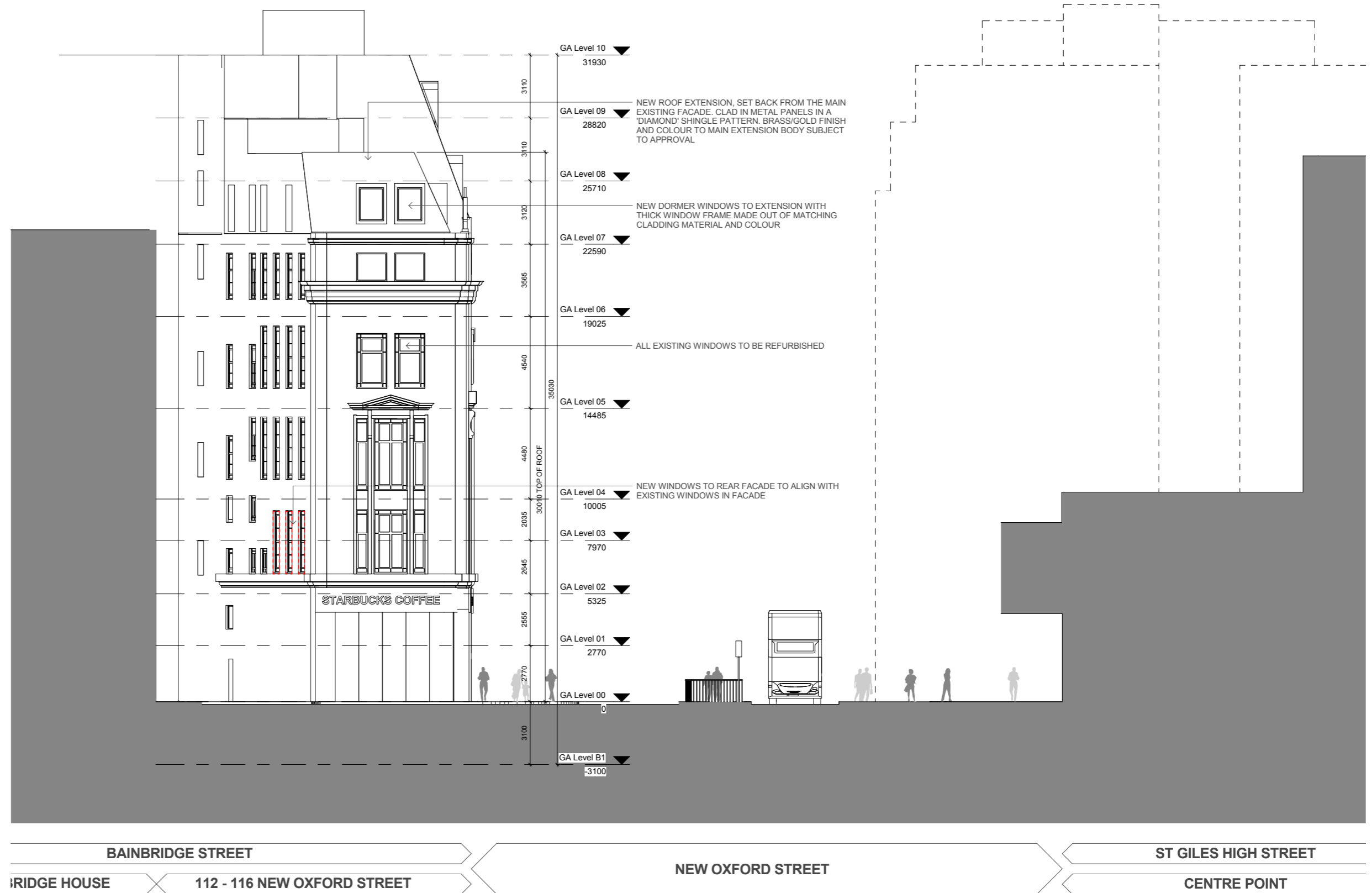
| Area Schedule (Gross Building) |                       |
|--------------------------------|-----------------------|
| Level                          | Area                  |
| GA Level B1                    | 37.61 m <sup>2</sup>  |
| GA Level 00                    | 44.45 m <sup>2</sup>  |
| GA Level 01                    | 23.81 m <sup>2</sup>  |
| GA Level 02                    | 174.74 m <sup>2</sup> |
| GA Level 03                    | 80.04 m <sup>2</sup>  |
| GA Level 04                    | 174.65 m <sup>2</sup> |
| GA Level 05                    | 174.65 m <sup>2</sup> |
| GA Level 06                    | 174.63 m <sup>2</sup> |
| GA Level 07                    | 148.42 m <sup>2</sup> |
| GA Level 08                    | 125.00 m <sup>2</sup> |
| 1157.99 m <sup>2</sup>         |                       |

# 5.15: Proposed Development : New Oxford Street Elevation

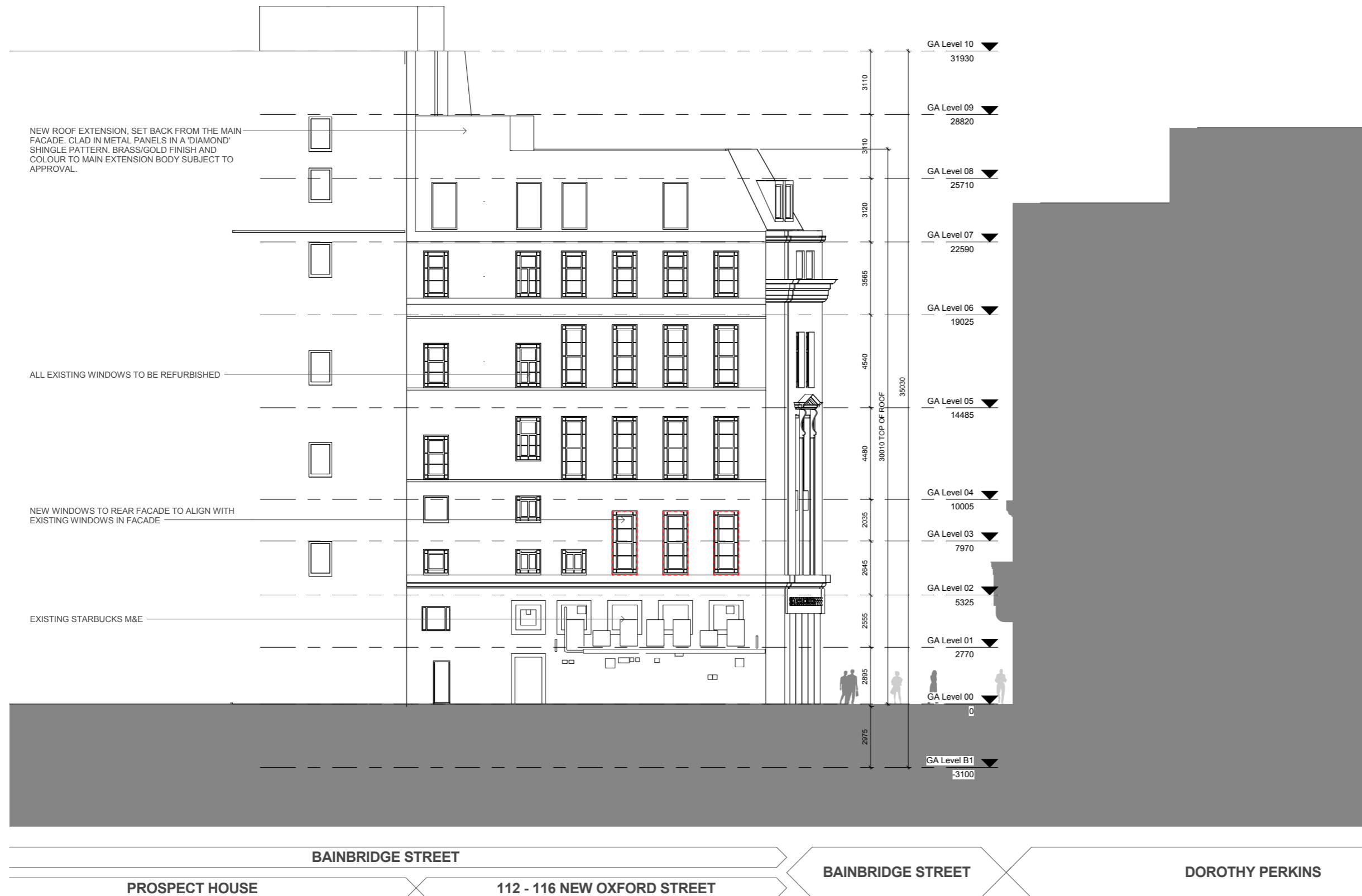


1 GA South Elevation 1:100

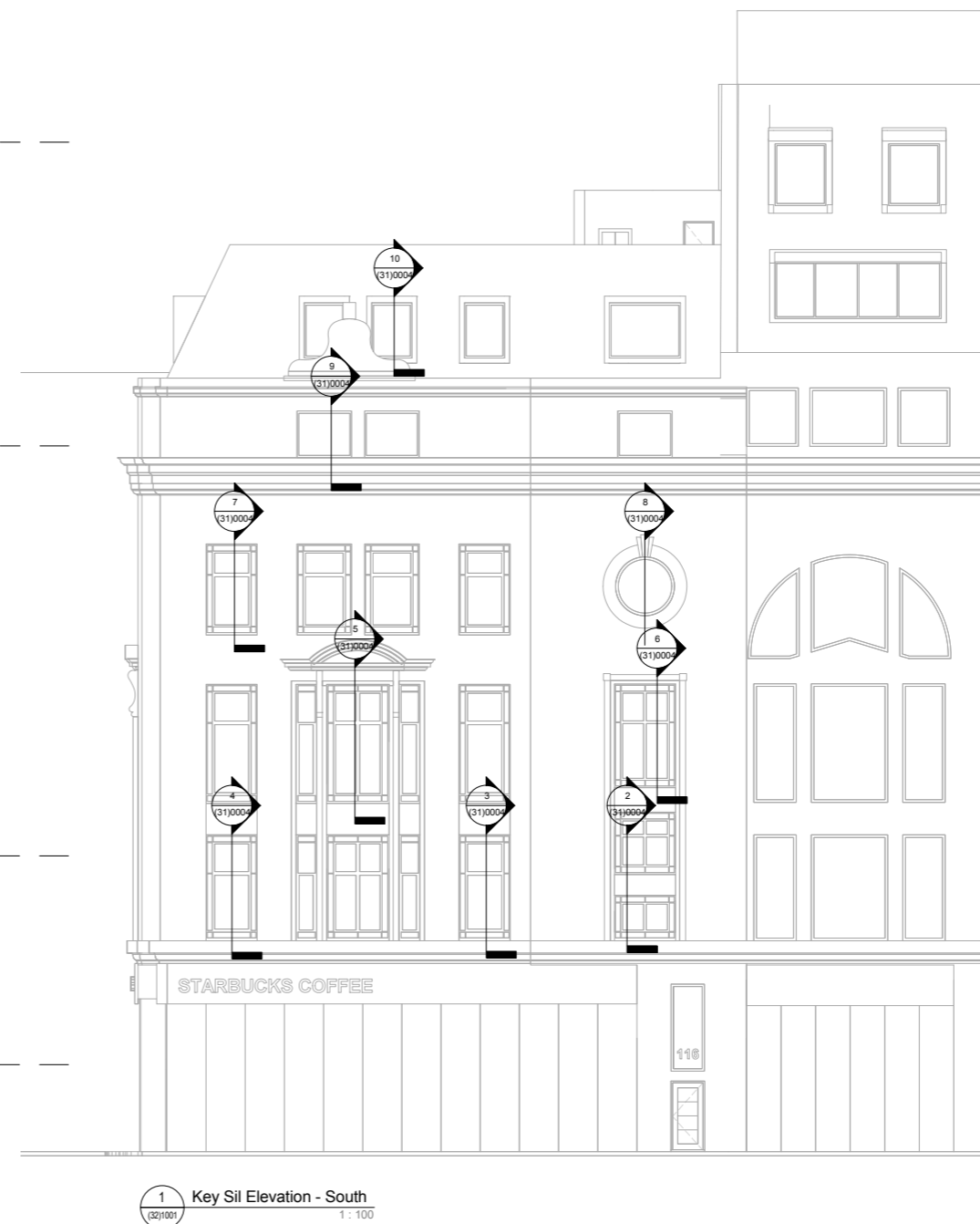
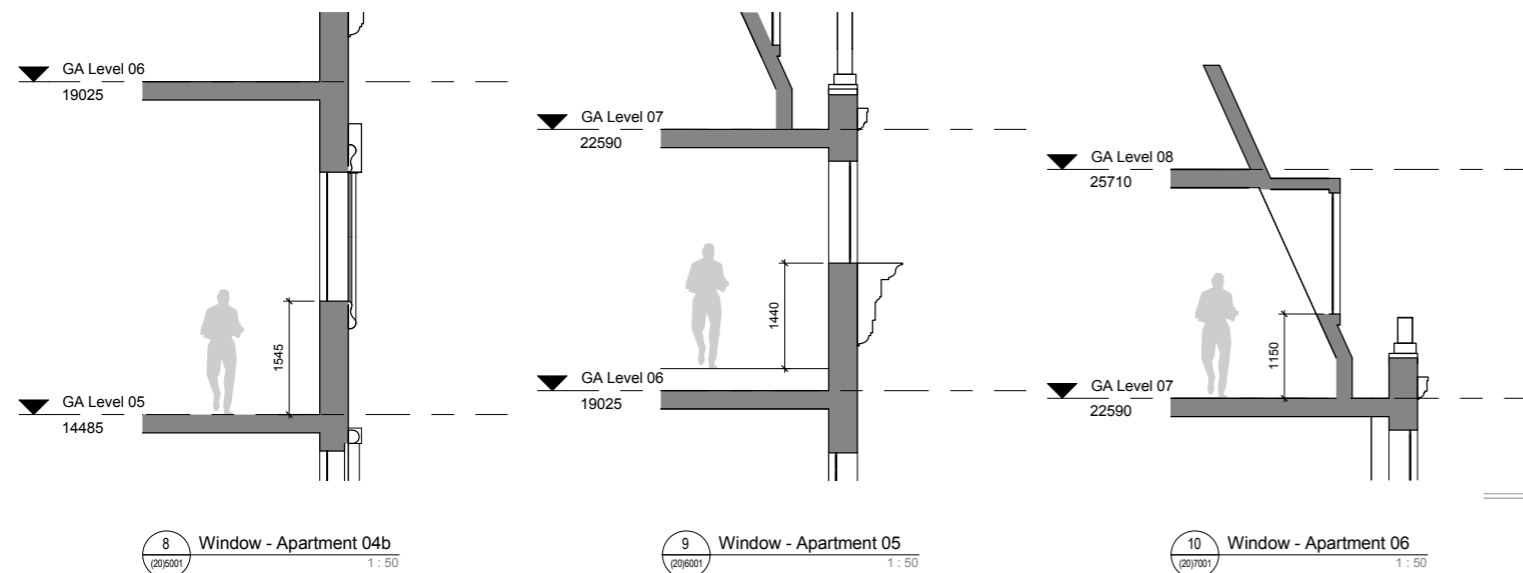
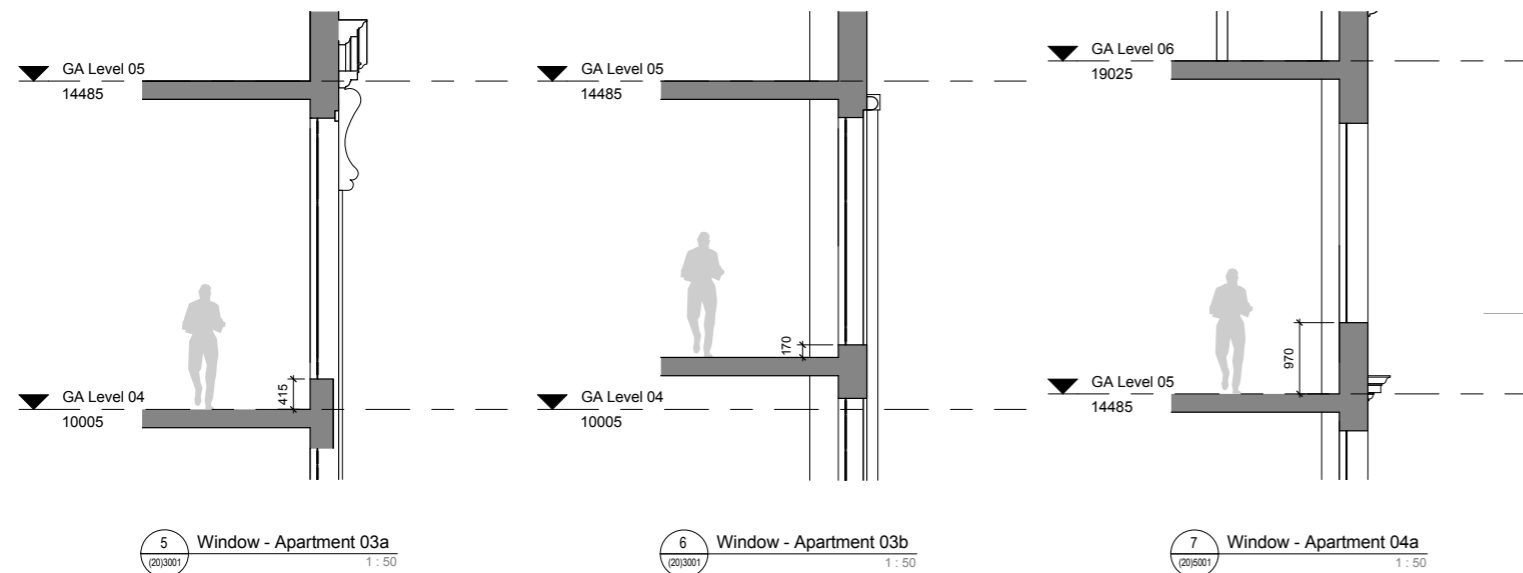
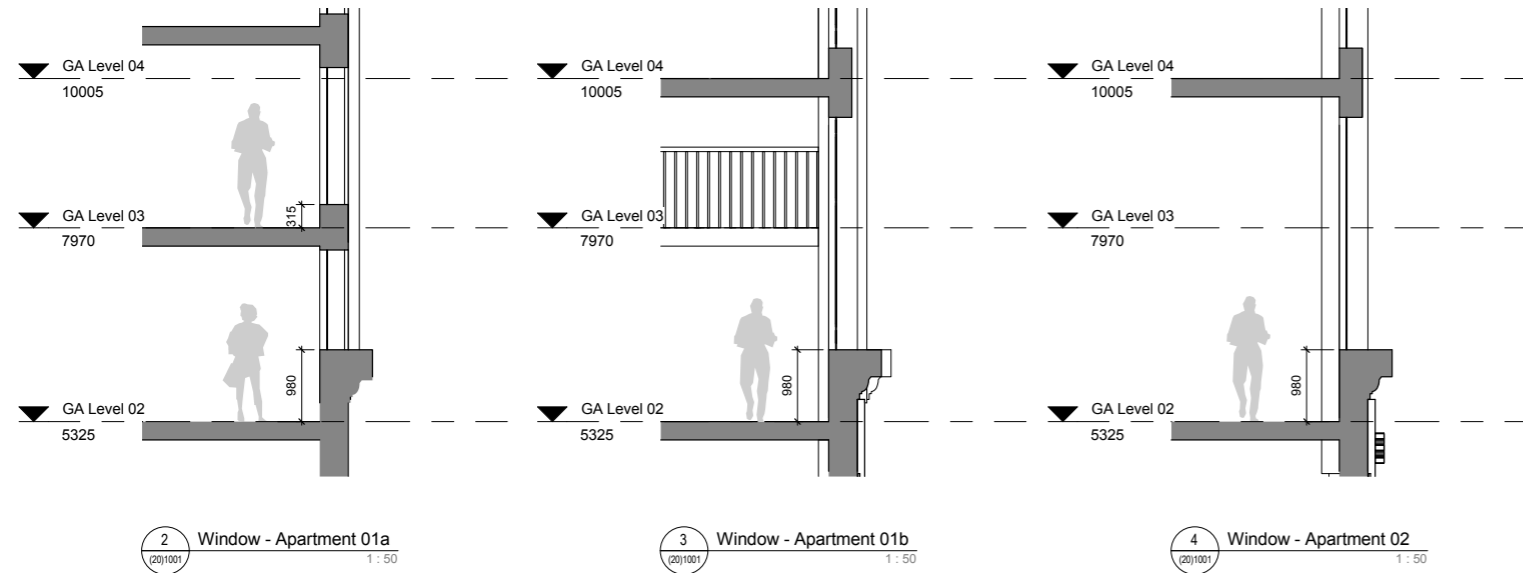
# 5.16: Proposed Development : Bainbridge Street Elevation



# 5.17: Proposed Development : Bainbridge Street Elevation



# 5.18: Proposed Development : Window Sill Heights





**5.18: Proposed Development :**  
**Coloured Elevations;**  
**New Oxford Street**



**5.19: Proposed Development :**  
Coloured Elevation; Bainbridge Street

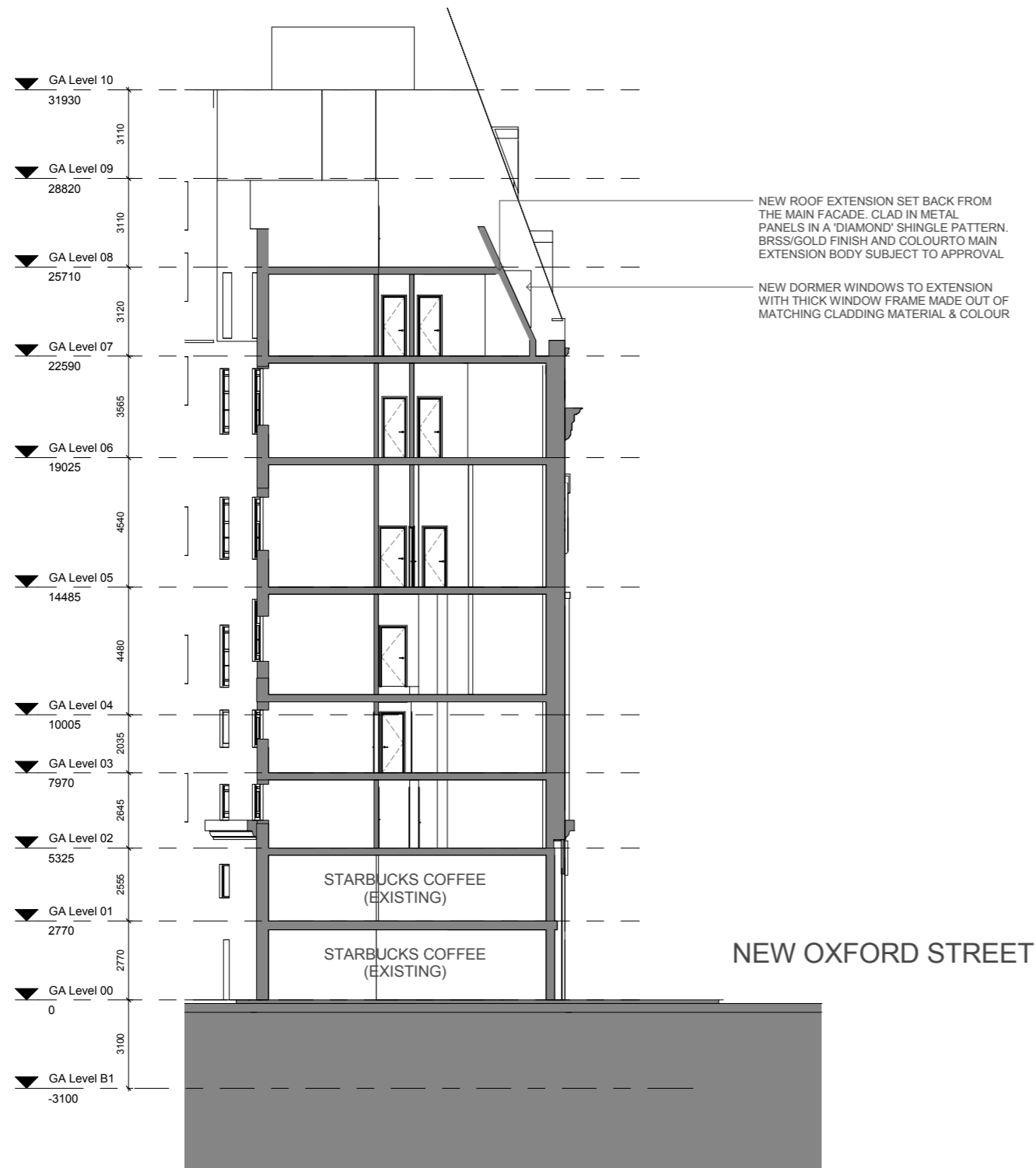


5.20: Proposed Development :  
Coloured Elevation;  
Bainbridge Street

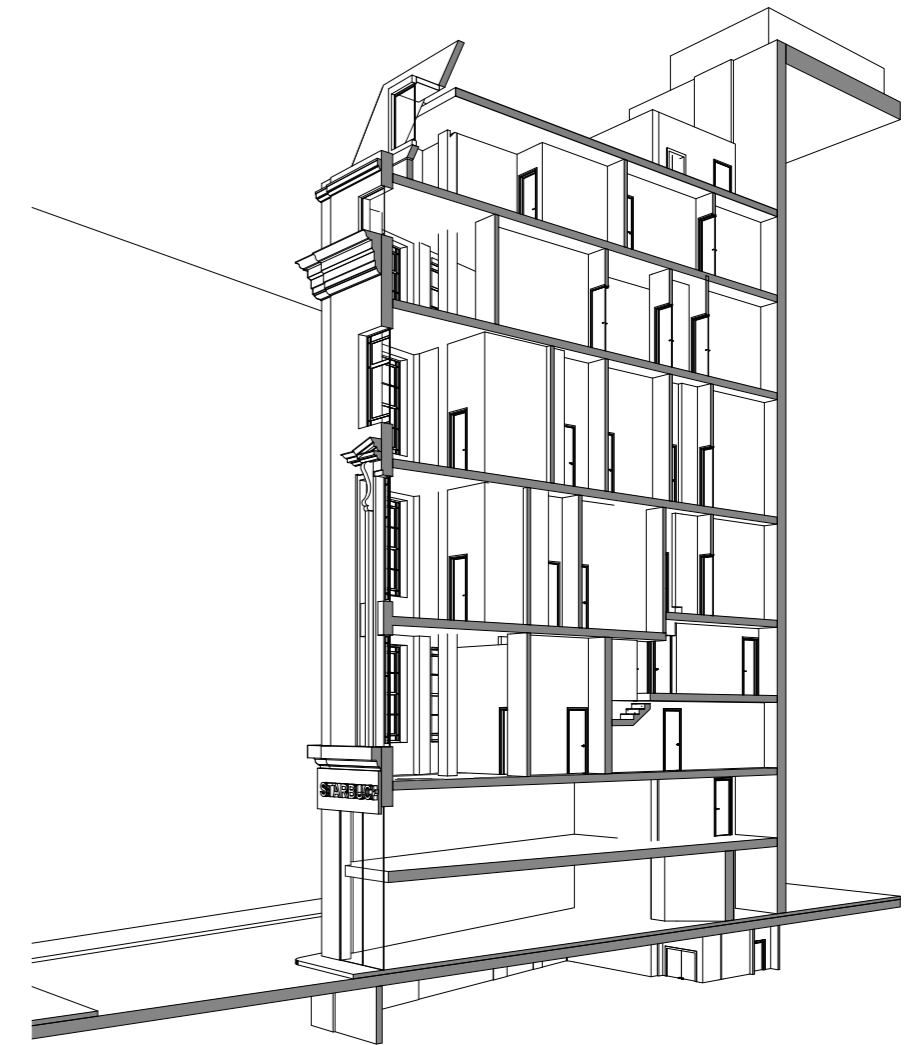
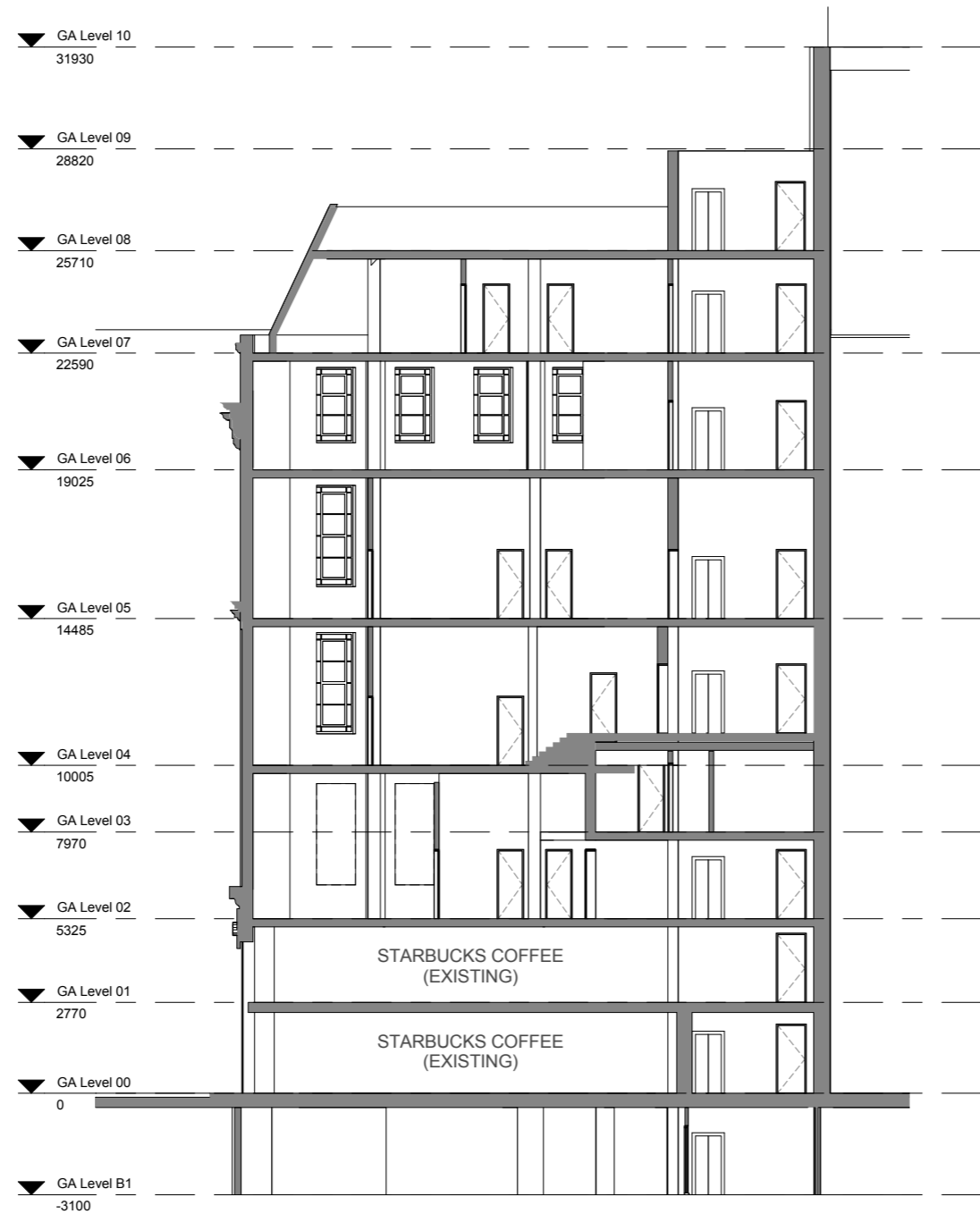




## 5.21: Proposed Development : Short Cross Section



# 5.22: Proposed Development : Long Cross Section



**6.0: Proposed Development :**  
Photomontage Within Context  
View From Tottenham Court Road  
Junction



**6.0: Proposed Development :**  
Photomontage Within Context  
View From New Oxford Street





## 7.0: Supporting Statements:

In addition to the provision of the planning and regeneration benefits which are intrinsic to the proposed scheme, it is anticipated that an appropriate package of Section 106 contributions will be negotiated and agreed with London Borough of Camden in due course in accordance with the test set out in the Community Infrastructure Regulations 2010.

It is anticipated that planning obligations could include the following areas:

- Affordable Housing
- Education
- Public Open Space
- Transport
- CIL ( Community Infrastructure levy )

As part of the Planning Submission we are aware that a series of statements and reports have been requested by the camden Council which are listed below:

- Marketing
- local procurement and Local Employment
- Listed Building / Conservation Area Appraisal
- Affordable Housing
- Secure By Design
- Accessibility Statement
- Life Time Homes
- Service management Plan
- Construction Management Plan

# 7.1: Supporting Statements : Marketing Report



**Report relating to**  
**112-116 New Oxford Street, W1**

## Contents

1. **Introduction and location**
2. **Market Commentary**
  - 2.1 Supply
  - 2.2 Development
  - 2.3 Take-up
3. **Summary**

### Important Note



## 1. Introduction and location

For research reporting purposes the subject property is classed as Grade B office space due to the fact that it has not undergone any significant refurbishment/development works in the last five-years and due to its configuration and size of floor plates.

The subject property lies on the southern edge of the Camden borough close to the boundary with the City of Westminster. Its location aligns it more closely with characteristics of the West End office market as opposed to Camden, in terms of supply and demand trends. The majority of office stock in Camden falls within the Savills research boundary of the Noho submarket. Noho runs from Woburn Place/Southampton Row to Portland Place, and is bounded to the north and south by Euston Road and Oxford Street respectively.

For clarity, analysis of the supply and demand trends for the purposes of this report will be based on the Noho submarket.



# 7.1: Supporting Statements: Marketing Report



## 2. Market Commentary

### 2.1 Supply

The Noho submarket is the West End's largest submarket with an office stock figure of approximately 13m sq ft, this is 11% of the West End's total office stock.

We estimate there is 592,000 sq ft of available space in the submarket, this equates to a vacancy rate of 5%, this is above the overall vacancy rate of the wider West End which currently stands at 3.8%.

58% of space is of Grade A quality, this is just under 343,000 sq ft of available Grade A space. The recent rise in Grade A space in Noho is the result of 90,000 sq ft of developments completing in Noho and entering the supply figures this year. 42% of all space available in Noho is of Grade B quality, this is 250,000 sq ft of available Grade B space.

Our supply data estimates that office property in Noho has been vacant on average around 1.3 years. When analysing the amount of time Grade A and Grade B quality space has been available, the difference is significant, on average Grade A space has been vacant for 0.7 years whilst Grade B space on average is available for 1.7 years.

Figure 1 shows the percentage breakdown of available office property in Noho. 100% of all office space available more than two years in the submarket is of Grade B quality, putting this in to context this equates to 149,000 sq ft of Grade B office space being vacant for more than two years.

Figure 2.1 Years vacant by grade

| Years Vacant            | Grade A | Grade B |
|-------------------------|---------|---------|
| Less than 1 year        | 80%     | 20%     |
| More than 1 less than 2 | 56%     | 44%     |
| More than 2 less than 3 | 0%      | 100%    |
| More than 3 less than 4 | 0%      | 100%    |
| More than 4 less than 5 | 0%      | 100%    |
| More than 5             | 0%      | 100%    |

An important factor to take in to consideration when assessing the potential impact of a loss in office space is to look at the 'years of supply' in the area. In the national market place two years of supply suggests an average level of supply.

Across all grades of office space in Noho, years of supply stands at 1 year, suggesting that the market is under supplied, however this is more or less in-line with the wider West End market. 11 out of 12 submarkets in the West End are currently under supplied in terms of years of supply.



## 2.2 Development

After four years of restricted levels of development activity in the West End, 2013 will see a return to average levels of development activity reaching 1.8m sq ft.

In Noho, development activity has also picked up with approximately 678,000 sq ft of developments and extensive refurbishments to enter the supply figures over the next two years (2013-14). The average level of completions seen per annum in Noho is 290,000 sq ft, in 2013 220,200 sq ft will be complete, down on the average. 2014 however, will see a return to above average levels of completions at 457,500 sq ft.

Figure 2 shows a list of developments that are due for completion in the Noho submarket over the next two years (2013-14).

Figure 2.2 Development pipeline in Noho

| Building                 | STREET                              | PC  | TYPE   | SPECULATIVE | Timing  | STATUS |
|--------------------------|-------------------------------------|-----|--------|-------------|---------|--------|
| St George's Court, 2-12  | Bloomsbury Way / 2-28 New Oxford St | WC1 | refurb | 152,239     | Q3 2013 | U/C    |
| 2                        | Stephen Street, W1                  | W1  | refurb | 68,000      | Q3 2013 | U/C    |
| Walmar House, 288/300    | Regent street                       | w1  | refurb | 40,000      | Q1 2014 | U/C    |
| 1                        | Mabledon Place                      | WC1 | dev    | 87,500      | Q1 2014 | PPG    |
| Fitzroy Place            | Mortimer Street                     | W1  | dev    | 260,000     | Q4 2014 | APP    |
| Regent House             | Edgware Road/George St              | W1  | dev    | 50,000      | Q4 2014 | site   |
| 61-63                    | Tottenham Court Road                | W1  | dev    | 20,000      | Q4 2014 | PPG    |
| West End Delivery Office | Newman Street/Rathbone place        | W1  | dev    | 230,000     | Unknown | SITE   |
| Euston Station           |                                     | NW1 | dev    | 150,000     | Unknown | APP    |

Although not in the immediate vicinity of the subject property the regeneration of King's Cross will play an important part in shaping the future of the wider Camden office market. The site spans 67 acres and over the next 10 years, 50 buildings totalling 8m sq ft, 20 new streets and 10 new public spaces will be created. 3.4m sq ft office space will be delivered, up to 2,000 homes and serviced apartments, 500,000 sq ft of retail, up to 300 hotel bedrooms and 650 student units.

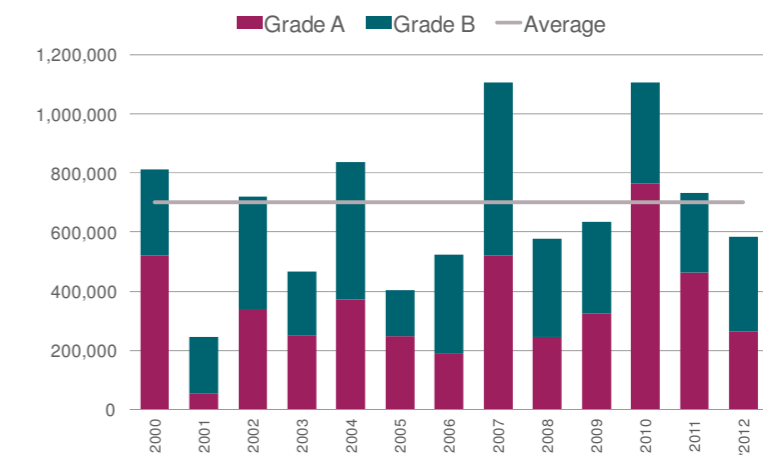
Focussing on the office element, 3.4m sq ft of office space in some 23 buildings will be built. A number of these buildings are already designed and some have consented planning. 184,000 sq ft in two buildings is being speculatively built at the scheme, 57,000 sq ft at 1 Pancras Square will be delivered in Q3 2013 and 127,000 sq ft at 2 Pancras Square will be delivered in Q2 2014. 568,000 sq ft has already been pre-let at the scheme, including BNP Paribas taking 350,000 sq ft in 2010, in 2011 Camden Council took 150,000 sq ft, Hoare Lea took 22,000 sq ft and Argent took 9,000 sq ft.



## 2.3 Take-up

Take-up in 2011 reached 731,500 sq ft, this is up on the 10-year average of 600,000 sq ft. As the graph below demonstrates there has been a bias towards Grade A quality space in recent years in the Noho market. Over a five-year period (2007-11) 56% of space taken has been of Grade A quality. 63% of space taken in 2011 was of the best quality.

Figure 2.3 Take-up in Noho



\*As at end Sept 12

As at end September 2012 take-up has reached 583,000 sq ft, this was boosted by two large deals of 97,000 sq ft at Greater London House to Asos and 44,000 sq ft at Oxford House, 76 Oxford Street to Publicis. Both deals were Grade B lettings, thus skewing Grade A office take-up in 2012 to be just 45%, down on the average of 56%. With just under 120,000 sq ft of space under offer in Noho, we estimate take-up levels to come in at average levels.

The structure of office demand in Noho mirrors that of the West End as a whole, with no dependency on any one business sector. The most dominant business sector over the period of 2007-2011 has been the Creative sector, taking a 21% share. The Professional and Public Services sector take the next largest shares with 14% and 16% respectively.

Going forward, the Public Sector's share of take-up in this market is likely to decline as the Government Property Unit (GPU) seeks to rationalise its central London office property needs. According to figures from the GPU, the government occupies 10m sq ft offices in central London, 57% of which is leasehold. The GPU's aspiration is to reduce occupancy by 45-50% over the next decade. Furthermore, over the next three years (2012-14), Oxford Economics forecasts Public sector employment to fall by 3.3% in Westminster and 3.1% in Camden. These factors are likely to result in a rise of tenant returns from this sector of Grade B quality office space back in to the market.

# 7.1: Supporting Statements :

## Marketing Report



### 3. Summary

- There is a substantial amount of long term vacant (more than 2 years) Grade B office floor space available in Noho, approximately 149,000 sq ft.
- Development pipeline in Noho is returning to average levels, we estimate 678,000 sq ft of developments to enter the supply figures over the next two years (2013-14). This will help up soak up average levels of demand expected over the next three years.
- The biggest take-up of new space by tenants is of Grade A floorspace (on average).
- There is a significant amount of new Grade A floor space at Kings Cross.
- The strategic relocation of Government Departments to outside of London will increase supply and vacancy levels.

### Important Note

Finally, in accordance with our normal practice, we would state that this report is for general informative purposes only and does not constitute a formal valuation, appraisal or recommendation. It is only for the use of the persons to whom it is addressed and no responsibility can be accepted to any third party for the whole or any part of its contents. It may not be published, reproduced or quoted in part or in whole, nor may it be used as a basis for any contract, prospectus, agreement or other document without prior consent, which will not be unreasonably withheld.

As is customary with such reports, our findings should be regarded as valid for a limited period of time and should be subject to examination at regular intervals.

Whilst every effort has been made to ensure that the data contained in it is correct, no responsibility can be taken for omissions or erroneous data provided by a third party or due to information being unavailable or inaccessible during the research period. The estimates and conclusions contained in this report have been conscientiously prepared in the light of our experience in the property market and information that we were able to collect, but their accuracy is in no way guaranteed.



## 7.2: Supporting Statements: Local Procurement and Local Employment

The proposed development at 112-116 New Oxford Street is for residential use. With this use there is no perceived local or long term employment associated with our Planning Application.

Naturally, there is some potential employment in terms of 'types' of services the apartments could generate, (EG Cleaning, Laundry etc).

Potentially there could be a requirement for an inhouse secure/commissionaire 'role' but this would need to be discussed at length with the developer and form part of a service plan for the residential development long term.

During the construction phase, it is likely that the contractor would be using local tradesman, or subcontractors. Any materials being used for the construction would be sourced locally through building suppliers.

All sub-consultants on the client side are likely to be London based.

## 7.3: Supporting Statements : Affordable Housing / Viability

The proposed development at 112-116 New Oxford Street will have 8 new apartments within it.

The building Gross External Area (GEA) is 1157.99 sq m (gross) including the proposed extension.

The requirement for affordable housing does not therefore apply as the development does not:-

- Provide an additional 1,000 sq m. or more (gross) of housing in use class C3 or C4, or
- Provide an addition of 200 sq m or more (gross) of non-residential floor space.
- Involves the loss of affordable housing floor space.
- Provide 10 apartments.

The apartments type breakdown is as follows numbers are 4, 3 bedroom apartments and 1, 1 bedroom studio apartment, and 2, 2 bedroom apartment.

This provides us with 57.1% 3 bedroom apartments which meets the Councils requirements for a mix of greater than 28.5% of 2 bedroom apartments, 14.2% of 1 bedroom apartments.

Whilst the proposals are to a high standard and will provide well designed accommodation that meets the needs of a range of occupiers it is not practical to include affordable housing within this development which is relatively small and primarily market housing.

## 7.4: Supporting Statements : Conservation Area Appraisal Design Statement

The Design Team, have had consultations with Camden Council Planning Officers and The Principal Planner (Conservation and Design). The design proposal was explained to both Camden Council officers along with the aid explanatory visuals.

After these meetings our design booklet was sent to local conservation area bodies, Covent Garden Community Association and The Bloomsbury Association for their review. (The responses received by the Design Team from these organisations are on the facing page). The Design Team have taken note of the comments made, and have responded by amending their original design to align itself with certain concerns raised.

The building is not listed, however it is considered to make a positive contribution to the character and appearance of the conservation area. The Design Team has, from the outset being aware of the local significance of the 112-116 New Office Street location. Not just in terms of its strong presence from the corner of Oxford Street and Tottenham Court Road, but also with its facade forming the 'end piece' to Prospect House.

The proposed extension has not been conceived or designed as a dominant piece of architecture, but as a modest 'addition' which is read as part of the City's 'Skyscape'. Its form responds to the floor plan of the main building below. The extension also sits back from the New Oxford Street facade edge, and the facade turning the corner onto Bainbridge Street. But it sits flush with the main rear Bainsbridge facade. All new window openings within the extension have been designed as 'Dormer' types, which is in keeping with the wider architectural context.

The proposed materials for the new extension will be metal panels, in the form of 'Diamond' shingles. The colour will be a Brass/Gold colour, which over time will mute to give a softer colour. The Dormer windows within the new extension will also be of the same material finish and will give a strong 'frame' to the new windows. The new portion of stone which will form the completed Sixth floor level shall match the main facade.

The main facade to New Oxford Street will not be altered externally, all existing windows will be maintained and refurbished. The Bainsbridge Street rear facade will have new windows inserted into it, but these will follow (where possible) the current fenestration rhythm. The existing windows both on the front and rear facades will be refurbished during the construction.

Demolition of some 'parts' of the existing building will be necessary to complete the proposed redevelopment, the Design Team have limited the extent of any demolition work, the main area where this takes place will be at roof level. The proposed demolition will allow for the new extension to take place. To make the apartments work on certain floors, new window openings will be needed these will be cut into the existing rear brickwork facade. Any work carried out will be made good and repaired with matching materials. (Please refer back to section 3.0 As Existing drawings to see the extent of the proposed demolition work).



## 7.5: Supporting Statements : Conservation Area Appraisal Comments On Proposed Design

RECEIVED 9th OCTOBER 2012

Thank you for the updated drawing. In my view this is a significant improvement. The roof extension is much more contextual whilst still retaining a distinctly contemporary appearance. It would also be useful to have some perspective drawings from street level as the roof extension does appear bulkier than it is likely to be from the public realm. We will still need to be satisfied that the roof extension sits comfortably on the building in terms of those key medium and long distance views along New Oxford Street.

Thank you

Hannah Walker

Principal Planner (Conservation and Design)

RECEIVED 24th SEPTEMBER 2012

We've read the documentation re the above property and have also seen Bloomsbury's response to it. The property is right on the border between Bloomsbury and Covent Garden, at least it is in terms of how we've divided the area between us for commenting purposes.

Stephen Heath has provided comprehensive comment and we particularly support the comments on the following:

1. Any type of short-term rental is something we feel very strongly about as we see a steady stream of conversions from office to residential with small units being proposed that are clearly aimed at the letting market. Such usage has no positive effect on the local community.

2. We support Bloomsbury's proposal to aggregate S106 monies in order to provide affordable housing within the immediate area where the money is created. At the moment it disappears into a general pot.

4. The views mentioned by Stephen are of concern to us also.

The other points are not ones to which we are likely to add very much.

Thank you for inviting our comment.

Regards

Mike Leeson

Covent Garden Community Association

RECEIVED 16th SEPTEMBER 2012

Thank you for getting in touch with us prior to the application being submitted. You have asked for our initial comments and these follow.

1. In terms of use, whilst residential is the obvious choice for this and other low grade office buildings in the area, we would be nervous about serviced apartments or any other form of short-term rental. However, we would like to see the case for this change clearly set out and consideration given to the points we make below.

2. Under current policy, affordable housing provision will need to be addressed. Your client will not wish to provide it on site and the Council will probably settle for a financial contribution. We feel that off-site local provision is becoming an increasingly attractive proposition through change of use and refurbishment of low grade office buildings elsewhere in established residential 'quarters' such as Bloomsbury Village, Covent Garden and Soho. We will be looking to promote this as a solution as we have done for the adjacent change of use of Centre Point to residential. This, in itself, has proved controversial and there would seem to be an intriguing possibility for your client to enter into some sort of agreement with Almacantar whereby the affordable housing generated by Centre Point might itself be provided in 112-116 New Oxford Street.

3. An issue that is starting to concern many is loss of this type of office accommodation which is driving many smaller businesses out of the area so a change of use to residential is not such a clear issue with us as it might once have been. We will seek to encourage change of use in established residential 'quarters' but we do not view this as the character of New Oxford Street.

4. We are impressed by the thought that has gone into the design proposal so far. In principle, we see it as an improvement - an approach that we feel we could support - but suggest that the extension of the building needs to be considered more carefully with the oblique street views of the terrace of which it is a part. There is a consistent architectural expression that extends from Bainbridge Street to Dyott Street, into which a contemporary intervention needs to be inserted very carefully, particularly in its relationship to neighbouring listed buildings. The sense of continuity and the trace of history should not be entirely negated. The massing images in Sections 5 and 6 of the Extensions Studies document need to show the adjoining buildings in more detail for the proposals to be convincing and we are not sure that the analysis undertaken so far has fully addressed all the issues. We would like the views over the top of the Dominion Theatre from Bedford Square to be taken into account along with the very prominent view from the top of Charing Cross Road. VVIs for key views should be submitted with the application.

5. Roofscape is important and we expect to see a more thorough analysis of what sort of plant is likely to be at roof level. Building Control is unlikely to be very happy with a single stair serving a building of this height and this infers a fire engineered solution with roof mounted smoke extract plant. How is the proposal going to accommodate this? Also how is window cleaning going to be dealt with? In any solution, we would like to see some evidence of a legally binding agreement with the adjoining owner to deal with the unsightly and obtrusive plant at roof level adjacent to the party wall that presently dominates the view from Oxford Street.

6. Street level impact is crucial not only in terms of urban design but also for making the development commercially attractive, particularly on the Bainbridge Street frontage. There are serious problems here with drug related crime and anti-social behaviour and the lack of any active frontage on this side of the street is a major contributory factor. We would like to see early consideration given to this in a crime impact assessment that is developed with the local Police Safer Neighbourhood Team with the ambition of establishing some form active frontage to Bainbridge Street. It would be unfortunate if it is only a refuse store. A sensitive approach to retail signage and CCTV would also be beneficial.

7. We are not at all happy with Park House being quoted as a design precedent to emulate. It was a mistake that Westminster will regret for decades and we would not like to see any references to its visual vulgarity at the other end of Oxford Street.

8. As mentioned earlier, being located in an area that is of interest to Covent Garden Community Association and the Soho Society, as well as ourselves, we suggest that you also seek their views. We are therefore copying this message to them and we may, in due course, decide to submit joint comments on the application.

We hope that this is constructive and would be happy to let you have our further thoughts on proposals as they develop.

Regards,

Stephen Heath

On behalf of the Bloomsbury Association

## 7.6: Supporting Statements : Secured-By-Design

The Design Team, have been in consultation with the local Secure-by-design officer, where the project was described in detail.

The principle points covered in our meeting were the:

- Change of use
- The shared escape with Starbucks from the first floor and Back of House basement area.
- Accessibility at the ground floor.
- Crime prevention methods to main front door.
- The use of external lighting to ground floor areas.

Below is a list of the keys points which will be reviewed and actioned in more detail when 112-116 New Oxford Street moves into development stage.

1. All communal and residential doors will be to BS pas 23/24 2012. This will include every flat entrance door. Fire doors on stairs to this standard will be required. There should not be a mix at any level between residents and customers of the ground level shop.
2. Windows - None applicable.
3. Refuse and cycle store - These will have fit for purpose self closing and locking door. If further entry can be gained into the building then a further door to BS PAS 23/24 must be fitted. This is the general requirements, although specific details are not known at this time.
4. Post boxes - A through the wall scheme could be fitted or a foyer with BS PAS 23/24 2012 door fitted with post boxes located in this foyer.
5. Lighting of the property will be to a uniform level.
6. Utility meters will be located in central location.
7. Access control will be video and audio and No trades button fitted.
8. An alarm should be considered. The scheme requires a fused spur be fitted near the entrance to each flat to facilitate an alarm.
9. CCTV should be considered and the information commissioner's guidelines complied with. <http://www.ico.gov.uk>;
10. Lift control may be activated with the use of a fob.



## 7.7: Supporting Statements: Service Management Plan

The basic planning arrangement will comprise of 6 dwellings above an existing 'Starbucks' Coffee Shop.

### GENERAL:

The main entrance is on New Oxford Street this will be for residents to enter their property on a daily basis's. There are two lobbies proposed an outer lobby and an inner lobby. The outer lobby will contain wall mounted post boxes for all the apartments, the inner lobby will be kept clear to allow for maximum space in front and around the lift doors.

The existing entrance on Bainbridge Street will be maintained, but used for Means of escape from the apartments and 'Existing Starbucks' coffee shop and service entrance for the apartments (this would entail removal of refuse, and goods deliveries).

The main stair will be clear of obstacles, doors on to every apartment floor will have provision for them to be locked, and access to them via keys provided to residents.

### CLEANING/REFUSE:

It is hoped that as part of the agreement between the building owner and any tenants that all apartments would be cleaned by the same cleaning company allowing for all refuse to be removed (both from the apartments and the building) by one organisation. This arrangement could extend to recycling and window cleaning. A clearly defined area (within the basement) has been allocated for the storage of refuse and recycling as marked on the proposed drawings.

### BIKE STORAGE:

In section 7.10, we explain in more detail our aspiration in providing cycles for each of the apartments to be created within this development. But this storage would be within the basement area allowing residents to store their cycles without the need for having them within their apartments or main circulation areas.

### INCOMING SERVICES METERS:

These would be installed within one of the basement rooms, these would be set within a cupboard which would allow meter reading to take place without the need for external meter reading staff to enter individual apartments. The access to this room could be made via the Bainsbridge Street service door.

## 7.8: Supporting Statements : Accessibility Statement

### Underlying Philosophy

The client for the project, Zania Universal, is committed to a policy of equality, inclusion and accessibility in the delivery of the proposed re-development of 112-116 New Oxford Street. This statement aims to ensure maximum awareness by the design team of the various needs of those with physical and/or mental impairments, as well as other groups with access needs such as parents with children, and the elderly.

### Consultation

The project is being designed to comply with the following in so far as they apply to each use:

- The Building Regulations 2000 'Access to and use of Buildings' Approved Document 'M' 2004 edition.
- British Standard Code of Practice 8300:2009, 'Design of Buildings and their Approaches to meet the needs of Disabled People'.
- EN 81-70: 2003 'Accessibility to lifts for persons including persons with high disability'
- Disability Discrimination Act 1995 and 2005.
- DDA Code of Practice - 'Rights of Access: services to the public, public authority functions, private clubs and premises'.
- British Standards 5588- '8': Code of Practice for means of escape for disabled people (no longer current but cited in the Building Regulations).
- British Standard 9999.
- Guidance in the use of Tactile Planning: DTLR Mobility and Inclusion Unit.

### Other informative documents consulted include:

- Inclusive Environments 'Designing for Accessibility' 2004 Edition.

## 7.8: Supporting Statements : Accessibility Statement

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| 2.4  | Access within flats  |
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|-----|--|
| 1.0 | Introduction   |
| 1.1 | Purpose of Report - This access statement includes an assessment of the level of access and provision for people with disabilities, considering the guidance laid out in Approved document M and Camden Planning Guidance CPG2.  |
| 1.2 | Proposal - The proposal is to extend and refurbish an existing building which currently comprises a shop at ground and first floors with offices above on four floors. It is proposed that an additional floors is incorporated and the offices are converted to provide 6 flats.  |
|     |  |
| 2.0 | Provision for Access to and use of building  |
| 2.1 | Principle entrance from street – The entrance to the building is on New Oxford Street and is level with a clear opening door width of at least 775mm and an accessible threshold.  |
| 2.2 | Entrance hallway – The hallway is 1500mm wide.   |
| 2.3 | Access to upper storeys – A lift will be provided that has a) a clear landing of 1500mm x 1500mm in front of its entrance, b) a door will be 800mm wide, c) a car whose width is at least 900mm and depth of 1250mm, d) has landing and car controls which are not less than 900mm and not more than 1200mm above the landing and the car floor, at a distance of not more than 400mm from the front wall, e) with suitable tactile indication on the landing and adjacent to the lift call button to identify the storey in question, f) with suitable tactile indication on or adjacent to the lift buttons within the car to confirm the floor selected, g) incorporates a signalling system which gives visual notification that the lift is answering a landing call and a “dwell time” of 5 seconds before its doors begins to close after they are fully open; the system may be overridden by a door re-activating device which relies on appropriate electronic methods, but not a door edge pressure system, provided that the minimum time for a lift door to remain fully open is 3 seconds and; h) incorporates visual and audible indication of the floor reached. |
| 2.4 | Access within flats – The corridors within all flats have an unobstructed width of 1150mm and all door widths will be a minimum of 800mm which complies with AD – M, table 4. This is to facilitate access into habitable rooms and a room containing a WC.  |
| 2.5 | Wheelchair housing standards provision for 1 no flat – CPG 2 requires that 10% of flats will comply with wheelchair housing standards and meet the criteria for Lifetime homes. Flat number 06 has been planned to meet these standards including the 16 Lifetime homes criteria demonstrated in the schedule within this section.   |

## 7.9: Supporting Statements : Life Time Homes

| LIFETIME HOMES CRITERIA  | KEY OBJECTIVES  | DETAILED CRITERIA   | PROPOSALS TO MEET STANDARD   |
|--|---|---|--|
| Parking (width or widening capability)                             | <p>Provide, or enable by cost effective adaptation, parking that makes getting into and out of the vehicle as convenient as possible for the widest range of people (including those with reduced mobility and/or those with children).</p> <p>General Note: Criterion 1 is not relevant to developments that do not contain any parking provision (for specific requirements refer to Camden Development Policy – DP18 Parking standards and limiting the availability of car parking – which specifically discourages on-site parking</p> | <p>a) 'On plot' (non-communal) parking:<br/>Where a dwelling has car parking within its individual plot (or title) boundary, at least one parking space length should be capable of enlargement to achieve a minimum width of 3300mm.</p> <p>b) Communal or shared parking:<br/>Where parking is provided by communal or shared bays, spaces should be provided with a width of 3300mm and in accordance with the specification give in Appendix 2 on page 65 or <a href="http://www.lifetime-homes.org.uk">www.lifetime-homes.org.uk</a></p> | This criterion is not relevant as the development does not contain parking provision.  |
| Approach to dwelling from parking (distance, gradients and widths) | Enable convenient movement between the vehicle and dwelling for the widest range of people, including those with reduced mobility and/or those carrying children or shopping.   | The distance from the car parking space of Criterion 2 to the dwelling entrance (or relevant block entrance or lift core), should be kept to a minimum and be level or gently sloping. The distance from visitors parking to relevant entrances should be as short as practicable and be level or gently sloping.   | This criterion is not relevant as the development does not contain parking provision.  |
| Approach to all entrances  | Enable, as far as practicable, convenient movement along other approach routes to dwelling (in addition to the principal approach from a vehicle required by Criterion 2) for the widest range of people.   | The approach to all entrances should preferably by level or gently sloping, and in accordance with the specification give at <a href="http://www.lifetime-homes.org.uk">www.lifetime-homes.org.uk</a>   | The approach to the development is level along the existing pavements of New Oxford Street Main front entrance and Bainbridge Street to the rear means of escape and servicing only.   |
| Entrances  | <p>Enable ease of use of all entrances for the widest range of people.</p> <p>Note: For the purpose of requirement d) and e) of this Criterion, main entrances are deemed to be; the front door to an individual dwelling, the main communal entrance door to a block of dwellings, plus any other entrance door associated with the approach route from parking required by Criterion 2.</p>   | <p>All entrances should:</p> <p>a) Be illuminated</p> <p>b) Have level access over the threshold; and</p> <p>c) Have effective clear opening widths and nibs as specified given at <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a></p> <p>d) In addition, main entrances should also:</p> <p>e) Have adequate weather protection*</p> <p>f) Have a level external landing.*</p>  | <p>a)The main communal entrance is illuminated by existing street lamps in New Oxford Street this will be enhanced by the provision of new wall mounted lighting.</p> <p>Entrances to all apartments will be illuminated by ceiling or wall mounted lights.</p> <p>b) The main communal entrance and all apartment entrances have level access over the threshold.</p> <p>c) The main entrance door has a minimum width of 800mm and all entrances to apartments have a minimum width of 775mm.</p> <p>e) The main communal entrance is existing and does not have the weather protection that a canopy or porch would provide. As the entrance is off a main street we consider that a canopy would not be appropriate. In any event the entrance is not in an exposed location in terms of weather.</p> <p>f) The main entrance has a level external landing which is the existing pavement.</p> |

## 7.9: Supporting Statements : Life Time Homes

| LIFETIME HOMES CRITERIA                | KEY OBJECTIVES   | DETAILED CRITERIA   | PROPOSALS TO MEET STANDARD   |
|--|--|---|--|
| Communal stairs and lifts              | Enable access to dwellings above the entrance level to as many people as possible.                                       | <p>a) Communal Stairs</p> <p>Principal access stairs should provide easy access in accordance with the specification given at <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a>, regardless of whether or not a lift is provided.</p> <p>b) Communal Lifts</p> <p>Where a dwelling is reached by a lift, it should be fully accessible in accordance with the specification given at <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a></p> <p>Note: provision of a lift is not a Lifetime Homes requirement, but is recommended where dwellings are not entered at the same level as the main block entrance.</p> | <p>) The principal access stair to the apartments is existing and is 1040mm wide between the wall and the handrail. The risers are 179mm. Each flight comprises 8 risers which gives a total rise of 1432mm.</p> <p>b) A new communal lift is being installed which is fully accessible as noted in paragraph 2.3 of the access statement.</p> |
| Internal doorways and hallways         | Enable convenient movement in hallways and through doorways.   | Movement in hallways and through doorways should be as convenient to the widest range of people, including those using mobility aids or wheelchairs, and those moving furniture or other objects. As a general principle, narrower hallways and landing will need wider doorways in their side walls. The width of doorways and hallways should confirm to the specification given at <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a>  | Hallways are 1100mm wide. Doorways are 775mm wide.   |
| Circulation Space                      | Enable convenient movement in rooms for as many people as possible.  | There should be space for turning a wheelchair in dining areas and living rooms and basic circulation space for wheelchair users elsewhere.   | There is ample space for turning a wheelchair in the dining area as demonstrated on the annotated flat plan.   |
| Entrance level living space            | Provide accessible socialising space for visitors less able to use stairs.   | <p>A living room / living space should be provided on the entrance level of every dwelling (See Appendix 1 on page 65 or <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a> for definition of 'entrance level')</p> <p>Note: Entrance level generally means the storey containing the entrance door to the individual dwelling. It may refer to the first storey that contains a room (habitable or non-habitable) if the entrance door leads directly to an 'easy-going' stair.</p>  | The living room / living space is on the entrance level only, one apartment layout does not conform to this arrangement due to an existing floor level difference.   |
| Potential for entrance level bed-space | Provide space for a member of the household to sleep on the entrance level if they are temporarily unable to use stairs. | In dwellings with two or more storeys, with no permanent bedroom on the entrance level, there should be space on the entrance level that could be used as a convenient temporary bed-space (see Appendix 1 on page 65 or <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a> for definition of 'entrance level')   | All bedrooms are on the entrance level, one apartment layout does not conform to this arrangement due to an existing floor level difference. However two of the three bedrooms do conform to this requirement.   |

## 7.9: Supporting Statements : Life Time Homes

| LIFETIME HOMES CRITERIA   | KEY OBJECTIVES  | DETAILED CRITERIA   | PROPOSALS TO MEET STANDARD   |
|---|---|---|--|
| Entrance level toilet and shower drainage                         | Provide an accessible toilets and potential showering facilities for:<br>a) Any member of the household using the temporary entrance level bed space of Criteria 9, and:<br>b) Visitors unable to use stairs. | Where an accessible bathroom, in accordance with Criterion 14, is not provided on the entrance level of a dwelling, the entrance level should have an accessible toilet compartment, with potential for a shower to be installed – as detailed in the specification given at (see Appendix 1 on page 65 or <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a> for definition of 'entrance level')   | An accessible bathroom is provided. The en-suite is also capable of having a shower installed.   |
| Toilet and bathroom walls   | Ensure future provision of grab rails is possible, to assist with independent use of toilet and bathroom facilities.  | Walls in all bathrooms and toilet compartments should be capable of firm fixing and support for adaptations such as grab rails.   | Walls in toilets and bathrooms will accommodate grab rail fixings.   |
| Stairs and potential through-floor lift in dwelling               | Enable access to storeys above the entrance level for the widest range of households.   | The design within a dwelling of two or more storeys should incorporate both:<br>a) Potential for stair lift installation; and<br>b) A suitable identified space for a through-the-floor lift from the entrance level to a storey containing a main bedroom and a bathroom satisfying Criterion 14.  | All apartments are of a single storey.   |
| Potential for fitting of hoists and bedroom/bathroom relationship | Assist with independent living by enabling convenient movement between bedroom and bathroom facilities for a wide range of people.  | Structure above a main bedroom and bathroom ceilings should be capable of supporting ceiling hoists and the design should provide a reasonable route between this bedroom and the bathroom.   | The floors are existing and comprises of concrete encased steel beams with hollow pot infills and are capable of supporting a hoist.   |
| Bathrooms   | Provide an accessible bathroom that has ease of access to its facilities from the outset and potential or simple adaptation to provide for different needs in the future.                                     | An accessible bathroom, providing ease of access in accordance with the specification given at <a href="http://www.lifetimehomes.org.uk">www.lifetimehomes.org.uk</a> should be provided in every dwelling on the same storey as a main bedroom.  | The bathroom is of sufficient size to be wheelchair accessible and as such has potential for adaption for different needs.   |
| Glazing and window handle heights                                 | Enable people to have a reasonable line of sight from a seated position in the living room and to use at least one window for ventilation in each room.   | Windows in the principal living space (typically the living room), should allow people to see out when seated. In addition, at least on opening light in each habitable room should be approachable and usable by a wide range of people - including those with restricted movement and reach.<br><br>Note: in kitchens areas or bathrooms with only one window situated behind kitchen units or bathroom fittings, the requirement for a potential clear approach space to that window need to apply. However, the window handle height/control requirement remains applicable. Any other window within the kitchen area or bathroom, not behind fittings, is required to satisfy both the approach and window handle/control height requirements. | The windows are existing and part of an architecturally sensitive façade and as such will not comply in terms of height. However, the window handle height/controls will be selected to suit those with restricted movement and limited reach. |
| Location of service controls                                      | Locate regularly used service controls, or those needed in an emergency, so that they are usable by a wide range of household members – including those with restricted movement and limited reach.           | Service controls should be within a height band of 450mm to 1200mm from the floor and at least 300mm away from any internal room corner.  | Service controls will be within a height band of 450mm to 1200mm from the floor and at least 300mm away from any internal room corner in accordance with AD part M1 diagram 29.  |

## 7.10: Supporting Statements : Transport / Car Free Housing

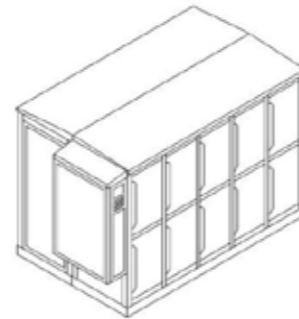
112-116 New Oxford Street Site has a high public transport accessibility rating (PTAL) of 6B. Its position sitting right next to the underground interchange of Tottenham Court Road Tube Station allows future residents easy access to the London underground system. This station is currently under going a massive enlargement and extension (the addition of Cross Rail) which will increase the accessibility for public transport to the site and surrounding context.

At street level there are ample bus stops within a short walk from the front door of the development which add to residents ability to travel locally and beyond by a secondary mode of public transport.

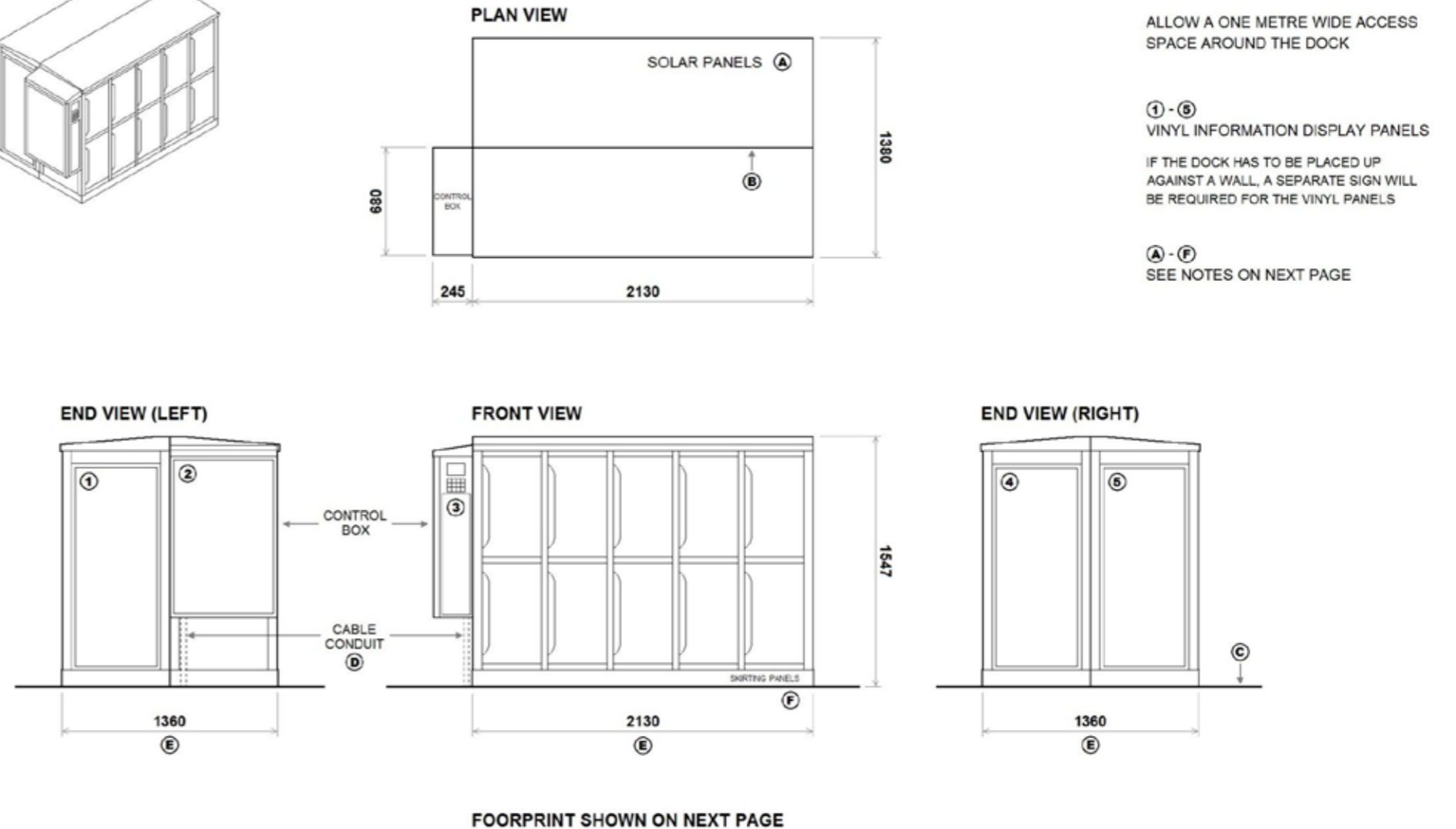
We have always believed that no car parking provision would be needed for the proposed development. However we are wishing to provide cycle provision (folding bikes) which would be securely stored within the basement area. These would be 'given' to each of the apartments created within the new development. Allowing the owner to make a choice of either public transport or cycling as a mode of transport around town.

The recommended minimum number of bicycles has been given to us as 9.

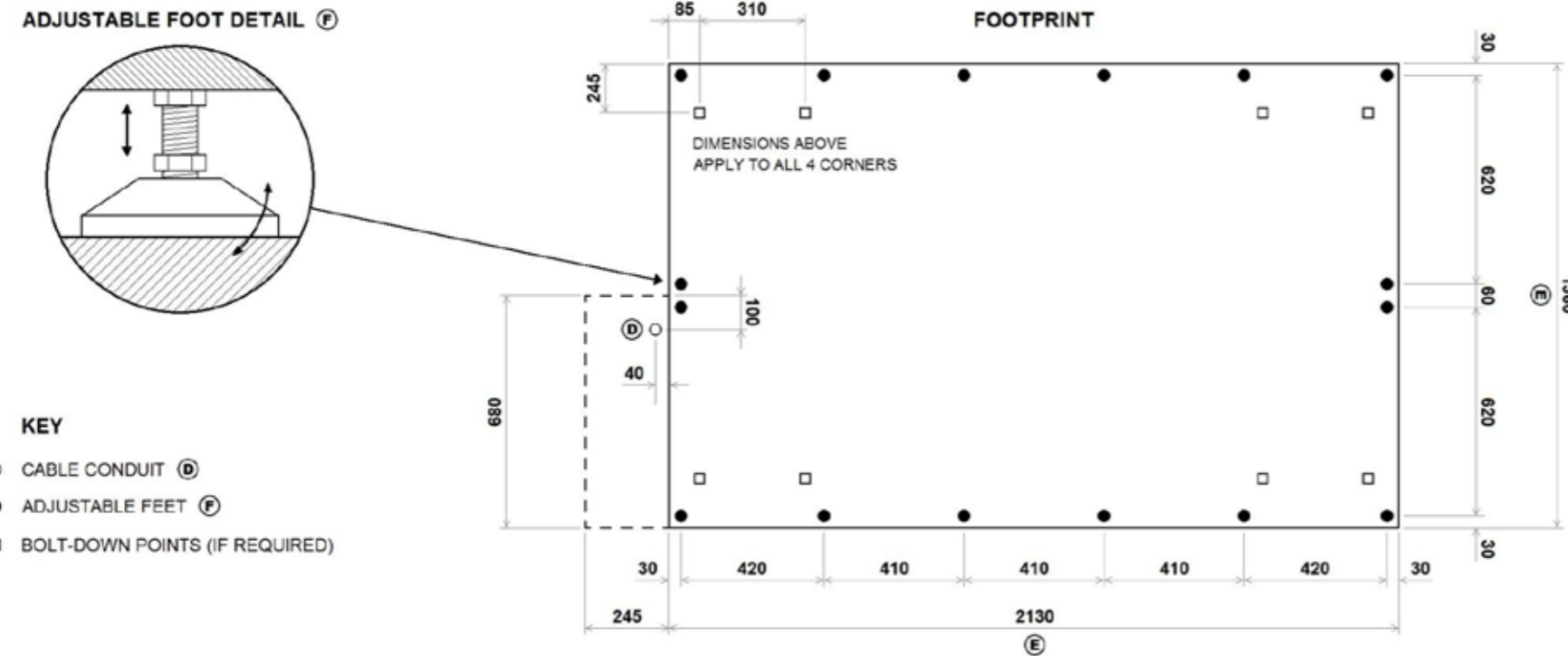
As part of our Planning Application Submission we are showing examples of the type of storage and bikes which could be provided within the development.



### BROMPTON DOCK 20-BAY UNIT (BACK-TO-BACK)



## 7.10: Supporting Statements: Transport / Car Free Housing



### DATA

|                                     |                |
|-------------------------------------|----------------|
| WEIGHT OF DOCK (LOADED WITH BIKES): | <b>1270 kg</b> |
| WEIGHT OF DOCK (EMPTY):             | <b>1050 kg</b> |
| WEIGHT OF ONE BIKE:                 | <b>11 kg</b>   |
| AVERAGE POINT LOAD ON EACH FOOT:    | <b>72.5 kg</b> |

### NOTES

- (A) Some docks will have a solar panel, which should be placed on a south-facing roof. Solar-powered docks do not require a mains electricity supply and there will be no cable conduit.
- (B) Back panels are not required along the centre of the dock.
- (C) Installation is easiest if the dock is placed on level concrete or tarmac. The adjustable feet can also accommodate ground which is sloping – see (F).
- (D) There will be a cable conduit if the dock is powered by mains electricity, in which case there will not be solar panels.
- (E) Add 4 mm to these dimensions if the skirting is to be included.
- (F) The feet can be adjusted so that the base of the dock is between 26 mm and 95 mm from the ground. This allows the dock to be placed on sloping ground. Skirting panels between 26 mm and 146 mm high can be provided to conceal the feet. If the slope is more extreme and the base of the dock needs to be raised more than 95 mm above the ground, then separate blocks will be required for the feet to stand on.





## 7.11: Supporting Statements : Construction Management Plan

|                     |  |
|---------------------|--|
| Project Address     | 112-116 NEW OXFORD STREET, LONDON, WC1A 1HH  |
| Client              | Zania Universal Properties   |
| Start Date          | TBC  |
| Programme           | TBC  |
| Contracts Manager   | TBC  |
| Review Date         | TBC  |
| Brief Scope of Work | General refurbishment and conversion works and additional single storey roof extension to seven storey steel framed building |

| # | Method Statement | Y | N | N/A | Site Specific Methodology   | General Methodology   |
|---|------------------|---|---|-----|---|---|
| 1 | Site setup       |   |   |     | <p><b>Asbestos (Pre Start)</b><br/>The existing building has already been stripped out and any potential asbestos has been removed</p> <p><b>Welfare and Site set up</b><br/>Site setup and welfare will be located in a temporary room constructed within the property being refurbished. This room will include power water and toilet facilities, a drying room and canteen area.</p> <p><b>Hoarding;</b><br/>The site hoarding will be minimal in this instance as the property is currently only accessible via the rear access door on Bainbridge Street. Hoarding and gates will be placed to the main entrance (subject to local authority approval).</p> <p><b>Access</b><br/>Primary access for deliveries will be via the rear access door at ground floor level on Bainbridge Street. This route will be kept clear for access, materials and in the case of emergency.</p> <p><b>Road and Street works;</b><br/>To be confirmed during works, street level evidence of water, gas and electric, also major foul drainage through site. Incoming services will be located and identified as part of the works. See services section below.</p> <p>We do not anticipate any works in the public highway other than demolished materials and site refuse operations. Banksman will be in attendance and where necessary we will employ road cleaners to ensure any exported material is not left on the local road network.</p> | <ul style="list-style-type: none"> <li>Site setup and welfare will be located in a in a temporary room constructed in the property. This room will include power water and toilet facilities, a drying room and canteen area.</li> <li>Arrange for and obtain all necessary local &amp; statutory authority permits and licences from the local authority.</li> <li>Deliver skips and construct welfare facilities.</li> <li>Construct Hoarding to the proposed rear entrance. Paint, make good and erect safety signage and permissions. Door to be fitted with secure lock.</li> <li>Obtain all available information relating to existing services where applicable.</li> <li>Obtain all information relating to existing Asbestos content where applicable.</li> <li>Identify services and investigate by hand excavation.</li> <li>Identify incoming mains supply. Arrange for qualified electrician to erect and test temporary electrical installation with suitable RCD. Ensure the provision of Temporary electrical installation certificate.</li> <li>Where applicable and in agreement with the client, apply dust protection to ground floor.</li> </ul> |
| # | Method Statement | Y | N | N/A | Site Specific Methodology   | General Methodology   |
|   |                  |   |   |     | <p><b>Fire</b><br/>One site box will be set up in the site office and additional fire points will be installed as the works progress to each respective staircase landing level. The fire points will include for means of raising the alarm. We will develop and maintain our site fire plan for the site as the works progress.</p> <p><b>Site Electrics</b><br/>We assume a main board is available in which we will be utilising for works and possibly welfare. To be isolated and site supply will be taken from here, it is not anticipated this will be required to be moved. All will be isolated and temporary board provided for all 110v transformers.</p>  | <ul style="list-style-type: none"> <li>Foreman must ensure he has been fully briefed by his line manager in safety critical elements of the structural works including, but not exclusively;</li> <li>Location of Load bearing positions</li> <li>Location of incoming services including main sewer</li> <li>Sequence of works defined by engineers drawing. Suggested Structural sequence drawings available at time of writing.</li> </ul>   |

## 7.11: Supporting Statements: Construction Management Plan

|   |  |   |   |     |  |  |
|---|--|---|---|-----|--|--|
| 2 | General Site maintenance and housekeeping  |   |   |     | <p><b>Housekeeping (Throughout)</b><br/>Standard HSE procedures to be applied, ensure housekeeping through regular removal of waste to skips, control of material call offs and provision of adequate labour to maintain access and cleanliness. Be aware of existing resident and agree arrangements for waste management and general coordination, cooperation with others will be essential.</p>            | <p><b>General Issues:</b></p> <ul style="list-style-type: none"> <li>Housekeeping to be maintained at all times.</li> <li>Access routes and emergency escape routes to be kept free from debris, waste materials and training leads.</li> <li>Where possible, 110V distribution leads to be suspended from ceilings to prevent trips.</li> <li>Manual handling issues arise from the man handling of any material where there is a risk of injury. Operatives to be trained or instructed in the correct lifting and carrying procedures.</li> <li>Any mechanical aids identified (barrows, rollers, conveyors etc) to be in good condition and well serviced.</li> </ul> <p><b>Site Deliveries &amp; Waste:</b></p> <ul style="list-style-type: none"> <li>Location for the storage of materials to be identified before the delivery arrives.</li> <li>Deliveries to be bounded within the specified area and stacked in a safe manner.</li> <li>Any special wastes to be identified and segregated from general waste.</li> </ul> |
| 3 | Strip out and Demolitions  |   |   |     | <p><b>Demolition</b><br/>Demolition involves demolition of the existing part pitched roof construction. Temporary scaffolding will be installed as required by the temporary works engineer while the pitched roof is being removed.</p>   |  |
| # | Method Statement   | Y | N | N/A | Site Specific Methodology  | General Methodology  |
| 4 | Material Logistics   |   |   |     | <p><b>General Principles</b><br/>Due to the restricted nature of the access and the location of the site we will need to set up a compound within the existing building to temporarily house material/equipment. This compound will be located on one of the lower floors with easy access onto Bainbridge Street level.</p>   | <ul style="list-style-type: none"> <li>Temporarily close off footpath and divert pedestrians while filling any skips.</li> <li>Regular inspections of road surface to be made.</li> <li>Clean road surface regularly with brush.</li> <li>Ensure suitable lighting and signage on footpath and on the skip itself.</li> </ul>  |
| 5 | Steelwork and Temporary bracing  |   |   |     | <p><b>Structural Steelwork;</b><br/>Steel beams and framework along with metal stud infill walls will be installed in various locations across the building width in accordance with the engineers detail and sequencing. This is primarily to support the new single storey roof extension. Any potential temporary propping will remain in place in accordance with the temporary works design sequence.</p> |  |
| 6 | Existing Services<br>a. Service Moves (Gas, Water, Electric)<br>b. General Moves<br>c. Existing Drainage Moves |   |   |     | <p>Gas, water and electric services to be blocked at building entrance by specialist subcontractor. Free use of services must be supplied for the works.</p>   |  |
| 7 | Any other information  |   |   |     | <p>A considerable number of neighbouring buildings all of which will be sensitive to traditional statutory nuisance, noise ducts vibration etc.</p>  |  |

## 8.0: Appendixes :

# 8.1: Appendixes : Daylight / Sunlight Assessment



Daylight and Sunlight Study  
112 to 116 New Oxford Street, London WC1A 1HH

2<sup>nd</sup> January 2013

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## APPENDICES

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DAYLIGHT AND SUNLIGHT STUDY  
112 to 116 New Oxford Street, London WC1A 1HH

DAYLIGHT AND SUNLIGHT STUDY  
112 to 116 New Oxford Street, London WC1A 1HH

Page 1

# 8.1: Appendixes : Daylight / Sunlight Assessment

## 1 EXECUTIVE SUMMARY

### 1.1 Overview

- 1.1.1 Right of Light Consulting has been commissioned to undertake a daylight and sunlight study in connection with the development at 112 to 116 New Oxford Street, London WC1A 1HH. The aim of the study is to check whether or not the proposed habitable floors receive satisfactory levels of daylight and sunlight.
- 1.1.2 The study is based on the numerical tests laid down in the Building Research Establishment (BRE) guide 'Site Layout Planning for Daylight and Sunlight: a good practice guide' by P J Littlefair 2011.
- 1.1.3 Appendix 1 identifies the windows analysed in this study. The numerical test results (including all calculation workings) are provided in Appendix 2. No sky line contours are presented in Appendix 3.
- 1.1.4 Right of Light Consulting confirms that the proposed design satisfies all of the requirements set out in the BRE guide 'Site Layout Planning for Daylight and Sunlight'.

## 2 INFORMATION SOURCES

### 2.1 Documents Considered

- 2.1.1 This report is based on the following drawings:

|                |                            |       |
|----------------|----------------------------|-------|
| BNY-MA(20)0001 | Ground Floor Plan          | Rev 1 |
| BNY-MA(20)1001 | First Floor Plan           | Rev 1 |
| BNY-MA(20)2001 | Second Floor Plan          | Rev 1 |
| BNY-MA(20)3001 | Third Floor Plan           | Rev 1 |
| BNY-MA(20)4001 | Fourth Floor Plan          | Rev 1 |
| BNY-MA(20)5001 | Fifth Floor Plan           | Rev 1 |
| BNY-MA(20)6001 | Sixth Floor Plan           | Rev 1 |
| BNY-MA(20)7001 | Seventh Floor Plan         | Rev 1 |
| BNY-MA(21)AA01 | Elevation AA – South       | Rev 1 |
| BNY-MA(21)BB01 | Elevation BB – West        | Rev 1 |
| BNY-MA(21)CC01 | Elevation CC – North       | Rev 1 |
| BNY-MA(22)AA01 | Section AA - East / West   | Rev 1 |
| BNY-MA(22)BB01 | Section BB - North / South | Rev 1 |

## 3 METHODOLOGY OF THE STUDY

### 3.1 BRE Guide : Site Layout Planning for Daylight and Sunlight

- 3.1.1 The study is based on the numerical tests laid down in the Building Research Establishment (BRE) guide 'Site Layout Planning for Daylight and Sunlight: a good practice guide' by P J Littlefair 2011.
- 3.1.2 The standards set out in the BRE guide are intended to be used flexibly. In instances where there is a special requirement for daylight or sunlight, higher levels may be deemed necessary. In other situations, such as with urban developments, lower daylight and sunlight levels may be unavoidable. The following statement is quoted directly from the BRE guide:
- 3.1.3 "The guide is intended for building designers and their clients, consultants and planning officials. The advice given is not mandatory and this document should not be considered as an instrument of planning policy. Its aim is to help rather than constrain the designer. Although it gives numerical guidelines, these should be interpreted flexibly because natural lighting is only one of the many factors in site layout design."

### 3.2 Interior Daylighting

- 3.2.1 The interior daylighting recommendations set out in BRE guide are based on British Standard BS 8206 Part 2 and the Chartered Institute of Building Services Engineers Applications Manual on window design. Collectively, the guides set out three main criteria for interior daylighting. These are summarised as follows:

#### 3.2.2 Test 1 Average Daylight Factor (df)

The Average Daylight Factor can be calculated using the following formula:

$$df = \frac{T A_w \theta}{A (1-R^2)} \%$$

Where

- T is the diffuse visible transmittance of the glazing (BRE standard of 0.68)  
 A<sub>w</sub> is the net glazed area of the window (m<sup>2</sup>)  
 A is the total area of the room surfaces (m<sup>2</sup>)  
 R is their average reflectance  
 θ is the angle of visible sky in degrees

# 8.1: Appendixes :

## Daylight / Sunlight Assessment

The Average Daylight factor test is applied to habitable rooms within domestic properties. A kitchen is generally deemed to be a habitable room if it is large enough to accommodate a dining area. If the kitchen is small or if the property has a separate dining area then the accepted practice is to treat the kitchen as a non habitable room.

For the purpose of this study we have assumed BRE internal reflectance values pertaining to medium wooden floors, light painted walls and light painted ceilings.

The guide recommends an Average Daylight Factor of 5% or more if there is no supplementary electric lighting, or 2% or more if supplementary lighting is provided. There are additional minimum recommendations for dwellings of 2% for kitchens, 1.5% for living rooms and 1% for bedrooms.

A special procedure is required for floor to ceiling windows such as patio doors. If part of a window is below the height of the working plane (a horizontal plane 0.85m above the floor in housing), this portion should be treated as a separate window. The ADF for this window has an extra factor applied to it, to take account of the reduced effectiveness of low level glazing in lighting the room. A value equal to the floor reflectance may be taken for this factor. The ADF for the portion of the window above the working plane is calculated in the normal way without this additional factor, and the ADFs for the two portions are added together.

### 3.2.3 Test 2 Room Depth

If a daylit room is lit by windows in one wall only, the depth of the room L should not exceed the limiting value given by:

$$\frac{L}{W} + \frac{L}{H} \leq \frac{2}{1-R_b}$$

Where

W is the room width  
H is the window-head height above floor level  
R<sub>b</sub> is the average reflectance of the surfaces in the rear half of the room

### 3.2.4 Test 3 Position of the no sky line

If a significant area of the working plane lies beyond the no sky line (i.e. it receives no direct skylight), then the distribution of daylight in the room will look poor and supplementary electric lighting will be required.

The no sky line assessment is not applicable where a room derives its daylight solely from a light well or atrium. In these situations the room relies on borrowed light instead of direct skylight.

### 3.3 Sunlight to Windows

3.3.1 The BRE guide recommends that where possible each dwelling should have at least one main living room window that faces within 90 degrees of due south. However, the guide acknowledges that this is not always possible when it comes to flats.

3.3.2 The BRE sunlight tests should be applied to all main living rooms and conservatories which have a window which faces within 90 degrees of due south. The guide states that sunlight is viewed as less important in kitchens and bedrooms. In non-domestic buildings, any spaces which are deemed to have a specific requirement for sunlight should be checked.

3.3.3 The BRE guide recommends that main living room windows should receive 25% of the total annual probable sunlight hours, including 5% of the annual probable sunlight hours during the winter months between 21<sup>st</sup> September and 21<sup>st</sup> March.

## 4 RESULTS OF THE STUDY

### 4.1 Window Reference Points

4.1.1 Refer to Appendix 1 for a drawing which identifies the positions of the windows analysed in this study.

### 4.2 Numerical Results and No Sky Line Contours

4.2.1 The numerical test results including all calculation workings are provided in Appendix 2. No sky line contours for the habitable rooms are presented in Appendix 3.

### 4.3 Interior Daylighting

4.3.1 All rooms meet or surpass the BRE Average Daylight Factor targets.

4.3.2 All rooms pass the room depth test.

4.3.3 No sky line contours for all living rooms and kitchens are presented in Appendix 3. The BRE guide explains that daylight distribution to bedrooms is less important. However, for completeness we have also presented the no sky line contours for all bedrooms. The contours illustrate that all living rooms and kitchens receive good access to daylight over a significant part of the working plane. Two of the bedrooms do not achieve ideal daylight distribution. However, we are of the opinion that the distribution of daylight is acceptable bearing in mind there are no specific daylight distribution requirements for bedrooms. The proposed design meets the requirement set out in paragraph 2.1.13 which explains that where there is a choice it is best to site the living room and kitchen away from obstructions.

### 4.4 Sunlight to Windows

4.4.1 All living rooms have at least one main window which faces within 90 degrees of due south. All main windows pass both the total annual sunlight hours test and the winter sunlight hours test. The proposed development therefore satisfies the BRE direct sunlight to windows requirements.

## 8.1: Appendixes :

### Daylight / Sunlight Assessment

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#### 4.5 Conclusion

- 4.5.1 Right of Light Consulting confirms that the proposed design satisfies all of the requirements set out in the BRE guide 'Site Layout Planning for Daylight and Sunlight'.

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#### 5 CLARIFICATIONS

##### 5.1 General

- 5.1.1 The report provided is solely for the use of the client and no liability to anyone else is accepted.
- 5.1.2 We have undertaken the survey following the guidelines of the RICS publication "Surveying Safely".
- 5.1.3 Where limited access is available, reasonable assumptions will have been made.
- 5.1.4 Right of Light Consulting have endeavoured to include in the report those matters, which they have knowledge of or of which they have been made aware, that might adversely affect the validity of the opinion given.
- 5.1.5 Right of Light Consulting will notify those instructing them immediately and confirm in writing if for any reason the report requires any correction or qualification.
- 5.1.6 Right of Light Consulting confirm that they have used their best endeavours to ensure that the facts stated in this report are correct and that the opinions expressed represent a true and complete professional opinion.

##### 5.2 Project Specific

- 5.2.1 None

# 8.1: Appendixes : Daylight / Sunlight Assessment

## Appendix 2 - Average Daylight Factor (ADF) 112 to 116 New Oxford Street, London WC1A 1HH

APPENDIX 2  
DAYLIGHT AND SUNLIGHT CALCULATIONS

| Reference                 | Target ADF based on room use |      | Average Daylight Factor Coefficients |      |        |      |       | Actual ADF  |             |
|---------------------------|------------------------------|------|--------------------------------------|------|--------|------|-------|-------------|-------------|
|                           | Primary room use             | ADF  | T                                    | Aw   | A      | R    | Theta | ADF         | Result      |
| <u>Proposed 2nd Floor</u> |                              |      |                                      |      |        |      |       |             |             |
| Window 1                  | Bedroom                      | 1.0% | 0.68                                 | 1.99 | 60.65  | 0.69 | 59.8  | 2.5%        | Pass        |
| Window 2                  | Living Room                  | 1.5% | 0.68                                 | 3.88 | 95.24  | 0.71 | 61.1  | 3.4%        | Pass        |
| Window 3                  |                              |      | 0.68                                 | 1.57 | 124.44 | 0.68 | 59.3  | 1.0%        |             |
| Window 4                  |                              |      | 0.68                                 | 4.74 | 124.44 | 0.68 | 60.7  | 3.0%        |             |
| Window 5                  |                              |      | 0.68                                 | 1.55 | 124.44 | 0.68 | 59.4  | 0.9%        |             |
| <b>Total ADF for room</b> | Living Room                  | 1.5% |                                      |      |        |      |       | <b>4.9%</b> | <b>Pass</b> |
| Window 6                  |                              |      | 0.68                                 | 3.88 | 115.35 | 0.68 | 60.9  | 2.6%        |             |
| Window 7                  |                              |      | 0.68                                 | 1.45 | 115.35 | 0.68 | 43.0  | 0.7%        |             |
| Window 8                  |                              |      | 0.68                                 | 4.18 | 115.35 | 0.68 | 41.1  | 1.9%        |             |
| <b>Total ADF for room</b> | Bedroom                      | 1.0% |                                      |      |        |      |       | <b>5.2%</b> | <b>Pass</b> |
| Window 9                  | Kitchen                      | 2.0% | 0.68                                 | 3.04 | 52.83  | 0.72 | 31.0  | 2.5%        | Pass        |
| Window 10                 |                              |      | 0.68                                 | 1.24 | 57.84  | 0.68 | 29.4  | 0.8%        |             |
| Window 11                 |                              |      | 0.68                                 | 1.24 | 57.84  | 0.68 | 29.6  | 0.8%        |             |
| <b>Total ADF for room</b> | Bedroom                      | 1.0% |                                      |      |        |      |       | <b>1.6%</b> | <b>Pass</b> |
| <u>Proposed 3rd Floor</u> |                              |      |                                      |      |        |      |       |             |             |
| Window 12 (lower)         |                              |      | 0.68                                 | 0.34 | 83.82  | 0.69 | 61.5  | 0.0%        |             |
| Window 12 (upper)         |                              |      | 0.68                                 | 2.4  | 83.82  | 0.69 | 62.5  | 2.4%        |             |
| <b>Total ADF for room</b> | Living Room                  | 1.5% |                                      |      |        |      |       | <b>2.4%</b> | <b>Pass</b> |
| Window 13                 | Bedroom                      | 1.0% | 0.68                                 | 1.29 | 57.46  | 0.7  | 34.9  | 1.0%        | Pass        |
| <u>Proposed 4th Floor</u> |                              |      |                                      |      |        |      |       |             |             |
| Window 14 (lower)         |                              |      | 0.68                                 | 0.22 | 91.26  | 0.7  | 64.3  | 0.0%        |             |
| Window 14 (upper)         |                              |      | 0.68                                 | 4.32 | 91.26  | 0.7  | 65.7  | 4.1%        |             |
| <b>Total ADF for room</b> | Living Room                  | 1.5% |                                      |      |        |      |       | <b>4.1%</b> | <b>Pass</b> |
| Window 15 (lower)         |                              |      | 0.68                                 | 0.2  | 82.42  | 0.71 | 63.9  | 0.0%        |             |
| Window 15 (upper)         |                              |      | 0.68                                 | 4.16 | 82.42  | 0.71 | 65.6  | 4.6%        |             |
| <b>Total ADF for room</b> | Bedroom                      | 1.0% |                                      |      |        |      |       | <b>4.6%</b> | <b>Pass</b> |
| Window 16 (lower)         |                              |      | 0.68                                 | 0.08 | 125.82 | 0.68 | 62.0  | 0.0%        |             |
| Window 16 (upper)         |                              |      | 0.68                                 | 1.69 | 125.82 | 0.68 | 63.2  | 1.1%        |             |



## 8.1: Appendixes :

### Daylight / Sunlight Assessment

#### Appendix 2 - Average Daylight Factor (ADF) 112 to 116 New Oxford Street, London WC1A 1HH

| Reference                 | Target ADF based on room use |      | Average Daylight Factor Coefficients |      |        |      |             | Actual ADF |             |
|---------------------------|------------------------------|------|--------------------------------------|------|--------|------|-------------|------------|-------------|
|                           | Primary room use             | ADF  | T                                    | Aw   | A      | R    | Theta       | ADF        | Result      |
| Window 17 (lower)         | Living Room                  | 1.5% | 0.68                                 | 0.24 | 125.82 | 0.68 | 63.4        | 0.0%       | <b>Pass</b> |
| Window 17 (upper)         |                              |      | 0.68                                 | 5.09 | 125.82 | 0.68 | 64.2        | 3.3%       |             |
| Window 18 (lower)         |                              |      | 0.68                                 | 0.08 | 125.82 | 0.68 | 62.0        | 0.0%       |             |
| Window 18 (upper)         |                              |      | 0.68                                 | 1.66 | 125.82 | 0.68 | 63.2        | 1.1%       |             |
| <b>Total ADF for room</b> |                              |      |                                      |      |        |      |             |            |             |
| Window 19 (lower)         | Bedroom                      | 1.0% | 0.68                                 | 0.2  | 123.52 | 0.68 | 63.6        | 0.0%       | <b>Pass</b> |
| Window 19 (upper)         |                              |      | 0.68                                 | 4.16 | 123.52 | 0.68 | 65.2        | 2.8%       |             |
| Window 20 (lower)         |                              |      | 0.68                                 | 0.07 | 123.52 | 0.68 | 46.8        | 0.0%       |             |
| Window 20 (upper)         |                              |      | 0.68                                 | 1.55 | 123.52 | 0.68 | 49.7        | 0.8%       |             |
| Window 21 (lower)         |                              |      | 0.68                                 | 0.21 | 123.52 | 0.68 | 45.2        | 0.0%       |             |
| Window 21 (upper)         |                              |      | 0.68                                 | 4.49 | 123.52 | 0.68 | 48.1        | 2.2%       |             |
| <b>Total ADF for room</b> |                              |      |                                      |      |        |      | <b>5.8%</b> |            |             |
| Window 22                 | Kitchen                      | 2.0% | 0.68                                 | 3.04 | 53.55  | 0.72 | 43.4        | 3.4%       | <b>Pass</b> |
| Window 23                 | Bedroom                      | 1.0% | 0.68                                 | 2.15 | 79.56  | 0.7  | 45.1        | 1.6%       | <b>Pass</b> |
| Window 24 (lower)         |                              |      | 0.68                                 | 0.1  | 79.56  | 0.7  | 38.8        | 0.0%       |             |
| Window 24 (upper)         |                              |      | 0.68                                 | 2.05 | 79.56  | 0.7  | 42.1        | 1.4%       |             |
| <b>Total ADF for room</b> |                              |      |                                      |      |        |      |             |            |             |
| <u>Proposed 5th Floor</u> |                              |      |                                      |      |        |      |             |            |             |
| Window 25                 | Bedroom                      | 1.0% | 0.68                                 | 1.54 | 131.74 | 0.73 | 68.1        | 1.2%       | <b>Pass</b> |
| Window 26                 | Bedroom                      | 1.0% | 0.68                                 | 3.33 | 93.16  | 0.72 | 67.9        | 3.4%       | <b>Pass</b> |
| Window 27                 | Living Room                  | 1.5% | 0.68                                 | 3.55 | 202.85 | 0.66 | 67.8        | 1.4%       | <b>Pass</b> |
| Window 28                 |                              |      | 0.68                                 | 3.55 | 202.85 | 0.66 | 67.6        | 1.4%       |             |
| Window 29                 |                              |      | 0.68                                 | 3.33 | 202.85 | 0.66 | 67.3        | 1.3%       |             |
| Window 30                 |                              |      | 0.68                                 | 3.24 | 202.85 | 0.66 | 63.5        | 1.2%       |             |
| Window 31                 |                              |      | 0.68                                 | 3.24 | 202.85 | 0.66 | 62.2        | 1.2%       |             |
| <b>Total ADF for room</b> |                              |      |                                      |      |        |      | <b>6.5%</b> |            |             |
| Window 32                 | Kitchen                      | 2.0% | 0.68                                 | 3.04 | 69.98  | 0.7  | 63.4        | 3.7%       | <b>Pass</b> |
| Window 33                 |                              |      | 0.68                                 | 3.04 | 69.98  | 0.7  | 63.5        | 3.7%       |             |
| <b>Total ADF for room</b> |                              |      |                                      |      |        |      | <b>7.4%</b> |            |             |
| Window 34                 | Bedroom                      | 1.0% | 0.68                                 | 3.04 | 90.93  | 0.7  | 63.5        | 2.9%       | <b>Pass</b> |
| Window 35                 |                              |      | 0.68                                 | 2.15 | 90.93  | 0.7  | 60.9        | 1.9%       |             |
| <b>Total ADF for room</b> |                              |      |                                      |      |        |      |             |            |             |

# 8.1: Appendixes : Daylight / Sunlight Assessment

**Appendix 2 - Average Daylight Factor (ADF)  
112 to 116 New Oxford Street, London WC1A 1HH**

| Reference                 | Target ADF based on room use |      | Average Daylight Factor Coefficients |       |        |      |       | Actual ADF   |             |
|---------------------------|------------------------------|------|--------------------------------------|-------|--------|------|-------|--------------|-------------|
|                           | Primary room use             | ADF  | T                                    | Aw    | A      | R    | Theta | ADF          | Result      |
| <u>Proposed 6th Floor</u> |                              |      |                                      |       |        |      |       |              |             |
| Window 36                 | Bedroom                      | 1.0% | 0.68                                 | 1.81  | 104.59 | 0.72 | 71.0  | 1.7%         | Pass        |
| Window 37                 |                              |      | 0.68                                 | 1.34  | 205.6  | 0.64 | 35.6  | 0.3%         |             |
| Window 38 (lower)         |                              |      | 0.68                                 | 3.28  | 205.6  | 0.64 | 28.1  | 0.1%         |             |
| Window 38 (upper)         |                              |      | 0.68                                 | 11.14 | 205.6  | 0.64 | 43.5  | 2.7%         |             |
| Window 39 (lower)         |                              |      | 0.68                                 | 1.92  | 205.6  | 0.64 | 25.7  | 0.0%         |             |
| Window 39 (upper)         |                              |      | 0.68                                 | 6.54  | 205.6  | 0.64 | 46.1  | 1.7%         |             |
| Window 40                 |                              |      | 0.68                                 | 2.26  | 205.6  | 0.64 | 84.9  | 1.1%         |             |
| <b>Total ADF for room</b> | Kitchen/Living/Study         | 1.5% |                                      |       |        |      |       | <b>5.9%</b>  | <b>Pass</b> |
| Window 41                 | Bedroom                      | 1.0% | 0.68                                 | 2.26  | 81.88  | 0.7  | 84.5  | 3.1%         |             |
| Window 42                 |                              |      | 0.68                                 | 2.26  | 81.88  | 0.7  | 84.3  | 3.1%         |             |
| <b>Total ADF for room</b> |                              |      |                                      |       |        |      |       |              | <b>6.2%</b> |
| <u>Proposed 7th Floor</u> |                              |      |                                      |       |        |      |       |              |             |
| Window 43                 | Bedroom                      | 1.0% | 0.68                                 | 2.61  | 75.82  | 0.71 | 67.0  | 3.1%         | Pass        |
| Window 44                 |                              |      | 0.68                                 | 2.61  | 169.45 | 0.65 | 71.4  | 1.3%         |             |
| Window 45                 |                              |      | 0.68                                 | 2.61  | 169.45 | 0.65 | 71.2  | 1.3%         |             |
| Window 46                 |                              |      | 0.68                                 | 2.61  | 169.45 | 0.65 | 70.8  | 1.3%         |             |
| Window 47                 |                              |      | 0.68                                 | 9.76  | 169.45 | 0.65 | 113.5 | 7.7%         |             |
| <b>Total ADF for room</b> | Kitchen                      | 2.0% |                                      |       |        |      |       | <b>11.6%</b> | <b>Pass</b> |
| Window 48 (lower)         | Bedroom                      | 1.0% | 0.68                                 | 0.2   | 84.26  | 0.69 | 85.7  | 0.0%         |             |
| Window 48 (upper)         |                              |      | 0.68                                 | 2.07  | 84.26  | 0.69 | 86.4  | 2.8%         |             |
| Window 49 (lower)         |                              |      | 0.68                                 | 0.2   | 84.26  | 0.69 | 85.8  | 0.0%         |             |
| Window 49 (upper)         |                              |      | 0.68                                 | 2.07  | 84.26  | 0.69 | 86.5  | 2.8%         |             |
| <b>Total ADF for room</b> |                              |      |                                      |       |        |      |       | <b>5.7%</b>  | <b>Pass</b> |

## 8.1: Appendixes : Daylight / Sunlight Assessment

### Appendix 2 - Room Depth Calculation 112 to 116 New Oxford Street, London WC1A 1HH

| Room                      | Room Depth Coefficients |     |     |      | Room Depth Calculation |    |        | Result |
|---------------------------|-------------------------|-----|-----|------|------------------------|----|--------|--------|
|                           | L                       | W   | H   | Rb   | L/W + L/H              | <= | 2/1-Rb |        |
| <u>Proposed 2nd Floor</u> |                         |     |     |      |                        |    |        |        |
| Window 1                  | 2.9                     | 4.9 | 2.3 | 0.71 | 1.85                   | <= | 6.85   | Pass   |
| Window 2                  | 4.6                     | 3.3 | 4.2 | 0.74 | 2.49                   | <= | 7.61   | Pass   |
| Window 3                  | 4.8                     | 4.8 | 4.2 | 0.73 | 2.14                   | <= | 7.33   | Pass   |
| Window 4                  | 4.8                     | 4.8 | 4.2 | 0.73 | 2.14                   | <= | 7.33   | Pass   |
| Window 5                  | 4.8                     | 4.8 | 4.2 | 0.73 | 2.14                   | <= | 7.33   | Pass   |
| Window 6                  | 6.1                     | 3.6 | 4.2 | 0.74 | 3.15                   | <= | 7.69   | Pass   |
| Window 7                  | 3.6                     | 6.1 | 4.2 | 0.74 | 1.45                   | <= | 7.69   | Pass   |
| Window 8                  | 3.6                     | 6.1 | 4.2 | 0.74 | 1.45                   | <= | 7.69   | Pass   |
| Window 9                  | 2.7                     | 2.5 | 4.1 | 0.75 | 1.74                   | <= | 8.16   | Pass   |
| Window 10                 | 3.6                     | 4.2 | 2.3 | 0.71 | 2.42                   | <= | 6.89   | Pass   |
| Window 11                 | 3.6                     | 4.2 | 2.3 | 0.71 | 2.42                   | <= | 6.89   | Pass   |
| <u>Proposed 3rd Floor</u> |                         |     |     |      |                        |    |        |        |
| Window 12                 | 5.9                     | 5.4 | 2.5 | 0.72 | 3.45                   | <= | 7.05   | Pass   |
| Window 13                 | 3.7                     | 4.1 | 2.5 | 0.71 | 2.38                   | <= | 6.93   | Pass   |
| <u>Proposed 4th Floor</u> |                         |     |     |      |                        |    |        |        |
| Window 14                 | 2.9                     | 5.6 | 3.8 | 0.73 | 1.28                   | <= | 7.43   | Pass   |
| Window 15                 | 4.6                     | 2.6 | 4.3 | 0.75 | 2.84                   | <= | 7.9    | Pass   |
| Window 16                 | 4.8                     | 4.8 | 4.3 | 0.73 | 2.12                   | <= | 7.36   | Pass   |
| Window 17                 | 4.8                     | 4.8 | 4.3 | 0.73 | 2.12                   | <= | 7.36   | Pass   |
| Window 18                 | 4.8                     | 4.8 | 4.3 | 0.73 | 2.12                   | <= | 7.36   | Pass   |
| Window 19                 | 6.1                     | 3.6 | 4.3 | 0.74 | 3.11                   | <= | 7.76   | Pass   |
| Window 20                 | 3.6                     | 6.1 | 4.3 | 0.74 | 1.43                   | <= | 7.76   | Pass   |
| Window 21                 | 3.6                     | 6.1 | 4.3 | 0.74 | 1.43                   | <= | 7.76   | Pass   |
| Window 22                 | 2.7                     | 2.5 | 4.4 | 0.76 | 1.69                   | <= | 8.17   | Pass   |
| Window 23                 | 3.7                     | 4.2 | 3.8 | 0.73 | 1.85                   | <= | 7.48   | Pass   |
| Window 24                 | 3.7                     | 4.2 | 2.9 | 0.73 | 2.16                   | <= | 7.48   | Pass   |
| <u>Proposed 5th Floor</u> |                         |     |     |      |                        |    |        |        |
| Window 25                 | 4.8                     | 5.9 | 3.5 | 0.74 | 2.18                   | <= | 7.66   | Pass   |
| Window 26                 | 4.8                     | 3.1 | 4.0 | 0.75 | 2.75                   | <= | 7.85   | Pass   |
| Window 27                 | 6.1                     | 7.8 | 4.0 | 0.72 | 2.31                   | <= | 7.05   | Pass   |
| Window 28                 | 6.1                     | 7.8 | 4.0 | 0.72 | 2.31                   | <= | 7.05   | Pass   |

## 8.1: Appendixes : Daylight / Sunlight Assessment

### Appendix 2 - Room Depth Calculation 112 to 116 New Oxford Street, London WC1A 1HH

| Room                      | Room Depth Coefficients |     |     |      | Room Depth Calculation |    |        | Result |
|---------------------------|-------------------------|-----|-----|------|------------------------|----|--------|--------|
|                           | L                       | W   | H   | Rb   | L/W + L/H              | <= | 2/1-Rb |        |
| Window 29                 | 6.1                     | 7.8 | 4.0 | 0.72 | 2.31                   | <= | 7.05   | Pass   |
| Window 30                 | 7.8                     | 6.1 | 4.0 | 0.72 | 3.23                   | <= | 7.05   | Pass   |
| Window 31                 | 7.8                     | 6.1 | 4.0 | 0.72 | 3.23                   | <= | 7.05   | Pass   |
| Window 32                 | 2.1                     | 4.9 | 4.4 | 0.76 | 0.91                   | <= | 8.22   | Pass   |
| Window 33                 | 2.1                     | 4.9 | 4.4 | 0.76 | 0.91                   | <= | 8.22   | Pass   |
| Window 34                 | 3.7                     | 4.2 | 4.4 | 0.74 | 1.72                   | <= | 7.72   | Pass   |
| Window 35                 | 3.7                     | 4.2 | 3.5 | 0.74 | 1.94                   | <= | 7.72   | Pass   |
| <u>Proposed 6th Floor</u> |                         |     |     |      |                        |    |        |        |
| Window 36                 | 4.8                     | 5.4 | 3.4 | 0.73 | 2.3                    | <= | 7.42   | Pass   |
| Window 37                 | 2.6                     | 4.2 | 3.1 | 0.72 | 1.46                   | <= | 7.22   | Pass   |
| Window 38                 | 5.9                     | 9.5 | 3.1 | 0.72 | 2.52                   | <= | 7.22   | Pass   |
| Window 39                 | 9.5                     | 5.9 | 3.1 | 0.72 | 4.67                   | <= | 7.22   | Pass   |
| Window 40                 | 6.0                     | 9.1 | 3.5 | 0.72 | 2.37                   | <= | 7.22   | Pass   |
| Window 41                 | 3.5                     | 4.6 | 3.5 | 0.73 | 1.76                   | <= | 7.49   | Pass   |
| Window 42                 | 3.5                     | 4.6 | 3.5 | 0.73 | 1.76                   | <= | 7.49   | Pass   |
| <u>Proposed 7th Floor</u> |                         |     |     |      |                        |    |        |        |
| Window 43                 | 3.0                     | 4.5 | 3.2 | 0.73 | 1.6                    | <= | 7.4    | Pass   |
| Window 44                 | 5.9                     | 9.1 | 3.2 | 0.72 | 2.49                   | <= | 7.12   | Pass   |
| Window 45                 | 5.9                     | 9.1 | 3.2 | 0.72 | 2.49                   | <= | 7.12   | Pass   |
| Window 46                 | 5.9                     | 9.1 | 3.2 | 0.72 | 2.49                   | <= | 7.12   | Pass   |
| Window 48                 | 3.8                     | 4.6 | 3.0 | 0.73 | 2.09                   | <= | 7.38   | Pass   |
| Window 49                 | 3.8                     | 4.6 | 3.0 | 0.73 | 2.09                   | <= | 7.38   | Pass   |

**Appendix 2 - Sunlight to Windows**  
**112 to 116 New Oxford Street, London WC1A 1HH**

| Reference                 | Use Class            | Annual Probable Sunlight Hours |        |
|---------------------------|----------------------|--------------------------------|--------|
|                           |                      | Total                          | Winter |
| <u>Proposed 2nd Floor</u> |                      |                                |        |
| Window 2                  | Living Room          | 40%                            | 12%    |
| Window 4                  | Living Room          | 43%                            | 13%    |
| <u>Proposed 3rd Floor</u> |                      |                                |        |
| Window 12                 | Living Room          | 35%                            | 11%    |
| <u>Proposed 4th Floor</u> |                      |                                |        |
| Window 14                 | Living Room          | 41%                            | 13%    |
| Window 17                 | Living Room          | 44%                            | 15%    |
| <u>Proposed 5th Floor</u> |                      |                                |        |
| Window 28                 | Living Room          | 48%                            | 16%    |
| <u>Proposed 6th Floor</u> |                      |                                |        |
| Window 38                 | Kitchen/Living/Study | 26%                            | 10%    |
| <u>Proposed 7th Floor</u> |                      |                                |        |
| Window 45                 | Kitchen              | 64%                            | 22%    |

# 8.2: Appendixes :

## Energy / Renewable Energy Statement

### 112-116 New Oxford Street Energy Strategy Report

|          |                           |
|----------|---------------------------|
| Project: | 112-116 New Oxford Street |
| Version: | 1.0                       |
| Author:  | Stathis Eleftheriadis     |
| Date:    | 19 December 2012          |

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### EXECUTIVE SUMMARY

This report details the proposed energy strategy for the 112-116 New Oxford Street scheme, which entails the refurbishment of an existing property in the London Borough of Camden. The 7-storey development comprises of 7 refurbished flats and 1 additional new flat on the roof top.

The proposed development addresses national planning policies on energy; in particular, mitigation of climate change and energy security through energy efficiency enhancements and use of alternative energy technologies. In order to reduce the carbon footprint of the building beyond the requirements of current regulatory and market standards, the development will benefit from the following integrated systems:

- Passive design features
- Energy efficiency measures
- Low and zero carbon technologies

The building fabric U-values will meet or exceed the Part L 2010 requirements where applicable. Energy efficient light fittings will minimise the electricity demand for lighting.

An energy assessment has been carried out based on design information to identify the most appropriate renewable strategy. The proposed strategy has the potential to provide a 14.1% improvement over the baseline environmental performance of the new unit (TER) and 43% DER improvement for the refurbished units through a combination of measures.

Although, due to restrictions in available space on the development, the scheme only uses solar PV to contribute a 7.3% reduction of CO<sub>2</sub> emissions, the development does not achieve the policy for a 25% total reduction. However, considering the nature of the development this is the maximum improvement that can be achieved through passive design measures, energy efficient equipment and renewable technologies.



## 1. INTRODUCTION

### 1.1. Site analysis

The 112-116 New Oxford Street development is located in the London Borough of Camden. The development will involve 1 additional storey being added to the existing property, resulting in 8 1, 2 & 3 bedroom flats within a 7-storey building. The proposed development is mainly contained within the existing envelope of the building, with a new roof and external walls being erected for a 7th floor flat.



Fig 1 - Proposed front view of the 112-116 New Oxford Street development

### 1.2. Objective

This report summarises the work undertaken to support the development of an energy strategy for the 112-116 New Oxford Street scheme. This work has resulted in a strategy that requires design, technical and commercial decisions in order to continue the design development and ultimately select the final solution for ensuring a low carbon development.

This report outlines the energy strategy for the development, including passive design, energy and CO<sub>2</sub> footprint of the proposed scheme, and renewable energy options.

The final proposed strategy would allow the scheme to demonstrate compliance with the guidelines set out by the London Borough of Camden and the London Plan in demonstrating a positive commitment to sustainability through providing environmental improvements.

## 2. POLICY

### 2.1. London Borough of Camden

Policy CS13, paragraph 13.9

- All buildings, whether being updated or refurbished, are expected to reduce their carbon emissions by making improvements to the existing building. Work involving a change of use or an extension to an existing property is included. As a guide, at least 10% of the project cost should be spent on the improvements.
- Where retro-fitting measures are not identified at application stage we will most likely secure the implementation of environmental improvements by way of condition.
- Development involving a change of use or a conversion of 5 or more dwellings or 500sq m of any floorspace, will be expected to achieve 60% of the un-weighted credits in the Energy category in their EcoHomes or BREEAM assessment, whichever is applicable.
- Special consideration will be given to buildings that are protected e.g. listed buildings to ensure that their historic and architectural features are preserved.

### 2.2. The London Plan Policies on Energy

#### Policy 5.2: Minimising Carbon Dioxide Emissions

##### Planning decisions

Development proposals should make the fullest contribution to minimising carbon dioxide emissions in accordance with the following energy hierarchy:

1. Be lean: use less energy
2. Be clean: supply energy efficiently
3. Be green: use renewable energy

The Mayor will work with boroughs and developers to ensure that major developments meet the following targets for carbon dioxide emission reductions in buildings:

##### Residential buildings:

2010 – 2013: 25% improvement over Part L 2010

##### Non-domestic buildings:

2010 – 2013: 25% improvement over Part L 2010

Major development proposals should include a detailed energy assessment to demonstrate how the targets for carbon dioxide emissions reduction outlined above are to be met within the framework of the energy hierarchy. This report contains a detailed energy assessment in line with the requirements of policy 5.2.

## 8.2: Appendixes : Energy / Renewable Energy Statement

### Policy 5.7: Renewable Energy

Within the framework of the energy hierarchy (see Policy 5.2), major development proposals should provide a reduction in expected carbon dioxide emissions through the use of on-site renewable energy generation, where feasible.

There is a presumption that all major development proposals will seek to reduce carbon dioxide emissions by at least 20% through the use of on-site renewable energy generation wherever feasible. Development proposals should seek to utilise renewable energy technologies such as: biomass heating; cooling and electricity; renewable energy from waste; photovoltaics; solar water heating; wind and heat pumps. The Mayor encourages the use of a full range of renewable energy technologies, which should be incorporated wherever site conditions make them feasible and where they contribute to the highest overall and most cost effective carbon dioxide emissions savings for a development proposal.

### 2.3. The London Mayor's Energy Strategy

The Mayor of London has published strategies on air quality, biodiversity, noise, transport, waste and other environmental issues, aimed at improving the quality of life and promoting sustainable development within London. Among the aims and objectives of the Energy Strategy are minimising the impact of London's energy production and consumption on public health, and on the local and global environment, and reducing London's contribution to climate change by minimising emissions of CO<sub>2</sub> from all sectors (Commercial, domestic, industrial and transport) through energy efficiency, CHP, use of renewable energy and cleaner fuels.

Alongside the policies in The London Plan, the Energy Strategy emphasises the importance of energy and associated CO<sub>2</sub> emissions in planning decisions within the capital.

# 8.2: Appendixes : Energy / Renewable Energy Statement

## 3. APPROACH

The approach to achieving the planning policy energy objectives has been to consider strategies and technologies to achieve a low energy and carbon footprint for the scheme.

As a refurbishment development the energy strategy for the scheme follows the energy hierarchy:

- Using less energy by passive design
- Supplying energy efficiently
- Using renewable energy sources to reduce CO<sub>2</sub>

This energy strategy examines the energy performance of the proposed 112-116 New Oxford Street development as follows:

- Section 4 contains the passive design and energy efficiency measures that will be considered in the scheme. This section describes targets and recommended/proposed actions to achieve these targets.
- Section 5 contains the estimated carbon footprint for this site including passive design and energy efficiency measures identified in section 4.
- Section 6 analyses Low and Zero Carbon Energy Systems to offset emissions.
- Section 7 summarises the overall carbon reductions that could be achieved by the scheme.

## 4. PASSIVE DESIGN

Passive design measures have been considered throughout the pre-planning stage to reduce energy demand. Opportunities for daylighting, efficient ventilation and passive solar heating have been identified.

### 4.1 Solar Gain Control & Daylighting

The U-Values of all glazed elements will exceed Building Regulations standards, and incorporate low emissivity coating, resulting in an efficient balance between passive solar gain and the thermal losses from each room.

Daylight levels are high throughout and are supplemented with 100% use of low energy lighting. The use of a roof light within the basement kitchen will help ensure optimum levels of daylight throughout the day.

### 4.2 Energy Efficiency

Studies have been carried out to determine the energy and carbon emissions benefits of various enhancements to the thermal performance of the new proposed building envelope, by using increased U-Values for new elements and improving overall air tightness, resulting in a significant improvement over Building Regulations standards. The property has been designed to be naturally ventilated, reducing additional energy loads for the building.

Table 4-1 shows a summary of the proposed U-values, air tightness, heating and ventilation strategy for the development. These measures will be considered for the development and have been assumed for the analysis at this stage.

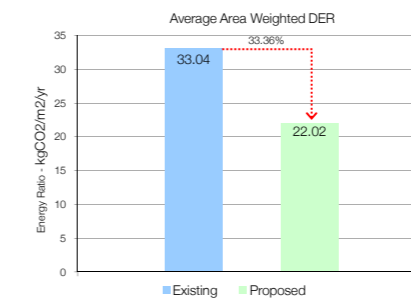
| Element                              | Measure  |
|--------------------------------------|--|
| External Walls- Refurbished          | 0.20 W/m <sup>2</sup> K                                    |
| External Walls- New                  | 0.15 W/m <sup>2</sup> K                                    |
| Roof                                 | 0.13 W/m <sup>2</sup> K                                    |
| Windows (& Doors with > 60% Glazing) | 1.5 W/m <sup>2</sup> K                                     |
| Air Tightness - Refurbished          | 7 m <sup>3</sup> /m <sup>2</sup> /h                        |
| Air Tightness - New                  | 5 m <sup>3</sup> /m <sup>2</sup> /h                        |
| Thermal Bridging                     | Default(0.150)   |
| Heating System                       | (Modulating) Gas fired boilers (90% efficient)             |
| Ventilation System                   | Natural Ventilation with extract fans for bathroom/kitchen |

Table 4-1: Passive design measures and proposed services

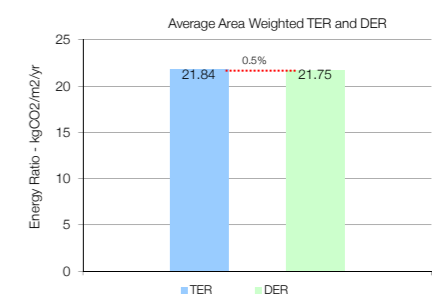
## 4.3 Energy Conservation Measures

Additional energy conservation measures that will help to reduce energy consumption in use have been identified as follows:

- All new white goods selected for this development are rated A or A+ in the EU energy-labelling scheme for domestic appliances and B rated wash dryers if specified.
- Low use water fittings throughout (water consumption is to be less than 125 litres/person/day); helping to reduce hot and cold water demand.
- Movement and daylight sensors fitted to lighting for common and external areas.
- Time and temperature zone space heating controls.



Graph 4-2: Percentage improvement of Dwelling Emission Rate (DER) – Refurbished units



Graph 4-3: Percentage improvement of Dwelling Emission Rate (DER) over the Target Emission Rate (TER) for the base case – New Unit



5. ESTIMATED ENERGY AND CO<sub>2</sub> FOOTPRINT

Table 5-1 below outlines the estimated total energy demand and associated carbon emissions for the 112-116 New Oxford Street development, taking into account the passive measures identified in the previous section. The consumption is estimated based on the use of typical systems utilising gas central heating, in order to estimate the baseline CO<sub>2</sub> emissions for the site. Alternative fuel sources are investigated in the following sections. Any CO<sub>2</sub> savings from the use of renewable technologies are compared with the 'typical' gas case, as this is the lowest carbon solution for dwellings not benefitting from renewables.

The calculations have been based on SAP outputs, with an inclusion for appliance use (un-regulated emissions) not covered by SAP (based on BRE methodology). Full details of assumptions are included in Appendix A.

|              | Energy & CO <sub>2</sub> |                    |                |                             |                       |                   |                     |                |  |                       |                               |
|--------------|--------------------------|--------------------|----------------|-----------------------------|-----------------------|-------------------|---------------------|----------------|--|-----------------------|-------------------------------|
|              | Gas Demand               |                    |                | Electricity Demand          |                       |                   |                     |                |  |                       |                               |
|              | Space heating (kWh/yr)   | Hot Water (kWh/yr) | Total (kWh/yr) | Gas CO <sub>2</sub> (kg/yr) | Pumps & Fans (kWh/yr) | Lighting (kWh/yr) | Appliances (kWh/yr) | Total (kWh/yr) | Electricity CO <sub>2</sub> (kg CO <sub>2</sub> /yr) | Total Energy (kWh/yr) | Total CO <sub>2</sub> (kg/yr) |
| Refurbished  | 32,067                   | 14,763             | 46,830         | 9,272                       | 965                   | 2,106             | 17,774              | 20,845         | 10,777   | 67,675                | 20,049                        |
| New Unit     | 6,454                    | 2,426              | 8,880          | 1,758                       | 175                   | 376               | 3,145               | 3,696          | 1,911  | 12,576                | 3,669                         |
| <b>Total</b> | <b>38,521</b>            | <b>17,189</b>      | <b>11,030</b>  | <b>2,297</b>                | <b>1,140</b>          | <b>2,482</b>      | <b>20,919</b>       | <b>24,541</b>  | <b>12,688</b>  | <b>80,251</b>         | <b>23,718</b>                 |

Table 5-1: Estimated energy demand and CO<sub>2</sub> emissions of the site by energy source

6. LOW AND ZERO CARBON ENERGY SYSTEMS

There is a target within the borough to achieve a 20% reduction of CO<sub>2</sub> emissions through the use of on-site renewable technologies. The following table outlines the LZC technologies that have been considered for the site and the technical feasibility for each has been discussed based on the energy demand and site constraints.

| Technology                      | Description   | Advantages   | Disadvantages  | Feasibility  |   |
|---------------------------------|---|--|--|--|---|
| <b>Solar Thermal Collectors</b> | Solar thermal collectors can be used to provide hot water<br><br>They can provide up to approximately 50% of the hot water demand | No noise issues associated with Solar thermal collectors<br><br>No additional land use from the installation of solar thermal collectors<br><br>Low maintenance and easy to manage<br><br>Low capital cost   | The hot water cylinder will need to be larger than a traditional cylinder<br><br>Consideration will need to be given to the space required for the solar array and the orientation<br><br>Needs unobstructed space on roof | The development has a small flat onto which a small solar thermal array could be placed<br><br>However due to the nature of the development it is a little impractical to use a centralised hot water system, making it difficult to distribute the hot water between the residential and office spaces  | x |
| <b>Photovoltaic Panels (PV)</b> | Photovoltaic (PV) panels provide noiseless, low-maintenance, carbon free electricity using the energy emitted from the sun        | Can have significant impact on carbon by offsetting electricity which has a high carbon footprint<br><br>Low maintenance<br><br>No noise issues<br><br>No additional land use from the installation of PV panels<br><br>Bolt on technology that does not need significant amounts of auxiliary equipment | High capital investment required<br><br>RHI tariffs to be reduced, so less financially attractive<br><br>Needs unobstructed space on roof  | The development has a small flat roof onto which a small solar PV array could be placed. This would help contribute to the electricity demand of the property<br><br>There is no other available space within the development due to limits on the front roof and so only a small sized array could be installed – it is not expected that this can achieve a 20% reduction in CO <sub>2</sub> emissions alone | ✓ |

## 8.2: Appendixes : Energy / Renewable Energy Statement

| Technology                             | Description  | Advantages   | Disadvantages  | Feasibility   |   |
|--|--|--|--|---|---|
| <b>CHP (Combined Heat &amp; Power)</b> | CHP systems use an engine driven alternator to generate electricity while using the waste heat from the engine, jacket and exhaust to provide heating and hot water. Economic viability relies on at least 4000 hours running time per annum | Mature technology<br><br>High CO <sub>2</sub> savings  | Cost of the system is relatively high for small schemes such as this<br><br>Only appropriate for large development with high heat loads  | The development is not large enough for CHP to be a viable system   | x |
| <b>Biomass Heating</b>                 | Solid, liquid or gaseous fuels derived from plant material can provide boiler heat for space and water heating, though most commonly in the form of wood chip boilers  | Potential to reduce large component of the total CO <sub>2</sub><br><br>A biomass boiler would replace a standard gas heating system so some of the cost may be offset through money saved on a traditional boiler | Regular maintenance will be required<br><br>Availability of fuel may become a problem, therefore limited cost saving for residents<br><br>The noise generated by a biomass boiler is similar to that of a gas boiler. It is advisable not to locate next to particularly sensitive areas such as bedrooms<br><br>A plant room and fuel store will be required which may take substantial space from the proposed development or surroundings<br><br>The fuel will need to be delivered, which can cause issues with access<br><br>Biomass is often not a favoured technology in new developments due to the potential local impacts of NOx emissions and delivery vehicles | Biomass is not considered feasible for such a development due to issues of fuel storage, access for delivery vehicles and local NOx emissions | x |

# 8.2: Appendixes : Energy / Renewable Energy Statement

|  |   |  |   |  |   |
|--|---|--|---|--|---|
| <b>Wind Turbines (Vertical Axis)</b>                           | Most small-scale (1-25kW) wind turbines can be mounted on buildings though this is generally not recommended. Larger turbines require concrete foundations at ground level in a suitable, unobstructed site   | Low noise<br><br>Bolt on technology that does not need significant amounts of auxiliary equipment  | Low energy output particularly in urban environments, therefore not suitable here<br><br>High visual impact<br><br>Noise (and sometimes vibration) impact<br><br>High capital cost  | The development is not appropriate for this technology as wind speeds and profiles are inadequate in this urban area   | ✘ |
| <b>Ground Source Heat Pumps (GSHP) – Heating &amp; Cooling</b> | A ground loop heat exchanger offers efficient heating of a space in winter, as the temperature of the ground (below approx 2m) remains almost constant all year round<br><br>The same loop of pipe and compressor allows heat from the building to be rejected (via a highly efficient compressor) into the soil, dissipating heat from the space and providing cooling | Low maintenance and easy to manage<br><br>Optimum efficiency when used with under-floor heating systems<br><br>As heat pumps would replace standard heating systems, some of the cost may offset through money saved on a traditional boiler | The heat pump has a noise level around 45-60dB so some attenuation may be required and it should be sensibly located<br><br>Relatively high capital cost<br><br>Requires electricity to run the pump, therefore limited carbon savings in most cases<br><br>For communal systems a plant room is required which may take additional land from the proposed development/surroundings | There is very limited external space associated with the development; therefore a horizontal loop system is not practical<br><br>A borehole system could be utilised, however the cost of such a system is considered not financially viable for a project of this scale | ✘ |

|  |  |  |   |   |   |
|--|--|--|---|---|---|
| <b>Air Source Heat Pump (ASHP) - Heating</b> | Air Source Heat Pumps extract latent energy from the air in a manner similar to ground source heat pumps | Low maintenance and easy to manage<br><br>Optimum efficiency with under-floor heating systems<br><br>As heat pumps would replace standard heating systems, some of the cost may offset through money saved on a traditional boiler | The heat pump has a noise level around 50-60dB so some attenuation may be required and it should be sensibly located. The potential noise from the external unit may mean there is local opposition to their installation<br><br>Requires electricity to run the pump, therefore limited carbon savings in most cases<br><br>For communal systems plant room required which may take additional land from the proposed development/surroundings<br><br>Potential noise issues | The use of an ASHP is unlikely to be feasible due to the poor performance of such as system | ✘ |
|--|--|--|---|---|---|

**Table 6-1:** Feasibility of LZC technologies for the site

Due to the space restrictions of this site, the majority of the LZC technologies are unpractical for use on this development. There is a small space suitable for a solar panel installation on the roof and it is proposed that a solar PV system be installed as the energy generated can be easily distributed between the residential flats.

To achieve a 20% reduction in CO<sub>2</sub> emissions through the sole use of on-site renewables, a second LZC system would need to be employed. The only appropriate systems would be Ground Source Heat Pumps with vertical boreholes or Air Source Heat Pump. Both systems are considered financially impractical and instead it is proposed that CO<sub>2</sub> emission reductions are achieved through the combination of a solar PV system and an improved building fabric to reduce energy demand.

## 7. SUMMARY OF ESTIMATED CO<sub>2</sub> EMISSIONS REDUCTIONS

The energy demand and potential impact on CO<sub>2</sub> of the inclusion of renewable technologies has been considered for the development. Due to space limitations on the site there is little scope for a financially viable LZC technology to be utilised and achieve a 20% reduction in CO<sub>2</sub> emissions alone. The development has a small flat roof and it is proposed that a solar PV array is installed here to contribute as much as possible to the site's energy demand. Further reductions of CO<sub>2</sub> emissions can be achieved by using a high performing building fabric, energy efficient equipment and mechanical ventilation heat recovery within the flats.

| Renewable Systems  | Energy provided by technology (kWh/yr) | Energy & CO <sub>2</sub>         |   |   | Life cycle carbon and cost analysis   |                                |                        |   |
|--|--|----------------------------------|---|---|---------------------------------------|--------------------------------|------------------------|---|
|  |  | % of site electricity demand met | CO <sub>2</sub> saved by technology (kgCO <sub>2</sub> /yr) | % site CO <sub>2</sub> saving (inc appliance) | Improvement in DER over TER(New unit) | 25 year CO <sub>2</sub> saving | Estimated capital cost | Payback time (including capital & installation costs, maintenance etc.) |
| Photovoltaics (4.25 kWp) for the residential flats<br>Total Gross panel area ~23.6m <sup>2</sup><br>@ 10° orientation<br>Module output ~0.18 kWp/m <sup>2</sup><br>(Area and efficiency may vary on specification at tender stage) | 3,267                                  | 13.3%                            | 1,728   | 7.3%  | 14.1%                                 | 43,200                         | £7-10k                 | ~6-11yrs <sup>1</sup>   |

**Table 0-1:** CO<sub>2</sub> savings from renewable technologies

The above table shows the CO<sub>2</sub> savings from the largest PV system array that can be installed on the site, taking into account available roof area and limitation of the technologies. The PV system will offset 7.3% of the site's CO<sub>2</sub> emissions (Figure 7-1) and result in a 14.1% improvement over Part L 2010 for the new unit (Figure 7-2). For the refurbished units the average area weighted DER improvement is 43 % (Figure 7-3) over the existing development. For a detailed breakdown of the DER & TER; refer to the SAP worksheets in the Appendix.

Figures 7-1, 7-2 and 7-3 below show the overall impacts in terms of carbon of renewable technologies.

<sup>1</sup> This payback time has been calculated based on the assumption that FIT payments will be claimed

# 8.2: Appendixes : Energy / Renewable Energy Statement

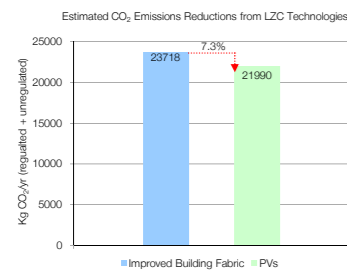


Figure 7-1: Estimated Reduction in CO<sub>2</sub> Emissions with Solar PV

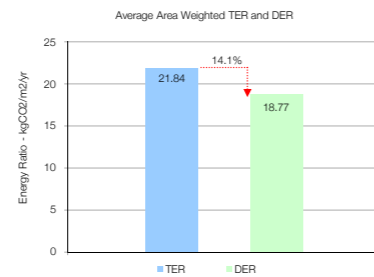


Figure 7-2: Site improvement in DER over TER - New Unit

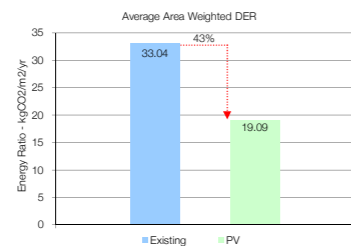


Figure 7-3: Percentage improvement of Dwelling Emission Rate (DER) - Refurbished units

## 7.1 BREEAM Credits

The SAP calculations carried out for the refurbished flats confirm that credits can be achieved for the BREEAM Domestic Refurbishment assessment as follows.

### Ene 1 – Improvement in Energy Efficiency Rating

For the refurbished units the improvement in EER from the existing property to the proposed dwelling is 9.7, which equates to 2 credits being achieved.

### Ene 2 – Energy Efficiency Rating Post Refurbishment

The post refurbishment EER is 82.75 which equates to 7 credits.

### Ene 3 – Primary Energy Demand

For the refurbished units the primary energy demand is 101.75 kWh/m<sup>2</sup>/yr which equates to 14 credits.

## 8. CONCLUSION

For the 112-116 New Oxford Street development, a combination of passive design measures has been identified to help to reduce the energy load.

Significant improvements to the building fabric, energy efficient equipment, improved water use efficiency, the use of occupant controls and a solar PV array has been demonstrated to provide a 14.1% improvement over the baseline levels for the new unit and 43% improvement for the refurbished units.

The 112-116 New Oxford Street development has been shown to demonstrate a significant improvement from the existing condition. Although on-site renewable technologies have not been able to contribute to a 20% reduction in CO<sub>2</sub> emissions alone, given the limitations on site and the size of the development, solar PV has been shown to provide a 7.3% reduction in CO<sub>2</sub> emissions for the site.

The advised option will be considered at the detailed design and construction stages and adequate provisions made to ensure that the various carbon reduction targets are met.

The figures in this report are based on preliminary analysis only, and further detailed studies will be required before specifying any of the potential systems.

# 8.2: Appendixes : Energy / Renewable Energy Statement

## APPENDIX A

A-1 The following tables show the energy assumptions used for the energy and CO<sub>2</sub> calculations.

The calculations have been based on SAP results with an inclusion for appliance use not covered by SAP (based on BRE methodology) for the student accommodation units.

The appliances figure is based on the BRE calculation formula for appliances and cooking. Taken from Code for Sustainable Homes in ENE 7 Table 1.4 notes, as below:

A-2 [3] Kg CO<sub>2</sub>/year from appliances and cooking. See Ene 1:

$$99.9 \times (TFA \times N)^{0.4714} - (3.267 \times TFA) + (32.23 \times N) + 72.6$$

Where TFA = Total Floor area and N = Number of Occupants

For TFA < 43 m<sup>2</sup>; N = 1.46

TFA ≥ 43 m<sup>2</sup>; N = 2.844 × (1 - exp(-0.000391 × TFA<sup>2</sup>))

| Residential         |                       |                  |
|---------------------|-----------------------|------------------|
| Energy Demands      |                       | Source           |
| Use Type            | Demand/m <sup>2</sup> |                  |
| Heating             | 66.06                 | SAP Calculations |
| DHW                 | 29.48                 |                  |
| Fans/Pumps/Controls | 1.96                  |                  |
| Lighting            | 4.26                  |                  |
| Appliances          | 35.9                  |                  |

## APPENDIX B

The following tables show figures used in the energy and CO<sub>2</sub> calculations to estimate energy produced and CO<sub>2</sub> savings from renewable technologies. These figures can be used to validate the results.

| CO <sub>2</sub> Intensity Values     |                              |
|--------------------------------------|------------------------------|
| Gas Intensity                        | 0.198 kgCO <sub>2</sub> /kWh |
| Electricity Intensity                | 0.517 kgCO <sub>2</sub> /kWh |
| Grid displaced electricity intensity | 0.529 kgCO <sub>2</sub> /kWh |
| Biodiesel carbon intensity           | 0.025 kgCO <sub>2</sub> /kWh |

| Renewable Technology Efficiencies      |                         |
|--|-------------------------|
| PV energy produced per kWp             | 858.4 kWh/kWp           |
| PV kWp per m <sup>2</sup> panel        | 0.18 kWp/m <sup>2</sup> |
| Efficiency of solar thermal collectors | 600 kWh/m <sup>2</sup>  |
| COP of GSHP                            | 4                       |
| Boiler efficiency                      | 90%                     |

| Fuel Prices |           |
|-------------|-----------|
| Gas         | £0.04/kWh |
| Electricity | £0.11/kWh |

## APPENDIX C

### Available Grants

The following table summarises grants that may be available for funding renewable technologies for this project.

| Grant   | Run By                           | Who Can Apply                                | What Microgeneration Technologies Are Covered?   | Grant Availability   |
|---|----------------------------------|--|--|--|
| Feed in Tariff                                | Ofgem (paid by energy companies) | Open to all (max system sizes apply)         | <ul style="list-style-type: none"> <li>Anaerobic Digestion</li> <li>Hydro</li> <li>Micro CHP (pilot)</li> <li>PV</li> <li>Wind</li> </ul>  | Applies to all MCS (Microgeneration Certification Scheme - <a href="http://www.microgenerationcertification.org">www.microgenerationcertification.org</a> ) Installations post 15 <sup>th</sup> July 2009. (PV – new lower tariff for installations post 1 <sup>st</sup> April 2012) |
| Renewable Heat Incentive (RHI)                | Ofgem                            | Open to all (max system sizes apply)         | <ul style="list-style-type: none"> <li>Biomass</li> <li>Bioliqids</li> <li>Biogas</li> <li>GSHP</li> <li>ASHP</li> <li>Solar Thermal</li> </ul>  | Applies to all MCS (Microgeneration Certification Scheme - <a href="http://www.microgenerationcertification.org">www.microgenerationcertification.org</a> ) Installations post 15 <sup>th</sup> July 2009. Recently announced that RHI will be going ahead in June 2011.             |
| Community Sustainable Energy Programme (CSEP) | BRE                              | Not-for-profit community based organisations | <ul style="list-style-type: none"> <li>Solar photovoltaics</li> <li>Solar thermal hot water</li> <li>Wind turbines</li> <li>Heat pumps</li> <li>Automated wood pellet stoves</li> <li>Wood fuelled boiler systems</li> <li>Micro-hydro turbines</li> </ul> | Both capital and project development grants are available under this scheme. Capital grants are available. Money is allocated in rounds. Please visit <a href="http://www.communitysustainable.org.uk">www.communitysustainable.org.uk</a> for more information.                     |

|   |  |  |   |  |
|---|--|--|---|--|
| Carbon Emission Reduction Target (CERT) | Energy                                       | Housing sector (new & existing)  | <ul style="list-style-type: none"> <li>Energy efficiency measures in existing homes. Renewable technologies installed to offset carbon emissions over and above planning requirements.</li> </ul> | <p>CERT money comes direct from energy companies and can usually be accessed through renewable technology suppliers who have set up deals with these companies.</p> <p>E.g. EON provide funding for GSHP &amp; ASHP through Calorex.</p> <p>Find out from suppliers if they have access to this funding when getting costs.</p>  |
| Bioenergy Capital Grant                 | (DECC) Department of Energy & Climate Change | <p>Industrial, commercial sector (This includes, but is not restricted to, public and private limited companies (Ltd and plc), sole traders, farmers etc)</p> <p>Community sector (This includes, but is not restricted to, schools, colleges, universities, hospitals, local authorities, housing associations, charities etc.)</p> | <ul style="list-style-type: none"> <li>Biomass heat boilers and biomass combined heat and power (CHP) equipment, including anaerobic digesters for heat-only or CHP.</li> </ul>                   | <p>Up to 40% of the capital cost &amp; installation of the difference in cost of installing the biomass boiler or CHP plant compared to installing the fossil fuel alternative.</p> <p>Max £500,000.</p> <p>Funding is available in rounds. Check <a href="http://www.bioenergycapitalgrants.org.uk/">http://www.bioenergycapitalgrants.org.uk/</a> to see if a round is open now or will be available in time for your development.</p> |

## APPENDIX D

### Domestic 'As Designed' SAP Calculations

# 8.2: Appendixes : Energy / Renewable Energy Statement

### Full SAP Calculation Printout

**Property Reference:** 21686\_New Oxford Street\_03Flat  
**Survey Reference:** PVS  
**Property:** 112-116, New Oxford Street, LONDON, WC1A 1HH.

**Issued on Date:** 17.Dec.2012  
**Prop Type Ref:**

**SAP Rating:** 83 B **CO2 Emissions (t/year):** 0.71 **DER:** 20.17 Pass **Reduction:** 8.6% **FEE:** 50.5 **ZCH:** 0.00  
**Environmental:** 89 B **General Requirements Compliance:** Pass **TER:** 22.06 **HLP:** 1.26 **Energy cost:** £ 247

**CSH Results** **Version:** CSH November 2010 **ENE1 Credits:** 1.0 **ENE2 Credits:** 0.0 **ENE7 Credits:** 0 **CSH Level:** 3

**Surveyor:** admin admin, Tel: unknown  
**Address:**  
**Client:**

**Software Version:** Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18  
**SAP version:** SAP 2009, Regs Region: England and Wales (Part L1A 2010), Calculation Type: New Dwelling As Designed

**CALCULATION DETAILS for survey reference no 'PVS'**  
**SAP2009 - 9.81 input data (DesignData) -**

Page: 1 of 22

SAP2009 Input Data

|                             |  |
|-----------------------------|--|
| FullRefNo:                  | PVS  |
| Sap Version:                | SAP 2009   |
| Regs Region:                | England & Wales  |
| Region:                     | Thames Valley  |
| Calculation Type:           | New Build (As Designed)  |
| DwellingOrientation:        | South East   |
| Property Type:              | Flat, End-Terrace  |
| Storeys:                    | 1  |
| Date Built:                 | 2012   |
| Sheltered Sides:            | 2  |
| Sunlight Shade:             | Average or unknown   |
| Measurements                | Perimeter, Floor Area, Storey Height   |
| 1st Storey:                 | 19.4, 38.86, 2.74  |
| Living Area:                | 20.88 m2, fraction: 53.7%  |
| Thermal Mass:               | Simple calculation   |
| Thermal Mass Simple:        | Medium   |
| Thermal MassValue:          | 250  |
| External Walls              | Nett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  |
| External Wall               | 20.106, 25.076, 190, , CavityWallDensePlasterDenseBlock, , Cavity, 0, 0.4, Calculate   |
| Corridor Wall               | 26.19, 28.08, 190, , CavityWallDensePlasterDenseBlock, , Cavity, 0.43, 0.225733634311512, Gross                              |
| Party Walls                 | Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal   |
| Party Wall                  | 44.02, 180, , PartyWallDensePlaster, , Solid, 0, 0   |
| External Roofs              | Nett Area, Gross Area, Kappa, Construction, Element, UValueFinal   |
| Party Ceilings              | Area, Kappa, Construction, Element   |
| Ceiling                     | 38.86, 100, PartyFloorConcreteSlab, ,  |
| Heat Loss Floors            | Area, Kappa, Construction, Element, Type, UValueFinal, ShelterFactor   |
| Party Floors                | Area, Kappa, Construction, Element   |
| Floor                       | 38.86, 100   |
| Description                 | Data Source, Type, Glazing, Glazing Gap, Argon Filled, Solar Trans, Frame Type, Frame Factor, U Value                        |
| Windows                     | Manufacturer, Window, Double glazed, , , 0.76, , 0.7,  |
| Door                        | Manufacturer, Solid Door, , , , ,  |
| Openings                    | Opening Type, Location, Orientation, Curtain Type, Overhang Ratio, Wide Overhang, Width, Height, Count, Area, Curtain Closed |
| Windows SE                  | Window, External Wall, Southeast, None, 0, , 0, 0, 0, 3.42,  |
| Windows NW                  | Window, External Wall, Northwest, None, 0, , 0, 0, 0, 1.55,  |
| Door                        | Solid Door, Corridor Wall, Northeast, , , , 0, 0, 0, 1.89,   |
| Conservatory:               | None   |
| Draught Proofing:           | 100  |
| Draught Lobby:              | No   |
| Thermal Bridges             | Default,   |
| Y                           | 0.15   |
| Pressure Test:              | True   |
| Designed q50:               | 7  |
| AsBuilt q50:                | 4  |
| Property Tested:            | False  |
| Mechanical Ventilation      | None   |
| Chimneys MRS:               | 0  |
| Chimneys SHS:               | 0  |
| Chimneys Other:             | 0  |
| Chimneys Total:             | 0  |
| Open Flues MRS:             | 0  |
| Open Flues SHS:             | 0  |
| Open Flues Other:           | 0  |
| Open Flues Total:           | 0  |
| Intermittent Fans:          | 2  |
| Passive Vents:              | 0  |
| Flueless Gas Fires:         | 0  |
| Cooling System              | None   |
| Light Fittings:             | 5  |
| L&L Fittings:               | 5  |
| Percentage of L&L Fittings: | 100  |
| External Lights Fitted:     | No   |
| External L&Ls Fitted:       | No   |
| Electricity Tariff:         | Standard   |
| Main Heating 1              | Description  |
| Percentage                  | 100  |
| MRS                         | BGW - Mains gas BGW Post 98 Combi condens. with auto ign.  |
| SAP Code                    | 104  |
| Boiler Efficiency Type      | SeDbuk 2009  |
| Efficiency                  | 90   |
| Model Name                  | tbc  |
| Manufacturer                | tbc  |
| MRS Controls                | CB1  |
| Delayed Start Stat          | No   |
| Ctrl SAP Code               | 2110   |

# 8.2: Appendixes :

## Energy / Renewable Energy Statement

**CALCULATION DETAILS for survey reference no 'PVs' SAP2009 - 9.81 input data (DesignData) -** Page: 2 of 22

Burner Control On/Off  
 Boiler Compensator None  
 Flue Type Balanced  
 Fan Assisted Flue Yes  
 Pumped Pump in heated space  
 Heat Emitter Resistors  
 Combi boiler type Standard Combi  
 Combi keep hot type None  
 Main heating 2 None  
 Smoke Control Area Unknown  
 Community Heating None  
 Secondary heating None  
 Water Heating MainHeating1  
 Type HR1  
 Low Water Usage Yes  
 SAP Code 901  
 Hot Water Cylinder None  
 Flue Gas Heat Recovery System None  
 Waste Water Heat Recovery none  
 PV Unit One Dwelling  
 PVUnit 1 Cells Peak = 0.28, Orientation = South, Elevation = Horizontal, Overshading = NoneOrLittle  
 Wind Turbine None  
 Terrain Type Urban  
 Small Scale Hydro None  
 Special Features None

**CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF FABRIC ENERGY EFFICIENCY** Page: 3 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
 CALCULATION OF FABRIC ENERGY EFFICIENCY  
 Calculated by program Eimhurst Energy Systems SAP2009 Calculator (Design System) version 3.07:18

1. Overall dwelling dimensions

| Area (m2)  | Storey height (m) | Volume (m3)          |
|--|-------------------|----------------------|
| Ground floor   | 2.7400 (2b)       | 106.4764 (1b) - (3b) |
| Total floor area FFA = (1a)+(1b)+(1c)+(1d)+(1e)...(1n) | 38.8600           | 106.4764 (5)         |
| Dwelling volume  |                   | 106.4764 (5)         |

2. Ventilation rate

| main heating | secondary heating | other | total    | m3 per hour  |
|--------------|-------------------|-------|----------|--------------|
| 0            | 0                 | 0     | 0 + 40 = | 0.0000 (6a)  |
| 0            | 0                 | 0     | 0 + 20 = | 0.0000 (6b)  |
| 0            | 0                 | 0     | 2 * 10 = | 20.0000 (7a) |
| 0            | 0                 | 0     | 0 * 10 = | 0.0000 (7b)  |
| 0            | 0                 | 0     | 0 * 40 = | 0.0000 (7c)  |

3. Heat losses and heat loss parameter

| Element  | Gross m2 | Openings m2 | NetArea m2           | U-value W/m2K | A x U W/K     | K-value k2/m2K | A x K k2/K    |
|--|----------|-------------|----------------------|---------------|---------------|----------------|---------------|
| Door   | 1.8900   | 0.0000      | 1.8900               | 1.4151        | 2.6613        | 0.8829         | 1.6613 (26)   |
| Windows (Uw = 1.50)  | 25.0760  | 4.9700      | 20.1060              | 0.2000        | 4.0212        | 0.0000         | 0.0000 (27)   |
| External Wall  | 28.0800  | 1.8900      | 26.1900              | 0.2257        | 5.9120        | 0.0000         | 0.0000 (29a)  |
| Corridor Wall  | 53.1560  | 0.0000      | 53.1560              | 0.0000        | 0.0000        | 0.0000         | 0.0000 (31)   |
| Fabric heat loss, W/K = Sum (A x U)                        |          |             | (26)...(30) + (32) = |               | 18.8562       |                | 18.8562 (33)  |
| Party Wall   | 44.0200  | 0.0000      | 44.0200              | 0.0000        | 0.0000        | 0.0000         | 0.0000 (32)   |
| Floor  | 38.8600  | 0.0000      | 38.8600              | 0.0000        | 0.0000        | 0.0000         | 0.0000 (32b)  |
| Ceiling  | 38.8600  | 0.0000      | 38.8600              | 0.0000        | 0.0000        | 0.0000         | 0.0000 (32b)  |
| Thermal mass parameter (TMP = Cm / FFA) in kJ/m2K          |          |             |                      |               | 250.0000      |                | 250.0000 (35) |
| Thermal bridges (Default value 0.150 * total exposed area) |          |             |                      |               | 7.9734        |                | 7.9734 (36)   |
| Total fabric heat loss                                     |          |             |                      |               | (33) + (36) = |                | 26.8296 (37)  |

4. Water heating energy requirements (kWh/year)

| Jan     | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov          | Dec          |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------------|--------------|
| 24.2604 | 23.5375 | 23.5375 | 22.2157 | 21.4262 | 21.0591 | 20.7102 | 20.7102 | 21.6167 | 22.2157 | 22.8559      | 23.5375 (38) |
| 39.5398 | 51.0900 | 50.3671 | 49.0453 | 48.2558 | 47.8886 | 47.5398 | 48.4463 | 49.0453 | 49.6855 | 50.3671 (39) |              |
| 1.3147  | 1.2961  | 1.2961  | 1.2621  | 1.2418  | 1.2323  | 1.2234  | 1.2234  | 1.2467  | 1.2621  | 1.2783 (40)  |              |
| 31      | 28      | 31      | 30      | 31      | 30      | 31      | 31      | 30      | 31      | 31           | 31 (41)      |

**CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF FABRIC ENERGY EFFICIENCY** Page: 4 of 22

Utilisation factor for gains for living area, nil/m (see Table 9a)

| Jan     | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov     | Dec         |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------------|
| 52.8208 | 53.5789 | 53.5789 | 55.0229 | 55.9230 | 56.3518 | 56.7653 | 56.7653 | 55.7031 | 55.0229 | 54.3138 | 53.5789     |
| 4.5214  | 4.5719  | 4.5719  | 4.6682  | 4.7282  | 4.7688  | 4.7844  | 4.7844  | 4.7135  | 4.6682  | 4.6209  | 4.5719      |
| 0.9967  | 0.9933  | 0.9847  | 0.9636  | 0.9363  | 0.9403  | 0.9403  | 0.9403  | 0.9237  | 0.9079  | 0.8939  | 0.8971 (86) |

7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Thi (C)

| Jan     | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov     | Dec          |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------------|
| 19.4274 | 19.7995 | 20.0736 | 20.3810 | 20.7173 | 20.9187 | 20.9872 | 20.9847 | 20.8510 | 20.4665 | 19.9536 | 19.4608 (87) |
| 19.8322 | 19.8467 | 19.8467 | 19.8733 | 19.8893 | 19.8967 | 19.9039 | 19.9039 | 19.8934 | 19.8733 | 19.8604 | 19.8467 (88) |
| 0.9955  | 0.9910  | 0.9790  | 0.9494  | 0.8535  | 0.6543  | 0.4036  | 0.4229  | 0.7633  | 0.9115  | 0.9915  | 0.9960 (89)  |
| 19.9889 | 18.7813 | 19.0526 | 19.3732 | 19.6965 | 19.8590 | 19.9011 | 19.9005 | 19.8063 | 19.4588 | 19.4462 | 18.4486 (90) |
| 19.1515 | 19.3284 | 19.6012 | 19.9147 | 20.2450 | 20.4284 | 20.4847 | 20.4284 | 20.3677 | 20.0007 | 19.4875 | 19.1952 (92) |

8. Space heating requirement

| Jan                                      | Feb      | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec            |              |
|--|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------------|--------------|
| 0.9946                                   | 0.9896   | 0.9774   | 0.9500   | 0.8688   | 0.7030   | 0.4776   | 0.4993   | 0.8011   | 0.9539   | 0.9904   | 0.9952 (94)    |              |
| 297.4634                                 | 294.8257 | 319.3286 | 337.0582 | 319.7523 | 295.9560 | 167.6058 | 166.9527 | 249.0512 | 271.0532 | 251.9826 | 243.9501 (95)  |              |
| 4.5000                                   | 5.0000   | 6.8000   | 8.7000   | 11.7000  | 14.6000  | 16.9000  | 16.9000  | 14.3000  | 10.8000  | 7.0000   | 4.9000 (96)    |              |
| 748.5454                                 | 721.6793 | 644.7602 | 550.0277 | 412.3463 | 279.1142 | 170.4143 | 170.3368 | 293.9553 | 451.2526 | 620.4470 | 720.0053 (97)  |              |
| 365.3650                                 | 286.8456 | 242.1211 | 153.3180 | 68.8899  | 0.0000   | 0.0000   | 0.0000   | 134.0684 | 265.9824 | 354.3674 | 1870.5777 (98) |              |
| Space heating requirement in kWh/m2/year |          |          |          |          |          |          |          |          |          |          | (98) / (4) =   | 48.1363 (99) |

9. Space cooling requirement

| Jan                                      | Feb    | Mar    | Apr    | May    | Jun      | Jul      | Aug      | Sep     | Oct    | Nov    | Dec                    |               |
|--|--------|--------|--------|--------|----------|----------|----------|---------|--------|--------|------------------------|---------------|
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 15.4000  | 17.8000  | 17.8000  | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 411.8424 | 294.7470 | 294.7470 | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.8910   | 0.9579   | 0.9523   | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 366.9567 | 282.3422 | 280.6931 | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 492.2066 | 472.5025 | 455.9274 | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 3.1497   | 0.1342   | 0.1571   | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 90.1799  | 141.4793 | 130.3743 | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000   | 0.2500   | 0.2500   | 0.0000  | 0.0000 | 0.0000 | 0.0000                 |               |
| 0.0000                                   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000   | 22.5450  | 35.3698  | 32.5936 | 0.0000 | 0.0000 | 0.0000                 |               |
| Space cooling requirement in kWh/m2/year |        |        |        |        |          |          |          |         |        |        | Total = Sum(107)6, 8 = | 90.5084 (107) |
|  |        |        |        |        |          |          |          |         |        |        | (107) / (4) =          | 2.2629 (108)  |

10. Fabric Energy Efficiency

Fabric Energy Efficiency rounded (99) + (108) = 50.5 (109)

# 8.2: Appendixes : Energy / Renewable Energy Statement

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF DATA FOR RENEWABLE HEAT INCENTIVE (RHI) Page: 5 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF DATA FOR RENEWABLE HEAT INCENTIVE (RHI)  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

1. Overall dwelling dimensions

| Area (m <sup>2</sup> )   | Storey height (m) | Volume (m <sup>3</sup> ) |
|--|-------------------|--------------------------|
| 38.8600 (1b)   | 2.7400 (2b)       | 106.4764 (1b) - (3b)     |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)...(1n) = 38.8600 (4) |                   |                          |
| Dwelling volume = (3a)+(3b)+(3c)+(3d)+(3e)...(3n) = 106.4764 (5)     |                   |                          |

2. Ventilation rate

| main heating | secondary heating | other | total | m <sup>3</sup> per hour |
|--------------|-------------------|-------|-------|-------------------------|
| 0            | 0                 | 0     | 0     | 0.0000 (6a)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6b)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6c)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6d)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6e)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6f)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6g)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6h)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6i)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6j)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6k)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6l)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6m)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6n)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6o)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6p)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6q)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6r)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6s)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6t)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6u)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6v)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6w)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6x)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6y)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6z)             |

3. Heat losses and heat loss parameter

| Element  | Gross m <sup>2</sup> | Openings m <sup>2</sup> | NetArea m <sup>2</sup> | U-value W/m <sup>2</sup> K | A x U  | K-value kJ/m <sup>2</sup> K | A x K         |
|--|----------------------|-------------------------|------------------------|----------------------------|--------|-----------------------------|---------------|
| Door   |                      |                         | 1.8900                 | 1.0000                     | 1.8900 | 1.0000                      | 1.8900 (20)   |
| Windows (Dw = 1.50)  |                      |                         | 4.9700                 | 1.4131                     | 7.0330 | 1.4131                      | 7.0330 (27)   |
| External Wall  | 25.0760              | 4.9700                  | 20.1060                | 0.2000                     | 4.0212 | 0.2000                      | 4.0212 (29a)  |
| Corridor Wall  | 28.0800              | 1.8900                  | 26.1900                | 0.2257                     | 5.9120 | 0.2257                      | 5.9120 (29a)  |
| Total net area of external elements Aum(A, m <sup>2</sup> )    |                      |                         | 53.1560                |                            |        |                             | 53.1560 (31)  |
| Fabric heat loss, W/K = Sum (A x U)                            |                      |                         |                        |                            |        |                             | 18.8562 (33)  |
| Party Wall   |                      |                         | 44.0200                | 0.0000                     | 0.0000 | 0.0000                      | 0.0000 (32)   |
| Floor  |                      |                         | 38.8600                | 0.0000                     | 0.0000 | 0.0000                      | 0.0000 (32a)  |
| Ceiling  |                      |                         | 38.8600                | 0.0000                     | 0.0000 | 0.0000                      | 0.0000 (32b)  |
| Thermal mass parameter (TMP = Cm / TFA) in kJ/m <sup>2</sup> K |                      |                         |                        |                            |        |                             | 250.0000 (35) |
| Thermal bridges (Default value 0.150 * total exposed area)     |                      |                         |                        |                            |        |                             | 7.9734 (36)   |
| Total fabric heat loss   |                      |                         |                        |                            |        |                             | 26.8296 (37)  |

4. Water heating energy requirements (kWh/year)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Average |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| 31  | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  | 31      |

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF DATA FOR RENEWABLE HEAT INCENTIVE (RHI) Page: 6 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF DATA FOR RENEWABLE HEAT INCENTIVE (RHI)  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

6. Solar gains

| Area m <sup>2</sup> | Solar flux W/m <sup>2</sup> | Specific data or Table 6a | Specific data or Table 6b | Specific data or Table 6c | Specific data or Table 6d | Specific data or Table 6e | Specific data or Table 6f | Specific data or Table 6g | Specific data or Table 6h | Specific data or Table 6i | Specific data or Table 6j | Specific data or Table 6k | Specific data or Table 6l | Specific data or Table 6m | Specific data or Table 6n | Specific data or Table 6o | Specific data or Table 6p | Specific data or Table 6q | Specific data or Table 6r | Specific data or Table 6s | Specific data or Table 6t | Specific data or Table 6u | Specific data or Table 6v | Specific data or Table 6w | Specific data or Table 6x | Specific data or Table 6y | Specific data or Table 6z |
|---------------------|-----------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 3.4200              | 39.7858                     | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    | 0.7600                    |

7. Mean internal temperature (heating season)

| Jan     | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov     | Dec     | Average |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| 19.3889 | 19.5312 | 19.8329 | 20.1190 | 20.3904 | 20.4763 | 20.4921 | 20.4921 | 20.4559 | 20.2385 | 19.7418 | 19.4111 | 19.5312 |

8. Space heating requirement

| Jan    | Feb    | Mar    | Apr    | May    | Jun    | Jul    | Aug    | Sep    | Oct    | Nov    | Dec    | Average |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|
| 0.9670 | 0.9541 | 0.9185 | 0.8610 | 0.7044 | 0.4885 | 0.2725 | 0.2793 | 0.5750 | 0.8326 | 0.9447 | 0.9686 | 0.9670  |

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF ENERGY RATINGS Page: 7 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF ENERGY RATINGS  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

1. Overall dwelling dimensions

| Area (m <sup>2</sup> )   | Storey height (m) | Volume (m <sup>3</sup> ) |
|--|-------------------|--------------------------|
| 38.8600 (1b)   | 2.7400 (2b)       | 106.4764 (1b) - (3b)     |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)...(1n) = 38.8600 (4) |                   |                          |
| Dwelling volume = (3a)+(3b)+(3c)+(3d)+(3e)...(3n) = 106.4764 (5)     |                   |                          |

2. Ventilation rate

| main heating | secondary heating | other | total | m <sup>3</sup> per hour |
|--------------|-------------------|-------|-------|-------------------------|
| 0            | 0                 | 0     | 0     | 0.0000 (6a)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6b)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6c)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6d)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6e)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6f)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6g)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6h)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6i)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6j)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6k)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6l)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6m)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6n)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6o)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6p)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6q)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6r)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6s)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6t)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6u)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6v)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6w)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6x)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6y)             |
| 0            | 0                 | 0     | 0     | 0.0000 (6z)             |

3. Heat losses and heat loss parameter

| Element  | Gross m <sup>2</sup> | Openings m <sup>2</sup> | NetArea m <sup>2</sup> | U-value W/m <sup>2</sup> K | A x U  | K-value kJ/m <sup>2</sup> K | A x K         |
|--|----------------------|-------------------------|------------------------|----------------------------|--------|-----------------------------|---------------|
| Door   |                      |                         | 1.8900                 | 1.0000                     | 1.8900 | 1.0000                      | 1.8900 (20)   |
| Windows (Dw = 1.50)  |                      |                         | 4.9700                 | 1.4131                     | 7.0330 | 1.4131                      | 7.0330 (27)   |
| External Wall  | 25.0760              | 4.9700                  | 20.1060                | 0.2000                     | 4.0212 | 0.2000                      | 4.0212 (29a)  |
| Corridor Wall  | 28.0800              | 1.8900                  | 26.1900                | 0.2257                     | 5.9120 | 0.2257                      | 5.9120 (29a)  |
| Total net area of external elements Aum(A, m <sup>2</sup> )    |                      |                         | 53.1560                |                            |        |                             | 53.1560 (31)  |
| Fabric heat loss, W/K = Sum (A x U)                            |                      |                         |                        |                            |        |                             | 18.8562 (33)  |
| Party Wall   |                      |                         | 44.0200                | 0.0000                     | 0.0000 | 0.0000                      | 0.0000 (32)   |
| Floor  |                      |                         | 38.8600                | 0.0000                     | 0.0000 | 0.0000                      | 0.0000 (32a)  |
| Ceiling  |                      |                         | 38.8600                | 0.0000                     | 0.0000 | 0.0000                      | 0.0000 (32b)  |
| Thermal mass parameter (TMP = Cm / TFA) in kJ/m <sup>2</sup> K |                      |                         |                        |                            |        |                             | 250.0000 (35) |
| Thermal bridges (Default value 0.150 * total exposed area)     |                      |                         |                        |                            |        |                             | 7.9734 (36)   |
| Total fabric heat loss   |                      |                         |                        |                            |        |                             | 26.8296 (37)  |

4. Water heating energy requirements (kWh/year)

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Average |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| 31  | 28  | 31  | 30  | 31  | 30  | 31  | 31  | 30  | 31  | 30  | 31  | 31      |





# 8.2: Appendixes : Energy / Renewable Energy Statement

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE

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| CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE   |   |                |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
|--|---|----------------|---------------|---------------|----------|--------------|----------------------|---------|---------|--|--|--|-------|------|------------|---------------|---------------|--------|-------|--|----|------|-------------|-------------|--------|---|--|--|--|----------|-------------|----------|--|-----------|--------|---------|--------|--------|--------|--------------|-----------|--------|---------|--------|--------|--------|-------------|-----|-------|-------|-------|-------|-------|-------|----------------------|-------|-------|---------|--------|--------|---------|---------|--------|---------|---------|---------|---------|-------|-------|-------|-------|-------|----------|--------|----------|----------|----------|-------|--------|--------|--------|-----------|--------|--------|--------|-------|--------|--------|--------|-----------|--------|--------|--------|--------|-----------------|-----------|----------|------------|-------------|-----------|--------|----------------|-----------|--------|----------------|----------|--------|---------------|----------|--------|----------------|--------------------|---|-----------------|---------------|
| <p>(73)m 245.3814 243.3113 234.6130 221.1439 207.9085 194.8778 186.5658 191.4402 198.4688 212.0911 227.5979 238.9245 (73)</p> <hr/> <p>6. Solar gains</p> <hr/> <table border="1"> <thead> <tr> <th>[Jan]</th> <th>Area</th> <th>Solar Flux</th> <th>Specific data</th> <th>Specific data</th> <th>Access</th> <th>Gains</th> </tr> <tr> <th></th> <th>m2</th> <th>W/m2</th> <th>or Table 6a</th> <th>or Table 6c</th> <th>factor</th> <th>W</th> </tr> <tr> <th></th> <th></th> <th></th> <th>Table 6b</th> <th>or Table 6c</th> <th>Table 6d</th> <th></th> </tr> </thead> <tbody> <tr> <td>Southeast</td> <td>1.4200</td> <td>37.3877</td> <td>0.7600</td> <td>0.7000</td> <td>0.7700</td> <td>47.1411 (77)</td> </tr> <tr> <td>Northwest</td> <td>1.5500</td> <td>11.5098</td> <td>0.7600</td> <td>0.7000</td> <td>0.7700</td> <td>6.5772 (81)</td> </tr> </tbody> </table> <hr/> <p>(83)m 53.7183 93.8221 129.6873 169.2292 194.1996 200.7729 195.3476 175.9184 146.4152 108.1544 64.8194 45.6337 (83)</p> <p>(84)m 299.0997 337.1334 364.3002 390.3730 402.1081 395.6507 381.9135 367.3585 344.8840 320.2455 292.4173 284.5581 (84)</p> <hr/> <p>7. Mean internal temperature (heating season)</p> <hr/> <p>Temperature during heating periods in the living area from Table 9, TH1 (C) 21.0000 (85)</p> <p>Utilisation factor for gains for living area, n1/m (see Table 9a)</p> <table border="1"> <thead> <tr> <th>tau</th> <th>alpha</th> <th>(86)m</th> <th>(87)m</th> <th>(88)m</th> <th>(89)m</th> <th>(90)m</th> <th>Living area fraction</th> <th>(92)m</th> <th>(93)m</th> </tr> </thead> <tbody> <tr> <td>52.8208</td> <td>4.5214</td> <td>0.9940</td> <td>19.7196</td> <td>19.8322</td> <td>0.9920</td> <td>18.1599</td> <td>18.9980</td> <td>18.9980</td> <td>18.9980</td> </tr> </tbody> </table> <hr/> <p>8. Space heating requirement</p> <table border="1"> <thead> <tr> <th>(94)m</th> <th>(95)m</th> <th>(96)m</th> <th>(97)m</th> <th>(98)m</th> </tr> </thead> <tbody> <tr> <td>296.1247</td> <td>4.5000</td> <td>740.7007</td> <td>330.7645</td> <td>330.7645</td> </tr> </tbody> </table> <hr/> <p>9a. Energy requirements - Individual heating systems, including micro-CHP</p> <p>Fraction of space heat from secondary/supplementary system (Table 11) 0.0000 (201)</p> <p>Fraction of space heat from main system(s) 1.0000 (202)</p> <p>Efficiency of main space heating system 1 (in %)</p> <p>Efficiency of secondary/supplementary heating system, %</p> <hr/> <p>9b. Space heating requirements (kWh/year)</p> <table border="1"> <thead> <tr> <th>(98)m</th> <th>(211)m</th> <th>(212)m</th> <th>(213)m</th> </tr> </thead> <tbody> <tr> <td>1833.3445</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> </tr> </tbody> </table> <hr/> <p>9c. Space cooling requirement</p> <p>Not applicable</p> <hr/> <p>9d. Energy requirements - Individual heating systems, including micro-CHP</p> <p>Fraction of space heat from secondary/supplementary system (Table 11) 0.0000 (201)</p> <p>Fraction of space heat from main system(s) 1.0000 (202)</p> <p>Efficiency of main space heating system 1 (in %)</p> <p>Efficiency of secondary/supplementary heating system, %</p> <hr/> <p>9e. Space heating requirements (kWh/year)</p> <table border="1"> <thead> <tr> <th>(98)m</th> <th>(211)m</th> <th>(212)m</th> <th>(213)m</th> </tr> </thead> <tbody> <tr> <td>1833.3445</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> </tr> </tbody> </table> <hr/> <p>9f. Energy requirements - Individual heating systems, including micro-CHP</p> <p>Electricity for pumps, fans and electric keep-hot (Table 4f):</p> <p>Electricity for lighting (calculated in Appendix L)</p> <hr/> <p>9g. Energy requirements - Individual heating systems, including micro-CHP</p> <table border="1"> <thead> <tr> <th>Energy</th> <th>Emission factor</th> <th>Emissions</th> </tr> <tr> <th>kWh/year</th> <th>kg CO2/kWh</th> <th>kg CO2/year</th> </tr> </thead> <tbody> <tr> <td>1833.3445</td> <td>0.1980</td> <td>363.0022 (261)</td> </tr> <tr> <td>1709.5669</td> <td>0.1980</td> <td>338.4942 (264)</td> </tr> <tr> <td>175.0000</td> <td>0.5170</td> <td>90.4750 (267)</td> </tr> <tr> <td>204.4860</td> <td>0.5170</td> <td>105.7192 (268)</td> </tr> </tbody> </table> <hr/> <p>9h. Energy requirements - Individual heating systems, including micro-CHP</p> <table border="1"> <thead> <tr> <th>Total CO2, kg/year</th> <th>Dwelling Carbon Dioxide Emission Rate (DER)</th> </tr> </thead> <tbody> <tr> <td>1113.8747 (269)</td> <td>20.1700 (273)</td> </tr> </tbody> </table> <hr/> <p>16 CO2 EMISSIONS ASSOCIATED WITH APPLIANCES AND COOKING AND SITE-WIDE ELECTRICITY GENERATION TECHNOLOGIES</p> |   |                |               |               |          |              |                      |         |         |  |  |  | [Jan] | Area | Solar Flux | Specific data | Specific data | Access | Gains |  | m2 | W/m2 | or Table 6a | or Table 6c | factor | W |  |  |  | Table 6b | or Table 6c | Table 6d |  | Southeast | 1.4200 | 37.3877 | 0.7600 | 0.7000 | 0.7700 | 47.1411 (77) | Northwest | 1.5500 | 11.5098 | 0.7600 | 0.7000 | 0.7700 | 6.5772 (81) | tau | alpha | (86)m | (87)m | (88)m | (89)m | (90)m | Living area fraction | (92)m | (93)m | 52.8208 | 4.5214 | 0.9940 | 19.7196 | 19.8322 | 0.9920 | 18.1599 | 18.9980 | 18.9980 | 18.9980 | (94)m | (95)m | (96)m | (97)m | (98)m | 296.1247 | 4.5000 | 740.7007 | 330.7645 | 330.7645 | (98)m | (211)m | (212)m | (213)m | 1833.3445 | 0.0000 | 0.0000 | 0.0000 | (98)m | (211)m | (212)m | (213)m | 1833.3445 | 0.0000 | 0.0000 | 0.0000 | Energy | Emission factor | Emissions | kWh/year | kg CO2/kWh | kg CO2/year | 1833.3445 | 0.1980 | 363.0022 (261) | 1709.5669 | 0.1980 | 338.4942 (264) | 175.0000 | 0.5170 | 90.4750 (267) | 204.4860 | 0.5170 | 105.7192 (268) | Total CO2, kg/year | Dwelling Carbon Dioxide Emission Rate (DER) | 1113.8747 (269) | 20.1700 (273) |
| [Jan]  | Area  | Solar Flux     | Specific data | Specific data | Access   | Gains        |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
|  | m2  | W/m2           | or Table 6a   | or Table 6c   | factor   | W            |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
|  |   |                | Table 6b      | or Table 6c   | Table 6d |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| Southeast  | 1.4200                                      | 37.3877        | 0.7600        | 0.7000        | 0.7700   | 47.1411 (77) |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| Northwest  | 1.5500                                      | 11.5098        | 0.7600        | 0.7000        | 0.7700   | 6.5772 (81)  |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| tau  | alpha                                       | (86)m          | (87)m         | (88)m         | (89)m    | (90)m        | Living area fraction | (92)m   | (93)m   |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 52.8208  | 4.5214                                      | 0.9940         | 19.7196       | 19.8322       | 0.9920   | 18.1599      | 18.9980              | 18.9980 | 18.9980 |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| (94)m  | (95)m                                       | (96)m          | (97)m         | (98)m         |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 296.1247   | 4.5000                                      | 740.7007       | 330.7645      | 330.7645      |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| (98)m  | (211)m                                      | (212)m         | (213)m        |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 1833.3445  | 0.0000                                      | 0.0000         | 0.0000        |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| (98)m  | (211)m                                      | (212)m         | (213)m        |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 1833.3445  | 0.0000                                      | 0.0000         | 0.0000        |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| Energy   | Emission factor                             | Emissions      |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| kWh/year   | kg CO2/kWh                                  | kg CO2/year    |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 1833.3445  | 0.1980                                      | 363.0022 (261) |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 1709.5669  | 0.1980                                      | 338.4942 (264) |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 175.0000   | 0.5170                                      | 90.4750 (267)  |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 204.4860   | 0.5170                                      | 105.7192 (268) |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| Total CO2, kg/year   | Dwelling Carbon Dioxide Emission Rate (DER) |                |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |
| 1113.8747 (269)  | 20.1700 (273)                               |                |               |               |          |              |                      |         |         |  |  |  |       |      |            |               |               |        |       |  |    |      |             |             |        |   |  |  |  |          |             |          |  |           |        |         |        |        |        |              |           |        |         |        |        |        |             |     |       |       |       |       |       |       |                      |       |       |         |        |        |         |         |        |         |         |         |         |       |       |       |       |       |          |        |          |          |          |       |        |        |        |           |        |        |        |       |        |        |        |           |        |        |        |        |                 |           |          |            |             |           |        |                |           |        |                |          |        |               |          |        |                |                    |   |                 |               |

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE

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| CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE   |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
|--|-------------------|-------------|------------|-----------------------|-----------|----------------|------------|----------|----------|----------|----------|----------|--------------|-------------------|-------|-------|-------------|---|---|---|---|----------------------|---|---|---|---|----------------------|---|---|---|---|-----------------------|---|---|---|---|----------------------|---|---|---|---|----------------------|------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|----------|-------------|------------|---------------|-----------|----------------|------------|-------|--|--|--------|--------|--------|--------|------|---------------------|--|--|--------|--------|---------|---------|------|---------------|---------|--------|---------|--------|---------|---------|------|---|--|--|---------|--|--|--|------|-------------------------------------|--|--|---------|--|---------|---------|------|------------|--|--|--------|--|--------|--------|------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|----|----|----|----|----|----|----|----|----|----|----|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|----------|----------|----------|---------|---------|---------|---------|---------|---------|---------|----------|-------------------------|--|--|--|--|--|--|--|--|--|--|--|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--|--|--|--|--|--|--|--|--|--|--|--|--|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-------|----------|----------|----------|----------|----------|---------|----------|----------|----------|----------|----------|----------|-------|-------|-------|-------|---------|---------|---------|-------|---------|---------|---------|-------|----------|----------|----------|
| <p>DER 20.1700 ZC1</p> <p>Total Floor Area 38.8600</p> <p>Assumed number of occupants 5</p> <p>CO2 emission factor in Table 12 for electricity displaced from grid 1.3764</p> <p>CO2 emissions from appliances, equation (L14) 18.4459 ZC2</p> <p>CO2 emissions from cooking, equation (L14) 3.9323 ZC3</p> <p>Total CO2 emissions 42.5282 ZC4</p> <p>Residual CO2 emissions offset from biofuel CHP 0.0000 ZC5</p> <p>Additional allowable electricity generation, kWh/m2/year 0.0000 ZC6</p> <p>Resulting CO2 emissions offset from additional allowable electricity generation 0.0000 ZC7</p> <p>Net CO2 emissions 42.5282 ZC8</p>  |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
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| <p>2. Ventilation rate</p> <table border="1"> <thead> <tr> <th>main heating</th> <th>secondary heating</th> <th>other</th> <th>total</th> <th>m3 per hour</th> </tr> </thead> <tbody> <tr> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0 + 40 = 0.0000 (8a)</td> </tr> <tr> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0 + 20 = 0.0000 (8b)</td> </tr> <tr> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>2 * 10 = 20.0000 (7a)</td> </tr> <tr> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0 * 10 = 0.0000 (7b)</td> </tr> <tr> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0 + 40 = 0.0000 (7c)</td> </tr> </tbody> </table> <hr/> <p>Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 20.0000 / (5) = 0.1878 (8)</p> <p>Pressure test</p> <p>Measured/design g/s 10.0000</p> <p>If based on air permeability value, then (18) = [(17)/20]+(9), otherwise (18) = (16) 2</p> <p>Number of sides on which dwelling is sheltered 2 (19)</p> <hr/> <p>Shelter factor (20) = 1 - [0.075 x (19)] = 0.8500 (20)</p> <p>Infiltration rate adjusted to include shelter factor (21) = (18) x (20) = 0.5847 (21)</p> <hr/> <table border="1"> <thead> <tr> <th>Wind speed</th> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> </thead> <tbody> <tr> <td>Wind factor</td> <td>1.3500</td> <td>1.2750</td> <td>1.2750</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> </tr> <tr> <td>(22b)m</td> <td>0.7893</td> <td>0.7454</td> <td>0.7454</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> </tr> <tr> <td>Effective a/ch</td> <td>0.8115</td> <td>0.7778</td> <td>0.7778</td> <td>0.7163</td> <td>0.6796</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> </tr> </tbody> </table> <hr/> <p>3. Heat losses and heat loss parameter</p> <table border="1"> <thead> <tr> <th>Element</th> <th>Gross m2</th> <th>Openings m2</th> <th>NetArea m2</th> <th>U-value W/m2K</th> <th>A x U W/K</th> <th>K-value kJ/m2K</th> <th>A x K kJ/K</th> </tr> </thead> <tbody> <tr> <td>Doors</td> <td></td> <td></td> <td>1.8500</td> <td>2.0000</td> <td>3.7000</td> <td>2.7000</td> <td>(25)</td> </tr> <tr> <td>Windows (Dw = 2.00)</td> <td></td> <td></td> <td>7.8600</td> <td>1.8519</td> <td>14.2648</td> <td>14.2648</td> <td>(26)</td> </tr> <tr> <td>External Wall</td> <td>53.1560</td> <td>9.7150</td> <td>43.4410</td> <td>0.3500</td> <td>15.2044</td> <td>15.2044</td> <td>(27)</td> </tr> <tr> <td>Total net area of external elements (Aem, m2)</td> <td></td> <td></td> <td>53.1560</td> <td></td> <td></td> <td></td> <td>(28)</td> </tr> <tr> <td>Fabric heat loss, W/K = Sum (A x U)</td> <td></td> <td></td> <td>44.0200</td> <td></td> <td>33.4692</td> <td>33.4692</td> <td>(29)</td> </tr> <tr> <td>Party Wall</td> <td></td> <td></td> <td>0.0000</td> <td></td> <td>0.0000</td> <td>0.0000</td> <td>(30)</td> </tr> </tbody> </table> <hr/> <p>Thermal mass parameter (TMP = Cm / TPA) in kJ/m2K 250.0000 (35)</p> <p>Thermal bridges (User defined value 0.110 * total exposed area) 5.8472 (36)</p> <p>Total fabric heat loss (33) + (36) = 39.3163 (37)</p> <hr/> <p>Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5)</p> <table border="1"> <thead> <tr> <th>(38)m</th> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> </thead> <tbody> <tr> <td>(38)m</td> <td>28.5135</td> <td>27.3312</td> <td>27.3312</td> <td>25.1692</td> <td>23.8781</td> <td>23.2775</td> <td>22.7070</td> <td>22.7070</td> <td>24.1896</td> <td>25.1692</td> <td>26.2164</td> <td>27.3312</td> </tr> <tr> <td>(39)m</td> <td>67.8298</td> <td>66.6475</td> <td>66.6475</td> <td>64.4855</td> <td>63.1944</td> <td>62.5938</td> <td>62.0233</td> <td>62.0233</td> <td>63.5059</td> <td>64.4855</td> <td>65.5327</td> <td>66.6475</td> </tr> <tr> <td>(40)m</td> <td>1.7455</td> <td>1.7151</td> <td>1.7151</td> <td>1.6594</td> <td>1.6262</td> <td>1.6108</td> <td>1.5961</td> <td>1.5961</td> <td>1.6342</td> <td>1.6594</td> <td>1.6864</td> <td>1.7151</td> </tr> <tr> <td>(41)m</td> <td>31</td> <td>28</td> <td>31</td> <td>30</td> <td>31</td> <td>30</td> <td>31</td> <td>31</td> <td>30</td> <td>31</td> <td>32</td> <td>31</td> </tr> </tbody> </table> <hr/> <p>4. Water heating energy requirements (kWh/year)</p> <p>Assumed occupancy, N 1.3764 (42)</p> <p>Annual average hot water usage in litres per day Vd,average = (23 x N) + 36 70.0944 (43)</p> <p>Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)</p> <table border="1"> <thead> <tr> <th>(44)m</th> <th>(45)m</th> <th>(46)m</th> <th>(47)m</th> <th>(48)m</th> <th>(49)m</th> <th>(50)m</th> <th>(51)m</th> <th>(52)m</th> <th>(53)m</th> <th>(54)m</th> <th>(55)m</th> </tr> </thead> <tbody> <tr> <td>(44)m</td> <td>77.4504</td> <td>74.6340</td> <td>71.8176</td> <td>69.0012</td> <td>66.1849</td> <td>63.3685</td> <td>60.5521</td> <td>57.7357</td> <td>54.9193</td> <td>52.1029</td> <td>49.2865</td> </tr> <tr> <td>(45)m</td> <td>115.1314</td> <td>100.6947</td> <td>103.9079</td> <td>90.5894</td> <td>86.9227</td> <td>75.0077</td> <td>69.5056</td> <td>79.7587</td> <td>80.7113</td> <td>94.0613</td> <td>102.6752</td> </tr> <tr> <td>Energy content (annual)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>(46)m</td> <td>17.2497</td> <td>15.1042</td> <td>15.5862</td> <td>13.5884</td> <td>13.0384</td> <td>11.2512</td> <td>10.4258</td> <td>11.9638</td> <td>12.1067</td> <td>14.1092</td> <td>15.4013</td> </tr> <tr> <td>Water storage loss:</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>b) If manufacturer declared cylinder loss factor is not known:</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Cylinder volume (litres) including any solar storage within same cylinder 150.0000 (50)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Hot water storage loss factor from Table 2a (kWh/litre/day) 0.0191 (51)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Volume factor from Table 2a 0.9283 (52)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Temperature factor from Table 2b 0.5400 (53)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>Enter (49) or (54) in (55) 1.4364 (55)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>(57)m</td> <td>44.5282</td> <td>40.2190</td> <td>44.5282</td> <td>43.0918</td> <td>44.5282</td> <td>43.0918</td> <td>44.5282</td> <td>44.5282</td> <td>43.0918</td> <td>44.5282</td> <td>43.0918</td> <td>44.5282</td> </tr> <tr> <td>Primary circuit loss (annual) from Table 3 610.0000 (58)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>(59)m</td> <td>51.8082</td> <td>46.7945</td> <td>51.8082</td> <td>50.1370</td> <td>51.8082</td> <td>50.1370</td> <td>51.8082</td> <td>51.8082</td> <td>50.1370</td> <td>51.8082</td> <td>50.1370</td> <td>51.8082</td> </tr> <tr> <td>(62)m</td> <td>211.4678</td> <td>187.7082</td> <td>200.2443</td> <td>183.8182</td> <td>183.2591</td> <td>168.2365</td> <td>165.8421</td> <td>176.0952</td> <td>173.9401</td> <td>190.3977</td> <td>195.9040</td> <td>207.8350</td> </tr> <tr> <td>(63)m</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> <td>0.0000</td> </tr> <tr> <td>Water heat. 211.4678</td> <td>187.7082</td> <td>200.2443</td> <td>183.8182</td> <td>183.2591</td> <td>168.2365</td> <td>165.8421</td> <td>176.0952</td> <td>173.9401</td> <td>190.3977</td> <td>195.9040</td> <td>207.8350</td> </tr> <tr> <td>(65)m</td> <td>115.3503</td> <td>103.0918</td> <td>111.6185</td> <td>104.7040</td> <td>105.9709</td> <td>99.5231</td> <td>100.1798</td> <td>103.5889</td> <td>101.4195</td> <td>108.3445</td> <td>108.7225</td> <td>114.1424</td> </tr> </tbody> </table> <hr/> <p>5. Internal gains (see Table 5) and 5a)</p> <p>Metabolic gains (Table 5), Watts</p> <table border="1"> <thead> <tr> <th>(66)m</th> <th>(67)m</th> <th>(68)m</th> </tr> </thead> <tbody> <tr> <td>(66)m</td> <td>68.8188</td> <td>68.8188</td> <td>68.8188</td> </tr> <tr> <td>(67)m</td> <td>18.0914</td> <td>16.0686</td> <td>13.0679</td> </tr> <tr> <td>(68)m</td> <td>118.6774</td> <td>119.9089</td> <td>116.8055</td> </tr> </tbody> </table> |                   |             |            |                       |           |                |            |          |          |          |          |          | main heating | secondary heating | other | total | m3 per hour | 0 | 0 | 0 | 0 | 0 + 40 = 0.0000 (8a) | 0 | 0 | 0 | 0 | 0 + 20 = 0.0000 (8b) | 0 | 0 | 0 | 0 | 2 * 10 = 20.0000 (7a) | 0 | 0 | 0 | 0 | 0 * 10 = 0.0000 (7b) | 0 | 0 | 0 | 0 | 0 + 40 = 0.0000 (7c) | Wind speed | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | Wind factor | 1.3500 | 1.2750 | 1.2750 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | (22b)m | 0.7893 | 0.7454 | 0.7454 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | Effective a/ch | 0.8115 | 0.7778 | 0.7778 | 0.7163 | 0.6796 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | Element | Gross m2 | Openings m2 | NetArea m2 | U-value W/m2K | A x U W/K | K-value kJ/m2K | A x K kJ/K | Doors |  |  | 1.8500 | 2.0000 | 3.7000 | 2.7000 | (25) | Windows (Dw = 2.00) |  |  | 7.8600 | 1.8519 | 14.2648 | 14.2648 | (26) | External Wall | 53.1560 | 9.7150 | 43.4410 | 0.3500 | 15.2044 | 15.2044 | (27) | Total net area of external elements (Aem, m2) |  |  | 53.1560 |  |  |  | (28) | Fabric heat loss, W/K = Sum (A x U) |  |  | 44.0200 |  | 33.4692 | 33.4692 | (29) | Party Wall |  |  | 0.0000 |  | 0.0000 | 0.0000 | (30) | (38)m | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | (38)m | 28.5135 | 27.3312 | 27.3312 | 25.1692 | 23.8781 | 23.2775 | 22.7070 | 22.7070 | 24.1896 | 25.1692 | 26.2164 | 27.3312 | (39)m | 67.8298 | 66.6475 | 66.6475 | 64.4855 | 63.1944 | 62.5938 | 62.0233 | 62.0233 | 63.5059 | 64.4855 | 65.5327 | 66.6475 | (40)m | 1.7455 | 1.7151 | 1.7151 | 1.6594 | 1.6262 | 1.6108 | 1.5961 | 1.5961 | 1.6342 | 1.6594 | 1.6864 | 1.7151 | (41)m | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 32 | 31 | (44)m | (45)m | (46)m | (47)m | (48)m | (49)m | (50)m | (51)m | (52)m | (53)m | (54)m | (55)m | (44)m | 77.4504 | 74.6340 | 71.8176 | 69.0012 | 66.1849 | 63.3685 | 60.5521 | 57.7357 | 54.9193 | 52.1029 | 49.2865 | (45)m | 115.1314 | 100.6947 | 103.9079 | 90.5894 | 86.9227 | 75.0077 | 69.5056 | 79.7587 | 80.7113 | 94.0613 | 102.6752 | Energy content (annual) |  |  |  |  |  |  |  |  |  |  |  | (46)m | 17.2497 | 15.1042 | 15.5862 | 13.5884 | 13.0384 | 11.2512 | 10.4258 | 11.9638 | 12.1067 | 14.1092 | 15.4013 | Water storage loss: |  |  |  |  |  |  |  |  |  |  |  | b) If manufacturer declared cylinder loss factor is not known: |  |  |  |  |  |  |  |  |  |  |  | Cylinder volume (litres) including any solar storage within same cylinder 150.0000 (50) |  |  |  |  |  |  |  |  |  |  |  | Hot water storage loss factor from Table 2a (kWh/litre/day) 0.0191 (51) |  |  |  |  |  |  |  |  |  |  |  | Volume factor from Table 2a 0.9283 (52) |  |  |  |  |  |  |  |  |  |  |  | Temperature factor from Table 2b 0.5400 (53) |  |  |  |  |  |  |  |  |  |  |  | Enter (49) or (54) in (55) 1.4364 (55) |  |  |  |  |  |  |  |  |  |  |  | (57)m | 44.5282 | 40.2190 | 44.5282 | 43.0918 | 44.5282 | 43.0918 | 44.5282 | 44.5282 | 43.0918 | 44.5282 | 43.0918 | 44.5282 | Primary circuit loss (annual) from Table 3 610.0000 (58) |  |  |  |  |  |  |  |  |  |  |  |  | (59)m | 51.8082 | 46.7945 | 51.8082 | 50.1370 | 51.8082 | 50.1370 | 51.8082 | 51.8082 | 50.1370 | 51.8082 | 50.1370 | 51.8082 | (62)m | 211.4678 | 187.7082 | 200.2443 | 183.8182 | 183.2591 | 168.2365 | 165.8421 | 176.0952 | 173.9401 | 190.3977 | 195.9040 | 207.8350 | (63)m | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | Water heat. 211.4678 | 187.7082 | 200.2443 | 183.8182 | 183.2591 | 168.2365 | 165.8421 | 176.0952 | 173.9401 | 190.3977 | 195.9040 | 207.8350 | (65)m | 115.3503 | 103.0918 | 111.6185 | 104.7040 | 105.9709 | 99.5231 | 100.1798 | 103.5889 | 101.4195 | 108.3445 | 108.7225 | 114.1424 | (66)m | (67)m | (68)m | (66)m | 68.8188 | 68.8188 | 68.8188 | (67)m | 18.0914 | 16.0686 | 13.0679 | (68)m | 118.6774 | 119.9089 | 116.8055 |
| main heating   | secondary heating | other       | total      | m3 per hour           |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| 0  | 0                 | 0           | 0          | 0 + 40 = 0.0000 (8a)  |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| 0  | 0                 | 0           | 0          | 0 + 20 = 0.0000 (8b)  |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| 0  | 0                 | 0           | 0          | 2 * 10 = 20.0000 (7a) |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| 0  | 0                 | 0           | 0          | 0 * 10 = 0.0000 (7b)  |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| 0  | 0                 | 0           | 0          | 0 + 40 = 0.0000 (7c)  |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Wind speed   | Jan               | Feb         | Mar        | Apr                   | May       | Jun            | Jul        | Aug      | Sep      | Oct      | Nov      | Dec      |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Wind factor  | 1.3500            | 1.2750      | 1.2750     | 1.2250                | 1.2250    | 1.2250         | 1.2250     | 1.2250   | 1.2250   | 1.2250   | 1.2250   | 1.2250   |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (22b)m   | 0.7893            | 0.7454      | 0.7454     | 0.6577                | 0.6577    | 0.6577         | 0.6577     | 0.6577   | 0.6577   | 0.6577   | 0.6577   | 0.6577   |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Effective a/ch   | 0.8115            | 0.7778      | 0.7778     | 0.7163                | 0.6796    | 0.6625         | 0.6625     | 0.6625   | 0.6625   | 0.6625   | 0.6625   | 0.6625   |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Element  | Gross m2          | Openings m2 | NetArea m2 | U-value W/m2K         | A x U W/K | K-value kJ/m2K | A x K kJ/K |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Doors  |                   |             | 1.8500     | 2.0000                | 3.7000    | 2.7000         | (25)       |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Windows (Dw = 2.00)  |                   |             | 7.8600     | 1.8519                | 14.2648   | 14.2648        | (26)       |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| External Wall  | 53.1560           | 9.7150      | 43.4410    | 0.3500                | 15.2044   | 15.2044        | (27)       |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Total net area of external elements (Aem, m2)  |                   |             | 53.1560    |                       |           |                | (28)       |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Fabric heat loss, W/K = Sum (A x U)  |                   |             | 44.0200    |                       | 33.4692   | 33.4692        | (29)       |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Party Wall   |                   |             | 0.0000     |                       | 0.0000    | 0.0000         | (30)       |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (38)m  | Jan               | Feb         | Mar        | Apr                   | May       | Jun            | Jul        | Aug      | Sep      | Oct      | Nov      | Dec      |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (38)m  | 28.5135           | 27.3312     | 27.3312    | 25.1692               | 23.8781   | 23.2775        | 22.7070    | 22.7070  | 24.1896  | 25.1692  | 26.2164  | 27.3312  |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (39)m  | 67.8298           | 66.6475     | 66.6475    | 64.4855               | 63.1944   | 62.5938        | 62.0233    | 62.0233  | 63.5059  | 64.4855  | 65.5327  | 66.6475  |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (40)m  | 1.7455            | 1.7151      | 1.7151     | 1.6594                | 1.6262    | 1.6108         | 1.5961     | 1.5961   | 1.6342   | 1.6594   | 1.6864   | 1.7151   |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (41)m  | 31                | 28          | 31         | 30                    | 31        | 30             | 31         | 31       | 30       | 31       | 32       | 31       |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (44)m  | (45)m             | (46)m       | (47)m      | (48)m                 | (49)m     | (50)m          | (51)m      | (52)m    | (53)m    | (54)m    | (55)m    |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (44)m  | 77.4504           | 74.6340     | 71.8176    | 69.0012               | 66.1849   | 63.3685        | 60.5521    | 57.7357  | 54.9193  | 52.1029  | 49.2865  |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (45)m  | 115.1314          | 100.6947    | 103.9079   | 90.5894               | 86.9227   | 75.0077        | 69.5056    | 79.7587  | 80.7113  | 94.0613  | 102.6752 |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Energy content (annual)  |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (46)m  | 17.2497           | 15.1042     | 15.5862    | 13.5884               | 13.0384   | 11.2512        | 10.4258    | 11.9638  | 12.1067  | 14.1092  | 15.4013  |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Water storage loss:  |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| b) If manufacturer declared cylinder loss factor is not known:   |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Cylinder volume (litres) including any solar storage within same cylinder 150.0000 (50)  |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Hot water storage loss factor from Table 2a (kWh/litre/day) 0.0191 (51)  |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Volume factor from Table 2a 0.9283 (52)  |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Temperature factor from Table 2b 0.5400 (53)   |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Enter (49) or (54) in (55) 1.4364 (55)   |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (57)m  | 44.5282           | 40.2190     | 44.5282    | 43.0918               | 44.5282   | 43.0918        | 44.5282    | 44.5282  | 43.0918  | 44.5282  | 43.0918  | 44.5282  |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Primary circuit loss (annual) from Table 3 610.0000 (58)   |                   |             |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (59)m  | 51.8082           | 46.7945     | 51.8082    | 50.1370               | 51.8082   | 50.1370        | 51.8082    | 51.8082  | 50.1370  | 51.8082  | 50.1370  | 51.8082  |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (62)m  | 211.4678          | 187.7082    | 200.2443   | 183.8182              | 183.2591  | 168.2365       | 165.8421   | 176.0952 | 173.9401 | 190.3977 | 195.9040 | 207.8350 |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (63)m  | 0.0000            | 0.0000      | 0.0000     | 0.0000                | 0.0000    | 0.0000         | 0.0000     | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| Water heat. 211.4678   | 187.7082          | 200.2443    | 183.8182   | 183.2591              | 168.2365  | 165.8421       | 176.0952   | 173.9401 | 190.3977 | 195.9040 | 207.8350 |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (65)m  | 115.3503          | 103.0918    | 111.6185   | 104.7040              | 105.9709  | 99.5231        | 100.1798   | 103.5889 | 101.4195 | 108.3445 | 108.7225 | 114.1424 |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (66)m  | (67)m             | (68)m       |            |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (66)m  | 68.8188           | 68.8188     | 68.8188    |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (67)m  | 18.0914           | 16.0686     | 13.0679    |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |
| (68)m  | 118.6774          | 119.9089    | 116.8055   |                       |           |                |            |          |          |          |          |          |              |                   |       |       |             |   |   |   |   |                      |   |   |   |   |                      |   |   |   |   |                       |   |   |   |   |                      |   |   |   |   |                      |            |     |     |     |     |     |     |     |     |     |     |     |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |                     |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |  |  |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |          |          |          |          |          |          |          |          |          |       |        |        |        |        |        |        |        |        |        |        |        |        |                      |          |          |          |          |          |          |          |          |          |          |          |       |          |          |          |          |          |         |          |          |          |          |          |          |       |       |       |       |         |         |         |       |         |         |         |       |          |          |          |

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF TARGET EMISSIONS

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| CALCULATION OF TARGET EMISSIONS  |           |                   |   |               |           |                |            |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
|--|-----------|-------------------|---|---------------|-----------|----------------|------------|---------|---------|---------|----------|---------|--------------|-----------|-------------------|-------------|---|---------|-------------|----------------------|-----------------|-----|-----|---|-----|-------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|----------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|----------|-------------|------------|---------------|-----------|----------------|------------|-------|--|--|--------|--------|--------|--------|------|---------------------|--|--|--------|--------|---------|---------|------|---------------|---------|--------|---------|--------|---------|---------|------|---|--|--|---------|--|--|--|------|-------------------------------------|--|--|---------|--|---------|---------|------|------------|--|--|--------|--|--------|--------|------|-------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|----|----|----|----|----|----|----|----|----|----|----|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|----------|----------|----------|---------|---------|---------|---------|---------|---------|---------|----------|-------------------------|--|--|--|--|--|--|--|--|--|--|--|-------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|
| <p>SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90</p> <p>CALCULATION OF TARGET EMISSIONS</p> <p>Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07:18</p>  |           |                   |   |               |           |                |            |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| <p>1. Overall dwelling dimensions</p> <table border="1"> <thead> <tr> <th>Ground floor</th> <th>Area (m2)</th> <th>Storey height (m)</th> <th>Volume (m3)</th> </tr> </thead> <tbody> <tr> <td>Total floor area TFA = (1a)+(1b)+(1c)+(1d)+...+(1n)</td> <td>38.8600</td> <td>2.7400 (2b)</td> <td>106.4764 (1b) - (3b)</td> </tr> <tr> <td>Dwelling volume</td> <td></td> <td></td> <td>(3a)+(3b)+(3c)+(3d)+...+(3n) = 106.4764 (5)</td> </tr> </tbody> </table>   |           |                   |   |               |           |                |            |         |         |         |          |         | Ground floor | Area (m2) | Storey height (m) | Volume (m3) | Total floor area TFA = (1a)+(1b)+(1c)+(1d)+...+(1n) | 38.8600 | 2.7400 (2b) | 106.4764 (1b) - (3b) | Dwelling volume |     |     | (3a)+(3b)+(3c)+(3d)+...+(3n) = 106.4764 (5) |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Ground floor   | Area (m2) | Storey height (m) | Volume (m3)                                 |               |           |                |            |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+...+(1n)  | 38.8600   | 2.7400 (2b)       | 106.4764 (1b) - (3b)                        |               |           |                |            |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Dwelling volume  |           |                   | (3a)+(3b)+(3c)+(3d)+...+(3n) = 106.4764 (5) |               |           |                |            |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| <p>2. Ventilation rate</p> <p>Infiltration rate adjusted to include shelter factor (21) = (18) x (20) = 0.5847 (21)</p> <hr/> <table border="1"> <thead> <tr> <th>Wind speed</th> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> </thead> <tbody> <tr> <td>Wind factor</td> <td>1.3500</td> <td>1.2750</td> <td>1.2750</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> <td>1.2250</td> </tr> <tr> <td>(22b)m</td> <td>0.7893</td> <td>0.7454</td> <td>0.7454</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> <td>0.6577</td> </tr> <tr> <td>Effective a/ch</td> <td>0.8115</td> <td>0.7778</td> <td>0.7778</td> <td>0.7163</td> <td>0.6796</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> <td>0.6625</td> </tr> </tbody> </table> <hr/> <p>3. Heat losses and heat loss parameter</p> <table border="1"> <thead> <tr> <th>Element</th> <th>Gross m2</th> <th>Openings m2</th> <th>NetArea m2</th> <th>U-value W/m2K</th> <th>A x U W/K</th> <th>K-value kJ/m2K</th> <th>A x K kJ/K</th> </tr> </thead> <tbody> <tr> <td>Doors</td> <td></td> <td></td> <td>1.8500</td> <td>2.0000</td> <td>3.7000</td> <td>2.7000</td> <td>(25)</td> </tr> <tr> <td>Windows (Dw = 2.00)</td> <td></td> <td></td> <td>7.8600</td> <td>1.8519</td> <td>14.2648</td> <td>14.2648</td> <td>(26)</td> </tr> <tr> <td>External Wall</td> <td>53.1560</td> <td>9.7150</td> <td>43.4410</td> <td>0.3500</td> <td>15.2044</td> <td>15.2044</td> <td>(27)</td> </tr> <tr> <td>Total net area of external elements (Aem, m2)</td> <td></td> <td></td> <td>53.1560</td> <td></td> <td></td> <td></td> <td>(28)</td> </tr> <tr> <td>Fabric heat loss, W/K = Sum (A x U)</td> <td></td> <td></td> <td>44.0200</td> <td></td> <td>33.4692</td> <td>33.4692</td> <td>(29)</td> </tr> <tr> <td>Party Wall</td> <td></td> <td></td> <td>0.0000</td> <td></td> <td>0.0000</td> <td>0.0000</td> <td>(30)</td> </tr> </tbody> </table> <hr/> <p>Thermal mass parameter (TMP = Cm / TPA) in kJ/m2K 250.0000 (35)</p> <p>Thermal bridges (User defined value 0.110 * total exposed area) 5.8472 (36)</p> <p>Total fabric heat loss (33) + (36) = 39.3163 (37)</p> <hr/> <p>Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5)</p> <table border="1"> <thead> <tr> <th>(38)m</th> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> </thead> <tbody> <tr> <td>(38)m</td> <td>28.5135</td> <td>27.3312</td> <td>27.3312</td> <td>25.1692</td> <td>23.8781</td> <td>23.2775</td> <td>22.7070</td> <td>22.7070</td> <td>24.1896</td> <td>25.1692</td> <td>26.2164</td> <td>27.3312</td> </tr> <tr> <td>(39)m</td> <td>67.8298</td> <td>66.6475</td> <td>66.6475</td> <td>64.4855</td> <td>63.1944</td> <td>62.5938</td> <td>62.0233</td> <td>62.0233</td> <td>63.5059</td> <td>64.4855</td> <td>65.5327</td> <td>66.6475</td> </tr> <tr> <td>(40)m</td> <td>1.7455</td> <td>1.7151</td> <td>1.7151</td> <td>1.6594</td> <td>1.6262</td> <td>1.6108</td> <td>1.5961</td> <td>1.5961</td> <td>1.6342</td> <td>1.6594</td> <td>1.6864</td> <td>1.7151</td> </tr> <tr> <td>(41)m</td> <td>31</td> <td>28</td> <td>31</td> <td>30</td> <td>31</td> <td>30</td> <td>31</td> <td>31</td> <td>30</td> <td>31</td> <td>32</td> <td>31</td> </tr> </tbody> </table> <hr/> <p>4. Water heating energy requirements (kWh/year)</p> <p>Assumed occupancy, N 1.3764 (42)</p> <p>Annual average hot water usage in litres per day Vd,average = (23 x N) + 36 70.0944 (43)</p> <p>Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)</p> <table border="1"> <thead> <tr> <th>(44)m</th> <th>(45)m</th> <th>(46)m</th> <th>(47)m</th> <th>(48)m</th> <th>(49)m</th> <th>(50)m</th> <th>(51)m</th> <th>(52)m</th> <th>(53)m</th> <th>(54)m</th> <th>(55)m</th> </tr> </thead> <tbody> <tr> <td>(44)m</td> <td>77.4504</td> <td>74.6340</td> <td>71.8176</td> <td>69.0012</td> <td>66.1849</td> <td>63.3685</td> <td>60.5521</td> <td>57.7357</td> <td>54.9193</td> <td>52.1029</td> <td>49.2865</td> </tr> <tr> <td>(45)m</td> <td>115.1314</td> <td>100.6947</td> <td>103.9079</td> <td>90.5894</td> <td>86.9227</td> <td>75.0077</td> <td>69.5056</td> <td>79.7587</td> <td>80.7113</td> <td>94.0613</td> <td>102.6752</td> </tr> <tr> <td>Energy content (annual)</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> </tr> <tr> <td>(46)m</td> <td>17.2497</td> <td>15.1042</td> <td>15.5862</td> <td>13.5884</td> <td>13.0384</td> <td>11.2512</td> <td>10.4258</td> <td>11.9638</td> <td>12.1067</td> <td>14.1092</td> <td>15.4013</td></tr></tbody></table> |           |                   |   |               |           |                |            |         |         |         |          |         | Wind speed   | Jan       | Feb               | Mar         | Apr   | May     | Jun         | Jul                  | Aug             | Sep | Oct | Nov   | Dec | Wind factor | 1.3500 | 1.2750 | 1.2750 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | 1.2250 | (22b)m | 0.7893 | 0.7454 | 0.7454 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | 0.6577 | Effective a/ch | 0.8115 | 0.7778 | 0.7778 | 0.7163 | 0.6796 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | 0.6625 | Element | Gross m2 | Openings m2 | NetArea m2 | U-value W/m2K | A x U W/K | K-value kJ/m2K | A x K kJ/K | Doors |  |  | 1.8500 | 2.0000 | 3.7000 | 2.7000 | (25) | Windows (Dw = 2.00) |  |  | 7.8600 | 1.8519 | 14.2648 | 14.2648 | (26) | External Wall | 53.1560 | 9.7150 | 43.4410 | 0.3500 | 15.2044 | 15.2044 | (27) | Total net area of external elements (Aem, m2) |  |  | 53.1560 |  |  |  | (28) | Fabric heat loss, W/K = Sum (A x U) |  |  | 44.0200 |  | 33.4692 | 33.4692 | (29) | Party Wall |  |  | 0.0000 |  | 0.0000 | 0.0000 | (30) | (38)m | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | (38)m | 28.5135 | 27.3312 | 27.3312 | 25.1692 | 23.8781 | 23.2775 | 22.7070 | 22.7070 | 24.1896 | 25.1692 | 26.2164 | 27.3312 | (39)m | 67.8298 | 66.6475 | 66.6475 | 64.4855 | 63.1944 | 62.5938 | 62.0233 | 62.0233 | 63.5059 | 64.4855 | 65.5327 | 66.6475 | (40)m | 1.7455 | 1.7151 | 1.7151 | 1.6594 | 1.6262 | 1.6108 | 1.5961 | 1.5961 | 1.6342 | 1.6594 | 1.6864 | 1.7151 | (41)m | 31 | 28 | 31 | 30 | 31 | 30 | 31 | 31 | 30 | 31 | 32 | 31 | (44)m | (45)m | (46)m | (47)m | (48)m | (49)m | (50)m | (51)m | (52)m | (53)m | (54)m | (55)m | (44)m | 77.4504 | 74.6340 | 71.8176 | 69.0012 | 66.1849 | 63.3685 | 60.5521 | 57.7357 | 54.9193 | 52.1029 | 49.2865 | (45)m | 115.1314 | 100.6947 | 103.9079 | 90.5894 | 86.9227 | 75.0077 | 69.5056 | 79.7587 | 80.7113 | 94.0613 | 102.6752 | Energy content (annual) |  |  |  |  |  |  |  |  |  |  |  | (46)m | 17.2497 | 15.1042 | 15.5862 | 13.5884 | 13.0384 | 11.2512 | 10.4258 | 11.9638 | 12.1067 | 14.1092 | 15.4013 |
| Wind speed   | Jan       | Feb               | Mar   | Apr           | May       | Jun            | Jul        | Aug     | Sep     | Oct     | Nov      | Dec     |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Wind factor  | 1.3500    | 1.2750            | 1.2750                                      | 1.2250        | 1.2250    | 1.2250         | 1.2250     | 1.2250  | 1.2250  | 1.2250  | 1.2250   | 1.2250  |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (22b)m   | 0.7893    | 0.7454            | 0.7454                                      | 0.6577        | 0.6577    | 0.6577         | 0.6577     | 0.6577  | 0.6577  | 0.6577  | 0.6577   | 0.6577  |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Effective a/ch   | 0.8115    | 0.7778            | 0.7778                                      | 0.7163        | 0.6796    | 0.6625         | 0.6625     | 0.6625  | 0.6625  | 0.6625  | 0.6625   | 0.6625  |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Element  | Gross m2  | Openings m2       | NetArea m2                                  | U-value W/m2K | A x U W/K | K-value kJ/m2K | A x K kJ/K |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Doors  |           |                   | 1.8500                                      | 2.0000        | 3.7000    | 2.7000         | (25)       |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Windows (Dw = 2.00)  |           |                   | 7.8600                                      | 1.8519        | 14.2648   | 14.2648        | (26)       |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| External Wall  | 53.1560   | 9.7150            | 43.4410                                     | 0.3500        | 15.2044   | 15.2044        | (27)       |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Total net area of external elements (Aem, m2)  |           |                   | 53.1560                                     |               |           |                | (28)       |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Fabric heat loss, W/K = Sum (A x U)  |           |                   | 44.0200                                     |               | 33.4692   | 33.4692        | (29)       |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Party Wall   |           |                   | 0.0000                                      |               | 0.0000    | 0.0000         | (30)       |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (38)m  | Jan       | Feb               | Mar   | Apr           | May       | Jun            | Jul        | Aug     | Sep     | Oct     | Nov      | Dec     |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (38)m  | 28.5135   | 27.3312           | 27.3312                                     | 25.1692       | 23.8781   | 23.2775        | 22.7070    | 22.7070 | 24.1896 | 25.1692 | 26.2164  | 27.3312 |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (39)m  | 67.8298   | 66.6475           | 66.6475                                     | 64.4855       | 63.1944   | 62.5938        | 62.0233    | 62.0233 | 63.5059 | 64.4855 | 65.5327  | 66.6475 |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (40)m  | 1.7455    | 1.7151            | 1.7151                                      | 1.6594        | 1.6262    | 1.6108         | 1.5961     | 1.5961  | 1.6342  | 1.6594  | 1.6864   | 1.7151  |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (41)m  | 31        | 28                | 31  | 30            | 31        | 30             | 31         | 31      | 30      | 31      | 32       | 31      |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (44)m  | (45)m     | (46)m             | (47)m                                       | (48)m         | (49)m     | (50)m          | (51)m      | (52)m   | (53)m   | (54)m   | (55)m    |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (44)m  | 77.4504   | 74.6340           | 71.8176                                     | 69.0012       | 66.1849   | 63.3685        | 60.5521    | 57.7357 | 54.9193 | 52.1029 | 49.2865  |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (45)m  | 115.1314  | 100.6947          | 103.9079                                    | 90.5894       | 86.9227   | 75.0077        | 69.5056    | 79.7587 | 80.7113 | 94.0613 | 102.6752 |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| Energy content (annual)  |           |                   |   |               |           |                |            |         |         |         |          |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |
| (46)m  | 17.2497   | 15.1042           | 15.5862                                     | 13.5884       | 13.0384   | 11.2512        | 10.4258    | 11.9638 | 12.1067 | 14.1092 | 15.4013  |         |              |           |                   |             |   |         |             |                      |                 |     |     |   |     |             |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |                |        |        |        |        |        |        |        |        |        |        |        |        |         |          |             |            |               |           |                |            |       |  |  |        |        |        |        |      |                     |  |  |        |        |         |         |      |               |         |        |         |        |         |         |      |   |  |  |         |  |  |  |      |                                     |  |  |         |  |         |         |      |            |  |  |        |  |        |        |      |       |     |     |     |     |     |     |     |     |     |     |     |     |       |         |         |         |         |         |         |         |         |         |         |         |         |       |         |         |         |         |         |         |         |         |         |         |         |         |       |        |        |        |        |        |        |        |        |        |        |        |        |       |    |    |    |    |    |    |    |    |    |    |    |    |       |       |       |       |       |       |       |       |       |       |       |       |       |         |         |         |         |         |         |         |         |         |         |         |       |          |          |          |         |         |         |         |         |         |         |          |                         |  |  |  |  |  |  |  |  |  |  |  |       |         |         |         |         |         |         |         |         |         |         |         |

# 8.2: Appendixes : Energy / Renewable Energy Statement

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF TARGET EMISSIONS

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|       |          |          |          |          |          |          |          |          |          |          |          |          |          |      |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|------|
| (69)m | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | (69) |
| (70)m | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | (70) |
| (71)m | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | (71) |
| (72)m | 155.0408 | 153.4104 | 150.0249 | 145.4222 | 142.4340 | 138.2265 | 134.6502 | 139.2324 | 140.8605 | 145.6243 | 151.0035 | 153.4172 | 153.4172 | (72) |
| (73)m | 345.4551 | 343.0335 | 333.5439 | 319.1600 | 305.3342 | 292.1366 | 283.8268 | 289.2002 | 296.9324 | 311.4775 | 327.6943 | 339.0981 | 339.0981 | (73) |

| 6. Solar gains | Solar gains |            |               |               |          |          |          |          |          |          |          |          | Gains |         |      |
|----------------|-------------|------------|---------------|---------------|----------|----------|----------|----------|----------|----------|----------|----------|-------|---------|------|
| Jan            | Area        | Solar flux | g             | FF            | Access   |          |          |          |          |          |          |          | W     |         |      |
|                | m2          | Table 6a   | Specific data | Specific data | factor   |          |          |          |          |          |          |          |       |         |      |
|                |             | W/m2       | or Table 6b   | or Table 6c   | Table 6d |          |          |          |          |          |          |          |       |         |      |
| East           | 7.8650      | 19.8726    |               | 0.7200        | 0.7000   |          |          |          |          |          |          |          |       | 54.5904 | (76) |
| (83)m          | 54.5904     | 105.8117   | 169.1212      | 251.1049      | 305.5232 | 318.7979 | 309.4294 | 269.3032 | 202.1913 | 128.8588 | 67.8701  | 45.0317  | (83)  |         |      |
| (84)m          | 400.0456    | 448.8453   | 502.6651      | 570.2649      | 610.8573 | 610.9345 | 593.2562 | 558.5035 | 499.1237 | 440.3363 | 395.5644 | 384.1298 | (84)  |         |      |

| 7. Mean internal temperature (heating season) | Mean internal temperature (heating season) |         |         |         |         |                           |         |         |         |         |         |         |      |
|---|--|---------|---------|---------|---------|---------------------------|---------|---------|---------|---------|---------|---------|------|
| Jan   | Feb  | Mar     | Apr     | May     | Jun     | Jul                       | Aug     | Sep     | Oct     | Nov     | Dec     | 21.0000 |      |
| tau   | 39.7850                                    | 40.4908 | 40.4908 | 41.8483 | 42.7033 | 43.1130                   | 43.5096 | 42.4939 | 41.8483 | 41.1796 | 40.4908 |         |      |
| alpha   | 3.4523                                     | 3.6994  | 3.6994  | 3.7899  | 3.8469  | 3.8742                    | 3.9006  | 3.9006  | 3.7899  | 3.7453  | 3.6994  |         |      |
| (86)m   | 0.9849                                     | 0.9760  | 0.9524  | 0.8986  | 0.7781  | 0.6053                    | 0.4435  | 0.7256  | 0.9154  | 0.9752  | 0.9855  | (86)    |      |
| (87)m   | 19.4189                                    | 19.6233 | 19.9753 | 20.3792 | 20.7500 | 20.9313                   | 20.9879 | 20.9853 | 20.8594 | 20.4368 | 19.8293 | 19.4783 | (87) |
| (88)m   | 19.5135                                    | 19.5350 | 19.5986 | 19.5746 | 19.5986 | 19.6205                   | 19.5928 | 19.5746 | 19.5553 | 19.5350 | 19.5350 | (88)    |      |
| (89)m   | 0.9797                                     | 0.9680  | 0.9358  | 0.8643  | 0.7071  | 0.4937                    | 0.2829  | 0.3001  | 0.6167  | 0.8774  | 0.9655  | 0.9805  | (89) |
| (90)m   | 18.1477                                    | 18.3843 | 18.7059 | 19.1138 | 19.4494 | 19.5831                   | 19.6185 | 19.6180 | 19.5299 | 19.1776 | 18.5847 | 18.2239 | (90) |
| Living area fraction                          |  |         |         |         |         | fLA = Living area / (4) = |         |         |         |         |         | 0.5373  | (91) |
| (92)m   | 18.8307                                    | 19.0408 | 19.3880 | 19.7937 | 20.1481 | 20.3075                   | 20.3543 | 20.3527 | 20.2442 | 19.8542 | 19.2535 | 18.8974 | (92) |
| (93)m   | 18.8307                                    | 19.0408 | 19.3880 | 19.7937 | 20.1481 | 20.3075                   | 20.3543 | 20.3527 | 20.2442 | 19.8542 | 19.2535 | 18.8974 | (93) |

| 8. Space heating requirement              | Space heating requirement |          |          |          |          |          |          |          |          |          |          |           |      |
|---|---------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|------|
| Jan                                       | Feb                       | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec      |           |      |
| (94)m                                     | 0.9766                    | 0.9645   | 0.9338   | 0.8703   | 0.7372   | 0.5520   | 0.3568   | 0.3798   | 0.6710   | 0.8861   | 0.9629   | 0.9776    | (94) |
| (95)m                                     | 390.7002                  | 432.9241 | 469.3778 | 496.3100 | 450.2940 | 337.2308 | 211.6515 | 210.9777 | 334.9187 | 390.1993 | 380.9010 | 375.5155  | (95) |
| (96)m                                     | 4.5000                    | 0.0000   | 6.8000   | 8.7000   | 11.7000  | 14.6000  | 16.9000  | 14.6000  | 9.0000   | 4.6000   | 1.6000   | 0.0000    | (96) |
| (97)m                                     | 972.0490                  | 935.7813 | 836.9555 | 715.3832 | 533.8709 | 357.2323 | 214.2452 | 214.1456 | 377.4944 | 493.8645 | 603.0032 | 632.8844  | (97) |
| (98)m                                     | 432.5235                  | 337.9200 | 274.9658 | 157.7327 | 62.1812  | 0.0000   | 0.0000   | 0.0000   | 144.0869 | 303.9136 | 414.6899 | 414.6899  | (98) |
| Space heating (October to May) (kWh/year) |                           |          |          |          |          |          |          |          |          |          |          | 2128.0136 | (99) |
| Space heating requirement in kWh/year     |                           |          |          |          |          |          |          |          |          |          |          | 54.7650   | (99) |

| 8c. Space cooling requirement | Space cooling requirement |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------------|---------------------------|--|--|--|--|--|--|--|--|--|--|--|
| Not applicable                |                           |  |  |  |  |  |  |  |  |  |  |  |

| 9a. Energy requirements - Individual heating systems, including micro-CHP | Energy requirements |          |          |          |          |          |          |          |          |          |          |           |          |       |
|---|---------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|----------|-------|
| Jan   | Feb                 | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec      |           |          |       |
| Fraction of space heat from secondary/supplementary system (Table 11)     |                     |          |          |          |          |          |          |          |          |          |          | 0.1000    | (201)    |       |
| Fraction of space heat from main system(s)                                |                     |          |          |          |          |          |          |          |          |          |          | 0.9000    | (202)    |       |
| Efficiency of main space heating system s <sub>1</sub> (in %)             |                     |          |          |          |          |          |          |          |          |          |          | 78.9000   | (206)    |       |
| Efficiency of secondary/supplementary heating system, s <sub>2</sub>      |                     |          |          |          |          |          |          |          |          |          |          | 100.0000  | (208)    |       |
| Space heating:  | Jan                 | Feb      | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec       |          |       |
| (98)m   | 432.5235            | 337.9200 | 274.9658 | 157.7327 | 62.1812  | 0.0000   | 0.0000   | 0.0000   | 144.0869 | 303.9136 | 414.6899 | 414.6899  | (98)     |       |
| (211)m  | 493.7828            | 385.4601 | 313.6492 | 179.9232 | 70.3291  | 0.0000   | 0.0000   | 0.0000   | 164.3576 | 346.6695 | 473.0303 | 473.0303  | (211)    |       |
| (215)m  | 63.2523             | 33.7920  | 27.4966  | 15.7733  | 6.2181   | 0.0000   | 0.0000   | 0.0000   | 14.4087  | 30.3914  | 41.4690  | 41.4690   | (215)    |       |
| Annual totals kWh/year  |                     |          |          |          |          |          |          |          |          |          |          | 2427.3919 | (213)    |       |
| Space heating fuel used, main system 1                                    |                     |          |          |          |          |          |          |          |          |          |          | 212.8014  | (215)    |       |
| Space heating fuel used, secondary  |                     |          |          |          |          |          |          |          |          |          |          | 212.8014  | (215)    |       |
| Water heating   | (64)m               | 211.4678 | 187.7082 | 200.2443 | 183.8182 | 183.2591 | 168.2365 | 165.8421 | 176.0952 | 173.9401 | 190.3977 | 195.9040  | 207.8350 | (64)  |
| Efficiency of water heater  | (217)m              | 75.0233  | 74.7140  | 74.0387  | 72.8645  | 70.5239  | 68.8000  | 68.8000  | 68.8000  | 70.5634  | 74.3453  | 74.9637   | 74.9637  | (217) |
| (219)m  | 281.8704            | 251.2356 | 270.4589 | 252.2741 | 258.3883 | 244.5297 | 241.0495 | 255.9523 | 252.8199 | 262.3882 | 263.5057 | 277.2475  | 277.2475 | (219) |
| Water heating fuel used   |                     |          |          |          |          |          |          |          |          |          |          | 3111.7201 | (219)    |       |
| Electricity for pumps, fans and electric keep-hot (Table 4f):             |                     |          |          |          |          |          |          |          |          |          |          |           |          |       |
| Central heating pump  |                     |          |          |          |          |          |          |          |          |          |          | 130.0000  | (230c)   |       |
| Boiler with a fan-assisted flue   |                     |          |          |          |          |          |          |          |          |          |          | 45.0000   | (230e)   |       |
| Total electricity for the above, kWh/year                                 |                     |          |          |          |          |          |          |          |          |          |          | 175.0000  | (231)    |       |
| Electricity for lighting (calculated in Appendix I)                       |                     |          |          |          |          |          |          |          |          |          |          | 319.4991  | (232)    |       |

| 12a. CO2 emissions - Individual heating systems including micro-CHP | CO2 emissions   |             |  |  |  |  |  |  |  |  |  |           |        |
|---|-----------------|-------------|--|--|--|--|--|--|--|--|--|-----------|--------|
| Energy  | Emission factor | Emissions   |  |  |  |  |  |  |  |  |  |           |        |
| kWh/year  | kg CO2/kWh      | kg CO2/year |  |  |  |  |  |  |  |  |  |           |        |
| Space heating - main system 1                                       | 0.1940          | 470.9140    |  |  |  |  |  |  |  |  |  | (261)     |        |
| Space heating - secondary   | 0.4220          | 89.8022     |  |  |  |  |  |  |  |  |  | (263)     |        |
| Water heating cost (other fuel)                                     | 0.1940          | 603.6737    |  |  |  |  |  |  |  |  |  | (264)     |        |
| Space and water heating   |                 | 1164.3899   |  |  |  |  |  |  |  |  |  | (265)     |        |
| Pumps and fans  | 175.0000        | 0.4220      |  |  |  |  |  |  |  |  |  | 73.8500   | (267)  |
| Energy for lighting   | 319.4991        | 0.4220      |  |  |  |  |  |  |  |  |  | 134.8286  | (268)  |
| Total CO2, kg/year  |                 |             |  |  |  |  |  |  |  |  |  | 1773.0685 | (272)  |
| Emissions per m2 for space and water heating                        |                 |             |  |  |  |  |  |  |  |  |  | 31.8641   | (272a) |
| Emissions per m2 for lighting                                       |                 |             |  |  |  |  |  |  |  |  |  | 3.4696    | (272b) |
| Target Carbon Dioxide Emission Rate (TER)                           |                 |             |  |  |  |  |  |  |  |  |  | 22.0600   | (273)  |
| =[(31.8641 * 1.00 * 1.0206) + (3.4696 * 1.2251)] * 0.60             |                 |             |  |  |  |  |  |  |  |  |  |           |        |

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## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF TARGET EMISSIONS

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| 6. Solar gains | Solar gains |            |               |               |          |          |          |          |          |          |          |          | Gains |         |      |
|----------------|-------------|------------|---------------|---------------|----------|----------|----------|----------|----------|----------|----------|----------|-------|---------|------|
| Jan            | Area        | Solar flux | g             | FF            | Access   |          |          |          |          |          |          |          | W     |         |      |
|                | m2          | Table 6a   | Specific data | Specific data | factor   |          |          |          |          |          |          |          |       |         |      |
|                |             | W/m2       | or Table 6b   | or Table 6c   | Table 6d |          |          |          |          |          |          |          |       |         |      |
| East           | 7.8650      | 19.8726    |               | 0.7200        | 0.7000   |          |          |          |          |          |          |          |       | 54.5904 | (76) |
| (83)m          | 54.5904     | 105.8117   | 169.1212      | 251.1049      | 305.5232 | 318.7979 | 309.4294 | 269.3032 | 202.1913 | 128.8588 | 67.8701  | 45.0317  | (83)  |         |      |
| (84)m          | 400.0456    | 448.8453   | 502.6651      | 570.2649      | 610.8573 | 610.9345 | 593.2562 | 558.5035 | 499.1237 | 440.3363 | 395.5644 | 384.1298 | (84)  |         |      |

| 7. Mean internal temperature (heating season) | Mean internal temperature (heating season) |         |         |         |         |                           |         |         |         |         |         |         |      |
|---|--|---------|---------|---------|---------|---------------------------|---------|---------|---------|---------|---------|---------|------|
| Jan   | Feb  | Mar     | Apr     | May     | Jun     | Jul                       | Aug     | Sep     | Oct     | Nov     | Dec     | 21.0000 |      |
| tau   | 39.7850                                    | 40.4908 | 40.4908 | 41.8483 | 42.7033 | 43.1130                   | 43.5096 | 42.4939 | 41.8483 | 41.1796 | 40.4908 |         |      |
| alpha   | 3.4523                                     | 3.6994  | 3.6994  | 3.7899  | 3.8469  | 3.8742                    | 3.9006  | 3.9006  | 3.7899  | 3.7453  | 3.6994  |         |      |
| (86)m   | 0.9849                                     | 0.9760  | 0.9524  | 0.8986  | 0.7781  | 0.6053                    | 0.4435  | 0.7256  | 0.9154  | 0.9752  | 0.9855  | (86)    |      |
| (87)m   | 19.4189                                    | 19.6233 | 19.9753 | 20.3792 | 20.7500 | 20.9313                   | 20.9879 | 20.9853 | 20.8594 | 20.4368 | 19.8293 | 19.4783 | (87) |
| (88)m   | 19.5135                                    | 19.5350 | 19.5986 | 19.5746 | 19.5986 | 19.6205                   | 19.5928 | 19.5746 | 19.5553 | 19.5350 | 19.5350 | (88)    |      |
| (89)m   | 0.9797                                     | 0.9680  | 0.9358  | 0.8643  | 0.7071  | 0.4937                    | 0.2829  | 0.3001  | 0.6167  | 0.8774  | 0.9655  | 0.9805  | (89) |
| (90)m   | 18.1477                                    | 18.3843 | 18.7059 | 19.1138 | 19.4494 | 19.5831                   | 19.6185 | 19.6180 | 19.5299 | 19.1776 | 18.5847 | 18.2239 | (90) |
| Living area fraction                          |  |         |         |         |         | fLA = Living area / (4) = |         |         |         |         |         | 0.5373  | (91) |
| (92)m   | 18.8307                                    | 19.0408 | 19.3880 | 19.7937 | 20.1481 | 20.3075                   | 20.3543 | 20.3527 | 20.2442 | 19.8542 | 19.2535 | 18.8974 | (92) |
| (93)m   | 18.8307                                    | 19.0408 | 19.3880 | 19.7937 | 20.1481 | 20.3075                   | 20.3543 | 20.3527 | 20.2442 | 19.8542 | 19.2535 | 18.8974 | (93) |

| 8. Space heating requirement              | Space heating requirement |          |          |          |          |          |          |          |          |          |          |           |      |
|---|---------------------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|------|
| Jan                                       | Feb                       | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec      |           |      |
| (94)m                                     | 0.9766                    | 0.9645   | 0.9338   | 0.8703   | 0.7372   | 0.5520   | 0.3568   | 0.3798   | 0.6710   | 0.8861   | 0.9629   | 0.9776    | (94) |
| (95)m                                     | 390.7002                  | 432.9241 | 469.3778 | 496.3100 | 450.2940 | 337.2308 | 211.6515 | 210.9777 | 334.9187 | 390.1993 | 380.9010 | 375.5155  | (95) |
| (96)m                                     | 4.5000                    | 0.0000   | 6.8000   | 8.7000   | 11.7000  | 14.6000  | 16.9000  | 14.6000  | 9.0000   | 4.6000   | 1.6000   | 0.0000    | (96) |
| (97)m                                     | 972.0490                  | 935.7813 | 836.9555 | 715.3832 | 533.8709 | 357.2323 | 214.2452 | 214.1456 | 377.4944 | 493.8645 | 603.0032 | 632.8844  | (97) |
| (98)m                                     | 432.5235                  | 337.9200 | 274.9658 | 157.7327 | 62.1812  | 0.0000   | 0.0000   | 0.0000   | 144.0869 | 303.9136 | 414.6899 | 414.6899  | (98) |
| Space heating (October to May) (kWh/year) |                           |          |          |          |          |          |          |          |          |          |          | 2128.0136 | (99) |
| Space heating requirement in kWh/year     |                           |          |          |          |          |          |          |          |          |          |          | 54.7650   | (99) |

| 8c. Space cooling requirement | Space cooling requirement |  |  |  |  |  |  |  |  |  |  |  |
|-------------------------------|---------------------------|--|--|--|--|--|--|--|--|--|--|--|
| Not applicable                |                           |  |  |  |  |  |  |  |  |  |  |  |

| 9a. Energy requirements - Individual heating systems, including micro-CHP | Energy requirements |     |     |     |     |     |     |     |     |     |     |          |       |
|---|---------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----------|-------|
| Jan   | Feb                 | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |          |       |
| Fraction of space heat from secondary/supplementary system (Table 11)     |                     |     |     |     |     |     |     |     |     |     |     | 0.1000   | (201) |
| Fraction of space heat from main system(s)                                |                     |     |     |     |     |     |     |     |     |     |     | 0.9000   | (202) |
| Efficiency of main space heating system s <sub>1</sub> (in %)             |                     |     |     |     |     |     |     |     |     |     |     | 78.9000  | (206) |
| Efficiency of secondary/supplementary heating system, s <sub>2</sub>      |                     |     |     |     |     |     |     |     |     |     |     | 100.0000 | (208) |

# 8.2: Appendixes : Energy / Renewable Energy Statement

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF STANDARD ENE7 CO2

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|       |          |          |          |          |          |          |          |          |          |          |          |               |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------------|
| (66)m | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | 68.8188  | (66)          |
| (67)m | 11.5788  | 10.2842  | 8.3637   | 6.3319   | 4.7331   | 3.9959   | 4.3177   | 5.6123   | 7.5329   | 9.5647   | 11.1634  | 11.9007 (67)  |
| (68)m | 118.0774 | 119.9089 | 116.8055 | 110.1989 | 101.8592 | 94.0210  | 88.7847  | 87.5532  | 90.4565  | 97.2632  | 105.6029 | 113.4410 (68) |
| (69)m | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819  | 29.8819 (69)  |
| (70)m | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000  | 10.0000 (70)  |
| (71)m | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 | -55.0551 (71) |
| (72)m | 129.8371 | 128.0882 | 124.8720 | 120.4994 | 117.6607 | 113.6635 | 110.2660 | 114.6191 | 116.1658 | 120.6914 | 125.8017 | 128.0947 (72) |
| (73)m | 313.5389 | 311.9270 | 303.6868 | 290.6758 | 277.8986 | 265.3261 | 257.0141 | 261.4303 | 268.0008 | 281.1650 | 296.2136 | 307.0820 (73) |

### 6. Solar gains

| [Jan]     | Area<br>m2 | Solar flux<br>Table 6a<br>W/m2 | g<br>Specific data<br>or Table 6b | FF<br>Specific data<br>or Table 6c | Access<br>factor<br>Table 6d | Gains<br>W   |
|-----------|------------|--------------------------------|-----------------------------------|------------------------------------|------------------------------|--------------|
| Southeast | 3.4200     | 37.3877                        | 0.7600                            | 0.7000                             | 0.7700                       | 47.1411 (77) |
| Northwest | 1.5300     | 11.5098                        | 0.7600                            | 0.7000                             | 0.7700                       | 6.5792 (81)  |

|       |          |          |          |          |          |          |          |          |          |          |          |               |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------------|
| (83)m | 53.7183  | 93.8221  | 129.6873 | 169.2392 | 194.1896 | 200.7729 | 195.3476 | 175.9184 | 146.4152 | 108.1544 | 66.8194  | 45.6337 (83)  |
| (84)m | 367.2572 | 405.7491 | 433.3741 | 459.9050 | 472.0992 | 466.0990 | 452.3617 | 437.3487 | 414.4160 | 389.3194 | 361.0330 | 352.7157 (84) |

### 7. Mean internal temperature (heating season)

|   |                             |         |         |         |         |         |         |         |         |         |         |              |              |
|---|-----------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------------|--------------|
| Temperature during heating periods in the living area from Table 9, Th1 (C) |                             |         |         |         |         |         |         |         |         |         |         |              | 21.0000 (85) |
| Utilisation factor for gains for living area, nil,m (see Table 9a)          |                             |         |         |         |         |         |         |         |         |         |         |              |              |
| tau   | Jan                         | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov     | Dec          |              |
| alpha   | 4.5214                      | 4.5719  | 4.5719  | 4.6682  | 4.7282  | 4.7588  | 4.7844  | 4.7844  | 4.7135  | 4.6682  | 4.6209  | 4.5719       |              |
| (86)m   | 0.9867                      | 0.9780  | 0.9575  | 0.9147  | 0.8039  | 0.6239  | 0.4265  | 0.4405  | 0.7119  | 0.9033  | 0.9762  | 0.9873 (86)  |              |
| (87)m   | 19.8723                     | 20.0370 | 20.2932 | 20.5676 | 20.8353 | 20.9626 | 20.9953 | 20.9946 | 20.9298 | 20.6536 | 20.1896 | 19.9108 (87) |              |
| (88)m   | 19.8322                     | 19.8467 | 19.8467 | 19.8733 | 19.8893 | 19.8967 | 19.9039 | 19.9039 | 19.8854 | 19.8733 | 19.8604 | 19.8467 (88) |              |
| (89)m   | 0.9824                      | 0.9711  | 0.9437  | 0.8873  | 0.7450  | 0.5301  | 0.3148  | 0.3255  | 0.4196  | 0.4976  | 0.5832  | 0.6332 (89)  |              |
| (90)m   | 18.8408                     | 19.0139 | 19.2625 | 19.5419 | 19.7860 | 19.8810 | 19.9029 | 19.9028 | 19.8526 | 19.6251 | 19.1764 | 18.8908 (90) |              |
| Living area fraction  | = LIA = Living area / (4) = |         |         |         |         |         |         |         |         |         |         |              | 0.5373 (91)  |
| (92)m   | 19.3950                     | 19.5636 | 19.8163 | 20.0930 | 20.3498 | 20.4622 | 20.4898 | 20.4894 | 20.4314 | 20.1777 | 19.7208 | 19.4389 (92) |              |
| Temperature adjustment  |                             |         |         |         |         |         |         |         |         |         |         |              | 0.0000       |
| (93)m   | 19.3950                     | 19.5636 | 19.8163 | 20.0930 | 20.3498 | 20.4622 | 20.4898 | 20.4894 | 20.4314 | 20.1777 | 19.7208 | 19.4389 (93) |              |

### 8. Space heating requirement

| [94]m                                    | Jan      | Feb      | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec           |                |              |
|--|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------------|----------------|--------------|
| (94)m                                    | 0.9805   | 0.9690   | 0.9433   | 0.8933   | 0.7711   | 0.5796   | 0.3750   | 0.3875   | 0.6671   | 0.8846   | 0.9663   | 0.9813 (94)   |                |              |
| (95)m                                    | 360.0786 | 395.1875 | 408.7884 | 410.8889 | 364.0182 | 270.1503 | 169.8546 | 169.4818 | 276.4832 | 344.4066 | 348.8697 | 346.1231 (95) |                |              |
| (96)m                                    | 4.9000   | 5.0000   | 6.8000   | 8.7000   | 11.7000  | 14.6000  | 16.9000  | 14.3000  | 16.8000  | 7.0000   | 4.9000   | 4.9000 (96)   |                |              |
| (97)m                                    | 760.9871 | 733.5270 | 655.5925 | 558.7744 | 417.4039 | 280.7326 | 170.6604 | 170.6394 | 297.0440 | 459.9324 | 632.0402 | 732.2802 (97) |                |              |
| (98)m                                    | 298.2759 | 228.7081 | 183.6222 | 106.5064 | 39.7190  | 0.0000   | 0.0000   | 0.0000   | 85.9512  | 203.8827 | 287.3009 | 287.3009 (98) |                |              |
| Space heating (October to May) kWh/year  |          |          |          |          |          |          |          |          |          |          |          |               | 1433.9665 (99) |              |
| Space heating requirement in kWh/m2/year |          |          |          |          |          |          |          |          |          |          |          |               | (98) / (4) =   | 36.9008 (99) |

### 8c. Space cooling requirement

Not applicable

### 9a. Energy requirements - Individual heating systems, including micro-CHP

|   |                |          |          |          |          |          |          |          |          |          |                |                 |
|---|----------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------------|-----------------|
| Fraction of space heat from secondary/supplementary system (Table 11) | 0.1000 (201)   |          |          |          |          |          |          |          |          |          |                |                 |
| Fraction of space heat from main system(s)                            | 0.9000 (202)   |          |          |          |          |          |          |          |          |          |                |                 |
| Efficiency of main space heating system 1 (in %)                      | 88.9000 (208)  |          |          |          |          |          |          |          |          |          |                |                 |
| Efficiency of secondary/supplementary heating system, %               | 100.0000 (208) |          |          |          |          |          |          |          |          |          |                |                 |
| Space heating:  |                |          |          |          |          |          |          |          |          |          |                |                 |
| Jan   | Feb            | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec            |                 |
| (98)m   | 298.2759       | 228.7081 | 183.6222 | 106.5064 | 39.7190  | 0.0000   | 0.0000   | 0.0000   | 85.9512  | 203.8827 | 287.3009 (98)  |                 |
| (211)m  | 301.9666       | 231.5380 | 185.8943 | 107.8242 | 40.2104  | 0.0000   | 0.0000   | 0.0000   | 87.0147  | 206.4055 | 290.8558 (211) |                 |
| (215)m  | 29.8276        | 22.8708  | 18.3622  | 10.6506  | 3.9719   | 0.0000   | 0.0000   | 0.0000   | 8.5951   | 20.3883  | 28.7301 (215)  |                 |
| Annual totals kWh/year  |                |          |          |          |          |          |          |          |          |          |                | 1451.7097 (211) |
| Space heating fuel used, main system 1                                |                |          |          |          |          |          |          |          |          |          |                | 143.3967 (215)  |
| Space heating fuel used, secondary                                    |                |          |          |          |          |          |          |          |          |          |                | 143.3967 (215)  |
| Water heating   |                |          |          |          |          |          |          |          |          |          |                |                 |
| (64)m   | 184.4784       | 163.4954 | 173.8160 | 158.7408 | 157.6801 | 143.9381 | 141.1339 | 150.8743 | 149.3566 | 164.4617 | 170.2223       | 181.0272 (64)   |
| Efficiency of water heater  |                |          |          |          |          |          |          |          |          |          |                |                 |
| (217)m  | 84.4892        | 84.1267  | 83.4191  | 82.3213  | 80.4900  | 78.8000  | 78.8000  | 78.8000  | 78.8000  | 81.7719  | 83.7351        | 84.4430 (217)   |
| (219)m  | 218.3454       | 194.3442 | 208.3648 | 192.8309 | 195.9003 | 182.6626 | 179.1039 | 191.4649 | 189.5388 | 201.1226 | 203.2867       | 214.3781 (219)  |
| Water heating fuel used   |                |          |          |          |          |          |          |          |          |          |                | 2371.3433 (219) |
| Electricity for pumps, fans and electric keep-hot (Table 4f):         |                |          |          |          |          |          |          |          |          |          |                |                 |
| central heating pump  |                |          |          |          |          |          |          |          |          |          |                | 130.0000 (230c) |
| boiler with a fan-assisted flue                                       |                |          |          |          |          |          |          |          |          |          |                | 45.0000 (230e)  |
| Total electricity for the above, kWh/year                             |                |          |          |          |          |          |          |          |          |          |                | 175.0000 (231)  |
| Electricity for lighting (calculated in Appendix L)                   |                |          |          |          |          |          |          |          |          |          |                | 204.4860 (232)  |

### 12a. CO2 emissions - Individual heating systems including micro-CHP

|   |                 |                            |                       |
|---|-----------------|----------------------------|-----------------------|
| Space heating - main system 1               | Energy kWh/year | Emission factor kg CO2/kWh | Emissions kg CO2/year |
| Space heating - secondary                   | 143.3967        | 0.1980                     | 28.3925 (261)         |
| Water heating coat (other fuel)             | 2371.3433       | 0.5170                     | 1225.7844 (263)       |
| Space and water heating                     |                 |                            | 469.5260 (264)        |
| Pumps and fans                              | 175.0000        | 0.1980                     | 34.6500 (265)         |
| Energy for lighting                         | 204.4860        | 0.5170                     | 105.7192 (268)        |
| Total CO2, kg/year                          |                 |                            | 1027.2948 (273)       |
| Dwelling Carbon Dioxide Emission Rate (DER) |                 |                            | 26.4400 (273)         |

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF STANDARD ENE7 CO2

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## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF ENERGY RATINGS FOR IMPROVED DWELLING

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SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF ENERGY RATINGS FOR IMPROVED DWELLING  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07:18  
-----  
No improvements selected

# 8.2: Appendixes : Energy / Renewable Energy Statement

## CALCULATION DETAILS for survey reference no 'PVs' REGULATIONS COMPLIANCE REPORT - Approved Document L1A, 2010 Edition

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REGULATIONS COMPLIANCE REPORT - Approved Document L1A, 2010 Edition  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

New Build (As Designed)

1 TER and DER  
Fuel for main heating: Mains gas  
Fuel factor: 1.00 (mains gas)  
Target Carbon Dioxide Emission Rate (TER) 22.06 kg/m<sup>2</sup>  
Dwelling Carbon Dioxide Emission Rate (DER) 20.17 kg/m<sup>2</sup>OK

2 Fabric U-values  
Element Average Highest  
External wall 0.23 (max. 0.30) 0.25 (max. 0.70) OK  
Floor (no floor) OK  
Roof OK  
Openings 1.36 (max. 2.00) 1.50 (max. 3.30) OK

2a Thermal bridging  
Thermal bridging calculated using default y-value of 0.15

3 Design air permeability  
Design air permeability at 50 pascals: 7.00  
Maximum 10.0 OK

4 Heating efficiency  
Main heating system: Boiler system with radiators or underfloor - Mains gas  
Data from manufacturer  
tbc tbc  
Combi boiler  
Efficiency: 90.0% SEDBUK2009  
Minimum: 88.0% OK  
Secondary heating system: None

5 Cylinder insulation  
Hot water storage: No cylinder

6 Controls  
Space heating controls: Time and temperature zone control OK

Hot water controls: No cylinder

Boiler interlock: Yes OK

7 Low energy lights  
Percentage of fixed lights with low-energy fittings: 100%  
Minimum 75% OK

8 Mechanical ventilation  
Not applicable

9 Summertime temperature  
Overheating risk (Thames Valley): Not significant OK  
Based on:  
Overheating: Average  
Windows facing South East: 3.40 m<sup>2</sup>, No overhang  
Windows facing North West: 1.55 m<sup>2</sup>, No overhang  
Ventilation rates: 6.00  
Blinds/curtains: None

10 Key features  
Door U-value 1.00 W/m<sup>2</sup>K  
Party wall U-value 0.00 W/m<sup>2</sup>K  
Photovoltaic array

## CALCULATION DETAILS for survey reference no 'PVs' SAP 2009 OVERHEATING ASSESSMENT FOR New Build (As Designed) BRE SAP Worksheet 9.90

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SAP 2009 OVERHEATING ASSESSMENT FOR New Build (As Designed) BRE SAP Worksheet 9.90  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

Overheating Calculation Input Data

Dwelling type End Terrace Flat  
Number of storeys 1  
Cross ventilation possible Yes  
Region Thames Valley  
Front of dwelling faces South East  
Overheating Average or unknown  
Thermal mass parameter 250.0  
Night ventilation Yes  
Ventilation rate during hot weather (ach) 6.00 (Windows fully open)

Overheating Calculation

Summer ventilation heat loss coefficient 216.82 (P1)  
Transmission heat loss coefficient 26.83 (P7)  
Summer heat loss coefficient 237.65 (P2)

| Orientation | Ratio | Z overhangs | Overhang type |
|-------------|-------|-------------|---------------|
| South East  | 0.000 | 1.000       | None          |
| North West  | 0.000 | 1.000       | None          |

| Solar shading | Z blinds | Solar access | Z overhangs | Z summer   |
|---------------|----------|--------------|-------------|------------|
| South East    | 1.000    | 0.90         | 1.000       | 0.900 (P8) |
| North West    | 1.000    | 0.90         | 1.000       | 0.900 (P8) |

| [Jul]      | Area m <sup>2</sup> | Solar flux Table 6a W/m <sup>2</sup> | g Specific data or Table 6b | FF Specific data or Table 6c | Shading | Gains W         |
|------------|---------------------|--------------------------------------|-----------------------------|------------------------------|---------|-----------------|
| South East | 3.4200              | 116.7611                             | 0.7600                      | 0.7000                       | 0.9000  | 172.0763        |
| North West | 1.5500              | 88.9568                              | 0.7600                      | 0.7000                       | 0.9000  | 66.0958         |
|            |                     |                                      |                             |                              |         | total: 238.1721 |

|  | Jun             | Jul             | Aug             |      |
|--|-----------------|-----------------|-----------------|------|
| Solar gains  | 249             | 238             | 217             | (P3) |
| Internal gains   | 266             | 255             | 261             |      |
| Total summer gains                                     | 514             | 493             | 479             | (P5) |
| Summer gain/loss ratio                                 | 2.16            | 2.08            | 2.02            | (P6) |
| Summer external temperature                            | 15.40           | 17.80           | 17.80           |      |
| Thermal mass temperature increment (TMP = 250.0)       | 0.00            | 0.00            | 0.00            |      |
| Threshold temperature                                  | 17.81           | 20.13           | 20.07           | (P7) |
| Likelihood of high internal temperature                | Not significant | Not significant | Not significant |      |
| Assessment of likelihood of high internal temperature: | Not significant |                 |                 |      |

## CALCULATION DETAILS for survey reference no 'PVs' SAP 2009 IMPROVEMENTS

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SAP 2009 IMPROVEMENTS  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

21686\_New Oxford Street\_03Flat

Current energy efficiency rating: B B3  
Current environmental impact rating: B B9

(For testing purposes):

|                                  |                   |
|----------------------------------|-------------------|
| A                                | Not considered    |
| B                                | Not considered    |
| C                                | Not considered    |
| D                                | Not considered    |
| E Low energy lighting            | Already installed |
| F                                | Not considered    |
| G                                | Not considered    |
| H                                | Not considered    |
| I                                | Not considered    |
| J                                | Not considered    |
| K                                | Not considered    |
| L                                | Not considered    |
| M                                | Not considered    |
| N Solar water heating            | Not applicable    |
| O                                | Not considered    |
| P                                | Not considered    |
| Q                                | Not considered    |
| R                                | Not considered    |
| S                                | Not considered    |
| T                                | Not considered    |
| U Solar photovoltaic (PV) panels | Not applicable    |
| V Wind turbine                   | Not applicable    |

| Recommended measures: | SAP change | Cost change | CO2 change |
|-----------------------|------------|-------------|------------|
| (none)                |            |             |            |

| Lower cost measures (none) | Typical annual savings | Energy efficiency impact | Environmental impact |
|----------------------------|------------------------|--------------------------|----------------------|
| Sub Total                  | £0                     | 0.0000 kg/m <sup>2</sup> |                      |

| Higher cost measures (none) | Typical annual savings | Energy efficiency impact | Environmental impact |
|-----------------------------|------------------------|--------------------------|----------------------|
| Sub Total                   | £0                     | 0.0000 kg/m <sup>2</sup> |                      |

Potential energy efficiency rating: B B3  
Potential environmental impact rating: B B9  
Further improvements to achieve even higher standards (none)  
Total Savings £0 0.0000 kg/m<sup>2</sup>

Enhanced energy efficiency rating: B B3  
Enhanced environmental impact rating: B B9  
Fuel prices for cost data on this page from database revision number 327 TEST (31 Aug 2012)  
Recommendation texts revision number 3.9c (09 Jan 2012)

| Typical heating and lighting costs of this home (per year): | Current               | Potential             | Enhanced              |
|---|-----------------------|-----------------------|-----------------------|
| Electricity   | £49                   | £49                   | £49                   |
| Mains gas   | £226                  | £226                  | £226                  |
| Space heating   | £190                  | £190                  | £190                  |
| Water heating   | £59                   | £59                   | £59                   |
| Lighting  | £26                   | £26                   | £26                   |
| Generated (PV)  | -£28                  | -£28                  | -£28                  |
| Total cost  | £247                  | £247                  | £247                  |
| Carbon dioxide emissions                                    | 0.7 tonnes            | 0.7 tonnes            | 0.7 tonnes            |
| Primary energy  | 95 kWh/m <sup>2</sup> | 95 kWh/m <sup>2</sup> | 95 kWh/m <sup>2</sup> |

# 8.2: Appendixes : Energy / Renewable Energy Statement



## CALCULATION DETAILS for survey reference no 'PVs' SAP2009 - 9.81 input data (DesignData) -

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|                               |   |
|-------------------------------|---|
| Burner Control                | OnOff   |
| Boiler Compensator            | None  |
| Flue Type                     | Balanced  |
| Fan Assisted Flue             | Yes   |
| Pumped                        | Pump in heated space  |
| Heat Emitter                  | Radiators   |
| Combi boiler type             | Standard Combi  |
| Combi keep hot type           | None  |
| Main Heating 2                | None  |
| Smoke Control Area            | Unknown   |
| Community Heating             | None  |
| Secondary Heating             | None  |
| Water Heating                 | MainHeating1  |
| Type                          | BW -  |
| Low Water Usage               | Yes   |
| SAP Code                      | 901   |
| Hot Water Cylinder            | None  |
| Flue Gas Heat Recovery System | None  |
| Waste Water Heat Recovery     | None  |
| PV Unit                       | One Dwelling  |
| Type                          | Cells Peak = 0.66, Orientation = South, Elevation = Horizontal, Overhading = NoneOrLittle |
| Wind Turbine                  | None  |
| Terrain Type                  | Urban   |
| Small Scale Hydro             | None  |
| Special Features              | None  |

## Full SAP Calculation Printout

Property Reference: 21686\_New Oxford Street\_08Flat  
Survey Reference: PVs  
Property: 112-116, New Oxford Street, LONDON, WC1A 1HH, Issued on Date: 17.Dec.2012  
Prop Type Ref:

SAP Rating: 83 B CO2 Emissions (t/year): 1.57 DER: 18.77 Pass Reduction: 14.1% FEE: 72.5 ZC8: 0.00  
Environmental: 84 B General Requirements Compliance: Pass TER: 21.84 HLP: 2.04 Energy cost: £ 393

CFSH Results Version: CFSH November 2010 ENE1 Credits: 1.7 ENE2 Credits: 0.0 ENE7 Credits: 0 CFSH Level: 3

Surveyor: admin admin, Tel: unknown  
Address:  
Client:

Software Version: Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18  
SAP version: SAP 2009, Regs Region: England and Wales (Part L1A 2010), Calculation Type: New Dwelling As Designed

## CALCULATION DETAILS for survey reference no 'PVs' SAP2009 - 9.81 input data (DesignData) -

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SAP2009 Input Data

FullRefNo: PVS  
Sap Version: SAP 2009  
Regs Region: England & Wales  
Region: Thames Valley  
Calculation Type: New Build (As Designed)  
Dwelling Orientation: South East  
Property Type: Flat, Kind-Terrace  
Stores: 2  
Date Built: 2012  
Sheltered Sides: 1  
Sunlight Shade: Average or unknown  
Measurements: Perimeter, Floor Area, Storey Height  
1st Storey: 42.16, 89.97, 3.55  
Living Area: 25.63 m2, fraction: 28.5%  
Thermal Mass: Simple calculation  
Thermal Mass Simple: Medium  
Thermal Mass Value: 250

External Walls  
External Wall: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
Corridor Wall: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
Party Walls: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
Party Wall: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
External Roofs  
External Roof: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
Heat Loss Floors  
Party Floors: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
Floor: Mett Area, Gross Area, Kappa, Element, Construction, Type, ShelterFactor, UValueFinal  
Description: Data Source, Type, Glazing, Glazing Gap, Argon Filled, Solar Trans, Frame Type, Frame Factor, U Value  
Windows: Manufacturer, Window, Double glazed, . . . 0.76, 0.7,  
Door: Manufacturer, Solid Door, . . . . .  
Openings: Opening Type, Location, Orientation, Curtain Type, Overhang Ratio, Wide Overhang, Width, Height, Count, Area, Curtain Closed

Windows SE: Window, External Wall, Southeast, None, 0, 0, 0, 0, 12.84,  
Windows SW: Window, External Wall, Southwest, None, 0, 0, 0, 0, 18.24,  
Door: Solid Door, Corridor Wall, Northeast, . . . 0, 0, 0, 1.89,  
Windows NW: Window, External Wall, Northwest, None, 0, 0, 0, 0, 8.49,  
Conservatory: None  
Draught Proofing: 100  
Draught Lobby: No  
Thermal Bridges: Default, 0.15  
Pressure Test: True  
Designed q0: 5  
AsBuilt q0: 4  
Property Tested: False  
Mechanical Ventilation: None  
Chimneys M8S: 0  
Chimneys S8S: 0  
Chimneys Other: 0  
Chimneys Total: 0  
Open Flues M8S: 0  
Open Flues S8S: 0  
Open Flues Other: 0  
Open Flues Total: 0  
Intermittent Fans: 3  
Passive Vents: 0  
Flueless Gas Fires: 0  
Cooling System: None  
Light Fittings: 5  
LEL Fittings: 100  
Percentage of LEL Fittings: 100  
External Lights Fitted: No  
External LELs Fitted: No  
Electricity Tariff: Standard  
Main Heating 1  
Description: Percentage  
HRG: 100  
SAP Code: 104  
Boiler Efficiency Type: Sedbuk 2009  
Efficiency: 90  
Model Name: tbc  
Manufacturer: tbc  
HRG Controls: CH  
Delayed Start Stat: No  
Ctrl SAP Code: 2110

## CALCULATION DETAILS for survey reference no 'PVs' CALCULATION OF FABRIC ENERGY EFFICIENCY

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SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF FABRIC ENERGY EFFICIENCY  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

### 1. Overall dwelling dimensions

|  |   |                        |
|--|---|------------------------|
| Area   | Storey height                             | Volume                 |
| (m2)   | (m)                                       | (m3)                   |
| Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)...(1n) | 89.9700 (1b) x 3.3500 (2b)                | = 319.3935 (1b) - (3b) |
| Dwelling volume  | (3a) + (3b) + (3c) + (3d) + (3e)...(3n) = | 319.3935 (5)           |

### 2. Ventilation rate

|  | main heating  | secondary heating | other | total                       | m3 per hour           |
|--|---|-------------------|-------|-----------------------------|-----------------------|
| Number of chimneys   | 0   | 0                 | 0     | 0                           | 0 + 40 = 0.0000 (6a)  |
| Number of open flues   | 0   | 0                 | 0     | 0                           | 0 + 20 = 0.0000 (6b)  |
| Number of intermittent fans  | 0   | 0                 | 0     | 0                           | 3 * 10 = 30.0000 (7a) |
| Number of passive vents  | 0   | 0                 | 0     | 0                           | 0 * 10 = 0.0000 (7b)  |
| Number of flueless gas fires   | 0   | 0                 | 0     | 0                           | 0 + 40 = 0.0000 (7c)  |
| Infiltration due to chimneys, flues and fans   | = (6a)+(6b)+(7a)+(7b)+(7c) =                            |                   |       | 30.0000                     | (8)                   |
| Pressure test  | Measured/design q50                                     |                   |       | 0.0000                      | Yes                   |
| If based on air permeability value, then (18) = [(17)/20]*(9), otherwise (18) = (16) |   |                   |       | 0.0000                      | (18)                  |
| Number of sides on which dwelling is sheltered                                       |   |                   |       | 2                           | (19)                  |
| Shelter factor   |   |                   |       | (20) = 1 - [0.075 x (19)] = | 0.8500 (20)           |
| Infiltration rate adjusted to include shelter factor                                 |   |                   |       | (21) = (18) x (20) =        | 0.2923 (21)           |
| Air changes per hour   | = (6a)+(6b)+(7a)+(7b)+(7c) = 30.0000 / (5) = 0.0939 (8) |                   |       |                             |                       |

| Wind speed    | Jan    | Feb    | Mar    | Apr    | May    | Jun    | Jul    | Aug    | Sep    | Oct    | Nov    | Dec          |
|---------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------------|
| (22a)         | 5.4000 | 5.1000 | 5.1000 | 4.5000 | 4.1000 | 3.9000 | 3.7000 | 3.0000 | 4.2000 | 4.5000 | 4.5000 | 5.1000 (22)  |
| (22b)         | 1.3500 | 1.2750 | 1.2750 | 1.1250 | 1.0250 | 0.9750 | 0.9250 | 0.9250 | 1.0000 | 1.1250 | 1.2000 | 1.2750 (22a) |
| (22c)         | 0.3947 | 0.3727 | 0.3727 | 0.3289 | 0.2996 | 0.2850 | 0.2704 | 0.2704 | 0.3070 | 0.3289 | 0.3508 | 0.3727 (22b) |
| Effective ach | 0.5779 | 0.5695 | 0.5695 | 0.5541 | 0.5449 | 0.5406 | 0.5366 | 0.5366 | 0.5471 | 0.5541 | 0.5615 | 0.5695 (25)  |

### 3. Heat losses and heat loss parameter

| Element   | Gross m2 | Openings m2 | NetArea m2 | U-value W/m2K | A x U W/K            | K-value kJ/m2K | A x K kJ/K                  |          |          |          |          |               |
|---|----------|-------------|------------|---------------|----------------------|----------------|-----------------------------|----------|----------|----------|----------|---------------|
| Door  |          |             |            | 1.8900        | 1.8900               |                | 2.8900 (26)                 |          |          |          |          |               |
| Windows (Uw = 1.50)   |          |             |            | 39.3700       | 1.4151               | 55.9953        | 37.9333 (27)                |          |          |          |          |               |
| External Wall   |          |             |            | 0.1500        | 11.3174              |                | 1.6968 (29a)                |          |          |          |          |               |
| Corridor Wall   | 34.7200  | 1.8900      | 32.8300    | 0.2257        | 7.4108               |                | 0.5129 (29b)                |          |          |          |          |               |
| External Roof   | 89.9700  |             | 89.9700    | 0.1300        | 11.6961              |                | 1.0504 (30)                 |          |          |          |          |               |
| Total net area of external elements Aum(A, m2)                      |          |             | 239.7090   |               |                      |                | (31)                        |          |          |          |          |               |
| Fabric heat loss, W/K = Sum (A x U)                                 |          |             |            |               | (26)...(30) + (32) = | 88.3096        | (33)                        |          |          |          |          |               |
| Party Wall  |          |             |            | 10.6500       | 0.0000               | 0.0000         | 0.0000 (32)                 |          |          |          |          |               |
| Floor   |          |             |            | 89.9700       |                      |                | 0.0000 (32a)                |          |          |          |          |               |
| Thermal mass parameter (TMP = Cm / TFA) in kJ/m2K                   |          |             |            |               |                      |                | 250.0000 (35)               |          |          |          |          |               |
| Thermal bridges (Default value 0.150 * total exposed area)          |          |             |            |               |                      |                | 35.9564 (36)                |          |          |          |          |               |
| Total fabric heat loss  |          |             |            |               |                      |                | (33) + (36) = 124.2659 (37) |          |          |          |          |               |
| Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5) | Jan      | Feb         | Mar        | Apr           | May                  | Jun            | Jul                         | Aug      | Sep      | Oct      | Nov      | Dec           |
| (38)m   | 60.8982  | 60.0215     | 60.0215    | 58.4001       | 57.4318              | 56.9814        | 56.5535                     | 56.5535  | 57.6654  | 58.4001  | 59.1855  | 60.0215 (38)  |
| (39)m   | 185.1741 | 184.2874    | 184.2874   | 182.6660      | 181.6977             | 181.2473       | 180.8194                    | 180.8194 | 182.6660 | 183.4514 | 184.2874 | 184.2874 (39) |
| (40)m   | 2.0582   | 2.0483      | 2.0483     | 2.0303        | 2.0195               | 2.0145         | 2.0098                      | 2.0098   | 2.0221   | 2.0363   | 2.0390   | 2.0483 (40)   |
| (41)m   | 31       | 31          | 31         | 30            | 30                   | 31             | 31                          | 31       | 30       | 31       | 31       | 31 (41)       |

### 4. Water heating energy requirements (kWh/year)

Assumed occupancy, N: 2.4253 (42)  
Annual average hot water usage in litres per day Vd,average = (23 x N) + 36  
Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

|  | Jan      | Feb      | Mar      | Apr      | May      | Jun      | Jul     | Aug      | Sep      | Oct      | Nov      | Dec           |
|--|----------|----------|----------|----------|----------|----------|---------|----------|----------|----------|----------|---------------|
| (44)m                                      | 106.2062 | 102.3442 | 98.4821  | 94.6201  | 90.7580  | 86.8960  | 86.8960 | 90.7580  | 94.6201  | 98.4821  | 102.3442 | 106.2062 (44) |
| (45)m                                      | 157.8775 | 138.0807 | 142.4869 | 124.2236 | 119.1955 | 102.8566 | 95.3118 | 109.3717 | 110.6779 | 128.9844 | 140.7966 | 152.8960 (45) |
| Energy content (annual)                    |          |          |          |          |          |          |         |          |          |          |          |               |
| (46)m                                      | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000 (46)   |
| Water storage loss:                        |          |          |          |          |          |          |         |          |          |          |          |               |
| (57)m                                      | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000 (57)   |
| Primary circuit loss (annual) from Table 3 |          |          |          |          |          |          |         |          |          |          |          |               |
| (59)m                                      | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000 (59)   |
| (65)m                                      | 33.5490  | 29.3422  | 30.2785  | 26.3975  | 25.3290  | 21.8570  | 20.2538 | 23.2415  | 23.5191  | 27.4092  | 29.9193  | 32.4904 (65)  |

### 5. Internal gains (see Table 5 and 5a)

Metabolic gains (Table 5), Watts

|       | Jan       | Feb       | Mar       | Apr       | May       | Jun       | Jul       | Aug       | Sep       | Oct       | Nov       | Dec            |
|-------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------------|
| (66)m | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655 (66)  |
| (67)m | 21.3930   | 18.9265   | 15.3921   | 11.4528   | 8.7106    | 7.3538    | 7.9461    | 10.3286   | 11.8631   | 17.6023   | 20.5445   | 21.9013 (67)   |
| (68)m | 239.0225  | 241.5028  | 235.2525  | 221.9464  | 205.1498  | 189.3634  | 178.8711  | 176.3368  | 182.5871  | 195.8932  | 212.6898  | 228.4762 (68)  |
| (69)m | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265 (69)   |
| (70)m | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000    | 0.0000 (70)    |
| (71)m | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 (71) |
| (72)m | 45.0927   | 43.6639   | 40.6969   | 36.6632   | 34.0444   | 30.3570   | 27.2228   | 31.2385   | 32.6654   | 36.8403   | 41.5545   | 43.6697 (72)   |
| (73)m | 367.8039  | 366.4729  | 353.7211  | 332.6420  | 310.2845  | 289.4539  | 276.3656  | 280.2836  | 291.4951  | 312.7155  | 337.1685  | 356.4270 (73)  |

### 6. Solar gains





# 8.2: Appendixes : Energy / Renewable Energy Statement

**CALCULATION DETAILS for survey reference no 'Pvs'**  
**CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE** Page: 10 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BBE SAP Worksheet 9.90  
 CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE  
 Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07c18

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1. Overall dwelling dimensions

|  | Area<br>(m <sup>2</sup> ) | Storey height<br>(m)            | Volume<br>(m <sup>3</sup> ) |
|--|---------------------------|---------------------------------|-----------------------------|
| Total floor area FFA = (la)+(lb)+(lc)+(ld)+(le)...(ln) | 89.9700                   | 3.5500 (2b)                     | 319.3935 (1b) - (3b)        |
| Dwelling volume  |                           | (3a)+(3b)+(3c)+(3d)+(3e)...(3n) | 319.3935 (5)                |

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2. Ventilation rate

Number of chimneys heating: 0  
 Number of open fires heating: 0  
 Number of intermittent fans heating: 0  
 Number of passive vents heating: 0  
 Number of fireless gas fires heating: 0

Number of chimneys secondary heating: 0  
 Number of open fires secondary heating: 0  
 Number of intermittent fans secondary heating: 0  
 Number of passive vents secondary heating: 0  
 Number of fireless gas fires secondary heating: 0

Number of chimneys other heating: 0  
 Number of open fires other heating: 0  
 Number of intermittent fans other heating: 0  
 Number of passive vents other heating: 0  
 Number of fireless gas fires other heating: 0

Number of chimneys total heating: 0  
 Number of open fires total heating: 0  
 Number of intermittent fans total heating: 0  
 Number of passive vents total heating: 0  
 Number of fireless gas fires total heating: 0

Pressure test  
 Measured/design q<sub>50</sub>  
 If based on air permeability value, then (18) = [171/201] x (8), otherwise (18) = (16)  
 Number of sides on which dwelling is sheltered: 1

Shelter factor (20) = 1 - [0.075 x (19)] = 0.9250 (20)  
 Infiltration rate adjusted to include shelter factor (21) = (18) x (20) = 0.3181 (21)

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3. Heat losses and heat loss parameter

| Element   | Gross<br>m <sup>2</sup> | Openings<br>m <sup>2</sup> | Net Area<br>m <sup>2</sup> | U-value<br>W/m <sup>2</sup> K | A x U<br>W/K | K-value<br>kJ/m <sup>2</sup> K | A x K<br>kJ/K |
|---|-------------------------|----------------------------|----------------------------|-------------------------------|--------------|--------------------------------|---------------|
| Door  |                         |                            | 1.8900                     | 1.0000                        | 1.8900       |                                | (26)          |
| Windows (U <sub>w</sub> = 1.50)   |                         |                            | 35.5700                    | 1.4131                        | 50.2003      |                                | (27)          |
| External Wall   | 115.0190                | 39.5700                    | 75.4490                    | 0.1500                        | 11.3174      |                                | (29a)         |
| Corridor Wall   | 34.7200                 | 1.8900                     | 32.8300                    | 0.2257                        | 7.4108       |                                | (29b)         |
| External Roof   | 89.9700                 |                            | 89.9700                    | 0.1300                        | 11.6961      |                                | (30)          |
| Total net area of external elements A <sub>ext</sub> (A <sub>ext</sub> , m <sup>2</sup> ) |                         |                            | 239.7090                   |                               |              |                                | (31)          |
| Fabric heat loss, W/K = Sum (A x U)   |                         |                            |                            | (26)                          | (30) + (32)  | 88.3096                        | (33)          |
| Party Wall  |                         |                            | 10.6500                    |                               | 0.0000       |                                | (32)          |
| Floor   |                         |                            | 89.9700                    |                               | 0.0000       |                                | (32)          |
| Thermal mass parameter (TMP = Cm / FFA) in kJ/m <sup>2</sup> K                            |                         |                            |                            |                               |              |                                | 250.0000 (35) |
| Thermal bridges (Default value 0.150 * total exposed area)                                |                         |                            |                            |                               |              |                                | 35.9564 (36)  |
| Total fabric heat loss (33) + (36) =  |                         |                            |                            |                               |              |                                | 124.2659 (37) |

Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5)

|       | Jan      | Feb      | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec           |
|-------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------------|
| (38)m | 62.4206  | 61.3705  | 61.3705  | 59.4504  | 59.3036  | 57.7703  | 57.2636  | 57.2636  | 58.5803  | 59.4504  | 60.3805  | 61.3705 (38)  |
| (39)m | 186.6865 | 185.6364 | 185.6364 | 183.7163 | 182.5696 | 182.0362 | 181.5295 | 181.5295 | 182.8463 | 183.7163 | 184.6464 | 185.6364 (39) |
| (40)m | 2.0750   | 2.0633   | 2.0633   | 2.0420   | 2.0292   | 2.0232   | 2.0177   | 2.0177   | 2.0323   | 2.0420   | 2.0523   | 2.0633 (40)   |
| (41)m | 31       | 28       | 31       | 30       | 31       | 30       | 31       | 31       | 30       | 31       | 30       | 31 (41)       |

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4. Water heating energy requirements (kWh/year)

Assumed occupancy, N: 2.6253 (42)  
 Annual average hot water usage in litres per day V<sub>d,average</sub> = (25 x N) + 36: 96.5511 (43)  
 Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

|  | Jan      | Feb      | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec           |
|--|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|---------------|
| (44)m  | 108.2662 | 107.3442 | 98.4821  | 94.6201  | 90.7580  | 86.8960  | 86.8960  | 86.8960  | 88.4821  | 102.3442 | 106.2062 | (44)          |
| (45)m  | 157.8775 | 138.0807 | 142.4869 | 124.2236 | 119.1955 | 102.8566 | 95.3118  | 109.3717 | 110.6779 | 128.9844 | 140.7966 | 152.8960 (45) |
| (46)m  | 23.4816  | 20.7121  | 21.3700  | 18.6335  | 17.8793  | 15.4285  | 14.2968  | 16.4057  | 16.6017  | 19.3477  | 21.1195  | 22.9344 (46)  |
| (47)m  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000 (47)   |
| (48)m  | 50.9589  | 46.0274  | 50.1854  | 46.0620  | 46.2493  | 42.8528  | 44.2812  | 46.2493  | 44.6620  | 50.1854  | 49.3151  | 50.9589 (48)  |
| (49)m  | 208.8365 | 184.1081 | 192.6723 | 170.8855 | 165.4448 | 145.7094 | 139.5930 | 155.6210 | 157.3399 | 179.1698 | 190.1117 | 203.8549 (49) |
| (50)m  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000 (50)   |
| Water heat. (208.8365 184.1081 192.6723 170.8855 165.4448 145.7094 139.5930 155.6210 157.3399 179.1698 190.1117 203.8549 (64)) |          |          |          |          |          |          |          |          |          |          |          |               |
| (65)m  | 65.2340  | 57.4187  | 59.9233  | 52.9698  | 51.1948  | 44.9130  | 42.7615  | 47.9284  | 48.4659  | 55.4337  | 59.1436  | 63.5776 (65)  |

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5. Internal gains (see Table 5 and 5a)

Metabolic gains (Table 5), Watts

|       | Jan       | Feb       | Mar       | Apr       | May       | Jun       | Jul       | Aug       | Sep       | Oct       | Nov       | Dec            |
|-------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------------|
| (66)m | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655  | 131.2655 (66)  |
| (67)m | 21.3095   | 18.2945   | 15.3921   | 11.6528   | 8.7106    | 7.3538    | 7.9461    | 10.3286   | 13.8631   | 17.6023   | 20.5445   | 21.9013 (67)   |
| (68)m | 239.0225  | 241.5028  | 235.2525  | 221.9464  | 205.1498  | 189.3634  | 178.8171  | 176.3368  | 182.5871  | 195.8932  | 212.6898  | 228.4762 (68)  |
| (69)m | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265   | 36.1265 (69)   |
| (70)m | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000   | 10.0000 (70)   |
| (71)m | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 | -105.0124 (71) |
| (72)m | 87.6801   | 85.4445   | 80.5420   | 73.5692   | 68.8102   | 62.3792   | 57.4751   | 64.4199   | 67.3137   | 74.5076   | 82.1439   | 85.4538 (72)   |

**CALCULATION DETAILS for survey reference no 'Pvs'**  
**CALCULATION OF DWELLING EMISSIONS FOR REGULATIONS COMPLIANCE** Page: 11 of 22

(73)m 420.3913 418.2535 403.5663 379.5480 355.0503 331.4761 316.6179 323.4649 336.1435 360.3828 387.7579 408.2110 (73)

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6. Solar gains

| [Jan]     | Area<br>m <sup>2</sup> | Solar Flux<br>Table 6a<br>W/m <sup>2</sup> | Specific data<br>or Table 6b | Specific data<br>or Table 6c | Access<br>factor<br>Table 6d | Gain<br>W     |
|-----------|------------------------|--|------------------------------|------------------------------|------------------------------|---------------|
| Southwest | 12.8400                | 37.3877                                    | 0.7600                       | 0.7000                       | 0.7700                       | 176.9858 (77) |
| Southwest | 18.2400                | 37.3877                                    | 0.7600                       | 0.7000                       | 0.7700                       | 251.4190 (79) |
| Northwest | 8.4900                 | 11.5098                                    | 0.7600                       | 0.7000                       | 0.7700                       | 36.0262 (81)  |

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(83)m 464.4510 804.0344 1093.7130 1398.0337 1878.6352 1623.4121 1583.4393 1463.1030 1224.8073 921.8117 559.0942 395.3948 (83)  
 (84)m 884.8224 1222.2878 1497.2792 1777.5818 1934.6855 1954.8882 1900.0572 1766.9680 1561.0008 1282.1945 946.8521 803.6050 (84)

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7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, T<sub>th</sub> (C): 21.0000 (85)  
 Utilization factor for gains for living area, nil/m (see Table 9a)

| tau                          | Jan     | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov     | Dec          |
|------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|--------------|
| alpha                        | 33.4474 | 33.6567 | 33.6567 | 34.0085 | 34.2221 | 34.3224 | 34.4182 | 34.4182 | 34.1703 | 34.0085 | 33.8372 | 33.6567      |
| (86)m                        | 0.9873  | 0.9662  | 0.9242  | 0.8480  | 0.7142  | 0.5467  | 0.3806  | 0.4068  | 0.6465  | 0.8860  | 0.9756  | 0.9896 (86)  |
| (87)m                        | 19.0286 | 19.3987 | 19.8792 | 20.3245 | 20.7155 | 20.9133 | 20.9811 | 20.9769 | 20.8340 | 20.3374 | 19.5106 | 19.0369 (87) |
| (88)m                        | 19.2910 | 19.2986 | 19.2986 | 19.3124 | 19.3208 | 19.3247 | 19.3284 | 19.3284 | 19.3188 | 19.3124 | 19.3057 | 19.2986 (88) |
| (89)m                        | 0.9827  | 0.9547  | 0.8983  | 0.7987  | 0.6286  | 0.4239  | 0.2306  | 0.2476  | 0.5405  | 0.8353  | 0.9654  | 0.9857 (89)  |
| (90)m                        | 16.8157 | 17.3488 | 18.0207 | 18.6179 | 19.0500 | 19.2807 | 19.3247 | 19.3238 | 19.2214 | 18.6642 | 17.5224 | 16.8332 (90) |
| Living area fraction (92)m   | 17.4461 | 17.9328 | 18.5501 | 19.1040 | 19.5530 | 19.7457 | 19.7966 | 19.7948 | 19.6808 | 19.1409 | 18.0888 | 17.4610 (92) |
| Temperature adjustment (93)m | 17.4461 | 17.9328 | 18.5501 | 19.1040 | 19.5530 | 19.7457 | 19.7966 | 19.7948 | 19.6808 | 19.1409 | 18.0888 | 17.4610 (93) |

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8. Space heating requirement

|  | Jan       | Feb       | Mar       | Apr       | May       | Jun      | Jul      | Aug      | Sep      | Oct       | Nov       | Dec            |
|--|-----------|-----------|-----------|-----------|-----------|----------|----------|----------|----------|-----------|-----------|----------------|
| (94)m  | 0.9750    | 0.9417    | 0.8840    | 0.7926    | 0.6418    | 0.4560   | 0.2738   | 0.2936   | 0.5707   | 0.8288    | 0.9547    | 0.9791 (94)    |
| (95)m  | 862.6894  | 1151.0652 | 1323.5417 | 1408.9837 | 1241.6048 | 891.3586 | 520.2701 | 518.6490 | 890.8428 | 1062.6535 | 903.9168  | 786.7952 (95)  |
| (96)m  | 4.5000    | 5.0000    | 6.8000    | 8.7000    | 11.7000   | 14.6000  | 16.9000  | 16.9000  | 14.3000  | 10.8000   | 7.0000    | 4.9000 (96)    |
| (97)m  | 2416.8595 | 2400.7939 | 2181.2521 | 1911.3900 | 1433.7254 | 936.7127 | 525.8130 | 525.4851 | 983.8598 | 1532.3516 | 2047.5067 | 2331.7755 (97) |
| (98)m  | 1156.3026 | 839.8176  | 638.1365  | 361.7325  | 142.9377  | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 349.4554  | 823.3847  | 1149.4653 (98) |
| Space heating (October to May) (kWh/year)                          |           |           |           |           |           |          |          |          |          |           |           |                |
| Space heating requirement in kWh/m <sup>2</sup> /year (98) / (4) = |           |           |           |           |           |          |          |          |          |           |           | 60.7006 (99)   |

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9a. Energy requirements - Individual heating systems, including micro-CHP

Fraction of space heat from secondary/supplementary system (Table 11): 0.0000 (201)  
 Fraction of space heat from main systems (a): 1.0000 (202)  
 Efficiency of main space heating system 1 (in %): 80.8000 (206)  
 Efficiency of secondary/supplementary heating system, %: 0.0000 (208)

Space heating:

|  | Jan       | Feb      | Mar      | Apr      | May      | Jun    | Jul    | Aug    | Sep    | Oct      | Nov      | Dec             |
|--|-----------|----------|----------|----------|----------|--------|--------|--------|--------|----------|----------|-----------------|
| (98)m                                  | 1156.3026 | 839.8176 | 638.1365 | 361.7325 | 142.9377 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 349.4554 | 823.3847 | 1149.4653 (98)  |
| (211)m                                 | 1273.4610 | 924.9093 | 702.7936 | 398.3838 | 157.4204 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 384.8628 | 906.8114 | 1265.9310 (211) |
| (215)m                                 | 0.0000    | 0.0000   | 0.0000   | 0.0000   | 0.0000   | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000   | 0.0000   | 0.0000 (215)    |
| Annual totals kWh/year                 |           |          |          |          |          |        |        |        |        |          |          |                 |
| Space heating fuel used, main system 1 |           |          |          |          |          |        |        |        |        |          |          | 6014.5732 (211) |
| Space heating fuel used, secondary     |           |          |          |          |          |        |        |        |        |          |          | 0.0000 (215)    |

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4. Water heating energy requirements (kWh/year)

Water heating (64)m 208.8365 184.1081 192.6723 170.8855 165.4448 145.7094 139.5930 155.6210 157.3399 179.1698 190.1117 203.8549 (64)  
 Efficiency of water heater: (217)m 89.2422 88.9744 88.4591 87.5931 85.5620 81.5000 81.5000 81.5000 81.5000 81.5000 80.8772 89.2656 (217)  
 (219)m 234.0110 206.9225 217.8096 195.0901 193.3625 178.7846 171.2798 190.9460 193.0530 204.9553 213.8557 228.3688 (219)  
 Water heating fuel used 2428.4409 (219)

Electricity for pumps, fans and electric keep-hot (Table 4f):  
 boiler with a fan-assisted flue  
 Total electricity for the above, kWh/year 130.0000 (230c)  
 Electricity for lighting (calculated in Appendix I) 45.0000 (230e)  
 Total electricity for the above, kWh/year 175.0000 (231)  
 Electricity for lighting (calculated in Appendix I) 376.3242 (232)

Energy saving/generation technologies (Appendices M, N and Q)  
 PV Unit 0 (0.80 \* 0.66 \* 961 \* 1.00) -507.4080 (233)

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12a. CO<sub>2</sub> emissions - Individual heating systems including micro-CHP

|   | Energy<br>kWh/year | Emission factor<br>kg CO <sub>2</sub> /kWh | Emissions<br>kg CO <sub>2</sub> /year |
|---|--------------------|--|---------------------------------------|
| Space heating - main system 1               | 6014.5732          | 0.1980                                     | 1190.8855 (261)                       |
| Space heating - secondary                   | 0.0000             | 0.0000                                     | 0.0000 (263)                          |
| Water heating cost (other fuel)             | 2428.4409          | 0.1980                                     | 480.8333 (264)                        |
| Space and water heating                     | 8443.0141          |  | 1671.7188 (265)                       |
| Pumps and fans                              | 175.0000           | 0.5170                                     | 90.4750 (267)                         |
| Energy for lighting                         | 376.3242           | 0.5170                                     | 194.5596 (268)                        |
| Energy saving/generation technologies       | -507.4080          | 0.5290                                     | -268.4188 (269)                       |
| PV Unit                                     | -507.4080          | 0.5290                                     | -268.4188 (269)                       |
| Total CO <sub>2</sub> , kg/year             |                    |  | 1680.3326 (272)                       |
| Dwelling Carbon Dioxide Emission Rate (DER) |                    |  | 18.7700 (273)                         |



# 8.2: Appendixes : Energy / Renewable Energy Statement

CALCULATION DETAILS for survey reference no 'PVs'  
CALCULATION OF TARGET EMISSIONS Page: 13 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF TARGET EMISSIONS  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.0718

1. Overall dwelling dimensions

| Ground floor area | Total floor area |
|-------------------|------------------|
| 89.9700           | 89.9700          |

2. Ventilation rate

| main heating | secondary heating | other | total |
|--------------|-------------------|-------|-------|
| 0            | 0                 | 0     | 0     |

3. Heat losses and heat loss parameter

| Element             | Gross m2 | Openings m2 | Net Area m2 | U-value W/m2K | A x U W/K | K-value kJ/m2K | A x K kJ/K |
|---------------------|----------|-------------|-------------|---------------|-----------|----------------|------------|
| Doors               | 20.6425  | 0.8500      | 19.7925     | 2.0000        | 3.9500    | 2.0000         | 39.5000    |
| Windows (Dv = 2.00) | 149.7390 | 22.4925     | 127.2465    | 1.4919        | 38.2769   | 0.3500         | 44.3363    |
| External Wall       | 89.9700  | 0.1600      | 89.8100     | 0.1600        | 14.3952   | 0.1600         | 14.3952    |
| External Roof       | 235.7090 | 0.0000      | 235.7090    | 0.0000        | 0.0000    | 0.0000         | 0.0000     |
| Party Wall          | 10.6500  | 0.0000      | 10.6500     | 0.0000        | 0.0000    | 0.0000         | 0.0000     |

4. Water heating energy requirements (kWh/year)

| Jan     | Feb     | Mar     | Apr     | May     | Jun     | Jul     | Aug     | Sep     | Oct     | Nov     | Dec     | Total     |
|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-----------|
| 77.1783 | 74.5341 | 74.5341 | 69.6988 | 66.8111 | 65.4680 | 64.1920 | 64.1920 | 67.5078 | 69.6988 | 72.0409 | 74.5341 | 1003.3120 |

5. Internal gains (see Table 5 and 5a)

| Jan      | Feb      | Mar      | Apr      | May      | Jun      | Jul      | Aug      | Sep      | Oct      | Nov      | Dec      | Total     |
|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|
| 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 131.2655 | 1575.1866 |

CALCULATION DETAILS for survey reference no 'PVs'  
CALCULATION OF TARGET EMISSIONS Page: 14 of 22

6. Solar gains

| Month | Area m2 | Solar flux Table 6a W/m2 | Specific data g | Specific data or Table 6b | FF or Table 6c | Access factor Table 6d | Gains W |
|-------|---------|--------------------------|-----------------|---------------------------|----------------|------------------------|---------|
| Jan   | 20.6425 | 19.8726                  | 0.7200          | 0.7000                    | 0.7700         | 143.2782               |         |

7. Mean internal temperature (heating season)

| Month | Temp (C) |
|-------|----------|
| Jan   | 18.7197  |
| Feb   | 17.8061  |
| Mar   | 18.2367  |
| Apr   | 18.7489  |
| May   | 19.2837  |
| Jun   | 19.6026  |
| Jul   | 19.7255  |
| Aug   | 19.7197  |
| Sep   | 18.8505  |
| Oct   | 18.0779  |
| Nov   | 17.6482  |
| Dec   | 17.6482  |

8. Space heating requirement

| Month | Req (kWh/m2/year) |
|-------|-------------------|
| Jan   | 0.9888            |
| Feb   | 0.9809            |
| Mar   | 0.9603            |
| Apr   | 0.9156            |
| May   | 0.8157            |
| Jun   | 0.6488            |
| Jul   | 0.4224            |
| Aug   | 0.4533            |
| Sep   | 0.7738            |
| Oct   | 0.9373            |
| Nov   | 0.9824            |
| Dec   | 0.9898            |

9a. Energy requirements - Individual heating systems, including micro-CHP

Fraction of space heat from secondary/supplementary system (Table 11): 0.1000 (201)  
Fraction of space heat from main system(s): 0.9000 (202)  
Efficiency of main space heating system 1 (in %): 78.9000 (206)  
Efficiency of secondary/supplementary heating system, %: 100.0000 (208)

Space heating:

| Month     | Jan       | Feb       | Mar       | Apr       | May       | Jun       | Jul       | Aug       | Sep       | Oct       | Nov       | Dec       | Total       |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-------------|
| 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 9055.5425 | 108666.5100 |

12a. CO2 emissions - Individual heating systems including micro-CHP

| Energy kWh/year | Emission factor kg CO2/kWh | Emissions kg CO2/year |
|-----------------|----------------------------|-----------------------|
| 9055.5425       | 0.1940                     | 1756.7752 (261)       |
| 793.8692        | 0.4220                     | 335.0128 (263)        |
| 3704.7892       | 0.1940                     | 718.7291 (264)        |

CALCULATION DETAILS for survey reference no 'PVs'  
CALCULATION OF TARGET EMISSIONS Page: 15 of 22

12b. CO2 emissions - Individual heating systems including micro-CHP

| Energy kWh/year | Emission factor kg CO2/kWh | Emissions kg CO2/year |
|-----------------|----------------------------|-----------------------|
| 9055.5425       | 0.1940                     | 1756.7752 (261)       |
| 793.8692        | 0.4220                     | 335.0128 (263)        |
| 3704.7892       | 0.1940                     | 718.7291 (264)        |

# 8.2: Appendixes : Energy / Renewable Energy Statement

**CALCULATION DETAILS for survey reference no 'PVs'  
CALCULATION OF STANDARD EN7 CO2**

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SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF STANDARD EN7 CO2  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

1. Overall dwelling dimensions

|  |                        |                   |                          |
|--|------------------------|-------------------|--------------------------|
| Ground floor area                                  | Area (m <sup>2</sup> ) | Storey height (m) | Volume (m <sup>3</sup> ) |
| Total floor area FFA = (la)+(lb)+(lc)+(ld)+(le)... | 89.9700                | 3.5500            | 319.3935                 |

2. Ventilation rate

Number of chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) = 30.0000 / (3) = 0.0939 (8)

Number of open flues = 0 + 0 + 0 = 0 \* 10 = 0.0000 (6b)

Number of intermittent fans = 0 + 0 + 0 = 0 \* 10 = 0.0000 (7a)

Number of passive vents = 0 + 0 + 0 = 0 \* 10 = 0.0000 (7b)

Number of fireless gas fires = 0 \* 40 = 0.0000 (7c)

3. Heat losses and heat loss parameter

| Element   | Gross m <sup>2</sup> | Openings m <sup>2</sup> | NetArea m <sup>2</sup> | U-value W/m <sup>2</sup> K | A x U W/K | K-value kJ/m <sup>2</sup> K | A x K kJ/K                  |          |          |          |               |               |
|---|----------------------|-------------------------|------------------------|----------------------------|-----------|-----------------------------|-----------------------------|----------|----------|----------|---------------|---------------|
| Door  | 1.8900               |                         | 1.8900                 | 1.0000                     | 1.8900    | 1.0000                      | 1.8900 (20)                 |          |          |          |               |               |
| Windows (Uw = 1.50)   |                      |                         | 35.5700                | 1.4131                     | 50.2646   | 1.4131                      | 50.2646 (27)                |          |          |          |               |               |
| External Wall   | 115.0190             | 39.5700                 | 75.4490                | 0.1500                     | 11.3174   | 0.1500                      | 11.3174 (29a)               |          |          |          |               |               |
| Corridor Wall   | 34.7200              | 1.8900                  | 32.8300                | 0.2257                     | 7.4108    | 0.2257                      | 7.4108 (29b)                |          |          |          |               |               |
| External Roof   | 89.9700              |                         | 89.9700                | 0.1300                     | 11.6961   | 0.1300                      | 11.6961 (30)                |          |          |          |               |               |
| Total net area of external elements Aum(A, m <sup>2</sup> )         |                      |                         | 239.7090               |                            |           |                             |                             |          |          |          |               |               |
| Fabric heat loss, W/K = Sum(A x U)                                  |                      |                         | (26) + (30) + (32) =   |                            | 88.3096   |                             | 88.3096 (33)                |          |          |          |               |               |
| Party Wall  |                      |                         | 10.6500                | 0.0000                     | 0.0000    |                             | 0.0000 (32)                 |          |          |          |               |               |
| Floor   | 89.9700              |                         | 89.9700                |                            |           |                             |                             |          |          |          |               |               |
| Thermal mass parameter (TmP = Cm / TFA) in kJ/m <sup>2</sup> K      |                      |                         |                        |                            |           |                             | 250.0000 (35)               |          |          |          |               |               |
| Thermal bridges (Default value 0.150 * total exposed area)          |                      |                         |                        |                            |           |                             | 35.9564 (36)                |          |          |          |               |               |
| Total fabric heat loss  |                      |                         |                        |                            |           |                             | (33) + (36) = 124.2659 (37) |          |          |          |               |               |
| Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5) |                      |                         |                        |                            |           |                             |                             |          |          |          |               |               |
| (38)m   | Jan                  | Feb                     | Mar                    | Apr                        | May       | Jun                         | Jul                         | Aug      | Sep      | Oct      | Nov           | Dec           |
| (39)m   | 62.4206              | 61.3705                 | 61.3705                | 59.4504                    | 59.3036   | 57.7703                     | 57.2636                     | 57.2636  | 58.5803  | 59.4504  | 60.3905       | 61.3705 (38)  |
| (39)m   | 186.6865             | 185.6364                | 185.6364               | 183.7163                   | 182.5696  | 182.0362                    | 181.5295                    | 181.5295 | 182.8463 | 183.7163 | 184.6664      | 185.6364 (39) |
| (40)m   | 2.0750               | 2.0633                  | 2.0633                 | 2.0420                     | 2.0292    | 2.0233                      | 2.0177                      | 2.0122   | 2.0253   | 2.0420   | 2.0523        | 2.0633 (40)   |
| (41)m   | 31                   | 28                      | 31                     | 30                         | 31        | 30                          | 31                          | 31       | 30       | 31       | 30            | 31 (41)       |
| Jan   | Feb                  | Mar                     | Apr                    | May                        | Jun       | Jul                         | Aug                         | Sep      | Oct      | Nov      | Dec           |               |
| (44)m   | 106.2062             | 102.3442                | 98.4821                | 94.6201                    | 90.7580   | 86.8960                     | 86.8960                     | 84.8221  | 102.3442 | 106.2062 | 110.2902 (44) |               |
| (45)m   | 157.8775             | 153.0807                | 142.4869               | 124.2236                   | 119.1955  | 102.8566                    | 95.3118                     | 109.3737 | 110.2902 | 124.2236 | 157.8775 (45) |               |
| (46)m   | 23.4816              | 20.7121                 | 21.3730                | 18.6335                    | 17.8793   | 15.4285                     | 14.2968                     | 16.4057  | 16.6017  | 19.3477  | 21.1195       | 22.9344 (46)  |
| Jan   | Feb                  | Mar                     | Apr                    | May                        | Jun       | Jul                         | Aug                         | Sep      | Oct      | Nov      | Dec           |               |

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**CALCULATION DETAILS for survey reference no 'PVs'  
CALCULATION OF STANDARD EN7 CO2**

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6. Solar gains

| [Jan]     | Area m <sup>2</sup> | Solar Flux Table 6a W/m <sup>2</sup> | Specific data or Table 6b | Specific data or Table 6c | Access factor Table 6d | Gains W   |          |          |          |           |              |                 |     |
|-----------|---------------------|--------------------------------------|---------------------------|---------------------------|------------------------|---|----------|----------|----------|-----------|--------------|-----------------|-----|
| Southeast | 12.8400             | 37.3877                              | 0.7600                    | 0.7000                    | 0.7700                 | 176.9858 (77)   |          |          |          |           |              |                 |     |
| Southwest | 8.2400              | 37.3877                              | 0.7600                    | 0.7000                    | 0.7700                 | 251.4190 (79)   |          |          |          |           |              |                 |     |
| Northwest | 8.4900              | 11.5098                              | 0.7600                    | 0.7000                    | 0.7700                 | 36.0265 (81)  |          |          |          |           |              |                 |     |
| (83)m     | 464.4310            | 804.0344                             | 1093.7130                 | 1398.0337                 | 1579.6352              | 1623.4121 1583.4393 1443.1030 1224.8573 921.8117 559.0942 395.3940 (83)   |          |          |          |           |              |                 |     |
| (84)m     | 948.4556            | 1285.9210                            | 1561.1723                 | 1842.1362                 | 1999.9012              | 2020.7652 1965.9342 1831.7837 1625.5552 1346.0876 1010.4853 667.2382 (84) |          |          |          |           |              |                 |     |
| tau       | alpha               | Jan                                  | Feb                       | Mar                       | Apr                    | May   | Jun      | Jul      | Aug      | Sep       | Oct          | Nov             | Dec |
| (87)m     | 19.0824             | 19.4462                              | 19.9212                   | 20.3555                   | 20.7324                | 20.9198   | 20.9827  | 20.9791  | 20.8470  | 20.3733   | 19.5620      | 19.0913 (87)    |     |
| (88)m     | 19.2910             | 19.2986                              | 19.2986                   | 19.3124                   | 19.3208                | 19.3247   | 19.3284  | 19.3284  | 19.3388  | 19.3124   | 19.3057      | 19.2986 (88)    |     |
| (89)m     | 0.9790              | 0.9485                               | 0.8888                    | 0.7869                    | 0.6141                 | 0.4105  | 0.2230   | 0.2390   | 0.5232   | 0.8195    | 0.9590       | 0.9823 (89)     |     |
| (90)m     | 17.6537             | 18.0146                              | 18.4639                   | 18.8634                   | 19.1739                | 19.2971   | 19.3261  | 19.3256  | 19.2584  | 18.9987   | 18.1374      | 17.6688 (90)    |     |
| (91)m     | 2531.5975           | 2491.7923                            | 2442.3142                 | 1945.2683                 | 1445.5647              | 939.1862  | 526.0815 | 525.8230 | 899.3682 | 1565.0369 | 2131.4154    | 2445.5798 (91)  |     |
| (92)m     | 18.0607             | 18.4230                              | 18.8791                   | 19.2884                   | 19.6179                | 19.7594   | 19.7980  | 19.7966  | 19.7109  | 19.3188   | 18.5432      | 18.0740 (92)    |     |
| (93)m     | 18.4230             | 18.8791                              | 19.2884                   | 19.6179                   | 19.7594                | 19.7980   | 19.7966  | 19.7109  | 19.3188  | 18.5432   | 18.0740 (93) |                 |     |
| Jan       | Feb                 | Mar                                  | Apr                       | May                       | Jun                    | Jul   | Aug      | Sep      | Oct      | Nov       | Dec          |                 |     |
| (94)m     | 0.4440              | 0.3938                               | 0.3004                    | 0.1763                    | 0.6308                 | 0.4440  | 0.2650   | 0.2637   | 0.5555   | 0.9197    | 0.9517       | 0.9174 (94)     |     |
| (95)m     | 923.2022            | 1208.4547                            | 1374.4832                 | 1448.0385                 | 1261.6365              | 897.1535  | 521.0565 | 519.6545 | 903.0026 | 1103.4505 | 961.6625     | 847.6123 (95)   |     |
| (96)m     | 4.5000              | 5.0000                               | 6.8000                    | 8.7000                    | 11.7000                | 14.6000   | 16.9000  | 16.9000  | 14.3000  | 10.8000   | 7.0000       | 4.9000 (96)     |     |
| (97)m     | 2531.5975           | 2491.7923                            | 2442.3142                 | 1945.2683                 | 1445.5647              | 939.1862  | 526.0815 | 525.8230 | 899.3682 | 1565.0369 | 2131.4154    | 2445.5798 (97)  |     |
| (98)m     | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (98)  |     |
| (99)m     | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (99)  |     |
| (100)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (100) |     |
| (101)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (101) |     |
| (102)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (102) |     |
| (103)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (103) |     |
| (104)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (104) |     |
| (105)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (105) |     |
| (106)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (106) |     |
| (107)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (107) |     |
| (108)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (108) |     |
| (109)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (109) |     |
| (110)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (110) |     |
| (111)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (111) |     |
| (112)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (112) |     |
| (113)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (113) |     |
| (114)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (114) |     |
| (115)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (115) |     |
| (116)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (116) |     |
| (117)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (117) |     |
| (118)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (118) |     |
| (119)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (119) |     |
| (120)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (120) |     |
| (121)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (121) |     |
| (122)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (122) |     |
| (123)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (123) |     |
| (124)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (124) |     |
| (125)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (125) |     |
| (126)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (126) |     |
| (127)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (127) |     |
| (128)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (128) |     |
| (129)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (129) |     |
| (130)m    | 1196.6461           | 862.4028                             | 645.6662                  | 358.0055                  | 136.8426               | 0.0000  | 0.0000   | 0.0000   | 0.0000   | 343.4203  | 842.2221     | 1188.8880 (130) |     |
| (131)m    | 1196.6461           |                                      |                           |                           |                        |   |          |          |          |           |              |                 |     |

# 8.2: Appendixes : Energy / Renewable Energy Statement

**CALCULATION DETAILS for survey reference no 'PVs'  
CALCULATION OF ENERGY RATINGS FOR IMPROVED DWELLING** Page: 19 of 22

SAP 2009 WORKSHEET FOR New Build (As Designed) BRE SAP Worksheet 9.90  
CALCULATION OF ENERGY RATINGS FOR IMPROVED DWELLING  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

No improvements selected

**CALCULATION DETAILS for survey reference no 'PVs'  
REGULATIONS COMPLIANCE REPORT - Approved Document L1A, 2010 Edition** Page: 20 of 22

REGULATIONS COMPLIANCE REPORT - Approved Document L1A, 2010 Edition  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

New Build (As Designed)

|   |                  |                  |    |
|---|------------------|------------------|----|
| <b>1 TER and DER</b>  |                  |                  |    |
| Fuel for main heating: Mains gas  |                  |                  |    |
| Fuel factor: 1.00 (Mains gas)   |                  |                  |    |
| Target Carbon Dioxide Emission Rate (TER) 21.84 kg/m <sup>2</sup>           |                  |                  |    |
| Dwelling Carbon Dioxide Emission Rate (DER) 18.77 kg/m <sup>2</sup> OK      |                  |                  |    |
| <b>2 Fabric U-values</b>  |                  |                  |    |
| Element   | Average          | Highest          |    |
| External wall   | 0.18 (max. 0.30) | 0.25 (max. 0.70) | OK |
| Floor   | (no floor)       | 0.13 (max. 0.35) | OK |
| Roof  | 0.13 (max. 0.20) | 0.13 (max. 0.35) | OK |
| Openings  | 1.48 (max. 2.00) | 1.50 (max. 3.30) | OK |
| <b>2a Thermal bridging</b>  |                  |                  |    |
| Thermal bridging calculated using default y-value of 0.15                   |                  |                  |    |
| <b>3 Design air permeability</b>  |                  |                  |    |
| Design air permeability at 50 pascals: 5.00                                 |                  |                  |    |
| Maximum 10.0 OK   |                  |                  |    |
| <b>4 Heating efficiency</b>   |                  |                  |    |
| Main heating system: Boiler system with radiators or underfloor - Mains gas |                  |                  |    |
| Data from manufacturer tbc tbc  |                  |                  |    |
| Combi boiler  |                  |                  |    |
| Efficiency: 90.0% SEDBUK2009  |                  |                  |    |
| Minimum: 88.0% OK   |                  |                  |    |
| Secondary heating system: None  |                  |                  |    |
| <b>5 Cylinder insulation</b>  |                  |                  |    |
| Hot water storage: No cylinder  |                  |                  |    |
| <b>6 Controls</b>   |                  |                  |    |
| Space heating controls: Time and temperature zone control OK                |                  |                  |    |
| Hot water controls: No cylinder   |                  |                  |    |
| Boiler interlock: Yes OK  |                  |                  |    |
| <b>7 Low energy lights</b>  |                  |                  |    |
| Percentage of fixed lights with low-energy fittings: 100%                   |                  |                  |    |
| Minimum 75% OK  |                  |                  |    |
| <b>8 Mechanical ventilation</b>   |                  |                  |    |
| Not applicable  |                  |                  |    |
| <b>9 Summertime temperature</b>   |                  |                  |    |
| Overheating risk (Thames Valley): Slight OK                                 |                  |                  |    |
| Based on:   |                  |                  |    |
| Overshading:  |                  |                  |    |
| Windows facing South East: 12.84 m <sup>2</sup> , No overhang               |                  |                  |    |
| Windows facing South West: 18.24 m <sup>2</sup> , No overhang               |                  |                  |    |
| Windows facing North West: 8.49 m <sup>2</sup> , No overhang                |                  |                  |    |
| Ventilation rate: 6.00  |                  |                  |    |
| Blinds/curtains: None   |                  |                  |    |
| <b>10 Key features</b>  |                  |                  |    |
| External wall U-value 0.18 W/m <sup>2</sup> K                               |                  |                  |    |
| Door U-value 1.00 W/m <sup>2</sup> K  |                  |                  |    |
| Party wall U-value 0.00 W/m <sup>2</sup> K                                  |                  |                  |    |
| Photovoltaic array  |                  |                  |    |

**CALCULATION DETAILS for survey reference no 'PVs'  
SAP 2009 OVERHEATING ASSESSMENT FOR New Build (As Designed) BRE SAP Worksheet 9.90** Page: 21 of 22

SAP 2009 OVERHEATING ASSESSMENT FOR New Build (As Designed) BRE SAP Worksheet 9.90  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

Overheating Calculation Input Data

|   |                           |
|---|---------------------------|
| Dwelling type                             | End Terrace Flat          |
| Number of storeys                         | 1                         |
| Cross ventilation possible                | Yes                       |
| Region                                    | Thames Valley             |
| Front of dwelling faces                   | South East                |
| Overshading                               | Average or unknown        |
| Thermal mass parameter                    | 250.0                     |
| Night ventilation                         | Yes                       |
| Ventilation rate during hot weather (ach) | 6.00 (Windows fully open) |

Overheating Calculation

|  |                     |                                      |                             |                              |         |          |
|--|---------------------|--------------------------------------|-----------------------------|------------------------------|---------|----------|
| Summer ventilation heat loss coefficient               | 632.40 (P1)         |                                      |                             |                              |         |          |
| Transmission heat loss coefficient                     | 124.27 (P7)         |                                      |                             |                              |         |          |
| Summer heat loss coefficient                           | 756.67 (P2)         |                                      |                             |                              |         |          |
| <b>Overhangs</b>                                       |                     |                                      |                             |                              |         |          |
| Orientation  | Ratio               | Z overhangs                          | Overhang type               |                              |         |          |
| South East   | 0.000               | 1.000                                | None                        |                              |         |          |
| South West   | 0.000               | 1.000                                | None                        |                              |         |          |
| North West   | 0.000               | 1.000                                | None                        |                              |         |          |
| <b>Solar shading</b>                                   |                     | Z blinds                             | Z overhangs                 | Z summer                     |         |          |
| Orientation  |                     |                                      |                             |                              |         |          |
| South East   | 1.000               | 0.90                                 | 1.000                       | 0.900 (P8)                   |         |          |
| South West   | 1.000               | 0.90                                 | 1.000                       | 0.900 (P8)                   |         |          |
| North West   | 1.000               | 0.90                                 | 1.000                       | 0.900 (P8)                   |         |          |
| [Jul]  | Area m <sup>2</sup> | Solar flux Table 6a W/m <sup>2</sup> | g Specific data or Table 6b | FF Specific data or Table 6c | Shading | Gains W  |
| South East   | 12.8400             | 116.7611                             | 0.7600                      | 0.7000                       | 0.9000  | 646.0408 |
| South West   | 18.2400             | 116.7611                             | 0.7600                      | 0.7000                       | 0.9000  | 917.7402 |
| North West   | 8.4900              | 88.9568                              | 0.7600                      | 0.7000                       | 0.9000  | 362.5364 |
| total: 1925.8155                                       |                     |                                      |                             |                              |         |          |
| Solar gains  |                     | Jun                                  | Jul                         | Aug                          |         |          |
| Internal gains   |                     | 2007                                 | 1926                        | 1778                         | (P3)    |          |
| Total summer gains                                     |                     | 469                                  | 450                         | 459                          | (P5)    |          |
|  |                     | 2476                                 | 2376                        | 2237                         | (P5)    |          |
| Summer gain/loss ratio                                 |                     | 3.27                                 | 3.14                        | 2.96                         | (P6)    |          |
| Summer external temperature                            |                     | 15.40                                | 17.80                       | 17.80                        |         |          |
| Thermal mass temperature increment (TMP = 250.0)       |                     | 0.00                                 | 0.00                        | 0.00                         |         |          |
| Threshold temperature                                  |                     | 18.92                                | 21.19                       | 21.01                        | (P7)    |          |
| Likelihood of high internal temperature                |                     | Not significant                      | Slight                      | Slight                       |         |          |
| Assessment of likelihood of high internal temperature: |                     | Slight                               |                             |                              |         |          |

# 8.2: Appendixes :

## Energy / Renewable Energy Statement

CALCULATION DETAILS for survey reference no 'PVs'  
SAP 2009 IMPROVEMENTS

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SAP 2009 IMPROVEMENTS  
Calculated by program Elmhurst Energy Systems SAP2009 Calculator (Design System) version 3.07r18

21686\_New Oxford Street\_08Flat

Current energy efficiency rating: B 83  
Current environmental impact rating: B 84

(For testing purposes):

|                                  |                   |
|----------------------------------|-------------------|
| A                                | Not considered    |
| B                                | Not considered    |
| C                                | Not considered    |
| D                                | Not considered    |
| E Low energy lighting            | Already installed |
| F                                | Not considered    |
| G                                | Not considered    |
| H                                | Not considered    |
| I                                | Not considered    |
| J                                | Not considered    |
| K                                | Not considered    |
| L                                | Not considered    |
| M                                | Not considered    |
| N Solar water heating            | Not applicable    |
| O                                | Not considered    |
| P                                | Not considered    |
| Q                                | Not considered    |
| R                                | Not considered    |
| S                                | Not considered    |
| T                                | Not considered    |
| U Solar photovoltaic (PV) panels | Not applicable    |
| V Wind turbine                   | Not applicable    |

Recommended measures:  
(none)

Typical annual savings Energy Environmental  
efficiency impact

Lower cost measures  
(none) Sub Total £0 0.0000 kg/m²

Higher cost measures  
(none) Sub Total £0 0.0000 kg/m²

Potential energy efficiency rating: B 83  
Potential environmental impact rating: B 84

Further improvements to achieve even higher standards  
(none) Total Savings £0 0.0000 kg/m²

Enhanced energy efficiency rating: B 83  
Enhanced environmental impact rating: B 84

Fuel prices for cost data on this page from database revision number 327 TEST (31 Aug 2012)  
Recommendation tests revision number 3.9c (09 Jan 2012)

Typical heating and lighting costs of this home (per year):

|                          | Current    | Potential  | Enhanced   |
|--------------------------|------------|------------|------------|
| Electricity              | £71        | £71        | £71        |
| Main gas                 | £387       | £387       | £387       |
| Space heating            | £327       | £327       | £327       |
| Water heating            | £23        | £23        | £23        |
| Lighting                 | £49        | £49        | £49        |
| Generated (PV)           | -£66       | -£66       | -£66       |
| Total cost               | £393       | £393       | £393       |
| Carbon dioxide emissions | 1.6 tonnes | 1.6 tonnes | 1.6 tonnes |
| Primary energy           | 91 kWh/m²  | 91 kWh/m²  | 91 kWh/m²  |

## 8.2: Appendixes : Energy / Renewable Energy Statement

## 8.3: Appendixes : Sustainability Statement

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Project No: 21686  
Report: v1  
Prepared for: Zania Universal  
Prepared by: Stathis Eleftheriadis  
Date: 19/12/2012

**PRICE & MYERS**

BREEAM Domestic Refurbishment

### Disclaimer

This report is produced on behalf of Price & Myers LLP. By receiving the report and acting on it, the client or any third party relying on it accepts that no individual is personally liable in contract, tort or breach or statutory duty (including negligence).

112-116 New Oxford Street

BREEAM Domestic Refurbishment Pre-Assessment Report

  
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## 8.3: Appendixes : Sustainability Statement

### Executive Summary

Price & Myers has been commissioned by Zania Universal to carry out a BREEAM pre-assessment for the 112-116 New Oxford Street development. The project involves the refurbishment of an existing property in the London Borough of Camden. The proposed 7-storey development comprises of 7 refurbished flats and 1 additional new flat on the roof top.

This report demonstrates that the refurbished dwellings have the potential to achieve a score of 68.85%, which equates to a Very Good rating.

The report details the performance of the 112-116 New Oxford Street development against the BREEAM Domestic Refurbishment criteria. The current score based on the credits targeted by the design team is 68.85%, which equates to a Very Good rating. This provides a buffer over the target score of 55% (the threshold for Very Good ratings) should credits be lost through design or cost constraints as the project progresses.

Credits such as the daylighting and cycle storage are currently potential credits, as these could be implemented later in the project should additional credits be required.

It is key for the design team to remain in contact with the assessor throughout the process and to check that all specifications are in line with the pre-assessment to ensure the required level is achieved upon construction.

### Contents

#### Contents

1. Introduction
2. BREEAM Refurbishment - Domestic Buildings
3. Score Summary
4. Credit Summary
5. Conclusion

#### Appendices

### 1. Introduction

Price & Myers has been commissioned to carry out a Preliminary BREEAM (BRE Environmental Assessment Method) Domestic Refurbishment assessment of the 112-116 New Oxford Street development for Zania Universal.

The development involves the refurbishment and extension of an existing property in the London Borough of Camden. The development will involve 1 additional storey being added to the property, resulting in 8 flats within a 7-storey building.



Fig 1 - Proposed front view of the 112-116 New Oxford Street development

The proposed development is mainly contained within the existing envelope of the building, with a new roof and walls being installed for the 7th floor flat.

Therefore the BREEAM Domestic Refurbishment scheme is applicable to this development. The London Borough of Camden requires dwellings to achieve a Very Good rating on the BREEAM Domestic Refurbishment scheme and minimum standards (% of un-weighted credits) for Energy, Water & Materials sections to be 60%, 60% & 40% respectively. The additional floor will create an entirely new building. The BREEAM for Domestic Refurbishment scheme cannot be applied to this one unit, as it is considered new build. The new flat will be designed to meet similar sustainability standards and improvement over Part L. This assessment applies to flat 1-7

This report comprises a pre-assessment of the development against the BREEAM Domestic Refurbishment scheme in support of the planning application. It concludes the BREEAM score and rating that the development can achieve based on the individual credits targeted by the design team.

# 8.3: Appendixes : Sustainability Statement

## 2. BREEAM Refurbishment - Domestic Buildings

BREEAM Domestic Refurbishment is a performance based assessment method and certification scheme for domestic buildings undergoing refurbishment.

The primary aim of the scheme is to improve the environmental performance of existing dwellings in a robust and cost effective manner. The performance of the dwelling on the scheme is quantified by a number of individual measures and associated criteria stretching across a range of environmental issues, categorised into the following sections:

- Management
- Health and Wellbeing
- Energy
- Water
- Materials
- Pollution
- Waste
- Innovation

### BREEAM Scoring

Within each of the BREEAM categories outlined above, there are a number of credit requirements that reflect the options available to designers and managers of buildings.

An environmental weighting is applied to the scores achieved under each category, illustrated in Table 3.1, in order to calculate the final BREEAM score. The weighting factors have been derived from consensus based research with various groups such as government, material suppliers and lobbyists. This research was carried out by BRE to establish the relative importance of each environmental issue.

The current rating benchmarks for this BREEAM scheme are detailed in the table below:

| BREEAM Rating | % Score |
|---------------|---------|
| Outstanding   | ≥ 85    |
| Excellent     | ≥ 70    |
| Very Good     | ≥ 55    |
| Good          | ≥ 45    |
| Pass          | ≥ 30    |
| Unclassified  | < 30    |

Table 2.1 - BREEAM rating benchmarks

## Minimum Standards

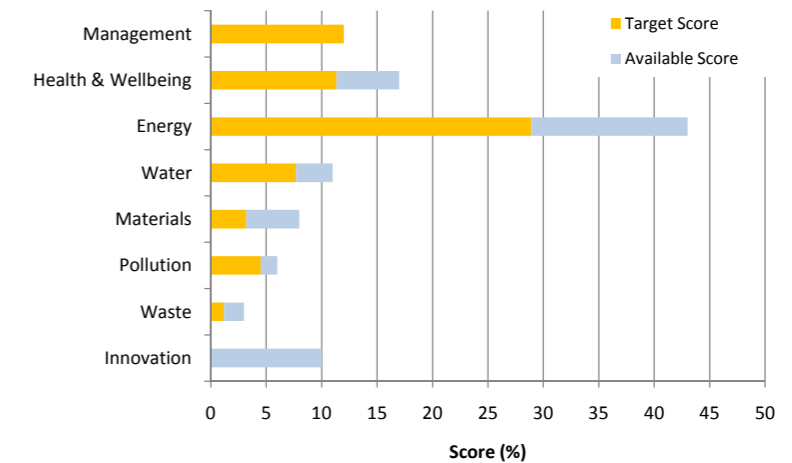
In order to achieve particular benchmark scores, there is a minimum performance requirement within the BREEAM schemes. The minimum performance requirements are detailed in the table below and a project cannot achieve a particular rating unless the minimum requirements have been met, irrespective of the overall percentage score.

| BREEAM Issue  | Minimum standards by rating level |                  |                  |                  |                  |
|---|-----------------------------------|------------------|------------------|------------------|------------------|
|   | Pass                              | Good             | Very Good        | Excellent        | Outstanding      |
| Ene 02: Energy Efficiency Rating Post Refurbishment | 0.5 Credits                       | 1 Credit         | 1.5 Credits      | 2.5 Credits      | 3.5 Credits      |
| Wat 01: Internal Water Use                          | -                                 | -                | 1 Credit         | 2 Credits        | 3 Credits        |
| Hea 05: Ventilation                                 | 1 Credit                          | 1 Credit         | 1 Credit         | 1 Credit         | 1 Credit         |
| Hea 06: Safety                                      | 1 Credit                          | 1 Credit         | 1 Credit         | 1 Credit         | 1 Credit         |
| Pol 03: Flooding                                    | -                                 | -                | -                | 2 Credits        | 2 Credits        |
| Mat 02: Responsible Sourcing of Materials           | Criterion 3 only                  | Criterion 3 only | Criterion 3 only | Criterion 3 only | Criterion 3 only |

Table 2.2 - Minimum BREEAM standards

## 3. Score Summary

The potential BREEAM score of the development has been determined based on discussions with the design team and is currently expected to achieve the following:



| BREEAM Section            | Credits Available | Credits Targeted | % of Credits Achieved | Section Weighting | Section Score    |
|---------------------------|-------------------|------------------|-----------------------|-------------------|------------------|
| Management                | 11                | 11               | 100.0%                | 12%               | 12.00            |
| Health & Wellbeing        | 12                | 8                | 66.7%                 | 17%               | 11.33            |
| Energy                    | 29                | 19.5             | 67.2%                 | 43%               | 28.91            |
| Water                     | 5                 | 3.5              | 70.0%                 | 11%               | 7.70             |
| Materials                 | 45                | 18               | 40.0%                 | 8%                | 3.20             |
| Pollution                 | 8                 | 6                | 75.0%                 | 6%                | 4.50             |
| Waste                     | 5                 | 2                | 40.0%                 | 3%                | 1.20             |
| Innovation                | 10                | 0                | 0.0%                  | 10%               | 0.00             |
| <b>Final BREEAM Score</b> |                   |                  |                       |                   | <b>68.85</b>     |
| <b>BREEAM Rating</b>      |                   |                  |                       |                   | <b>Very Good</b> |

Table 3.1 - Breakdown of the BREEAM score and rating

| Rating Level               | Minimum BREEAM Standards |      |           |           |             |
|----------------------------|--------------------------|------|-----------|-----------|-------------|
|                            | Pass                     | Good | Very Good | Excellent | Outstanding |
| Minimum Standards Achieved | Yes                      | Yes  | Yes       | No        | No          |

This report demonstrates that the 112-116 New Oxford Street development has met all of the minimum standards and can achieve a Very Good rating on the BREEAM Domestic Refurbishments scheme.



# 8.3: Appendixes : Sustainability Statement

## 4. Credit Summary

The following section details the BREEAM credits assessed under the scheme and whether they will be targeted for the 112-116 New Oxford Street development.

| Credit  | Criteria  | Available Score (%) | Status               | Targeted Score (%) | Pre-Assessment Stage Assumptions  |
|---|---|---------------------|----------------------|--------------------|---|
| <b>MANAGEMENT</b>   |   |                     |                      |                    |   |
| <b>Man 01</b> Home Users Guide                                  | Where a Home User Guide containing the information listed in the 'User Guide Contents List' has been produced and supplied to all homes   | 3.27                | Targeted             | 3.27               | A Home User Guide will be produced containing the information listed in the User Guide Content List.  |
| <b>Man 02</b> Responsible Construction Practices                | CCS Score 25 - 34<br>CCS Score 35 - 39  | 1.09<br>1.09        | Targeted<br>Targeted | 1.09<br>1.09       | The contractor will be expected to achieve a score of at least 35 on the CCS(a score of 7 in each of the 5 sections must be achieved).  |
| <b>Man 03</b> Construction Site Impacts                         | Where 2 or more of the following construction site impact actions are taken:<br>a. Monitor, report and set targets for CO2 production of energy use arising from site activities<br>b. Monitor, report and set targets for water consumption arising from site activities<br>c. A main contractor with an environmental materials policy<br>d. A main contractor that operates an Environmental Management System<br>e. 80% of site timber is reclaimed, re-used or responsibly sourced (And 100% is legally sourced) | 1.09                | Targeted             | 1.09               | The contractor will be expected to monitor and record activities on site during the construction works, to confirm that all site timber used on the project is sourced in accordance with the UK Government's Timber Procurement Policy and have EMS that follows best practice for pollution policies.     |
| <b>Man 04</b> Security  | Existing doors and windows meet minimum security requirement and new ones are appropriately certified<br>Achieve Secure by Design and implement the recommendations having consulted with an ALO or CPDA  | 1.09<br>1.09        | Targeted<br>Targeted | 1.09<br>1.09       | All doors and windows will be replaced/new and will meet the required PAS or LPS standards.<br>The design team have consulted with an ALO/CPDA and will implement their recommendations.<br>The design team will also achieve Secure by Design compliance.  |
| <b>Man 05</b> Protection and Enhancement of Ecological Features | Site survey carried out and any ecological aspects protected during site works (and no ecological features are removed)   | 1.09                | Targeted             | 1.09               | A member of the design team will carry out a site survey and all existing features of ecological value will be protected during the works.  |
| <b>Man 06</b> Project Management                                | Assign project roles and responsibilities<br>A handover meeting is arranged AND<br>2 or more of the following are committed to:<br>a. A site inspection within 3 months of occupation<br>b. Conduct post occupancy interviews with building occupants or a survey via phone or posted information within 3 months of occupation<br>c. Longer term after care e.g. a helpline, nominated individual or other appropriate system to support building users for at least the first 12 months of occupation               | 1.09<br>1.09        | Targeted<br>Targeted | 1.09<br>1.09       | The project manager will be expected to write a project implementation plan and hold an initiation meeting to assign individual and shared responsibilities amongst the project team including all trades on site.<br>A handover meeting will be arranged and at least 2 of the listed actions carried out. |

| Credit  | Criteria  | Available Score (%)  | Status                            | Targeted Score (%)   | Pre-Assessment Stage Assumptions   |
|---|---|----------------------|-----------------------------------|----------------------|--|
| <b>HEALTH &amp; WELLBEING</b>                   |   |                      |                                   |                      |  |
| <b>Hea 01</b> Daylighting                       | Existing dwellings and change of use projects (e.g. conversions) the refurbishment results in a neutral impact on the dwellings daylighting levels in the kitchen, living room, dining room and study<br>Where the property is being extended the new spaces achieve minimum daylighting levels and the extension does not reduce daylighting levels in the kitchen, living room, dining room or study of neighbouring properties<br>Dwelling achieves minimum daylighting levels in the kitchen (2%), living room, dining room and study (1.5%) + 80% of working plane receives direct sunlight  | 1.42                 | Potential                         | 1.42                 | It is currently unclear whether the credits can be achieved as the view of the sky is questionable. If calculations are undertaken this may be achievable.   |
| <b>Hea 02</b> Sound Insulation                  | Compliance with Part E<br>3dB improvement over Part E<br>5dB improvement over Part E  | 2.83<br>1.42<br>1.42 | Targeted<br>Targeted<br>Targeted  | 2.83<br>1.42<br>1.42 | The building is expected to achieve an airborne and impact sound attenuation performance 5dB better than that required by the Building Regulations through the use of robust detailing. A programme of pre-completion testing should be carried out by a compliant test body based on the normal programme of testing described in the Building Regulations or Standards for every flat or room for residential purposes |
| <b>Hea 03</b> Volatile Organic Compounds (VOCs) | Avoiding the use of VOCs in compliance with the BREEAM table  | 1.42                 | Potential                         | 1.42                 | All applicable internal finishes and fittings will be specified to avoid the use of volatile organic compounds (VOCs) but it is challenging to obtain appropriate evidence.  |
| <b>Hea 04</b> Inclusive Design                  | An access expert or suitably qualified member of the design team has completed section 1 of Checklist A8; Access Statement Template (An architect is expected to satisfy the requirements)<br>An access expert or suitably qualified member of the design team has completed sections 1 and 2 of Checklist A8; Access Statement Template (An architect is expected to satisfy the requirements)   | 1.42<br>1.42         | Targeted<br>Targeted              | 1.42<br>1.42         | A suitably qualified member of the design team will complete the access statement to demonstrate reasonable provision to provide accessibility to the dwelling, covering sections 1 and 2 of Checklist A-8. Refer to Appendix B2 for full details of Checklist A-8.  |
| <b>Hea 05</b> Ventilation                       | Minimum background ventilation in the form of trickle ventilation (or an equivalent means of ventilation) should be provided as follows:<br>- Habitable rooms: 5000mm <sup>2</sup> equivalent area;<br>- Kitchens, utility rooms and bathrooms: 2500mm <sup>2</sup> equivalent area;<br>- New rooms (in the case of an extension): 8000mm <sup>2</sup> equivalent area;<br>And a minimum level of extract ventilation is provided in all wet rooms (e.g. kitchen, utility and bath-rooms), compliant with section 5 of AD Part F 2010;<br>And a minimum level of purge ventilation is provided in all habitable rooms and wet rooms, compliant with section 7 of AD Part F 2010<br>Ventilation is provided for the dwelling that meets the requirements of Section 5 of Building Regulations Part F in full | 1.42<br>1.42<br>1.42 | Targeted<br>Targeted<br>Potential | 1.42<br>1.42<br>1.42 | Minimum background and extract ventilation will be provided to the flats in compliance of Section 5 in AD Part F 2010.<br>If possible, ventilation will be upgraded to achieve the 2nd credit.   |
| <b>Hea 06</b> Safety                            | Where the dwelling is supplied with mains gas or where any other form of fossil fuel is used within the building (e.g. coal), a compliant fire and carbon monoxide detector and alarm system is provided;<br>Where the project involves electrical re-wiring the power supply for the smoke alarm and compliant carbon monoxide alarm systems are derived from the dwelling's main electricity supply (and not battery powered)   | 1.42                 | Targeted                          | 1.42                 | As the dwelling is supplied with mains gas a compliant fire and carbon monoxide detector and alarm system will be provided.<br>The power supply for the smoke alarm and compliant carbon monoxide alarm systems must be derived from the dwelling's main electricity supply (and not battery powered)  |

| Credit  | Criteria  | Available Score (%)  | Status   | Targeted Score (%)   | Pre-Assessment Stage Assumptions   |
|---|---|--|--|--|--|
| <b>ENERGY</b>   |   |  |  |  |  |
| <b>Ene 01</b> Improvement in Energy Efficiency Rating     | ≥ 5 Improvement in EER as calculated from SAP 2009<br>≥ 9 Improvement in EER<br>≥ 13 Improvement in EER<br>≥ 17 Improvement in EER<br>≥ 21 Improvement in EER<br>≥ 26 Improvement in EER<br>≥ 31 Improvement in EER<br>≥ 36 Improvement in EER<br>≥ 42 Improvement in EER<br>≥ 48 Improvement in EER<br>≥ 54 Improvement in EER<br>≥ 60 Improvement in EER  | 0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74                 | Targeted<br>Targeted<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable<br>Not Achievable | 0.74<br>0.74<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00<br>0.00                 | Preliminary SAP calculations carried out by Price & Myers show that the improvement in EER from the existing property to the proposed dwelling is 9.7(Refer to Energy Strategy Report).  |
| <b>Ene 02</b> Energy Efficiency Rating Post Refurbishment | ≥ 50 EER rating post refurbishment as calculated from SAP 2009<br>≥ 55 EER rating post refurbishment<br>≥ 60 EER rating post refurbishment<br>≥ 65 EER rating post refurbishment<br>≥ 70 EER rating post refurbishment<br>≥ 75 EER rating post refurbishment<br>≥ 80 EER rating post refurbishment<br>≥ 85 EER rating post refurbishment  | 0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74   | Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Not Achievable   | 0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.00   | Preliminary SAP calculations carried out by Price & Myers show that the post refurbishment EER is 82.75.(Refer to Energy Strategy Report).   |
| <b>Ene 03</b> Primary Energy Demand                       | ≤ 400 kWh/m <sup>2</sup> /yr as calculated from SAP 2009<br>≤ 370 kWh/m <sup>2</sup> /yr<br>≤ 340 kWh/m <sup>2</sup> /yr<br>≤ 320 kWh/m <sup>2</sup> /yr<br>≤ 300 kWh/m <sup>2</sup> /yr<br>≤ 280 kWh/m <sup>2</sup> /yr<br>≤ 260 kWh/m <sup>2</sup> /yr<br>≤ 240 kWh/m <sup>2</sup> /yr<br>≤ 220 kWh/m <sup>2</sup> /yr<br>≤ 200 kWh/m <sup>2</sup> /yr<br>≤ 180 kWh/m <sup>2</sup> /yr<br>≤ 160 kWh/m <sup>2</sup> /yr<br>≤ 140 kWh/m <sup>2</sup> /yr<br>≤ 120 kWh/m <sup>2</sup> /yr  | 0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74 | Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted<br>Targeted                                     | 0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74<br>0.74 | Preliminary SAP calculations carried out by Price & Myers show a Primary Energy Demand of 101.75 kWh/m <sup>2</sup> /yr.   |
| <b>Ene 04</b> Renewable Technologies                      | ≥10% of Primary Energy Demand per annum is by LZC technologies AND<br>The dwelling has reduced energy demand prior to the specification of renewable technologies (Must use MCS certified products and installers)  | 1.48   | Not Achievable   | 0.00   | This credit is not currently being targeted, as the PV system will not save 10% for this development. However it is listed as a potential credit since LZC technologies could be implemented late on in the project.(Refer to Energy Strategy Report)  |
| <b>Ene 05</b> Energy Labelled White Goods                 | Fridges and freezers or fridge-freezers are recognised by the Energy Saving Trust Recommended labelling scheme<br>OR<br>If no white goods are provided to the dwelling(s), a EU Energy Efficiency Labelling Scheme Information Leaflet is provided to each dwelling<br>Washing machines and dishwashers are recognised by the Energy Saving Trust Recommended labelling scheme, carrying the Energy Saving Trust Recommended Label AND<br>Washer dryers and tumble dryers have a B rating under the EU Energy Efficiency Labelling Scheme<br>OR<br>Where a washer dryer or tumble dryer is not provided, the EU Energy Efficiency Labelling Scheme Information Leaflet is provided to each dwelling | 1.48<br>1.48   | Targeted<br>Targeted   | 1.48<br>1.48   | The specified fridge-freezers will be recognised by the Energy Saving Trust Recommended labelling scheme and carry the Energy Saving Trust Recommended Label.<br>The specified washing machines and dishwashers will be recognised by the Energy Saving Trust Recommended labelling scheme and carry the Energy Saving Trust Recommended Label.<br>Washer dryers and tumble dryers will have a B rating under the EU Energy Efficiency Labelling Scheme or if not specified, EU Energy Efficiency Labelling Scheme Information Leaflet is provided to each dwelling. |

# 8.3: Appendixes : Sustainability Statement

| Credit                               | Criteria   | Available Score (%) | Status         | Targeted Score (%) | Pre-Assessment Stage Assumptions  |
|--------------------------------------|--|---------------------|----------------|--------------------|---|
| <b>Ene 06</b> Drying Space           | Adequate (permanent) internal or external drying line of 4m+ (1-2 bed) or 6m+ (3+ bed)<br><br>This is either: a heated space with adequate, controlled ventilation, complying with AD Part F 2006, or an unheated outbuilding  | 1.48                | Targeted       | 1.48               | An adequate, secure internal space with posts and footings, or fixings holding will be provided   |
| <b>Ene 07</b> Lighting               | External Lighting - Energy efficient space lighting and security lighting (if present) is provided<br>AND<br>Appropriate control systems i.e. Passive Infra Red (PIR), 'Dusk to Dawn' daylight sensors or time switches  | 1.48                | Targeted       | 1.48               | Energy Efficient Space lighting (including lighting in communal areas) and Energy Efficient Security lighting (where applicable) will be provided to external areas, along with appropriate controls.   |
|                                      | Internal Lighting - Maximum average wattage across the total floor area of the dwelling of 9 W/m <sup>2</sup>  | 1.48                | Targeted       | 1.48               | The internal lighting will be designed such that the maximum average wattage across the total floor area of the dwelling of 9 watts/m <sup>2</sup> .  |
| <b>Ene 08</b> Energy Display Devices | Current electricity consumption OR<br>Current primary heating fuel consumption data is displayed to occupants<br><br>Current electricity AND primary heating fuel consumption data are displayed to occupants<br>OR<br>Where electricity is the primary heating fuel and current electricity consumption data are displayed to occupants | 0.00                | Targeted       | 0.00               | Current electricity and primary heating fuel consumption data will be displayed to occupants by a compliant Energy Display Device (or Visual Display Unit).   |
|                                      |  | 2.97                | Targeted       | 2.97               | An additional exemplary credit is available where the EDD has the capability to record and store energy consumption data.   |
| <b>Ene 09</b> Cycle Storage          | Studios or 1 bed - 1 cycle for every two dwellings<br>2/3 bed - 1 cycle per dwelling<br>4+ bed - 2 cycles per dwelling<br><br>Studios or 1 bed - 1 cycle per dwelling<br>2/3 bed - 2 cycle per dwelling<br>4+ bed - 4 cycles per dwelling  | 1.48                | Potential      | 1.48               | There is a storage room within the basement of the property which can be utilised as a cycle storage. In order to meet the requirements 1 cycle space will need to be provided for every 1, 2 and 3 bed flats.  |
|                                      |  | 1.48                | Not Achievable | 0.00               |   |
| <b>Ene 10</b> Home Office            | Sufficient space and services for a home office:<br>- 1.8m wall length space<br>- Two double power sockets<br>- Telephone point<br>- Window (either the width and height are to be >450mm)<br>- Adequate ventilation (0.5m <sup>2</sup> openable area or meet credit HEA 05)   | 1.48                | Targeted       | 1.48               | A space and facilities for a home office will be provided in each flat.<br><br>For the dwellings with 3+ bedrooms, this will be in a room other than the kitchen, living room, master bedroom or bathroom.<br><br>For the 2 bed dwelling, this will be in a room other than the kitchen, living room or bathroom. |

| Credit              | Criteria  | Available Score (%) | Status   | Targeted Score (%) | Pre-Assessment Stage Assumptions |
|---------------------|---|---------------------|----------|--------------------|----------------------------------|
| <b>WATER</b>        |   |                     |          |                    |                                  |
| <b>Wat 01</b> Water | Water fitting will be specified such that the Total Water | 1.10                | Targeted | 1.10               |                                  |

| Credit  | Criteria   | Available Score (%) | Status         | Targeted Score (%) | Pre-Assessment Stage Assumptions   |
|---|--|---------------------|----------------|--------------------|--|
| <b>MATERIALS</b>                                |  |                     |                |                    |  |
| <b>Mat 01</b> Environmental Impact of Materials | Assessment of the following building elements based on their Green Guide to Specification rating and Thermal Performance:<br><br>- Roof<br>- External Walls<br>- Internal Walls (Including separating walls)<br>- Upper and Ground Floor<br>- Windows  | 0.18                | Targeted       | 0.18               | The following materials have been proposed:<br><br>- Roof (Metal roof)<br><br>- External Walls (Retained brickwork/blockwork)<br><br>- Internal Walls (Timber/Metal stud and blockwork for party & separating walls)<br><br>- Upper and Ground Floor (Retained Concrete Floors)<br><br>- Windows (Metal Sash frame)<br><br>It is expected that 10 credits can be achieved.               |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
| <b>Mat 02</b> Responsible Sourcing of Materials | Based on responsible sourcing tier for materials within the building elements, fixtures and fittings<br>≥9% Achieved in BREEAM Calculator Tool<br><br>≥18% Achieved in BREEAM Calculator Tool<br><br>≥27% Achieved in BREEAM Calculator Tool<br><br>≥36% Achieved in BREEAM Calculator Tool<br><br>≥45% Achieved in BREEAM Calculator Tool<br><br>≥54% Achieved in BREEAM Calculator Tool<br><br>All new timber is sourced in line with the UK Gov's Timber Procurement Policy | 0.36                | Targeted       | 0.36               | Materials will be responsibly sourced (i.e. FSC, PEFC, EMS certification) as to achieve at least 18% of credits within the BREEAM Mat 02 calculator tool.<br><br>All new timber and wood-derived products will be sourced from only independently verifiable legal and sustainable sources or FLEGT (forest law enforcement, governance and trade) licensed timber or equivalent timber. |
|   |  | 0.36                | Targeted       | 0.36               |  |
|   |  | 0.36                | Not Achievable | 0.00               |  |
|   |  | 0.36                | Not Achievable | 0.00               |  |
|   |  | 0.36                | Not Achievable | 0.00               |  |
|   |  | 0.36                | Not Achievable | 0.00               |  |
| <b>Mat 03</b> Insulation                        | Where the (BREEAM) Insulation Index for new insulation used in the buildings is ≥2 based on the Green Guide rating and thermal performance for insulation within the:<br>- External walls<br>- Ground floor<br>- Roof<br>- Building services<br><br>Where ≥ 80% of the new thermal insulation used in the building elements is responsibly sourced (for key processes and supply chain)  | 0.18                | Targeted       | 0.18               | All new insulation for external walls, roof and building services will be specified with a Green Guide rating of A or A+ (where possible) to achieve at least 2 credits.<br><br>At least 80% of the new thermal insulation will be responsibly sourced (i.e. with EMS certification).  |
|   |  | 0.18                | Targeted       | 0.18               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
|   |  | 0.18                | Not Achievable | 0.00               |  |
| <b>POLLUTION</b>                                |  |                     |                |                    |  |
| <b>Pol 01</b> Nitrogen Oxide Emissions (NOx)    | Dry NOx emissions of space heating and hot water systems are <100 mg/kWh<br><br>Dry NOx emissions of space heating and hot water systems are <70 mg/kWh<br><br>Dry NOx emissions of space heating and hot water systems are <40 mg/kWh   | 0.75                | Targeted       | 0.75               | The current M&E strategy is to use gas fired boilers and so it is expected that the dry NOx emissions will be less than 40 mg/kWh.   |
|   |  | 0.75                | Targeted       | 0.75               |  |
|   |  | 0.75                | Targeted       | 0.75               |  |
| <b>Pol 02</b> Surface Water Runoff              | Neutral impact on surface water<br>Reducing run-off from site: Basic<br><br>Reducing run-off from site: Advanced   | 0.75                | Targeted       | 0.75               | The existing site is impermeable and the proposed site will not add any landscaping. Therefore a neutral impact on surface water run-off is expected.<br><br>The additional credits are not expected to be achieved as compliant SUDS (infiltration) will not be provided for this development.  |
|   |  | 0.75                | Not Achievable | 0.00               |  |
| <b>Pol 03</b> Flooding                          | Flood Risk Assessment (FRA) carried out and a Low Flood Risk   | 1.50                | Targeted       | 1.50               | A Flood Risk Assessment (FRA) will be carried out and the assessed dwellings are defined as having a low   |

| Credit                                 | Criteria  | Available Score (%) | Status         | Targeted Score (%) | Pre-Assessment Stage Assumptions  |
|--|---|---------------------|----------------|--------------------|---|
| <b>WASTE</b>                           |   |                     |                |                    |   |
| <b>Was 01</b> Household Waste          | If a LA or private collection scheme in place:<br>- 3 internal recycling containers provided where recycling is not sorted post collection<br>- 1 internal recycling container provided where recycling is sorted post collection<br>- Minimum 30l total capacity, no single container less than 7l<br>- Dedicated location   | 0.60                | Targeted       | 0.60               | A LA collection scheme exists and 3 internal recycling containers (in addition to a container for non-recyclable waste) will be provided within a kitchen cupboard. The bins will each have a capacity of at least 7l, with a total capacity (of the 3 bins) of at least 30l. |
|  | Private external space ≥ 4.5m <sup>2</sup> (Houses) or ≥ 1m <sup>2</sup> per bedroom (Flats):<br>Where a composting service or facility is provided for green/garden waste, kitchen waste and an interior container is provided for kitchen composting waste of at least 7l   | 0.60                | Potential      | 0.60               | There are no current plans to provide composting facilities, however this credit could be targeted at a later date should other credits be lost.  |
|  | Private external space < 4.5m <sup>2</sup> (Houses) or < 1m <sup>2</sup> per bedroom (Flats):<br>Where a composting service or facility is provided for kitchen waste and an interior container is provided for kitchen composting waste of at least 7l   | 0.60                | Potential      | 0.60               |   |
| <b>Was 02</b> Refurbishment Site Waste | A compliant SWMP is in place<br><br>First credit achieved<br><br>Where Non-hazardous construction waste generated by the dwellings refurbishment is ≤26.52m <sup>3</sup> or 16.9 Tonnes (per £110k project value)<br><br>Where the amount of waste generated against £100k of project value is recorded in the SWMP<br><br>Where a pre-refurbishment audit of the existing building is completed<br>Where the demolition is included as part of the refurbishment programme, then the audit should also cover demolition materials<br><br>First 2 credits achieved<br><br>≤ 70% (by volume) or 60% (by Tonnes) of non-hazardous construction waste is diverted from landfill<br><br>AND<br>≤ 80% (by volume) or 90% (by Tonnes) of non-hazardous demolition waste is diverted from landfill | 0.60                | Targeted       | 0.60               | A Site Waste Management Plan will be put into place for this development.   |
|  |   | 0.60                | Potential      | 0.60               | This credit is not being targeted as the waste generated cannot be accurately predicted at this stage. The credits may still be achievable if waste levels are recorded.  |
|  |   | 0.60                | Not Achievable | 0.00               |   |

# 8.3: Appendixes : Sustainability Statement

| Credit  | Criteria   | Available Score (%) | Status         | Targeted Score (%) | Pre-Assessment Stage Assumptions  |
|---|--|---------------------|----------------|--------------------|---|
| <b>INNOVATION</b>   |  |                     |                |                    |   |
| <b>Man 02</b> Responsible Construction Practices                | CCS Score 40 +   | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Man 05</b> Protection and Enhancement of Ecological Features | SQE appointed and adopt all general ecological recommendations and 30% of additional recommendations | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Man 06</b> Project Management                                | BREEAM Accredited Professional (AP) has been appointed   | 1.00                | Potential      | 1.00               | This credit is not currently targeted, but could be achieved is a BREEAM AP attends key meetings and produces written reports to the design team. |
|   | Thermographic Surveying and Airtightness Testing carried out   | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Hea 04</b> Inclusive Design                                  | Lifetime Homes and Part M compliance   | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Ene 02</b> Energy Efficiency Rating Post Refurbishment       | ≥ 90 EER rating post refurbishment   | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
|   | ≥ 100 EER rating post refurbishment  | 1.00                | Not Achievable | 0.00               |   |
| <b>Ene 06</b> Energy Display Devices                            | Where any specified Energy Display Devices is capable of recording consumption data                  | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Wat 01</b> Water Consumption                                 | ≤ 80 litres / person / day   | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Pol 02</b> Surface Water Runoff                              | Where all run-off from the developed site is managed on site using source control                    | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |
| <b>Was 02</b> Refurbishment Site Waste                          | SWMP implemented and achieving higher waste reduction targets  | 1.00                | Not Achievable | 0.00               | This credit is not being targeted.  |

### 5. Conclusion

This pre-assessment report details the expected BREEAM score and rating for the 112-116 New Oxford Street development, which comprises the refurbishment of a residential property situated in the London Borough of Camden.

It demonstrates that a Very Good rating can be achieved, with a score of 68.85%, based on the credits targeted by the design team. The development performs especially well within the Energy, Management and Pollution sections. The minimum credits under Energy, Water & Materials have been achieved as per Borough of Camden.

Additional credits have been highlighted as potential credits, such as the daylighting and cycle storage, as these can be adopted later on in the project should additional credits be required.

It is key for the design team to remain in contact with the assessor throughout the process and to check that all specifications are in line with the pre-assessment to ensure that the credit criteria is followed through into the design stages and that the required BREEAM rating is achieved upon construction.

### Appendices

#### Appendix A - Management

- A1: MAN 01 - Home Users Guide
- A2: Man 03 - Construction Site Impacts
- A3: Man 04 - Security
- A4: Man 06 - Project Management

#### Appendix B - Health & Wellbeing

- B1: Hea 03 - VOCs
- B2: Hea 04 - Inclusive Design

#### Appendix C - Energy

- C1: Ene 07 - Lighting
- C2: Ene 08 - Energy Display Devices
- C3: Ene 09 - Cycle Storage

#### Appendix D - Materials

- D1: Mat 02 - Responsible Sourcing of Materials
- D2: Mat 03 - Insulation

#### Appendix E - Pollution

- E1: Pol 02 - Surface Water Run-off

#### Appendix F - Waste

- F1: Was 02 - SWMP

# 8.3: Appendixes : Sustainability Statement

APPENDIX

BREEAM Domestic Refurbishment

APPENDIX

BREEAM Domestic Refurbishment

APPENDIX

BREEAM Domestic Refurbishment

## Appendix A - Management

### A1: MAN 01 – Home Users Guide

The list below indicates the type of information that should be included in the Home Users Guide and provided to occupants at handover. Where such features are not relevant to the dwelling (e.g. there are no renewables) or this is an occupied home and residents are already familiar with surrounding area (e.g. location of local amenities), information can be excluded from the Home Users Guide.

#### About BREEAM Domestic Refurbishment

Background about the scheme, category areas, scoring system (all of this information can be found at the front of the manual).

A copy or photocopy of the BREEAM Domestic Refurbishment certificate should also be provided with a summary of the environmental features that have been designed into the dwelling to help achieve the rating.

#### Recommendations report

A recommendations report for how the homes could be improved in the future including:

- How to improve the home to the next BREEAM Domestic Refurbishment rating band covering each category
- Use of sustainable material including low VOC materials, responsible sourcing and the Green Guide
- Use of contractors with good green credentials including site waste management, use of considerate constructors scheme or similar and awareness of environmental impacts
- Sources of further guidance on how to improve the home e.g. EST, Green Deal Advisors
- Information on potential funding mechanisms e.g. the Green Deal, Feed in Tariffs etc.
- How to obtain an assessment for future refurbishment work

#### Energy Efficiency

Information on energy-efficient features and strategies relating to the home, and also provide an overview of the reasons for their use, e.g. economic and environmental savings. Information could include:

- Information on the effective operation and reason for the use (e.g. environmental economic savings) of environmental features/design strategies such as passive solar design, super insulation, energy efficient timber windows, heat recovery systems, solar hot water systems, photovoltaics, passive vents or the use of certified timber or SUDS within the boundary of individual properties.
- Tips on other energy saving measures such as not leaving electrical appliances on standby etc and the cost/environmental savings they can give.
- Information as described in the Building Regulations ADL1b (requirement note L1c) (1) i.e. Sufficient information about the building and its building services and their maintenance requirements so that the building can be operated in such a manner as to use no more fuel and power than is reasonable in the circumstances. A way of complying would be to provide suitable set of operating and maintenance instructions aimed at achieving economy in the use of fuel and power in a way that the home owner / tenant can understand. The instructions should be directly related to the particular system/s installed in the dwelling.

The instructions should explain to the occupier how to operate the system(s) efficiently. These should include: the making of seasonal adjustments to control settings and what routine maintenance is needed to enable operating efficiency to be maintained at a reasonable level through the service live/s of the system/s.

Details of any renewable system/s and how it/they operate/s.

Details of low-energy light fittings (e.g. CFL, LED etc.), their use, their benefits and the benefits of purchasing high efficacy lamps, e.g. how much energy they save compared to traditional light fit-tings and what this can mean in terms of reduced energy bills and payback.

Details of the EU labelling scheme for white goods.

Include information on smoke detector/s. User guide in Plain English on the following technologies where included with basic user instructions labelled on equipment or controls where appropriate:

- Boiler
- Air Source Heat Pump
- Ground Source Heat Pump
- Mechanical Ventilation with Heat Recovery (MVHR)
- Solar hot water
- PV
- CHP
- Smart meter / display energy device
- Water meter

#### Water Use

Details of water saving features and their use and benefits, e.g. low/dual flush toilets, low water use showers, low water use white goods (washing machines, dishwashers etc), and tips as well as details of external water use and efficiency, e.g. the use of water butts or other type of rainwater recycling systems.

#### Transport Facilities

Include details of resident car-parking and cycle storage provision, cycle paths in the area including if available cycle path network maps for the whole town/local area plus local public transport information, maps and timetables where relevant (i.e. this may not be relevant to existing occupied homes).

Information on alternative methods of transport such as park and ride, car sharing schemes and/or car pools/car hire in the area and local 'green' transport initiatives should be included. Information on the location of amenities and places of interest/cultural value, areas of outstanding natural beauty (AONB's), nature reserves, allotments etc. Also details on how to get to local amenities in the area, using public transport or cycling as relevant.

#### Materials & Waste

Information on the use & benefits of:

- Low energy/low water white goods
- Electrical equipment, including light fittings and bulbs
- Timber products from sustainable sources

Information on the location of recyclable materials storage areas (especially within flats) and how to use them appropriately.

Information on responsible purchasing of:

- Low energy/low water white goods
- Electrical equipment, including light fittings and bulbs
- Timber products from sustainable sources
- Organic food procurement/food growing/local produce/local food provision, e.g. farmers markets, organic box schemes, etc

Recycling information as follows:

- Information about the Local Authority collection scheme (if applicable).
- If the home is not covered by a Local Authority collection scheme, details and location of communal recycling bins/skips/facilities.
- Information on the location and use of any recycling and compost bins.
- Information on Waste and Resource Action Plan (WRAP) (4), which can offer guidance on recycling and sustainable waste disposal.
- Information on what to do with waste not covered by the standard weekly Local Authority collection scheme for example fridges/freezers, computer equipment, batteries and other potentially hazardous equipment. In some areas the local authority will collect these items. If this is the case, details and information on such a collection scheme should be provided.
- Information and location detailing local recycling facilities and waste tips.

Environmental recommendations for consideration in any home improvement works, such as the use of low VOC products or the purchase of certified timber

#### Emergency Information

Information on smoke detector/s and carbon monoxide detectors  
Contact details for emergency services including the location of local minor injuries clinics, A&E departments and the nearest police/fire station

#### Local Amenities

The location of food shops, post boxes, postal facilities, bank/cash points, pharmacies, schools, medical centres, leisure centres, community centres, places of worship, public houses, children's play areas, outdoor open access public areas as deemed relevant occupiers.

Other local amenities such as places of interest/cultural value, areas of beauty / wildlife / conservation / allotments etc.

#### Provision of Information in Alternative Formats

Include details of the procedure for obtaining a copy of the guide in alternative formats, including foreign languages, Braille, large print or audio cassette / CD. It should include the contact details of the person/organisation responsible for producing the guide

#### SuperHomes network

SuperHomes is a network of over 100 energy aware households. The homeowners have refurbished their old homes to the highest standards of energy efficiency and have achieved at least 60% reduction on fossil fuel use. The homes are examples which are open for visits to aid other refurbishment projects. For more information about the SuperHomes network and the projects visit [www.superhomes.org.uk](http://www.superhomes.org.uk)

#### Links & References

This should include links to other information including websites, publications and organisations providing information on how to reduce the environmental impact in terms of transport, the use

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of local amenities, responsible purchasing etc. As a minimum, this should include links and address/telephone contact numbers to:

- The Energy Saving Trust good practice guidance
- The Local Authority
- The company responsible for the refurbishment of the property
- The company responsible for the management of the home (where applicable)
- Act on CO2

### A2: Man 03 – Construction Site Impacts Site monitoring

Requirements for monitoring reporting and target setting (for requirements a. energy monitoring and b. water monitoring):

- Monthly measurements of energy use will be/has been recorded and displayed on site.
- Appropriate target levels of energy/water consumption will be/were set and displayed (targets could be annual, monthly, or project targets).
- As a minimum, monitoring will/did include checking the meters and displaying some form of graphical analysis in the site office to show consumption over the project duration and how actual consumption compares to the targets set.
- The design/site management team will/did nominate an individual who will be responsible for the monitoring and collection of data.

#### Notes:

Targets for energy consumption during the refurbishment process should be set using DTI's Environmental KPI benchmarks. These documents do not specify targets but facilitate projects in setting appropriate targets (see references section of main credit for further details).

BREEAM does not require targets to be met but is encouraging the process of setting, monitoring and reporting against targets.

#### Environmental materials policy

The main contractor operates an environmental materials policy, used for sourcing of construction materials to be utilised on site. The policy should cover/promote the following:

- Use of local materials (where possible)
- Use of responsibly sourced materials
- Re use of materials
- Use of materials with a high recycled content
- Waste minimisation and recycling
- Use of non-toxic materials & refrigerants with a high global warming potential
- Use of materials with a low embodied impact
- Use of durable materials

#### EMS

Third party certified, to ISO14001/EMAS or equivalent standard. OR

The structure of the EMS is in compliance with British Standard 8555 2003 and has reached phase four of the implementation stage, 'implementation and operation of the environmental management system', and completed phase audits one to four, as defined in BS8555. 80% of timber used during construction, including formwork, site hoardings and other temporary site timber used for the purpose of facilitating construction, will be/was procured

from sustainably managed sources, independently certified by one of the top two levels as set out in the Responsible Sourcing of Materials Issues (BREEAM credit Mat 2). Re-used timber from off site can be counted as equivalent. Additionally 100% of all site timber will be/was legally sourced.

### A3: Man 04 – Security Requirements for new doors & windows:

External Door sets:  
PAS 24:2007 or  
LPS 1175 Issue 7 Security Rating 1 or equivalent

Windows are certified to:  
BS 7950:1997 (36)  
LPS 1175 Issue 7 Security Rating 1 or equivalent

#### Requirements for existing windows & doors:

External doors are of good quality with working key locks and a strong frame, where there is no sign of warping, splitting or rotting to the door or its frame. Where the door contains glazing this should be a minimum of double glazing. Putty or beading to glazed areas should be on the unexposed side of the door, in good condition, with no sign of degradation.

Accessible Windows should have a minimum of double glazing with working key locks. Putty or beading to glazed areas should be on the unexposed side of the window, in good condition, with no sign of degradation. The window frame should be strong with no sign of warping, splitting or rot.

### A4: Man 06 – Project Management

For large scale projects, the project manager assigns individual and shared responsibilities across the following key design and refurbishment stages:

- Planning and Building control notification
- Design
- Refurbishment
- Commissioning and handover
- Occupation

Key design team meetings should be held to define and make key decisions that influence/affect the dwelling's proposed designs, and their refurbishment in accordance with the design (and therefore the dwelling's sustainability impacts and BREEAM performance). These meetings may be site or office based and would typically include representatives from at least three of the parties (below).

- Representatives of the Client / Developer
- The Main Contractor
- The Architect
- Structural Engineers
- Building Services Engineers
- Cost Consultants
- Environmental Consultants
- Project Management Consultants

### Appendix B - Health & Wellbeing

#### B1: Hea 03 – VOCs

| Product   | European Standard   | Emission level required  |
|---|---|--|
| Decorative paints and varnishes   | BS EN 13300:2001 (24) referred to the requirements of Decorative Paint Directive 2004/42/CE | VOC (organic solvent) content (testing req. 6), requirement for Phase 2.<br>Fungal and algal resistant.  |
| Wood Panels<br>Particleboard,<br>Fibreboard includ-ing<br>MDF,<br>OSB,<br>Cement-bonded<br>particleboard<br>Plywood<br>Solid wood panel and<br>acoustic board | EN 13986:2004 (13)  | Formaldehyde E1 in accordance with EN 3986:2004 Annex B (see also compliance notes)<br>Verify that regulated wood preservatives are absent as defined by the standard. |
| Timber Structures<br>Glued laminated timber   | EN 14080:2005 (14)  | Formaldehyde E1 (Testing req 1)  |
| Wood flooring<br>parquet flooring   | EN 14342:2005 (15)  | Formaldehyde E1 (Testing req. 1)<br>Verify that regulated wood preservatives are absent as defined by the standard.  |
| Resilient, textile and laminated Floor coverings<br>Vinyl/linoleum<br>Cork and rubber<br>Carpet<br>Laminated wood flooring                                    | EN 14041:2004 (16)  | Formaldehyde E1 (Testing req. 1)<br>Verify that regulated preservatives are absent as defined by the standard.   |
| Suspended ceiling tiles   | EN 13964:2004 (17)  | Formaldehyde E1 (Testing req 1).<br>No asbestos.   |
| Flooring adhesives (and if relevant adhesives for rigid wall coverings)   | EN 13999-1:2007 (18)  | Verify that carcinogenic or sensitising volatile substances are absent.(Testing req. 2-4)  |

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|   |  |  |
|---|--|--|
| Wall-coverings<br>Finished wall-papers<br>Wall vinyls and plastic wall-cov-erings<br>Wallpapers for subsequent dec-oration.<br>Heavy duty wall-coverings<br>Textile wall-cov-erings | EN 233:1999 (19)<br>EN 234:1997 (20)<br>EN 259:2001 (21)<br>EN 266:1992 (22) | Formaldehyde (Testing req. 5) and Vinyl chloride monomer (VCM) (Testing req. 5) release should be low and within the BS EN standard for the material.<br>Verify that the migration of heavy metals and other toxic substances are within the EN standard for the material. |
| Adhesive for hanging flexible wall-coverings (for rigid wall coverings use flooring adhesives criteria)   | BS 3046:1981 (23)  | No harmful substances and preservatives used should be of minimum toxicity.  |

Table B1-1

Testing requirements:

1. EN 717-1:2004 (25)
2. EN 13999-2:2007—Volatile Organic Compounds (VOCs) (18)
3. EN 13999-3:2007—Volatile aldehydes (18)
4. EN 13999-4:2007—Volatile diisocyanates (18)
5. EN 12149:1998 (26)
6. BS EN ISO 11890-2:2006 (27)

## B2: Hea 04 - Inclusive Design

Suitably qualified design team member

A suitably Qualified member of the design team would need to poses the minimum competences and skills requirements listed by the National Register of Access Consultants (NRAC) for Access Auditors (actual qualification is not required).

Please refer to the following website for these competencies:

[http://www.nrac.org.uk/Information\\_pack.html#Anchor-44591](http://www.nrac.org.uk/Information_pack.html#Anchor-44591)

Access Statement

The requirements of the access statement template are detailed below.

### Section 1

Means of access into the dwelling - An accessible threshold is provided into the entrance.

Note: The design of an accessible threshold should also satisfy the requirements of Building regulations Part C.

Accessible switches and socket outlets in the dwelling(s) - switches and socket outlets for lighting and other equipment in habitable rooms at appropriate heights between 450mm and 1200mm from finished floor level

1. WC provision in the entrance storey of the building, as follows:

- a. WC is provided in the entrance storey of a dwelling which contains a habitable room; or where the dwelling is such that there are no habitable rooms in the entrance storey, if a WC is provided in either the entrance storey or the principal storey.
- b. The door to the WC compartment opens outwards, and is positioned to enable wheelchair users to access the WC and has a clear opening width in accordance with table Table B2-1.
- c. the WC compartment provides a clear space for wheelchair users to access the WC (see diagrams 31 and 32 within Approved Document M) and washbasin is positioned so that it does not impeded access.

### 2. Requirements for entrances should be adhered to as follows:

- a. All entrances to dwellings/communal entrances to blocks of dwellings should be illuminated.
- b. All entrances to dwellings, all communal entrances to blocks of dwellings and all associated communal doors should have level access over the threshold (threshold upstand should not exceed 15mm).
- c. Main entrances to dwellings and main entrances to blocks of dwellings should be covered.

### 3. Walls in bathrooms and toilets should be capable of taking adaptations such as handrails (wall reinforcements should be located between 300 and 1500mm from the floor).

### 4. The bathroom should be designed to incorporate ease of access to the bath, WC and wash basin (Although there is not a requirement for a turning circle in bathrooms, sufficient space should be provided so that a wheelchair user can use the bathroom).

### 5. Switches, sockets, ventilation and service controls should be at a height usable by all (i.e. between 450 and 1200mm from the floor).

| Minimum Widths of Corridors and Passageways for a Range of Doorway widths |                                    |
|---|------------------------------------|
| Doorway Clear Opening Width (mm)  | Corridor/Passageway width (mm)     |
| 750 or narrower   | 900 (when approached head-on)      |
| 750   | 1200 (when approached not head-on) |
| 775   | 1050 (when approached not head-on) |
| 800   | 900 (when approached not head-on)  |

Table B2-1

### Section 2

#### 1. Means of access

- a. Approach to the dwelling - within the plot of the dwelling, a suitable approach is provided from the point of access to the entrance The point of access should be reasonably level and the approach should not have crossfalls greater than 1 in 40. The whole, or part, of the approach may be a driveway. improvements made to meet Part M requirement as far as practical.
- b. Access Doors - An external door providing access for disabled people has a minimum clear opening width of 775mm.

#### 2. Circulation within the entrance storey of the dwelling(s):

- a. A corridor or other access route in the entrance storey or habitable room

- a. containing a WC (which may be a bathroom) on that level, has an unobstructed width in accordance with table x above.
- b. Vertical circulation - In exceptional circumstances, where severely sloping plots are involved, a stepped change of level within the entrance storey may be unavoidable. In those instances, the aim should be to provide a stair of reasonable width for ambulant disabled people to negotiate the steps with assistance and for handrails on both sides. Approved Document K of the Building Regulations contains guidance on the design of private stairs in dwellings. A stair providing vertical circulation within the entrance storey of the dwelling will satisfy requirement M1 if:
  - it has flights whose clear widths are at least 900mm;
  - there is a suitable continuous handrail on each side of the flight and any intermediate landings where the rise of the flight comprises three or more rises; and
  - the rise and going are in accordance with the guidance in the Approved Document for part K for private stairs

### 3. Passenger Lifts & Common Stairs in Blocks of flats

- a. A building containing flats, in which a passenger lift is not be installed, is provided with a suitable stair, with:
  - all step nosings distinguishable through contrasting brightness;
  - top and bottom landings whose lengths are in accordance with Part K1;
  - steps with suitable tread nosing profiles and uniform rise of each step, which is not more than 170mm;
  - uniform going of each step, which is not less than 250mm, which for tapered treads, should be measured at a point 270mm form the inside of the tread;
- b. In a building, or part of a building which contains flats above the entrance storey, any lift access with a minimum load capacity of 400kg must:
  - have a clear landing at least 1500mm wide and at least 1500mm long in front of its entrance;
  - has a door or doors which provide a clear opening width of at least 800mm;
  - have car whose width is at least 900mm and whose length is at least 1250mm (other dimensions may satisfy Requirement M1 where shown by test evidence or experience in use, or otherwise, to be suitable for an unaccompanied wheelchair user);
  - have landing and car controls which are not less than 900mm and not more than 1200mm above the landing and the car floor, at a distance of at least 400mm from the front wall;
  - is accompanied by suitable tactile indication on the landing and adjacent to the lift call button to identify the storey in question;
  - have suitable tactile indication on or adjacent lift within the car to confirm the floor selected;
  - incorporate a signalling system which gives visual notification that the lift is answering a landing call and a 'dwell time' of five seconds before its doors beginning to close after they are fully open; the system may be overridden by a door re-activating device which relies on appropriate electronic methods, but not a door edge pressure system, provided that the minimum time for a lift door to remain fully open is 3 seconds;
  - incorporates visual and audible indication of the floor reached (when the lift serves more than three storeys).

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## 4. WC Provision in the entrance storey

- a. WC is provided in the entrance storey of a dwelling which contains a habitable room; or where the dwelling is such that there are no habitable rooms in the entrance storey, if a WC is provided in either the entrance storey or the principal storey
- b. the door to the WC compartment opens outwards, and is positioned to enable wheelchair users to access the WC and has a clear opening width in accordance with (door openings wider than the minimum in accordance with the table allow easier manoeuvring and access to the WC by wheelchair users); and
- c. the WC compartment provides a clear space for wheelchair users to access the WC (see diagrams 31 and 32 within Approved Document) and washbasin is positioned so that it does not impeded access

## Section 3

Where there is car parking adjacent to the home, it should be capable of enlargement to attain 3300mm width - The general provision for a car parking space is 2400mm width. If an additional 900mm width is not provided at the outset, there must be provision (e.g. a grass verge) for enlarging the overall width to 3300mm at a later date. The distance from the car parking space to the home should be kept to a minimum and should be level or gently sloping (where topography prevents a level approach, refer to table B2-2 for maximum gradients).

| Distance | Gradient |
|----------|----------|
| <5m      | 1:12     |
| 5-10m    | 1:15     |
| >10m     | 1:20     |

Table B2-2

1. The approach to all entrances should be level or gently sloping (where topography prevents a level approach, refer to table x for maximum gradients).
2. Communal stairs & lifts
  - a. Minimum dimensions for communal stairs are as follows:
    - Uniform rise not more than 170mm;
    - Uniform going not less than 250mm;
    - Handrails extend 300mm beyond top and bottom step;
    - Handrail height 900mm from each nosing.
  - b. Minimum dimensions for lifts are as follows:
    - Clear landing entrances 1500mm x 1500mm;
    - Minimum internal dimensions 1100mm x 1400mm;
    - Lift controls between 900 and 1200mm from the floor and 400mm from the lift's internal front wall.
3. Doorways & Hallways
 

Doorway & hallways should comply with the requirements of table B2-3

| Doorway Clear Opening Width (mm) | Corridor/Passageway width (mm) |
|----------------------------------|--------------------------------|
| 750 or wider                     | 900 (when approached head-on)  |

|              |                                    |
|--------------|------------------------------------|
| 750 or wider | 1200 (when approached not head-on) |
| 750 or wider | 1050 (when approached not head-on) |
| 900          | 900 (when approached not head-on)  |

Table B2-3

- a. All front doors to dwellings and communal entrance doors should have a 800mm opening width and a 300mm leading edge
4. A turning circle of 1500mm diameter or a 1700mm x 1400mm in dining areas and living rooms and adequate circulation space for wheelchairs elsewhere.
5. The living room should be at entrance level.
6. In houses of two or more storeys, there should be space on the entrance level that could be used as a convenient bed-space.
7. There should be a wheelchair accessible entrance level WC, with drainage provision enabling a shower to be fitted in the future. For the fully accessible WC a wheelchair user should be able to close the door from within the closet and achieve side transfer from a wheelchair to at least one side of the WC. There must be at least 1100mm clear space from the front of the WC bowl. The shower provision must be within the closet or adjacent to the closet. In small two-bedroom dwellings (not including those on only one level) where the design has failed to achieve the above fully accessible standard WC, the Part M standard WC will meet this requirement.
8. The design should incorporate provision of a stair lift and a suitably identified space for a through-the-floor lift from the ground to the first floor, for example to a bedroom next to a bathroom. There must be a minimum of 900mm clear distance between the stair wall (on which the lift would normally be located) and the edge of the opposite handrail/balustrade. Unobstructed 'landings' are needed at the top and bottom of the stairs.
9. The design should provide a reasonable route for a potential hoist from a main bedroom to the bathroom - Most timber trusses today are capable of taking a hoist and tracking. Technological advances in hoist design mean that a straight run is no longer a requirement.
10. Living room window glazing should begin at 800mm or lower and windows should be easy to open/operate - People should be able to see out of the window whilst seated. Wheelchair users should be able to operate at least one window in each room.

## Appendix C – Energy

### C1: Ene 07 – Lighting

#### Energy Efficient Space Lighting

General space lighting:

- Lighting for external doors, porch, steps/pathways, patio, garage, garden, carports and any other outbuildings provided by dedicated energy efficient fittings, controlled by manual switching.

Space lighting in communal areas:

- Lighting in lobbies, main external entrances, internal entrance porches, external steps and pathways equipped with dedicated fluorescent fittings (or other efficient luminaires like SON or metal halide) and controlled by a time clock or day-light sensor.
- Lighting in Hallways, landings, stairwells, internal corridors and garages equipped with dedicated fluorescent fittings that are controlled by push button time switches/PIR sensors or equivalent.
- Lighting in communal rooms (laundries, cycle and other storage spaces etc) equipped with dedicated fluorescent fittings and manual switching or occupant sensors.

Energy Efficient Security Lighting:

- Security lighting, which are fittings designated for energy efficiency and are adequately controlled such that:
- Burglar security lights have a maximum wattage of 150 W, movement detection control devices (PIR) and daylight cut-off sensors.
- Other security lighting which has dedicated energy efficient fittings and is fitted with daylight cut-off sensors or timers.
- Lighting design for the affected areas should follow the requirements of the standard(s) applicable or CIBSE LG9, and should not compromise the safety of any persons using the building.

### C2: Ene 08 – Energy Display Devices Compliant energy display device

A system comprising a self-charging sensor(s) fixed to the incoming mains supply/supplies, to measure and transmit energy consumption data to a visual display unit. The visual display unit must be capable of displaying energy consumption data.

To obtain the exemplary credit, any energy display device installed in the dwelling must be capable of recording and storing energy consumption data. The consumption data that the device should be capable of displaying in order to achieve any credits is as follows:

- Current energy consumption (Watts)
- Current emissions (kg CO<sub>2</sub>)
- Current cost (£ per hour)
- Projected cost (£ per month and £ per year).

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## C3: Ene 09 – Cycle Storage

### Compliant cycle storage

- The space is covered overhead to protect from the weather
- Where cycle storage space is to be located externally, cycles can be secured within spaces in rack(s) or fixtures to allow cycles to be free-standing and locked. The rack(s) consists of fixings for one or more spaces.
- The covered area and the cycle racks or fixings are set in or fixed to a permanent structure (building or hard-standing). Alternatively the cycle storage may be located in a locked structure fixed to or part of a permanent structure.
- The distance between each cycle rack, and cycle racks and other obstructions (e.g. a wall), allows for appropriate access to the cycle storage space, to enable bikes to be easily stored and accessed including 1m<sup>2</sup> space for tools, where cycles are to be stored in a shed.
- Communal cycle storage is located within 100m of each dwellings main entrance (ideally within 50m), or within 100m of the main communal entrance in the case of flats

Cycle storage can be provided within the dwelling, provided the space is:

- of adequate size within a dedicated storage space such as. a dedicated space within a hallway, adequately sized cupboard or other suitable space with adequate fixtures allowing the cycles to be freestanding
- on the ground floor of the dwelling
- not in a lounge/living room, bedroom, bathroom, dining room or kitchen
- accessed without going through the lounge/living room, bed-rooms (where located on the ground floor), dining room, bathroom or kitchen
- there is adequate access to allow the cycle to be moved in and out of the dwelling taking account of the minimum width needed for a person pushing a bicycle (1.10m width), and 2.0m bike length for manoeuvring the cycle round corners. The storage space should not impede the intended use of that room.

## Appendix D – Materials

### D1: Mat 02 - Responsible Sourcing of Materials

Building elements to be included in assessment:

- Structural Frame
- Ground floor
- Upper floors (including separating floors)
- Roof
- External walls
- Internal walls (including separating walls)
- Foundation/substructure (excluding sub-base materials)
- Staircase
- Windows, External and internal doors
- Secondary fixes including skirting, panelling, fascias and balustrades
- Fixed furniture
- Any other significant use

Applicable materials within above elements:

- Brick (including clay tiles and other ceramics)
- Resin-based composite materials, including GRP and polymeric render
- Concrete (including in-situ and pre-cast concrete, blocks, tiles, mortars, cementitious renders etc.)
- Glass
- Plastics and rubbers (including EPDM, TPO, PVC and VET roofing membranes including polymeric renders)
- Metals (steel, aluminium etc.)
- Dressed or building stone including slate
- Timber, timber composite and wood panels (including structural laminated timber components, plywood, OSB, MDF, chip-board and cement bonded particleboard)
- Plasterboard and plaster
- Bituminous materials, such as roofing membranes and asphalt
- Other mineral-based materials, including fibre cement and calcium silicate
- Products with recycled content

All other materials should be ignored when providing information

| Responsible Sourcing & Tiers                                   |  |            |
|--|--|------------|
| Scheme   | Certification level/scope                                    | Tier level |
| BRE Global, BES6001 Product /Standard certification            | Excellent  | 2          |
|  | Very Good  | 3          |
|  | Good   | 4          |
|  | Pass   | 5          |
| Canadian Standards Association's (CSA) Chain of Custody Scheme | Chain of custody certification                               | 3          |
| Environmental Management System                                | Key process and supply chain extraction process <sup>4</sup> | 6          |

|  |   |   |
|--|---|---|
| (EMS) (certified)  |   |   |
| Environmental Management System (EMS) (certified)  | Key process   | 7 |
| Forest Stewardship Council (FSC)   | Chain of custody certification                        | 3 |
| Green Dragon Environmental Standard  | Level 4 and above                                     | 7 |
| Recycled materials   | Certified EMS for key process                         | 6 |
| Re-used materials  | -   | 3 |
| Malaysian Timber Certification Council (MTCC)  | Chain of custody certification                        | 6 |
| Programme for the Endorsement of Forest Certification (PEFC)   | Chain of custody certification                        | 3 |
| Sustainable Forestry Initiative (SFI)  | Chain of custody certification                        | 3 |
| Société Générale de Surveillance's (SGS) 'Timber Legality and Traceability' scheme                         | Timber Legality & Traceability Verification (TLTV)    | 6 |
| Rainforest Alliance's 'Verification of Legal Origin and Compliance' scheme (supersedes SmartWood Verified) | Verification of Legal Origin and Compliance (VLO/VLC) | 6 |

Table D1-1

| Key process and supply chain (extraction) processes by material type   |                               |   |
|--|-------------------------------|---|
| Material   | Key Process                   | Supply Chain Processes  |
| Brick (including clay tiles and other ceramics)  | Product Manufacture           | Clay Extraction   |
| Resin-based composites and materials (including GRP and polymeric render but excluding timber based composites)                  | Composite product manufacture | Glass fibre production (or other principle matrix material)<br>Polymer production |
| In situ Concrete (including ready mix and cementitious mortars and renders)  | Ready mixed concrete plant    | Cement production<br>Aggregate extraction and production                          |
| Precast concrete and other concrete products (including blocks, cladding, precast flooring, concrete or cementitious roof tiles) | Concrete product manufacture  | Cement production<br>Aggregate extraction and production                          |
| Glass  | Glass production              | Sand extraction<br>Soda Ash production or extraction                              |

Pre-Assessment Report

Pre-Assessment Report



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|  |   |   |
|--|---|---|
| Plastics and rubbers (including polymeric renders, EPDM, TPO, PVC and VET roofing membranes) | Plastic/rubber product manufacture                          | Main polymer production   |
| Metals (steel, aluminium etc)  | Metal Product manufacture - e.g. cladding production, steel | Metal production: Steel: Electric arc furnace or Basic oxygen furnace process |

Table D1-2

### D2: Mat 03 - Insulation

| Key process and supply chain (extraction) processes for insulation                     |                        |  |
|--|------------------------|--|
| Material   | Key Process            | Supply chain processes   |
| Foam Insulation  | Insulation manufacture | Principal Polymer production, e.g. Polystyrene, MDI , Phenolic resin or equivalent   |
| Stone wool, glass & cellular glass made using < 50% recycled input                     | Product manufacture    | Any quarried or mined mineral over 20% of input  |
| Wool   | Product manufacture    | Wool Scouring  |
| Products using > 50% recycled content except those using timber                        | Product manufacture    | Recycled content by default  |
| Timber-based insulation materials including those using recycled timber                | Product manufacture    | Recycled timber by default, all other timber from one of the recognised timber certification schemes in Mat 02 Responsible Sourcing of Materials |
| Other renewable-based insulation materials using agricultural by-products (e.g. straw) | Product manufacture    | By-product manufacture by default  |
| Any other product  | Product manufacture    | 1 or 2 main inputs with significant production or extraction impacts should be identified  |

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BREEAM Domestic Refurbishment

### Appendix E - Pollution

#### E1: Pol 02 – Surface Water Run-off

##### First credit – neutral impact on surface water

- Where any new hard standing areas are permeable, this must include all new pavements, drive-ways and where applicable public rights of way, car parks and non-adoptable roads (e.g. community scale refurbishment projects).
- Where the building is being extended onto any previously permeable surfaces, or an impermeable surface that drains onto a permeable surface (e.g. paving slabs set on concrete that drained onto soft landscaped areas) the additional run-off for rainfall depths up to 5 mm caused by the area of the extension must be managed on site using appropriate Sustainable Drainage Systems (SuDS) such as Soakaways.
- Any calculations necessary to demonstrate that criterion 2 will be achieved should be carried out by an Appropriately Qualified Professional (AQP) seeCN6.

##### Second credit – reducing run-off from site: basic

- Where all run-off from the roof for rainfall depths up to 5 mm, have been managed on site using source control methods (e.g. through infiltration, soakaways etc.). This should include runoff from all existing and new parts of the roof.
- Where required, an appropriately qualified professional should be used to design an appropriate drainage strategy for the site, ensuring criterion 1 is achieved

##### Third Credit – reducing run-off from site: advanced

- An appropriately qualified professional should be used to design an appropriate drainage strategy for the site.
- Where run-off as a result of the refurbishment is managed on site using source control achieving the following requirements:
  - The peak rate of run-off as a result of the refurbishment for the 1 in 100 year event has been reduced by 75% from the existing site.
  - The total volume of run-off discharged into the watercourses and sewers as a result of the refurbishment, for a 1 in 100 year event of 6 hour duration has been reduced by 75%.
  - An allowance for climate change must be included for all of the above calculations, in accordance with the current best practice (PPS25, 2010)

##### Exemplary level requirements

- The following outlines the exemplary level requirements to achieve an innovation credit for this BREEAM issue.
  - Where all run-off from the developed site is managed on site using source control. The following must be achieved to confirm compliance:
  - The peak rate of run-off as a result of the refurbishment for the 1 in 1 year event is reduced to zero.
  - The peak rate of run-off as a result of the refurbishment for the 1 in 100 year event is reduced to zero.
  - There is no volume of run-off discharged into the watercourses and sewers as a result of the refurbishment, for a 1 in 100 year event of 6 hour duration.
  - An allowance for climate change must be included for all of the above calculations, in accordance with current best practice (PPS25, 2010).
- Where an appropriately qualified professional has been employed to provide the above calculations and design an appropriate drainage strategy for the site, ensuring all above criteria are achieved.

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### Control source:

The control of run-off at or very near to its source. Source control measures acceptable as defined in the SuDS manual include:

- Permeable pavements
- Filter drains
- Filter Strips
- Swales
- Soakaways
- Infiltration trench
- Green Roofs
- Bioretention areas
- Rainwater Harvesting systems

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## 8.3: Appendixes :

# Sustainability Statement

APPENDIX

BREEAM Domestic Refurbishment

### Appendix F - Waste

#### F1: Was 02 - SWMP

To demonstrate a compliant SWMP for refurbishments over £300,000 the following must be met:

- A target benchmark for resource efficiency i.e. m3 of waste per £100,000 of project value or tonnes of waste per £100,000 of project value (in line with the credit available).
- Procedures and commitments for minimising non-hazardous construction waste in line with the benchmark and best practice
- Specify waste minimisation actions relating to at least 3 key waste groups as referenced in Table - 36 and recording decisions taken
- Procedures for minimising hazardous waste
- Procedures for sorting, reusing and recycling construction and demolition waste (if generated) (according to the waste streams generated by the scope of the works) either on site or through a licensed external contractor
- Procedures for measuring the amount of construction and demolition waste (if generated) diverted from land-fill.
- Licence details for the waste carrier, and permit details for the site the waste is taken to, if waste is removed off-site.
- The name or job title of the individual responsible for implementing the above.

## 8.3: Appendixes : Sustainability Statement

# 8.4: Appendixes : Acoustic Report



### 3. REVIEW OF SITE LOCATION & DEVELOPMENT PROPOSALS

The site is currently of a "Starbucks" coffee shop over ground and first floor levels with unoccupied commercial offices over second to seventh floors above at 112-116 New Oxford Street, London WC1. The site is bordered to the north and west by Bainbridge Street, to the east by adjoining commercial properties and to the south by New Oxford Street.

A planning application is to be submitted to London Borough of Camden Council for change of use of the second to seventh floors to Class C3 residential flats.

The surrounding area is primarily of commercial premises with shops facing onto New Oxford Street. Centre Point tower is directly opposite the proposed site. While the area is predominantly of commercial properties the author identified a number of existing residential dwellings in the immediate vicinity, including on New Oxford Street, Matilda Apartments and Centre Point House on St Giles High Street opposite the site and on both Bainbridge Street and Great Russell Street to the rear of the proposed development.

The junction of St Giles High Street and New Oxford Street, close to the bottom of Tottenham Court Road and directly opposite the proposed development, is a very busy area with high volume traffic during both day and night time hours, particularly following the re-routing of Charing Cross Road to allow for the current Crossrail construction works.

Noise levels incident on the site are primarily due to traffic on surrounding roads and pedestrian activity within the local area. During the author's visits to site to set up and collect the logging noise equipment then noise from nearby commercial properties was not considered to be audible nor dominant. Although not witnessed by the author at this site, based on manned noise surveys undertaken at other sites within the vicinity it is anticipated that noise levels overnight also currently include contribution from the nearby Crossrail station construction site.

**Site Address:** 112-116 New Oxford Street  
London  
WC1

**Client:** Zania Universal Limited  
c/o 37 Church Way  
London  
N20 0JZ

**Report Reference:** 121107-003

**Revision:** A: First Issue

**Author:** Rob Cant MIOA

**Date:** December 2012

## ASSESSMENT OF EXTERNAL NOISE INTRUSION TO A NEW RESIDENTIAL DEVELOPMENT AT 112-116 NEW OXFORD STREET, LONDON WC1

Report Reference: 121107-003A

Date: December 2012

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Report Reference: 121107-003A

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# 8.4: Appendixes : Acoustic Report



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## 0. SUMMARY

- The client, Zania Universal Limited, is preparing a planning application for the material change-of-use of upper floors at 112-116 New Oxford Street, London WC1 from offices to Class C3, residential use.
- ACA Acoustics Limited has been commissioned by Zania Universal Limited to assess noise incident on the proposed development site. The assessment is required by the Local Planning Authority (London Borough of Camden) to assist their consideration of the planning application for the development.
- A noise survey has been carried out at the site over nominally a 24-hour period between Monday 3<sup>rd</sup> December and Tuesday 4<sup>th</sup> December 2012. Results have been used to assess the site's separate daytime, evening and night time LAeq noise levels in accordance with London Borough of Camden's Local Development Framework Policy DP28.
- Existing ambient noise levels incident on the proposed development are primarily comprised of high-volume traffic and pedestrian activity in the area. Although not witnessed by the author at this site, based on manned noise surveys undertaken at other sites within the vicinity it is anticipated that noise levels overnight will also currently include contribution from the nearby Crossrail station construction site.
- Noise levels to the front façade of the proposed site during daytime hours and noise levels to the rear façade are within the range of values requiring attenuation measures to be implemented as defined by London Borough of Camden's Policy DP28. Noise levels to the front façade overlooking New Oxford Street during night-time periods are above the range of values shown in Table A of Policy DP28.
- Although noise levels overnight are at a level above the range of values at which, in accordance with London Borough of Camden Council's Policy DP28, planning permission would not normally be granted, it is the author's opinion that the site is suitable for residential development, subject to implementation of a very high performance scheme of noise insulation measures to ensure that noise levels inside rooms of the new residential properties are reasonable and achieve the guidance limits for noise intrusion into residential dwellings advised within British Standard BS8233:1999 "Sound insulation and noise reduction for buildings – Code of practice". A scheme of noise insulation measures is included in this report.
- In summary it is recommended that the site is suitable for residential development, subject to implementation of noise insulation measures as set out in this report.



## 1. INTRODUCTION

ACA Acoustics Limited has been commissioned by Zania Universal Limited to carry out a survey and assessment of external noise at the site of a proposed residential development at 112-116 New Oxford Street, London WC1.

The noise survey and assessment is required by the Local Planning Authority (London Borough of Camden Council) to assist their consideration of a planning application for the development.

The objective of the assessment is to determine the impact that existing noise sources would have on the proposed new development in accordance with London Borough of Camden Council's Local Development Framework Policy DP28 "Noise and Vibration" along with British Standard BS8233:1999 "Sound insulation and noise reduction for buildings – Code of practice" and other relevant British Standards and guidance documents.

This report presents results of the noise survey and assessment along with recommendation for sound insulation measures such that noise levels within the proposed residential development comply with guideline limits and includes:

- Description of the site and development proposals;
- Confirmation of London Borough of Camden Council planning consent requirements for noise;
- Measurement and assessment of existing ambient noise levels at the site;
- Review of sound insulation measures required to comply with London Borough of Camden Council's limits.

# 8.4: Appendixes : Acoustic Report



## 2. LONDON BOROUGH OF CAMDEN COUNCIL PLANNING CONSENT ACOUSTIC REQUIREMENTS

The proposed noise measurement and assessment methodology is based on ACA Acoustics Limited's experience of undertaking noise assessments for similar developments.

A review of relevant parts of each of the routinely used planning guidance documents and British Standards is provided below.

### 2.1 Camden Development Policies 2010-2025: Local Development Framework – Policy DP28

Policy DP28 of London Borough of Camden Council's Local Development Framework states that *"the Council will seek to ensure that noise and vibration is controlled and managed and will not grant planning permission for ... development sensitive to noise in locations with noise pollution, unless appropriate attenuation measures are provided"*.

Paragraph 28.3 of the supporting text to Policy DP28 advises that *"where uses sensitive to noise are proposed to an existing source of noise ... the Council will require an acoustic report to ensure compliance with PPG24: Planning and noise"*. Discussion of Planning Policy Guidance 24 (PPG24) is provided below.

In addition to the requirements of PPG24, London Borough of Camden have specific requirements for noise and vibration thresholds, set out in Tables A to E of paragraph 28.4. Copy of Policy DP28 and the associated supporting text is included in Appendix B.

ACA Acoustics Limited has carried out an assessment of general (traffic and pedestrian) noise to the proposed residential development in accordance with Policy DP28.

### 2.2 Planning Policy Guidance 24: Planning and Noise (PPG24)

PPG24 has been used extensively at the planning stage of many new residential developments to determine the suitability of the land for residential development and what noise insulation measures are required.

The document provides a simple mechanism for determining whether noise should be a major factor when granting planning permission and considering suitable planning conditions for a development. The method introduces the concept of Noise Exposure Categories (NEC) to rate the importance of noise in the planning process. The objective of the noise survey and assessment is to determine the noise impact that existing sources would have on the proposed residential development and advise on any mitigating measures to ensure that noise levels inside rooms of new residential properties are reasonable and comply with guidance limits for noise intrusion advised in British Standard BS8233:1999 *"Sound insulation and noise reduction for buildings – Code of practice"* (to which PPG24 makes reference).

PPG24 has recently been withdrawn; however no replacement technical guidance document has been issued by central Government to date.



### 2.3 National Planning Policy Framework (NPPF) and Noise Policy Statement for England (NPSE)

London Borough of Camden's Policy DP28 states that assessment should be carried out in accordance with guidelines set out in PPG24 with the results compared against criteria set out in Tables A to E (which in turn are based on the guidance in PPG24); It is acknowledged that Local Authorities will need significant time to establish and issue new policies relating to noise to replace PPG24. In view of this ACA Acoustics Limited considers that although withdrawn, continued use of the PPG24 measurement methodology in the interim period will allow Local Authorities to readily evaluate the effect of existing noise sources on proposed residential developments, albeit that adherence to the internal noise limits set out in the, still current, British Standard BS8233:1999 should take precedence above the outdated assessment conclusion of the withdrawn PPG24.

### 2.3 National Planning Policy Framework (NPPF) and Noise Policy Statement for England (NPSE)

The National Planning Policy Framework (referred to as NPPF) was published by the Department for Communities and Local Government in March 2012 and replaces the previous Planning Policy Statements (PPS) and Planning Policy Guidance (PPG) documents, including PPG24: Planning and Noise.

The NPPF sets out the Governments' planning policies for England and provides guidance on how these are expected to be applied, providing a framework within which Local Authorities can produce their own distinctive local and neighbourhood plans, which reflect the needs and priorities of their communities.

Paragraph 109 of the NPPF states that *"The planning system should contribute to and enhance the natural and local environment by: preventing both new and existing development from contributing to or being put at unacceptable risk from, or being adversely affected by unacceptable levels of soil, air, water or noise pollution or land instability"*.

It also talks specifically about noise and states that *"Planning policies and decisions should aim to:*

- *Avoid noise from giving rise to significant adverse impacts on health and quality of life as a result of new development;*
- *Mitigate and reduce to a minimum other adverse impacts on health and quality of life arising from noise from new development, including through the use of conditions;*
- *Recognise that development will often create some noise and existing businesses wanting to develop in continuance of their business should not have unreasonable restrictions put on them because of changes in nearby land uses since they were established; and*
- *Identify and protect areas of tranquillity which have remained relatively undisturbed by noise and are prized for their recreational amenity value for this reason."*

In March 2010 the Department for Environment, Food and Rural Affairs (Defra) issued Noise Policy Statement for England (referred to as NPSE). This sets out the Government's long-term policy aims that are intended to be considered by Local Planning Authorities when development their own Local Policies relating to noise. Stated aims of NPSE are *"Through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy of sustainable development:*



- *Avoid significant adverse impacts on health and quality of life;*
- *Mitigate and minimise adverse impacts on health and quality of life; and*
- *Where possible, contribute to the improvement of health and quality of life."*

Paragraphs 2.19 to 2.24 clarify the above aims, referring to established concepts from toxicology; NOEL (No Observed Effect Level) and LOAEL (Lowest Observed Adverse Effect Level). It also introduces a new concept relating to *"significant adverse"* of SOAEL (Significant Observed Adverse Effect Level), however stating that *"it is not possible to have a single objective noise-based measure that describes SOAEL that is applicable to all sources of noise in all situations. Consequently, the SOAEL is likely to be different for different noise sources, for different receptors and at different times"*.

The second aim of the NPSE refers to the situation where the impact lies somewhere between LOAEL and SOAEL. It requires that all reasonable steps should be taken to mitigate and minimise adverse effects on health and quality of life while also taking into account the guiding principles of sustainable development, as set out in the NPPF.

Paragraph 2.7 states that *"... the application of the NPSE should enable noise to be considered alongside other relevant issues and not to be considered in isolation. In the past, the wider benefits of a particular policy, development or other activity may not have been given adequate weight when assessing the noise implications"*. This provides clear guidance that noise must not be considered in isolation but as part of the overall scheme taking into account the overall sustainability and associated impacts of the proposed development; there is no benefit in reducing noise to an excessively low level if this creates or increases some other adverse impact. Similarly it may be appropriate in some cases for noise to have an adverse impact if this is outweighed by the reduction or removal of some other adverse impact that is of greater significance to the development as a whole.

Paragraph 2.8 of NPSE states that *"in the longer term, the Government hopes that existing policies could be reviewed (on a prioritised basis), and revised if necessary, so that the policies and any noise management measures being adopted accord with the vision, aims and principles of the NPSE"*.

As discussed above, it is acknowledged that Local Authorities will need significant time to establish and issue new policies relating to noise to replace PPG24 and to comply with the guiding principles of NPSE and NPPF and therefore the author considers that although withdrawn, continued use of the measurement methodology of PPG24, and in particular consideration of internal noise level limits provided in BS8233, in the interim period will allow Local Authorities to readily evaluate the effect of existing noise sources on proposed new residential developments.

## 8.4: Appendixes : Acoustic Report



### 2.4 British Standard BS8233:1999

In advising guidance on permissible noise levels inside residential dwellings and appropriate noise mitigation measures PPG24 makes frequent reference to British Standard BS8233:1999 "Sound insulation and noise reduction for buildings – Code of practice". Guidance limits for internal noise within living rooms and bedrooms, taken from Table 5 of BS8233, are shown in Table 1 below:

| Room         | Reference Time             | Design Range – LAeq, T |            |
|--------------|----------------------------|------------------------|------------|
|              |                            | Good                   | Reasonable |
| Living Rooms | Daytime (07:00 – 23:00)    | 30dB                   | 40dB       |
|              |                            | 30dB                   | 35dB       |
| Bedrooms     | Night time (23:00 – 07:00) | LAFmax ≤45dB           |            |

**Table 1:** BS8233 guideline internal noise levels

ACA Acoustics Limited's standard approach is to design noise to bedrooms to the lower "good" limit of Leq 30dBA and to the mid-range of maximum Leq 35dB for living rooms.

### 2.5 World Health Guidance

The World Health Organisation's guidance "Community Noise 1999" recommends a limit of Leq 30dBA for bedrooms at night as preventing sleep disturbance to vulnerable people. The WHO guidance also states that "for a good sleep, it is believed that indoor sound pressure levels should not exceed 45dB LAFmax more than 10-15 times per night".

The levels advised in The World Health Organisation's guidance correlate very well with those in BS8233 described above.



## 4. NOISE SURVEY

### 4.1 Noise Measurement and Assessment Procedure

To assess the impact of existing noise sources, noise samples were recorded at the development site generally in accordance with procedures set out in PPG24.

A single noise measurement position was selected as being worse case representative of the nearest part of the proposed residential façade overlooking New Oxford Street. The rear façade of the development will be set back further from the main noise source of New Oxford Street and with greater screening provided by the building itself.

The noise survey was carried out using an unmanned logging type sound level meter over nominally a 24-hour period between 3<sup>rd</sup> December and 4<sup>th</sup> December 2012. The weather included dry and calm periods during the survey. Noise measurements were recorded in terms of 5-minute samples of overall LAeq and LAFmax values.

In addition to the long-term measurements, short-term noise samples of octave band values were also obtained at front and rear facades to provide frequency content information of noise levels to assist with later acoustic calculations.

### 4.2 Instrumentation

The following equipment was used during the unattended noise survey; the sound level meter was calibrated before and after the survey measurements using the UKAS certified calibrator:

| Equipment   | Serial Number |
|---|---------------|
| Rion sound level meter type NL-31 Class 1 complete with weatherproof and lockable outdoor environmental kit | 00773045      |
| Bruel & Kjaer calibrator type 4231 (UKAS Certified)   | 02326801      |
| Microphone extension cable and telescopic boom arrangements   | -             |

**Table 2:** Equipment used

### 4.3 Noise Measurement Results and Observations

Complete LAeq and LAFmax value results of the noise survey over the 24-hour period are provided in graphical form in Appendix C.



Summary of the 12-hour daytime, 4-hour evening and 8-hour night-time period noise levels are shown in Table 3 below.

| Description                                     | Daytime                          | Evening                         | Night Time                      |
|---|----------------------------------|---------------------------------|---------------------------------|
|   | (07:00 – 19:00)<br>Leq (12 hour) | (19:00 – 23:00)<br>Leq (4 hour) | (23:00 – 07:00)<br>Leq (8 hour) |
| 3 <sup>rd</sup> – 4 <sup>th</sup> December 2012 | 74.2dBA                          | 73.0dBA                         | 71.5dBA                         |

**Table 3:** Summary noise survey results for daytime, evening and night time periods

During the survey visits subjectively noise levels at the front façade of the development are comprised of traffic on local routes and pedestrian activity within the area.

# 8.4: Appendixes : Acoustic Report



## 5. NOISE ASSESSMENT

London Borough of Camden Council's Policy DP28 assesses the impact of noise in terms of daytime LAeq, 12 hours (07:00 – 19:00), evening LAeq, 4 hours (19:00 – 23:00) and night time LAeq, 8 hours (23:00 – 07:00).

Equivalent free-field noise levels at the location of the proposed façade of the new development, compared with the noise limits specified in Policy DP28 are shown in Table 4 below. *Note that in accordance with procedures in PPG24, the 1m façade measured levels (shown in Section 4 and the graph in Appendix C) are taken to be 3dBA higher than the levels incident on the façade.*

| Description                                     | LAeq (dB) | Camden Policy DP28 Category                         |
|---|-----------|---|
| 3 <sup>rd</sup> – 4 <sup>th</sup> December 2012 |           |   |
| Daytime   | 71.2      | Daytime and Evening: Table B – Attenuation Required |
| Evening   | 70.0      | Night Time: Table A – Planning Not Normally Granted |
| Night time                                      | 68.5      |   |

**Table 4:** LAeq noise level incident on façade and corresponding Policy DP28 Table requirement

Noise levels during daytime and evening periods to the front façade are within the range of values shown in Table B of Policy DP28, requiring attenuation measures to be considered. During night time periods, noise levels to the front façade are above the threshold limits provided in Table A of Policy DP28. Development sites with measured noise levels exceeding the limits of Table A are indicative of a very noisy area; London Borough of Camden would not normally grant planning permission for residential development in these locations.

In this instance it is of benefit to consider the technical acoustic concept of the threshold limits.

The threshold limit provided in Table A of DP28 is taken from the noise levels corresponding to NEC D of PPG24. Annex B of PPG24 provides *“an explanation of how the noise levels in the NEC table in Annex 1 have been calculated or derived”*. Paragraph 11 of Annex B states that *“The upper limit is based on a Building Research Establishment (BRE) survey which has shown that the insulation package supplied under the Noise Insulation Regulations is inadequate for road traffic noise levels of 78dB LA10, 18h and above at a façade. This figure is equivalent to a ‘free-field’ level of 75dB LA10, 18h; which in turn is equivalent to 73dB LAeq, 16h. The 73dB LAeq 16h has been reduced by 1dB to 72dB LAeq 16h in the table, which is the maximum external level that the standard noise insulation package will reduce to an acceptable internal level”*.

The Noise Insulation Regulations to which PPG24 refers were issued in 1975 and included recommendation for mitigation measures to improve the sound insulation performance of external facades to an existing residential dwelling. Recommendations included installation of secondary glazing to windows with the new secondary glazing formed from glass of minimum 3mm thickness. Through-wall type acoustic ventilators were also recommended.



Design of modern high-performance acoustic glazing or secondary glazing systems is significantly superior to the 3mm thickness glass proposed in the Noise Insulation Regulations, often incorporated either units with toughened or laminated panes of glass. In addition improvements in design of acoustic seals to glazed units greatly increases the sound insulation performance achieved on site.

Use of whole-house ventilation systems (such as MVHR units) or very high performance passive ventilators are also significantly superior to those in the Noise Insulation Regulations.

Paragraph 14 of PPG24 Annex 2 states that *“The standard noise insulation package provides insulation of about 35dBA”*. Use of modern high specification façade elements can provide sound insulation in excess of 45dBA; at least 10dBA better than that proposed in the Noise Insulation Regulations.

It is to be expected that advances in construction techniques and proprietary acoustic products over the past 35 years have significantly increased the level of sound insulation performance possible and the above demonstrates that although use of the NEC limits of PPG24 (and in turn the values shown in London Borough of Camden Council's Policy DP28) is useful to provide an indication of the noise character of an area, the prescriptive limits provided in NEC D or Table A of DP28 are outdated and acceptable internal noise levels are readily achievable even at higher external noise levels.

The author considers that the overly prescriptive nature of the PPG24 assessment conclusion is likely one of the reasons for its withdrawal and that a more detailed assessment, considering actual noise levels inside a residential property, allowing for high performance façade sound insulation, rather than noise levels incident on the external façade, is of more benefit and will ensure that the amenity of future occupants is not compromised while allowing for much needed development within town and city centre locations.

As such, a very high performance scheme for sound insulation is proposed to ensure that noise levels inside rooms of the new flats are reasonable and comply with the requirements of BS8233:1999,

By achieving the internal noise limits of BS8233:1999 it is therefore considered that although external noise levels are above London Borough of Camden's typical maximum threshold, amenity of future residents would not be compromised and the site should be considered suitable for residential use.

The author considers that this approach fully complies with the aims of The Noise Policy Statement for England (NPSE) and National Planning Policy Framework (NPPF), whereby potential adverse impacts on health and quality of life due to noise are adequately mitigated and minimised through the careful design of façade sound insulation such that acceptable internal noise levels are achieved. This approach is also in accordance with London Borough of Camden's own policy, which states that *“the Council will seek to ensure that noise and vibration is controlled and managed and will not grant planning permission for ... development sensitive to noise in locations with noise pollution, unless appropriate attenuation measures are provided”*; it is the author's opinion that high-performance façade sound insulation should be considered as *“appropriate attenuation measures”*.



There are various existing residential flats within the vicinity of the proposed development. Whilst it is acknowledged that existing residential properties might not be retrospectively assessed for noise intrusion, presence of these properties does establish the nature of the area. This proposed development would therefore not be introducing a noise-sensitive use to an area where there are no existing noise-sensitive uses.

In summary it is considered the site is suitable for residential development providing that a high specification of appropriate sound insulation measures are incorporated into the scheme design to ensure noise levels inside rooms of the new residences achieve the guideline limits in British Standard BS8233:1999.



## 8.4: Appendixes : Acoustic Report



### 6. SCHEME OF FAÇADE SOUND INSULATION

By following the calculation procedures outlined in BS EN ISO 12354-3:2000 and Section 6.7 of BS8233:1999 a specification for the acoustic performance of façade elements has been established.

Copy of example acoustic calculations for daytime noise intrusion to a typical living room and night time noise intrusion into a bedroom within the façade of the development directly overlooking New Oxford Street are provided in Appendix D. The calculations use ACA Acoustics Limited's in-house computer calculation model based on BS EN ISO 12354-3 and BS8233. The calculations confirm that intrusive noise levels into rooms of the proposed residential flats will comply with guidance limits in British Standard BS8233 as set out in Section 2.4 of this report.

An item by item scheme for noise insulation measures to the proposed residential dwellings is provided below.

#### 6.1 Walls

External walls are of traditional masonry construction. Values in Table 5 below show the expected sound insulation performance for this type of wall construction. This will provide more than adequate sound insulation and no additional treatments are required.

| Description | Octave Band Centre Frequency – Hz (dB) |     |     |    |    |    | Rw (dB) |
|-------------|--|-----|-----|----|----|----|---------|
|             | 125                                    | 250 | 500 | 1k | 2k | 4k |         |
| Wall        | 41                                     | 45  | 47  | 55 | 60 | 60 | 53      |

**Table 5:** Traditional solid masonry external wall Sound Reduction Index R dB

#### 6.2 Glazing

Existing glazing to the property is of single pane float glass nominally 4mm thick within casement style metal frame. This type of glazing provides limited acoustic performance and it is recommended that the sound insulation performance of the glazing to façades with line-of-sight to New Oxford Street be improved significantly.

Values in Table 6 on the following page show a specification schedule of glazing sound insulation performance for different parts of the development.

Note that there are many permutations of possible configurations and different glazing suppliers will tend to use their own preferred configuration. Providing that the overall Rw performance and the individual octave band performance are not less than those shown in Table 6 then any alternative configuration can be used.



| Description                          | Octave Band Centre Frequency – Hz (dB) |     |     |    |    |    | Rw (dB) | Comments  |
|--------------------------------------|--|-----|-----|----|----|----|---------|---|
|                                      | 125                                    | 250 | 500 | 1k | 2k | 4k |         |   |
| Bedrooms to front & side façades     | 29                                     | 40  | 45  | 47 | 54 | 68 | 48      | Very high-performance IGU such as Pilkington Optiphon 16.8-20Ar-16.8 or secondary glazing |
| Bedrooms – rear façade               | 27                                     | 26  | 31  | 40 | 42 | 46 | 37      | Double glazing such as 4-16-6 IGU   |
| Living Rooms to front & side façades | 23                                     | 28  | 41  | 47 | 45 | 55 | 42      | High performance IGU such as Pilkington Optiphon 6-16Ar-10.8 or secondary glazing         |
| Living Rooms – rear façade           | 27                                     | 26  | 31  | 40 | 42 | 46 | 37      | Double glazing such as 4-16-6 IGU   |
| Non-habitable rooms                  | 24                                     | 20  | 26  | 35 | 38 | 42 | 31      | Double-glazing such as 4-16-4 IGU   |

**Table 6:** Specification for glazing Sound Reduction Index R dB

It is considered that existing windows of the development may have to be retained for conservation reasons. In this instance secondary glazing will be required to inside of the existing retained outer window for all windows within the new residential flats. In this instance specification for suitable secondary glazing will be provided to the client prior to construction works commencing.

For all living rooms and bedrooms, the window frames will need to have effective acoustic seals all around. Effective seals are rubber or neoprene beaded "P" or "O" profile type that compress all around on closure of the windows. Plastic type or brush type weathering seals are not classed as effective acoustic seals.

#### 6.3 Ventilation Scheme

With regard to ventilation requirements, it is usual to satisfy the noise limits with the background ventilation rate defined by Approved Document F of the Building Regulations, rather than for the rapid ventilation rate. It is therefore anticipated that it will be necessary to incorporate an acoustic ventilation scheme into the design such that residents are able to have background ventilation without necessarily needing to open windows.

Values in Table 7 on the following page show a specification schedule of ventilator sound insulation performance for the development.



Note that the ventilators proposed are very high performance type; around the maximum attainable for passive ventilators. An alternative to using passive acoustic ventilators would be to use mechanical ventilation with inline silencing. Suppliers such as Vent-Axia or Nuiare would be able to offer suitable ventilation systems for residential properties.

If mechanical ventilation (such as MVHR or similar) is used then it is important that any self-noise (i.e. noise from the fans) must not cause internal noise levels to exceed the design requirements. To achieve these limits then it is recommended that the overall noise from any mechanical ventilation system will need to be no higher than LAeq 30dB within living rooms (daytime) and LAeq 25dB within bedrooms (night time) to allow for accumulation of noise sources.

| Description         | Octave Band Centre Frequency – Hz (dB) |     |     |    |    |    | Dn,e,w (dB) | Comments   |
|---------------------|--|-----|-----|----|----|----|-------------|--|
|                     | 125                                    | 250 | 500 | 1k | 2k | 4k |             |  |
| All habitable rooms | 33                                     | 40  | 45  | 56 | 67 | 75 | 50          | Very high-performance acoustic ventilators such as Coice acoustic ventilator or equivalent |

**Table 7:** Specification for ventilators Element Normalized Level Difference Dn,e dB

# 8.4: Appendixes : Acoustic Report



## 7. SOUND INSULATION THROUGH SEPARATING WALLS & FLOORS

### 7.1 Sound Insulation between Flats

Separating walls and floors between the new flats will need to comply with the minimum performance requirement standards set out in the Building Regulations 2010 Approved Document E (2003 Edition).

Performance standards for separating walls and floors are given in Table 8, taken from Table 0.1a of Approved Document E.

| Description       |                         | Approved Document E<br>Performance Standard |
|-------------------|-------------------------|---|
| Walls             | DnT,w + C'tr (Airborne) | ≥ 43dB                                      |
| Floors and stairs | DnT,w + C'tr (Airborne) | ≥ 43dB                                      |
|                   | L'nT,w (Impact)         | ≤ 64dB                                      |

**Table 8:** Sound insulation performance standards for separating walls and floors between flats formed by material change of use

Compliance with the above minimum standards would normally be demonstrated by carrying out pre-completion airborne and impact sound insulation tests of the formed walls and floors between the flats at or near to completion of the development works. Results of the tests would be submitted to and approved by the Local Authority Building Control department or an approved inspector.

It is anticipated that as the project progresses ACA Acoustics Limited will undertake an acoustic design review of the development to ensure that proposed separating wall and floor constructions, along with associated flanking details, will achieve the above minimum requirements.

### 7.2 Sound Insulation of Separating Floor between Commercial Unit and Residential Flats

Any noise associated with the existing commercial unit at first floor level could potentially transmit to the proposed residential flats above through the building structure.

Where residential flats share a common structure with commercial properties it is anticipated that London Borough of Camden Council will require noise from the commercial unit to not exceed the "good" standards for internal noise within residential properties set out in BS8233:1999; this equates to designing noise transfer from the existing Starbucks coffee shop to not exceed a level of LAeq 30dB inside living rooms of the proposed flats.

Starbucks and equivalent coffee shops do not play amplified music internally and it is considered that any change of use of the commercial unit to allow amplified music to be played would require a planning application. Therefore assessment of noise from typical coffee shop with no amplified music has been carried out.



Based on measurements undertaken in similar premises by the author, it is anticipated that noise levels within the Starbucks will typically be within the range LAeq, 1 hour 50dB to 60dB and would not normally exceed LAeq, 1 hour 65dB.

This correlates with guideline noise limits for commercial cafeteria, canteens and retail shops provided in BS8233:1999 of LAeq, T 50dB to 55dB. Measured noise levels within a coffee shop or retail unit do not include high levels of low frequency (bass) noise and are typically of a "broadband" nature.

Based on upper measured noise levels of LAeq, 1 hour 65dB it is recommended that separating floors providing airborne sound insulation performance of DnT,w + C'tr ≥ 43dB would provide more than adequate sound insulation to control noise transfer to the residential flats above and will ensure that noise levels inside the residential flats due to operational noise from the Starbucks is below the "good" limits specified in BS8233:1999. This equates to the Building Regulations 2010 Approved Document E (2003 Edition) minimum requirements for airborne sound insulation between flats.

Note that in accordance with Diagram 0.1 of Approved Document E there is no minimum impact sound insulation performance requirement for the separating floor between first floor commercial unit and second floor proposed flats.

It is anticipated that as the project progresses ACA Acoustics Limited will undertake an acoustic design review of the development to ensure that the proposed separating floor construction, along with associated flanking details, will achieve the above minimum requirements.

## APPENDIX B

### London Borough of Camden – Local Development Framework Policy DP28

# 8.4: Appendixes : Acoustic Report

## DP28. Noise and vibration

28.1 Noise and vibration can have a major effect on amenity and health and therefore quality of life. Camden's high density and mixed-use nature means that disturbance from noise and vibration is a particularly important issue in the borough. Camden's Core Strategy recognises the importance of this issue for Camden's residents and policy DP28 contributes to implementing a number of Core Strategy policies, including CS5 – *Managing the impact of growth and development*, CS9 – *Achieving a successful Central London*, CS11 – *Promoting sustainable and efficient travel* and CS16 – *Improving Camden's health and well-being*.

### DP POLICY

#### DP28 – Noise and vibration

The Council will seek to ensure that noise and vibration is controlled and managed and will not grant planning permission for:

- a) development likely to generate noise pollution; or
- b) development sensitive to noise in locations with noise pollution, unless appropriate attenuation measures are provided.

Development that exceeds Camden's Noise and Vibration Thresholds will not be permitted.

The Council will only grant permission for plant or machinery if it can be operated without cause harm to amenity and does not exceed our noise thresholds.

The Council will seek to minimise the impact on local amenity from the demolition and construction phases of development. Where these phases are likely to cause harm, conditions and planning obligations may be used to minimise the impact.

28.2 The effect of noise and vibration can be minimised by separating uses sensitive to noise from development that generates noise and by taking measures to reduce any impact. Noise sensitive development includes housing, schools and hospitals as well as offices, workshops and open spaces, while noise is generated by rail, road and air traffic, industry, entertainment (e.g. nightclubs, restaurants and bars) and other uses.

28.3 The Council will only grant planning permission for development sensitive to noise in locations that experience noise pollution, and for development likely to generate noise pollution, if appropriate attenuation measures are taken, such as double-glazing. Planning permission will not be granted for development sensitive to noise in locations that have unacceptable levels of noise. Where uses sensitive to noise are proposed close to an existing source of noise or when development that generates noise is proposed, the Council will require an acoustic report to ensure compliance with PPG24: *Planning and noise*. A condition will be imposed to require that the plant and equipment which may be a source of noise pollution is kept working efficiently and within the required noise limits and time restrictions. Conditions may also be imposed to ensure that attenuation measures are kept in place and effective throughout the life of the development.

28.4 In assessing applications, we will have regard to the Noise and Vibration Thresholds, set out below. These represent an interpretation of the standards in PPG24 and include an evening period in addition to the day and night standards contained in the PPG, which provide a greater degree of control over noise and vibration during a period when noise is often an issue in the borough.

**Table A: Noise levels on residential sites adjoining railways and roads at which planning permission will not be granted**

| Noise description and location of measurement   | Period  | Time      | Sites adjoining railways | Sites adjoining roads |
|---|---------|-----------|--------------------------|-----------------------|
| Noise at 1 metre external to a sensitive façade | Day     | 0700-1900 | 74 dB LAeq12h            | 72 dB LAeq12h         |
| Noise at 1 metre external to a sensitive façade | Evening | 1900-2300 | 74 dB LAeq4h             | 72 dB LAeq4h          |
| Noise at 1 metre external to a sensitive façade | Night   | 2300-0700 | 66 dB LAeq8h             | 66 dB LAeq8h          |

**Table B: Noise levels on residential streets adjoining railways and roads at and above which attenuation measures will be required**

| Noise description and location of measurement   | Period  | Time      | Sites adjoining railways        | Sites adjoining roads           |
|---|---------|-----------|---------------------------------|---------------------------------|
| Noise at 1 metre external to a sensitive façade | Day     | 0700-1900 | 65 dB LAeq12h                   | 62 dB LAeq12h                   |
| Noise at 1 metre external to a sensitive façade | Evening | 1900-2300 | 60 dB LAeq4h                    | 57 dB LAeq4h                    |
| Noise at 1 metre external to a sensitive façade | Night   | 2300-0700 | 55 dB LAeq1h                    | 52 dB LAeq1h                    |
| Individual noise events several times an hour   | Night   | 2300-0700 | >82 dB LAmax (S time weighting) | >82 dB LAmax (S time weighting) |

**Table C: Vibration levels on residential sites adjoining railways and roads at which planning permission will not be granted**

| Vibration description and location of measurement                    | Period                 | Time      | Vibration levels       |
|--|------------------------|-----------|------------------------|
| Vibration inside critical areas such as a hospital operating theatre | Day, evening and night | 0000-2400 | 0.1 VDV ms-1.75        |
| Vibration inside dwellings   | Day and evening        | 0700-2300 | 0.2 to 0.4 VDV ms-1.75 |
| Vibration inside dwellings   | Night                  | 2300-0700 | 0.13 VDV ms-1.75       |
| Vibration inside offices   | Day, evening and night | 0000-2400 | 0.4 VDV ms-1.75        |
| Vibration inside workshops   | Day, evening and night | 0000-2400 | 0.8 VDV ms-1.75        |

Where dwellings may be affected by ground-borne regenerated noise internally from, for example, railways or underground trains within tunnels, noise levels within the rooms should not be greater than 35dB(A)max

**Table D: Noise levels from places of entertainment on adjoining residential sites at which planning permission will not be granted**

| Noise description and measurement location  | Period          | Time      | Sites adjoining places of entertainment   |
|---|-----------------|-----------|---|
| Noise at 1 metre external to a sensitive façade   | Day and evening | 0700-2300 | LAeq' 5m shall not increase by more than 5dB*   |
| Noise at 1 metre external to a sensitive façade   | Night           | 2300-0700 | LAeq' 5m shall not increase by more than 3dB*   |
| Noise inside any living room of any noise sensitive premises, with the windows open or closed | Night           | 2300-0700 | LAeq' 5m (in the 63Hz Octave band measured using the 'fast' time constant) should show no increase in dB* |

\* As compared to the same measure, from the same position, and over a comparable period, with no entertainment taking place

**Table E: Noise levels from plant and machinery at which planning permission will not be granted**

| Noise description and location of measurement  | Period                 | Time      | Noise level   |
|--|------------------------|-----------|---------------|
| Noise at 1 metre external to a sensitive façade  | Day, evening and night | 0000-2400 | 5dB(A) <LA90  |
| Noise that has a distinguishable discrete continuous note (whine, hiss, screech, hum) at 1 metre external to a sensitive façade. | Day, evening and night | 0000-2400 | 10dB(A) <LA90 |
| Noise that has distinct impulses (bangs, clicks, clatters, thumps) at 1 metre external to a sensitive façade.                    | Day, evening and night | 0000-2400 | 10dB(A) <LA90 |
| Noise at 1 metre external to sensitive façade where LA90>60dB  | Day, evening and night | 0000-2400 | 55dB LAeq     |

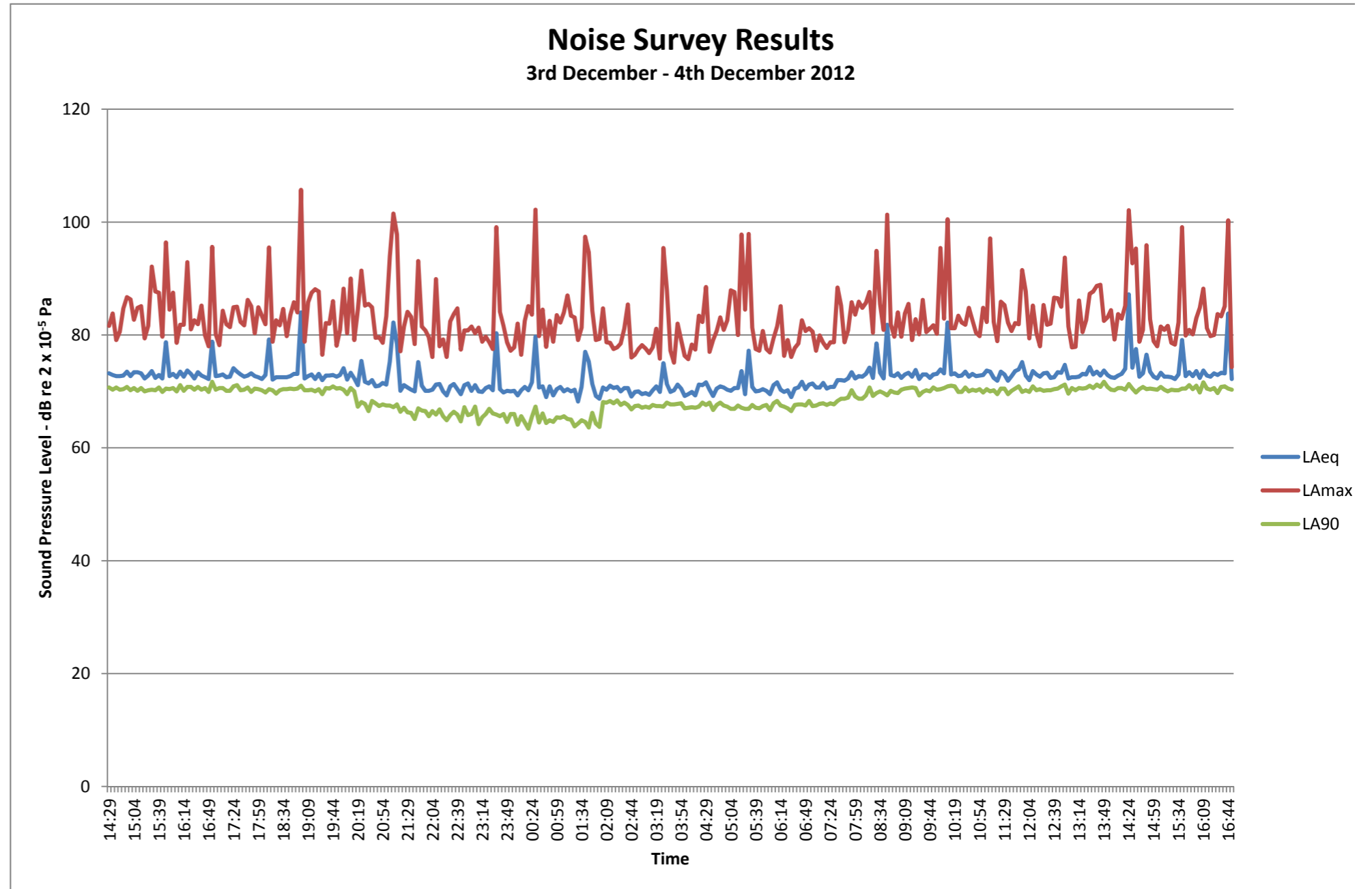
#### Key evidence and references

- Camden's Noise Strategy, 2002
- The London Plan (Consolidated with Alterations since 2004), 2008
- Planning Policy Guidance 24: Planning and noise

# 8.4: Appendixes : Acoustic Report

APPENDIX C

Noise Survey Results



# 8.4: Appendixes : Acoustic Report



## APPENDIX D

### Façade Sound Insulation – Acoustic Calculations

**Project:** 112-116 New Oxford Street, London WC1

**BS EN ISO 12354-3 - FAÇADE SOUND INSULATION CALCULATION**

**Room Reference:** Flat 2, Bedroom 2

**Measured Lp at Façade:**

|        | dBA  | 125 Hz | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
|--------|------|--------|--------|--------|-------|-------|
| Leq,ff | 68.5 | 65     | 66     | 66     | 65    | 60    |

**Façade 1:**

| Element                       | Construction                              | Area (m <sup>2</sup> ) |
|-------------------------------|---|------------------------|
| Wall (area including glazing) | Solid masonry                             | 24                     |
| Windows                       | 16.8-20Ar-16.8 Optiphon                   | 11.5                   |
| Ventilation                   | Caice acoustic ventilator (Dn,e,w = 50dB) | 1                      |
| Doors                         |   | 0                      |
| Roof / Ceiling                |   | 0                      |

**Element Sound Reduction Index**

| Surface            | Area (m <sup>2</sup> ) | Sound Reduction Index (R) - dB |        |        |       |       |
|--------------------|------------------------|--------------------------------|--------|--------|-------|-------|
|                    |                        | 125 Hz                         | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
| Walls              | 24                     | 41                             | 45     | 47     | 55    | 60    |
| Windows            | 11.5                   | 29                             | 40     | 45     | 47    | 54    |
| Ventilation (Dn,e) | 1                      | 33                             | 40     | 45     | 56    | 67    |
| Doors              | 0                      |                                |        |        |       |       |
| Roof / Ceiling     | 0                      |                                |        |        |       |       |

|   |    |
|---|----|
| Room Volume (m <sup>3</sup> ):              | 50 |
| Façade Area (m <sup>2</sup> ):              | 24 |
| Roof Area - Exposed Side (m <sup>2</sup> ): | 0  |

**Reverberation Time**

| Room Type:           | Bedroom | Reverberation Time - Seconds |        |        |       |       |
|----------------------|---------|------------------------------|--------|--------|-------|-------|
|                      |         | 125 Hz                       | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
| RT in Furnished Room |         | 0.4                          | 0.35   | 0.3    | 0.3   | 0.3   |

**CALCULATED EQUIVALENT INTERNAL SOUND PRESSURE LEVEL - LAeq**

|       | dBA  | 125 Hz | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
|-------|------|--------|--------|--------|-------|-------|
| Leq,2 | 26.9 | 38.1   | 29.5   | 24.4   | 18.4  | 6.5   |

**Project:** 112-116 New Oxford Street, London WC1

**BS EN ISO 12354-3 - FAÇADE SOUND INSULATION CALCULATION**

**Room Reference:** Flat 2, Living Room

**Measured Lp at Façade:**

|        | dBA  | 125 Hz | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
|--------|------|--------|--------|--------|-------|-------|
| Leq,ff | 71.4 | 68     | 68     | 69     | 68    | 63    |

**Façade 1:**

| Element                       | Construction                              | Area (m <sup>2</sup> ) |
|-------------------------------|---|------------------------|
| Wall (area including glazing) | Solid masonry                             | 14.8                   |
| Windows                       | 6-16Ar-10.8 Optiphon                      | 9.5                    |
| Ventilation                   | Caice acoustic ventilator (Dn,e,w = 50dB) | 1                      |
| Doors                         |   | 0                      |
| Roof / Ceiling                |   | 0                      |

**Element Sound Reduction Index**

| Surface            | Area (m <sup>2</sup> ) | Sound Reduction Index (R) - dB |        |        |       |       |
|--------------------|------------------------|--------------------------------|--------|--------|-------|-------|
|                    |                        | 125 Hz                         | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
| Walls              | 14.8                   | 41                             | 45     | 47     | 55    | 60    |
| Windows            | 9.5                    | 23                             | 28     | 41     | 47    | 45    |
| Ventilation (Dn,e) | 1                      | 33                             | 40     | 45     | 56    | 67    |
| Doors              | 0                      |                                |        |        |       |       |
| Roof / Ceiling     | 0                      |                                |        |        |       |       |

|   |      |
|---|------|
| Room Volume (m <sup>3</sup> ):              | 68   |
| Façade Area (m <sup>2</sup> ):              | 14.8 |
| Roof Area - Exposed Side (m <sup>2</sup> ): | 0    |

**Reverberation Time**

| Room Type:           | Living Room | Reverberation Time - Seconds |        |        |       |       |
|----------------------|-------------|------------------------------|--------|--------|-------|-------|
|                      |             | 125 Hz                       | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
| RT in Furnished Room |             | 0.7                          | 0.6    | 0.5    | 0.5   | 0.5   |

**CALCULATED EQUIVALENT INTERNAL SOUND PRESSURE LEVEL - LAeq**

|       | dBA  | 125 Hz | 250 Hz | 500 Hz | 1k Hz | 2k Hz |
|-------|------|--------|--------|--------|-------|-------|
| Leq,2 | 35.0 | 46.3   | 40.5   | 29.3   | 21.3  | 17.5  |

Report Reference: 121107-003A

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## APPENDIX E

### Typical Noise Mitigation Treatments



#### Pilkington Optiphon™

|  | dB sound reduction index by octave band – Hz |     |     |      |      |      | R <sub>w</sub> (C;C <sub>s</sub> ) | R <sub>w</sub> | R <sub>w</sub> +C | R <sub>w</sub> +C <sub>tr</sub> |
|--|--|-----|-----|------|------|------|------------------------------------|----------------|-------------------|---------------------------------|
|  | 125  | 250 | 500 | 1000 | 2000 | 4000 |                                    |                |                   |                                 |

##### Configuration single glazing

|                              |    |    |    |    |    |    |           |    |    |    |
|------------------------------|----|----|----|----|----|----|-----------|----|----|----|
| 6.8 mm Pilkington Optiphon™  | 21 | 26 | 31 | 35 | 37 | 38 | 35(-1;-3) | 35 | 34 | 32 |
| 8.8 mm Pilkington Optiphon™  | 24 | 28 | 34 | 38 | 37 | 43 | 37(-1;-4) | 37 | 36 | 33 |
| 10.8 mm Pilkington Optiphon™ | 28 | 31 | 36 | 38 | 39 | 47 | 38(-1;-2) | 38 | 37 | 36 |
| 12.8 mm Pilkington Optiphon™ | 30 | 32 | 37 | 39 | 41 | 51 | 39(-0;-2) | 39 | 39 | 37 |
| 16.8 mm Pilkington Optiphon™ | 29 | 34 | 37 | 39 | 46 | 55 | 40(-0;-2) | 40 | 40 | 38 |

##### Configuration Insulating Glass Unit (IGU), thickness in mm

|  |    |    |    |    |    |    |           |    |    |    |
|--|----|----|----|----|----|----|-----------|----|----|----|
| 6 / 6 to 20 mm / 6.8 Pilkington Optiphon™                          | 23 | 24 | 34 | 42 | 43 | 52 | 38(-2;-5) | 38 | 36 | 33 |
| 6 / 6 to 20 mm / 8.8 Pilkington Optiphon™                          | 24 | 26 | 40 | 48 | 46 | 54 | 41(-3;-7) | 41 | 38 | 34 |
| 6 / 6 to 20 mm / 10.8 Pilkington Optiphon™                         | 23 | 28 | 41 | 47 | 45 | 55 | 42(-3;-7) | 42 | 39 | 35 |
| 6 / 6 to 20 mm / 12.8 Pilkington Optiphon™                         | 20 | 29 | 43 | 47 | 46 | 49 | 42(-3;-8) | 42 | 39 | 34 |
| 8.8 Pilkington Optiphon™ / 6 to 20 mm / 12.8 Pilkington Optiphon™  | 26 | 36 | 46 | 50 | 52 | 63 | 47(-2;-7) | 47 | 45 | 40 |
| 16.8 Pilkington Optiphon™ / 6 to 20 mm / 16.8 Pilkington Optiphon™ | 29 | 40 | 45 | 47 | 54 | 68 | 48(-2;-6) | 48 | 46 | 42 |

The above IGUs with Pilkington K Glass™ on one pane and a 16 mm 90% Argon-filled cavity achieve a U value of 1.5 W/m²K. Further information on solar and thermal performance is available on the Pilkington website using the Spectrum program: [www.pilkington.com/spectrum](http://www.pilkington.com/spectrum)  
Impact classification EN12600 Class 1(B) for all above Pilkington Optiphon™ products  
R<sub>w</sub>(C;C<sub>s</sub>) are in accordance with EN717-1

#### Non Pilkington Optiphon™ glass products. Figures from BS EN 12354

|  | dB sound reduction index by octave band – Hz |     |     |      |      |      | R <sub>w</sub> (C;C <sub>s</sub> ) | R <sub>w</sub> | R <sub>w</sub> +C | R <sub>w</sub> +C <sub>tr</sub> |
|--|--|-----|-----|------|------|------|------------------------------------|----------------|-------------------|---------------------------------|
|  | 125  | 250 | 500 | 1000 | 2000 | 4000 |                                    |                |                   |                                 |

##### Configuration single glazing

|                   |    |    |    |    |    |    |           |    |    |    |
|-------------------|----|----|----|----|----|----|-----------|----|----|----|
| 4 mm Float Glass  | 17 | 20 | 26 | 32 | 33 | 26 | 29(-2;-3) | 29 | 27 | 26 |
| 6 mm Float Glass  | 18 | 23 | 30 | 35 | 27 | 32 | 31(-2;-3) | 31 | 29 | 28 |
| 8 mm Float Glass  | 20 | 24 | 29 | 34 | 29 | 37 | 32(-2;-3) | 32 | 30 | 29 |
| 10 mm Float Glass | 23 | 26 | 32 | 31 | 32 | 39 | 33(-2;-3) | 33 | 31 | 30 |
| 12 mm Float Glass | 27 | 29 | 31 | 32 | 38 | 47 | 34(-0;-2) | 34 | 34 | 32 |

##### Configuration Insulating Glass Unit (IGU), Float glass, thickness in mm

|                     |    |    |    |    |    |    |           |    |    |    |
|---------------------|----|----|----|----|----|----|-----------|----|----|----|
| 4 / 6 to 20 mm / 4  | 21 | 17 | 25 | 35 | 37 | 31 | 29(-1;-4) | 29 | 28 | 25 |
| 6 / 6 to 20 mm / 6  | 20 | 18 | 28 | 38 | 34 | 38 | 31(-1;-4) | 31 | 30 | 27 |
| 6 / 6 to 20 mm / 4  | 21 | 20 | 26 | 38 | 37 | 39 | 32(-2;-4) | 32 | 30 | 28 |
| 10 / 6 to 20 mm / 4 | 24 | 21 | 32 | 37 | 42 | 43 | 35(-2;-5) | 35 | 33 | 30 |
| 10 / 6 to 20 mm / 6 | 24 | 24 | 32 | 37 | 37 | 44 | 35(-1;-3) | 35 | 34 | 32 |

Note that these are conservative figures and cover all products by European glass manufacturers.  
R<sub>w</sub> = Weighted sound reduction. This scale allows for the response of the human ear and could be used for determining a suitable product to reduce noise such as voices.  
C = An adjustment to the R<sub>w</sub> scale that could be used for selecting a product to reduce noise from music, radio, tv, high speed traffic and other medium to high frequencies.  
C<sub>s</sub> = An adjustment to the R<sub>w</sub> scale that could be used for selecting a product to reduce noise from urban road traffic, disco music and other noises with a large component of low frequencies.  
Note that a 3 dB difference is barely discernible, 5 dB is clearly discernible and 10 dB is a doubling or halving of the noise.

## Classification report Airborne sound insulation of building elements

Test report 161 31740/1e\*)

\*) This is a translation of the test report No. 161 31740/1 dated 10<sup>th</sup> May 2006



Customer **SCHÜCO International KG**  
Karolinenstraße 1-15

33609 Bielefeld

Basis  
EN 20140-3 : 1995-01  
EN ISO 717-1 : 1996-12  
Corresponds to the national version of DIN EN 20140-3 and DIN EN ISO 717-1.  
Test report 161 26759/1.0.0 dated 5<sup>th</sup> May 2003

Product **Single window, single leaf**  
System designation **Schüco AWS 60**

External dimensions (W x H) **1230 mm x 1480 mm**

Material **Aluminium profile with thermal break, uncoated**

Type of opening **Tilt and turn**

Filling **Insulating glass unit, 6/16/4**

Special features **±**

#### Representation



Instructions for use  
This test report may be used to classify the sound insulation of building elements.

#### Validity

The data and results given relate solely to the described, tested object.  
Testing for sound insulation does not allow any statement to be made on further characteristics of the present structure which could define performance and quality.

#### Notes on publication

The ift notice "Conditions and notes for the use of ift test documents" applies.  
The cover sheet can be used as a summary.

#### Contents

The report comprises a total of 7 pages  
1 Object  
2 Procedure  
3 Detailed results  
Data sheet (1 page)

Weighted sound reduction index R<sub>w</sub>  
Spectrum adaptation terms C and C<sub>tr</sub>



R<sub>w</sub> (C; C<sub>tr</sub>) = 37 (-1;-4) dB

ift Rosenheim  
10<sup>th</sup> May 2006

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Anerkennung RAL, Überwachungs- und  
Zertifizierungsstelle nach  
Landesverordnung SAK 24  
Sachverständige Prüfstelle Gruppe I  
für Eignungs- und Güteprüfung nach DIN 4109

## Acoustic Ventilator



### Features

- High acoustic performance  $D_{n,e,w}$  50 dB
- Meets the ventilation requirements of Approved Document F 2006
- Unit dimensions to suit design requirements
- Choice of front or bottom inlet and discharge
- Simple design: replaces the brickwork above the window or can be built into the facade
- Easy to install: directly below the lintel and above the window
- Flush finish: complements the window design
- Thermal break can be incorporated
- Units can be polyester powder painted to match windows

### Ventilation Problems and the Solution

Providing natural ventilation to a room is essential for all modern buildings, however this can often lead to noise issues as using traditional trickle vents reduces the sound insulation performance of the façade, and consequently causes a rise in ambient noise levels within the room.

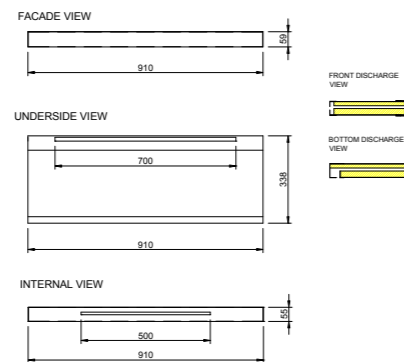
The Caice Acoustic Ventilator bridges the gap between the required ventilation as specified in Approved Document F 2006 and the typical criteria required for comfortable living ambient noise levels.

The acoustic ventilator is not designed to be part of the window, but part of the façade and therefore can sit above the window. Its dimensions are designed to simply replace a series of bricks, meaning that installation is straightforward and hassle free.

Of course not every window in a building will require a ventilator, so dummy panels can also be supplied to maintain a consistently superior look and finish to your building.

The acoustic ventilator shown was developed for a specific project and laboratory tests undertaken confirm the acoustic performance.

### Typical Ventilator Design



## Acoustic Ventilator

### Acoustic Performance

The acoustic ventilators have been tested at an independent test laboratory in accordance with BS EN 140-10, 1992; ISO 140-10, 1991 - Laboratory measurement of airborne sound insulation of small building elements. A measured performance of  $D_{n,e,w}$  50 dB was achieved.

|                | Octave Band Sound Reduction Index (dB) |     |     |    |    |    |    |
|----------------|--|-----|-----|----|----|----|----|
|                | 125                                    | 250 | 500 | 1k | 2k | 4k | 8k |
| $D_{n,e}$ (dB) | 33                                     | 40  | 45  | 56 | 67 | 75 | 69 |
| R (dB)         | 6                                      | 12  | 17  | 28 | 41 | 50 | 41 |

$D_{n,e,w}$  (C;Ctr) = 50 (-1,-5) dB

The difference between the  $D_{n,e}$  and R (the SRI) is that whereas  $D_{n,e}$  is the average composite loss of a typical wall structure with the vent installed, the SRI is the specific dB loss through the vent itself.

### Product Specification

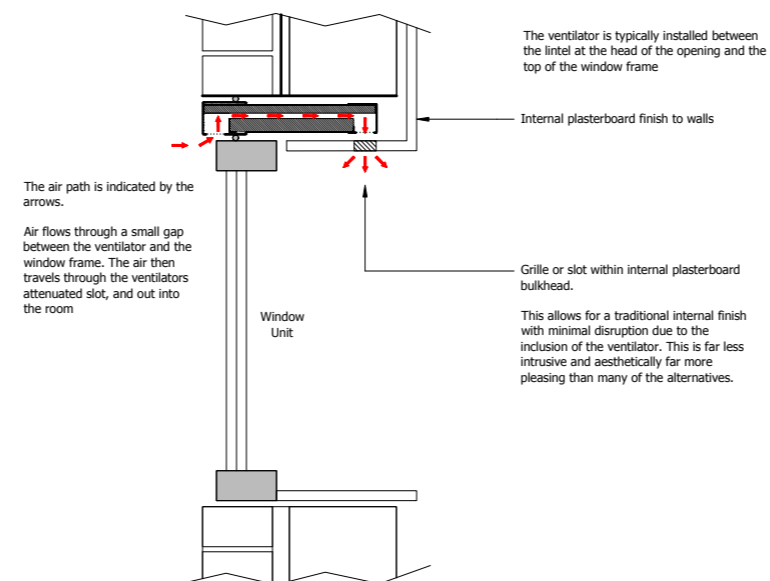
The outer casing shall be constructed with galvanised sheet steel. The acoustic media within the ventilator shall have a class "0" fire rating in accordance with BS 476 Part 24.

The ventilators shall be delivered to site suitably protected to prevent the ingress of dirt whilst on site, and shall be provided with labels detailing a description of the unit.

The manufacturer shall ensure that the ventilators will fit easily and correctly above the window and in the facade.

Polyester powder paints can be used to present the units in a manner that reflects the particular window design and colour scheme.

### Typical Installation







## List Of Companies :

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N20 0JZ

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210 High Holborn  
London WC1V 7DL  
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FAX +44 (0)20 7404 7980

ADS CONSULTANCY  
130 East Barnet Road,  
New Barnet,  
Herts EN4 8RE  
TEL (020) 8441 4123  
FAX (020) 8441 7114

SAVILLS  
Lansdowne House,  
57 Berkeley Square,  
London, W1J 6ER  
TEL +44 (0) 20 3320 8278

RIGHT OF LIGHT CONSULTING  
First Floor, Holborn Gate  
330 High Holborn  
London WC1V 7QT  
TEL 0800 197 4836

PRICE & MYERS  
30 Newman Street  
London W1T 1LT  
TEL 020 7631 5128  
FAX 020 7462 1390

ACA ACOUSTICS  
Hamilton House,  
Mabledon Place,  
Bloomsbury,  
London WC1H 9BB  
TEL 0207 554 8567  
FAX 0207 554 8501