## 25 Old Gloucester Street London

Environmental Noise Survey and Noise Impact Assessment Report

24421/NIA1 PL02 Rev3

18 July 2024

For: Box Associates Ltd Thompson House 42-44 Dolben House London SE1 0UQ



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## Environmental Noise Survey and Noise Impact Assessment Report 24421/NIA1 PL02 Rev3

## **Document Control**

Rev	Date	Comment	Prepared by	Authorised by
1	11/09/2023	Revised Planning Scheme 2	Nick Russell Principal Consultant MIOA	Robin Honey Director BA(Hons), MIOA
3	18/07/2024 Plant Details		N. mall	R. Hong
5	10/07/2024	Added	Nick Russell Principal Consultant MIOA	Robin Honey Director BA(Hons), MIOA



## Environmental Noise Survey and Noise Impact Assessment Report

## 24421/NIA1 PL02 Rev3

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- Appendix A Acoustic Terminology
- Appendix B Plant Noise Schedule
- Appendix C Time History Graphs

## 1.0 Introduction

25 Old Gloucester Street is to be refurbished as per the following description:

"Extension of basement to accommodate additional cultural centre accommodation (use class F1 and F2), replacement of second floor at rear to accommodate offices (class E1) and conversion of front part of building at second and third floor levels to create two new studio dwellings".

The apartments are to have a party wall and floor with the offices within the site and will overlook the front of the building.

It is also proposed to install building services plant on the roof of the building.

Hann Tucker have been commissioned to undertake an environmental noise survey in order to provide acoustic advice regarding the project.

This report presents the methodology and findings of our noise survey and assessment in the context of the National Planning Policy Framework (NPPF) and the requirements of the Local Authority.

## 2.0 Objectives

To assess the suitability of the site for the creation of residential properties based on noise data from our environmental noise survey.

To assess any likely transfer of noise from the commercial areas to the residential dwellings within the development.

To assess any likely transfer of noise from the commercial areas to the residential dwellings neighbouring the development.

To assess the likely plant noise and vibration emissions from proposed building services equipment.

### 2.1 Location

The site is located at 25 Old Gloucester Street, WC1N 3AF and falls within the jurisdiction of Camden London Borough Council. See Location Map below.



Location Map (Map Data ©2023 Google)

### 2.2 Description

The existing site is located at the south corner of Queen Square Park and Garden and is approximately 200m from Russell Square. There are a number of commercial properties surrounding the site and there are residential properties to the southeast. See Site Plan below.



Site Plan (Map Data ©2017 Google Imagery ©2023 The GeoInformation Group)

## 3.0 Acoustic Terminology

For an explanation of the acoustic terminology used in this report please refer to Appendix A enclosed.

## 4.0 Methodology

The survey was undertaken by Nick Russell MIOA and assisted by Luke Brough.

### 4.1 Procedure

Fully automated environmental noise monitoring was undertaken from approximately 13:15 hours on Thursday 25 May to 14:30 hours on Tuesday 30 May 2017.

Due to the nature of the survey, i.e. unmanned, it is not possible to accurately comment on the weather conditions throughout the entire survey period. However, at the beginning and end of the survey period the wind conditions were calm and the sky was generally clear with some occasional rain. We understand that generally throughout the survey period the weather conditions were very similar to this description and can therefore be considered as suitable for establishing typical background noise levels.

Measurements were taken continuously of the A-weighted (dBA) L<sub>90</sub>, L<sub>eq</sub> and L<sub>max</sub> sound

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pressure levels over 15-minute periods.

### 4.2 Measurement Positions

The noise level measurements were undertaken at two positions on the development site. The measurement positions are described in the table below.

Position No	Description
1	The microphone was attached to a pole and mounted out of a window on the front of the site. It was installed at a height of approximately 10m from ground level.
2	The microphone was mounted out of a window overlooking the disused play area at the rear of the site. It was installed at a height of approximately 1.5m from the play area roof.

These positions were chosen in order to establish typical noise levels at both the front and rear of the site.



Plan Showing Unmanned Measurement Positions

### 4.3 Instrumentation

The instrumentation used during the survey is presented in the table below:

Description	Manufacturer	Туре	Serial Number	Calibration
Type 1 Data Logging Sound Level Meter	Larson Davis	824	3444	Calibration on 11/07/2016
Type 1 ½" Condenser Microphone	РСВ	377B02	122885	Calibration on 11/07/2016
Type 1 Data Logging Sound Level Meter	Larson Davis	824	3443	Calibration on 10/03/2017
Type 1 ½" Condenser Microphone	PCB	377A02	107842	Calibration on 10/03/2017

## 5.0 Results

The results have been plotted on Time History Graphs 24421/TH1 to 24421/TH2 enclosed presenting the 15-minute A-weighted (dBA) L<sub>90</sub>, L<sub>eq</sub> and L<sub>max</sub> levels at each measurement position throughout the duration of the survey.

### 5.1 LA90 Noise Levels

The following table presents the lowest modal LA90 background noise levels during the survey:

	Lowest Modal L <sub>A90</sub> Background Noise Level (dB re 2 x 10 <sup>-5</sup> Pa)				
Position	Daytime (07:00 – 23:00) Hours	Night-Time (23:00 – 07:00) Hours	24 Hours		
1	48	45	45		
2	46	44	44		

### 5.2 Leq Noise Levels

In order to compare the results of our survey with suitable guidelines it is necessary to convert the measured  $L_{Aeq(15 \text{ minute})}$  noise levels into single figure daytime  $L_{Aeq(16 \text{ hour})}$  (07:00-23:00 hours) and night-time  $L_{Aeq(8 \text{ hour})}$  (23:00-07:00 hours) levels. The daytime  $L_{Aeq(16 \text{ hour})}$  and night-time  $L_{Aeq(8 \text{ hour})}$  noise levels for each position are presented in the tables below.

Position	Daytime L <sub>Aeq(16-hour)</sub>	Night-Time L <sub>Aeq(8-hour)</sub>
1	59dB	52dB
2	52dB	47dB

### 5.3 Night-time L<sub>max</sub> Results

The following table presents the number of  $L_{max}$  events which exceeded 80dBA during the night-time periods.

Doto	No of Events			
Date	Position 1	Position 2		
25/05/2017 to 26/05/2017	1	0		
26/05/2017 to 27/05/2017	2	0		
27/05/2017 to 28/05/2017	1	0		
28/05/2017 to 29/05/2017	2	1		
29/05/2017 to 30/05/2017	1	0		

## 6.0 Discussion Of Noise Climate

Due to the nature of the survey, i.e. unmanned, it is not possible to accurately describe the dominant noise sources, or specific noise events throughout the entire survey period. However, at the beginning and end of the survey period the dominant noise source was noted to be road traffic noise from the surrounding area.

## 7.0 Planning Policy/Guidance

## 7.1 National Planning Policy Framework (NPPF)

The following paragraph is from the NPPF:

"123.Planning policies and decisions should aim to:

- avoid noise from giving rise to significant adverse impacts on health and quality of life as a result of new development;
- mitigate and reduce to a minimum other adverse impacts on health and quality of life arising from noise from new development, including through the use of conditions;
- recognise that development will often create some noise and existing businesses wanting to develop in continuance of their business should not have unreasonable restrictions put on them because of changes in nearby land uses since they were established; and
- identify and protect areas of tranquillity which have remained relatively undisturbed by noise and are prized for their recreational and amenity value for this reason."

## 7.2 Local Authority Criteria

We understand Camden Council have imposed the following Condition (7) for external noise intrusion on the site:

"The design and structure of the residential parts of the development shall be of such a standard that it will protect residents within it from existing external noise so that they are not exposed to levels indoors of more than 35 dB LAeq 16 hrs daytime and of more than 30 dB LAeq 8 hrs in bedrooms at night."

Various reference documents including BS 8233: 2014 edition and WHO Community Noise Guidelines present acoustic criteria for residential premises, as outlined below. These guidelines are entirely discretional.

### 7.3 BS8233

British Standard 8233: 2014 "Guidance on sound insulation and noise reduction for buildings" provides guidance for the control of noise in and around buildings.

Section 7.7.2 "Internal ambient noise levels for dwellings" states:

In general for steady external noise sources, it is desirable that internal ambient noise levels do not exceed the following guideline values:

Λοτινίτι	Location	Desirable Internal Ambient Criteria		
Activity	Location	07:00 – 23:00	23:00 to 07:00	
Resting	Living Rooms	35 dB LAeq, 16hour	-	
Dining	Dining Room/Area	40 dB LAeq, 16hour	-	
Sleeping (Daytime Resting)	Bedroom	35 dB LAeq, 16hour	30 dB LAeq,8hour	

Note 7 states:

"Where development is considered necessary or desirable, despite external noise levels above WHO guidelines, the internal target levels may be relaxed by up to 5 dB and reasonable internal conditions still achieved".

Section 7.7.3.2 "Design criteria for external noise" states:

"For traditional external areas that are used for amenity space, such as gardens and patios, it is desirable that the external noise level does not exceed 50 dB  $L_{Aeq,T}$ , with an upper guideline value of 55 dB  $L_{Aeq,T}$  which would be acceptable in noisier environments. However, it is also recognized that these guideline values are not achievable in all circumstances where development might be desirable. In higher noise areas, such as city centres or urban areas adjoining the strategic transport network, a compromise between elevated noise levels and other factors, such as the convenience of living in these locations or making efficient use of land resources to ensure development needs can be met, might be warranted. In such a situation, development should be designed to achieve the lowest practicable levels in these external amenity spaces, but should not be prohibited".

### 7.4 Proposed Criteria

On the basis of the above we would propose the following internal noise levels be adopted as <u>minimum</u> design targets in the <u>worst</u> affected dwellings.

Activity	Location	Desirable Internal Ambient Criteria		
Activity	Location	07:00 - 23:00	23:00 to 07:00	
Resting	Living Rooms	35 dB L <sub>Aeq,16hour</sub>	-	
Dining	Dining Rooms	35 dB L <sub>Aeq,16hour</sub>	-	
Sleeping (Daytime Resting)	Bedroom	35 dB L <sub>Aeq,16hour</sub>	30 dB LAeq,8hour	

## 8.0 Achievable Internal Noise Levels

We have predicted the levels that would be achievable in the studio apartments from external noise ingress. A simple assessment based on a typical outside to inside sound reduction of 33dB(A) indicates the following noise levels may be expected within the proposed worst-case dwellings with typical thermal double or secondary glazing.

Façade	Daytime LAeq(16-hour)	Night-time LAeq(8-hour)
East	26dBA	19dBA
North	26dBA	19dBA

These predicted worst case internal noise levels meet the proposed criteria. It is thus demonstrated that acceptable internal noise levels are achievable.

# 9.0 Separating Floor Assessment (First Floor Office to Second Floor Residential)

There are offices proposed on the first floor at the east section of the building below the secondfloor studio apartment. These offices are independent of the community centre.

We understand that the intermediate floor slab is 250mm thick solid concrete and that a mass barrier ceiling will be installed in the offices. This ceiling shall have an air gap of 150mm with 50mm of mineral wool in the cavity. The lower ceiling will be constructed from two layers of 12.5mm Soundbloc plasterboard installed on acoustic hangers. Our assessment of this construction is that it should provide the following airborne sound reduction:

Description		Sound Reduction Indices, (dB) at Octave Band Frequencies (Hz)						
		125	250	500	1K	2K	4K	8K
250mm thick concrete slab with mass barrier ceiling detailed above		55	59	66	73	75	78	78

In order to achieve a low impact noise from the ground floor in the residential dwellings above we would recommend that a noise criterion of NR15 should be adopted.

In order to calculate the limiting noise levels permissible within the first floor in order to achieve a noise level of NR15 within the residential dwellings above, the following equation was used:

$$L_{pLIM} = L_{p2} + R - 10\log(Sp) + 10\log(A)$$

Where:

L <sub>P2</sub>	=	Required noise level in residence.
L <sub>PLIM</sub>	=	Limiting sound pressure level in Office
R	=	Approximate composite SRI of floor.
Sp	=	Approximate surface area of partition wall (m <sup>2</sup> ) (bedroom).
A	=	Total absorption in receive room (m <sup>2</sup> ).

The total absorption (A) was calculated by multiplying the absorption co-efficient ( $\alpha$ ) by the surface area of the room. Typical values for a bedroom were used in the calculation.

Description	Octave Band Centre Frequencies (Hz)							
Description	63	125	250	500	1k	2k	4k	8k
LP2 (NR15)	47	35	26	19	15	12	9	7
R	46	55	59	66	73	75	78	78
10logSp	9	9	9	9	9	9	9	9
α	0.1	0.18	0.25	0.27	0.31	0.32	0.32	0.35
Room Surface Area	45	45	45	45	45	45	45	45
10logA	7	9	11	11	12	12	12	12
LPLIM	91	90	87	87	91	90	90	88

The table below shows the details of our calculation:

Therefore, in order to achieve an internal level of NR15 in the residential dwellings above the ground floor, the maximum noise levels should be limited to the following:

First Floor Limiting Sound Pressure Levels (dB Lmax) at Octave Band Centre Frequency (Hz)								
63	125	250	500	1k	2k	4k	8k	dBA
91	90	87	87	91	90	90	88	97

The above limiting maximum sound pressure levels are significantly higher than those we have in our company database for typical office usage and hence we can see no reason why these offices should be a source of noise complaint from residents in the dwellings above. Suitable resilient layers within the residential floor will be installed to limit impact noise to the offices below from residents.

## **10.0 Separating Wall Assessment**

The proposed studio apartments have an adjoining party wall to the first-floor lecture hall and the second-floor offices as detailed in the following sketch:



The existing construction of the party walls is brickwork and as follows:

Studio 1- 350mm thick wall, 328mm brick and 25mm plaster.

Studio 2- 240mm thick wall, 215mm brick and 25mm plaster.

As part of the work on site these walls will be taken back to the brickwork and a new stud wall will be added for fire compartmentation and increasing U-values. This will comprise a new metal independent stud with 110mm insulation, a 25mm service zone and 12.5mm plasterboard with a 10mm parge coat.

### **10.1 Studio Apartment Walls**

Our assessment of the proposed construction of the studio apartment walls is that they should provide the following airborne sound reduction:

Description		Airborne Sound Reduction (dB) at Octave Band Frequencies (Hz)							
		125	250	500	1K	2K	4K	8K	
Studio 1 350mm thick brickwork, independent 135mm stud wall with 110mm insulation, 12.5mm plasterboard and 10mm parge coat	38	55	72	85	96	103	102	100	
Studio 2 240 mm thick brickwork, independent 135mm stud wall with 110mm insulation, 12.5mm plasterboard and 10mm parge coat	35	49	68	79	91	98	97	95	

In order to achieve a low impact noise from the ground floor in the residential dwellings above we would recommend that a noise criterion of NR15 should be adopted.

In order to calculate the limiting noise levels permissible within the first floor in order to achieve a noise level of NR15 within the residential dwellings above, the following equation was used:

$$L_{pLIM} = L_{p2} + R - 10\log(Sp) + 10\log(A)$$

Where:

- L<sub>P2</sub> = Required noise level in residence.
- L<sub>PLIM</sub> = Limiting sound pressure level in Office
- R = Approximate composite SRI of floor.
- Sp = Approximate surface area of partition floor  $(m^2)$  (bedroom).
- A = Total absorption in receive room  $(m^2)$ .

The total absorption (A) was calculated by multiplying the absorption co-efficient ( $\alpha$ ) by the

surface area of the room. Typical values for a bedroom were used in the calculation.

The table below shows the details of our calculation for the Studio 2 wall, which has the worst acoustic performance:

Description	Octave Band Centre Frequencies (Hz)							
Description	63	125	250	500	1k	2k	4k	8k
LP2 (NR15)	47	35	26	19	15	12	9	7
R	35	49	68	79	91	98	97	95
10logSp	9	9	9	9	9	9	9	9
α	0.1	0.18	0.25	0.27	0.31	0.32	0.32	0.35
Room Surface Area	45	45	45	45	45	45	45	45
10logA	7	9	11	11	12	12	12	12
LPLIM	80	84	96	90	109	113	109	105

Therefore, in order to achieve an internal noise level of NR15 in the residential dwellings above the ground floor, the maximum noise levels should be limited to the following:

Indicative First Floor Limiting Sound Pressure Levels (dB Lmax) at Octave Band Centre Frequency (Hz)								
63	125	250	500	1k	2k	4k	8k	dBA
80	84	96	90	109	113	109	105	117

The above limiting maximum airborne sound pressure levels, for the worst-case wall acoustically, are significantly higher than those we have in our company database for typical office usage and hence we can see no reason why these offices should be a source of noise complaint from residents in the dwellings above. The above calculation of the likely sound insulation should be checked by carrying out pre completion sound insulation testing.

It is understood that the Lecture Hall may be used as a meeting/lecture room with some religious ceremonies or lectures. It is understood that reproduced music could be played but will be limited to reasonable levels. Our database for religious ceremonies with some music indicates that the above limiting levels are unlikely to be exceeded. (It should be noted that the limiting levels above are for the Studio 2 wall; the Studio 1 wall levels are around 5dB higher in each octave).

Suitable resilient layers within the residential floors will be installed to limit impact noise to the offices below from residents.

## **11.0** Noise Breakout to Neighbouring Properties

We have also considered the potential noise breakout to other adjacent properties through the building fabric from typical internal noise levels associated with religious ceremonies containing reasonable levels of reproduced music. The adjacent properties comprise a number of residential dwellings at the rear of the building and a church to the north.

Our calculations indicate that with suitably designed secondary glazing, to the proposed ground floor lounge and the first-floor lecture hall, the external noise levels at one metre to the nearest neighbouring property should be around  $45dBL_{max}$  and  $35dB L_{Aeq}$ . The latter is approximately 17dB below the single figure daytime  $L_{Aeq(16-hour)}$  (07:00-23:00 hours) at Position 2 of 52dBA. In accordance with the National Planning Practice Guidance based upon the Noise Policy Statement for England this is not noticeable and hence no specific actions should be required.

## 12.0 Plant Noise Emission Criteria

The London Borough of Camden has imposed Condition 12 pertinent to noise from building services plant as detailed below.

"Prior to commencement of the development, details shall be submitted to and approved in writing by the Council, of the external noise level emitted from plant/ machinery/ equipment and mitigation measures as appropriate. The measures shall ensure that the external noise level emitted from plant, machinery/ equipment will be lower than the lowest existing background noise level by at least 10dBA, by 15dBA where the source is tonal, as assessed according to BS 4142:2014 "Methods for rating and assessing industrial and commercial sound" at the nearest and/or most affected noise sensitive premises, with all machinery operating together at maximum capacity. A post installation noise assessment shall be carried out where required to confirm compliance with the noise criteria and additional steps to mitigate noise shall be taken, as necessary. Approved details shall be implemented prior to occupation of the development and thereafter be permanently retained."

Based on the above and the measured noise levels summarised in Section 5.1, we therefore propose the following plant noise emission criteria to be met at 1m outside the nearest neighbouring residential property.

	Limiting Plant Noise Rating Level (dBA re 2x10-5 Pa)			
Position	Daytime (07:00–23:00 hours)	Night-time (23:00–07:00 hours)		
1	38	35		
2	36	34		

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It should be noted that the above criteria are subject to final approval by the London Borough of Camden.

## **13.0 Plant Noise Assessment**

### 13.1 Proposed Plant

The proposed new building services plant is as detailed in the following table.

Plant Description	Location	Qty	Plant Make	Model Number
Air Handling Unit	Roof	1	Nuaire	N17T/EN/ES/LWP
Kitchen Supply Fan	Roof	1	Nuaire	ESBHS5-E
Kitchen Extract Fan	Roof	1	Nuaire	SQFA44ES
External Condensers	Roof	2	Mitsubishi	PUHY-P700SNW-A2
External Condensers	Roof	2	Mitsubishi	PUHY-P450SNW-A2
MVHR Unit	Lower Roof	1	Nuaire	MRXBOXAB-XBC+25

### 13.2 **Operating Hours**

The plant is proposed to operate continuously.

### 13.3 Plant Noise Data

The manufacturer's noise data for the equipment is as detailed in our Plant Noise Schedule 24421/PNS in Appendix B.

### 13.4 Location of Plant

It is proposed to install the building services plant as detailed in the drawing below.



The nearest noise sensitive residential window to the plant area is at the rear of 26 Old Gloucester Street. These windows are at the same height as the plant and approximately 7 metres away to the southeast of the plant.

### 13.5 Plant Noise Impact Assessment

We understand that the plant could be operational continuously.

It should be noted that the proposed plant is not anticipated to exhibit any tonal or impulsive characteristics provided it is well maintained.

The following tables summarise our predictions of atmospheric noise emissions from the proposed plant location to the nearest noise sensitive residential window.

### 13.5.1 Condensers

The four condensers are to be installed in an acoustic enclosure that reduces the noise level by 25dBA. In addition, they will be located behind an imperforate screen that provides a reduction of at least 14dBA as an acoustic barrier effect in the direction of the rear of 26 Old Gloucester Street.

The following table details our calculations for the condensers.

	Sound Level (dBA)
Sound Power Level of Condenser	86
Cumulative Noise Level of 4 Condensers (+6dB)	92
Reduction of Acoustic Enclosure	-25
Barrier Correction Imperforate Screen	-14
Distance Correction 6m Hemispherical Radiation	-24
Façade Reflection	+3
Calculated Noise Level at Receptor	29dBA

### 13.5.2 Air Handling Unit

The air handling unit has two atmospheric ducts which are facing to the west of the site. These ducts will each have attenuators that reduce the noise to a maximum level of 50dBA at 1m.

The following table details our calculations for these ducts.

	Sound Pressure Level (dBA)
Sound Level of each Atmospheric Duct at 1m	50
Cumulative Noise Level of 2 Ducts (+3dB)	53
Distance Correction 6m Hemispherical Radiation 180 Degrees Directivity	-30
Façade Reflection	+3
Calculated Noise Level at Receptor	26dBA

### 13.5.3 Kitchen Fans

The supply and the extract fans have atmospheric ducts that are facing west and are approximately 13m away from the rear of 26 Old Gloucester Street. These ducts will each have attenuators that reduce the noise to a maximum level of 40dBA at 1m.

The following table details our calculations for these ducts.

	Sound Pressure Level (dBA)
Sound Level of each Atmospheric Duct at 1m	40
Cumulative Noise Level of 2 Ducts (+3dB)	43
Distance Correction 6m Hemispherical Radiation 0 Degrees Directivity	-16

Façade Reflection	+3
Calculated Noise Level at Receptor	30dBA

### 13.5.4 MVHR Unit

The MVHR unit has two atmospheric ducts which discharge vertically. These ducts will each have attenuators that reduce the noise to a maximum level of 40dBA at 1m.

The following table details our calculations for these ducts.

	Sound Pressure Level (dBA)
Sound Level of each Atmospheric Duct at 1m	40
Cumulative Noise Level of 2 Ducts (+3dB)	43
Distance Correction 6m Hemispherical Radiation 90 Degrees Directivity	-23
Façade Reflection	+3
Calculated Noise Level at Receptor	23dBA

### 13.5.5 Cumulative Noise Level of All Plant

The following table details our calculations for all of the plant operating if it operates together.

	Sound Pressure Level at Receptor (dBA)
Condensers	29
Air Handling Unit Atmospheric Ducts	26
Kitchen Fans Atmospheric Ducts	30
MVHR Units Atmospheric Ducts	23
Cumulative Noise Level at Receptor	33dBA

Our calculations therefore indicate that in the worst-case scenario of all plant operating at once, the proposed night-time noise criterion of 34dBA should be achieved.

### 13.6 Anti Vibration Measures

The London Borough of Camden have imposed Condition 6 as detailed below.

"Prior to use, machinery, plant or equipment at the development shall be mounted with proprietary anti-vibration isolators and fan motors shall be vibration isolated from the casing and adequately silenced and maintained as such."

All plant proposed for installation at the site will be installed on anti-vibration mounts that provide a minimum isolation efficiency of 95%. This should render any reradiated noise from the plant inaudible within the demise of the site and also in any adjoining properties. Plant will be maintained to ensure that vibration levels will constantly achieve the above isolation efficiency.

## 14.0 Conclusions

A detailed environmental noise survey has been undertaken in order to establish the currently prevailing environmental noise climate around the site.

Appropriate internal noise criteria have been proposed. These are achievable using conventional constructions.

The environmental noise impact upon the proposed dwellings has been assessed in the context of the NPPF and the requirements of the Local Authority. Mitigation advice to reduce to a minimum the adverse impact on health and quality life arising from environmental noise have been recommended.

An assessment of the noise impact from the first to second floor of the building has been undertaken, with regards to the internal second floor dwelling, and our calculations indicate that the intermediate structure proposed should provide suitable acoustic isolation.

An assessment of the noise impact from likely activities in the ground and first floors of the building to external neighbouring properties has been undertaken and our calculations indicate that with suitably designed glazing no specific actions are likely to be required acoustically.

Based upon the results of our survey and subsequent assessments the proposed development is considered compliant with the local policy of the London Borough of Camden and the Conditions imposed on noise and vibration.

## Appendix A

### **Acoustic Terminology**

The acoustic terms used in this report are defined as follows:

- dB Decibel Used as a measurement of sound level. Decibels are not an absolute unit of measurement but an expression of ratio between two quantities expressed in logarithmic form. The relationships between Decibel levels do not work in the same way that non-logarithmic (linear) numbers work (e.g. 30dB + 30dB = 33dB, not 60dB).
- dBA The human ear is more susceptible to mid-frequency noise than the high and low frequencies. The 'A'-weighting scale approximates this response and allows sound levels to be expressed as an overall single figure value in dBA. The A subscript is applied to an acoustical parameter to indicate the stated noise level is A-weighted

It should be noted that levels in dBA do not have a linear relationship to each other; for similar noises, a change in noise level of 10dBA represents a doubling or halving of subjective loudness. A change of 3dBA is just perceptible.

- $L_{90,T}$   $L_{90}$  is the noise level exceeded for 90% of the period T (i.e. the quietest 10% of the measurement) and is often used to describe the background noise level.
- $L_{eq,T}$   $L_{eq,T}$  is the equivalent continuous sound pressure level. It is an average of the total sound energy measured over a specified time period, *T*.
- L<sub>max</sub> L<sub>max</sub> is the maximum sound pressure level recorded over the period stated. L<sub>max</sub> is sometimes used in assessing environmental noise where occasional loud noises occur, which may have little effect on the L<sub>eq</sub> noise level.
- L<sub>p</sub> Sound Pressure Level (SPL) is the sound pressure relative to a standard reference pressure of 2 x 10<sup>-5</sup> Pa. This level varies for a given source according to a number of factors (including but not limited to: distance from the source; positioning; screening and meteorological effects).
- L<sub>w</sub> Sound Power Level (SWL) is the total amount of sound energy inherent in a particular sound source, independent of its environment. It is a logarithmic measure of the sound power in comparison to a specified reference level (usually 10<sup>-12</sup> W).

Appendix B

Plant Noise Schedule

Plant Noise Schedule

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Revision: 0	Date: 17 July 2024	Prepared by: Nick Russell		Comments: Plant Confirmed										
			Duty		Sound Level (dB) at   Data Octave Band Centre Frequency (Hz)								z)	
Plant Ref.	Location	Plant Type	m³/s	Ра	mfr/empir	Lw/Lp	63	125	250	500	1k	2k	4k	8k
AHU1	Roof	Air Handling Unit			mfr	Open Intake Lw	61	53	66	57	56	52	39	29
					mfr	Open Supply Lw	73	72	82	86	85	81	77	75
					mfr	Open Extract Lw	61	53	66	57	56	52	39	29
					mfr	Open Exhaust Lw	73	72	82	86	85	81	77	75
KSF1	Roof	Kitchen Supply Fan			mfr	In Duct Intake Lw		79	74	69	69	65	60	54
					mfr	In Duct Supply Lw		81	81	76	76	72	69	63
KEF1	Roof	Kitchen Extract Fan			mfr	In Duct Extract Lw		79	74	69	69	65	60	54
					mfr	In Duct Exhaust Lw		81	81	76	76	72	69	63
COND 1-3	Roof	External Condenser			mfr	Lp at 1m	70dBA							
MVHR1	Internal (Ducted to Roof)	Ventilation Unit			mfr	In Duct Intake Lw	77	71	69	71	66	62	54	53
					mfr	In Duct Supply Lw	82	83	78	82	72	72	68	70
					mfr	In Duct Extract Lw	76	70	68	71	65	62	54	54
					mfr	In Duct Exhaust Lw	83	84	78	81	72	72	70	71

#### 25 Old Gloucester Street, London

The above data represent 'maximum' noise levels which should therefore not be exceeded. It is essential that Hann Tucker Associates are appraised of any alterations or additions to this list. Page 1 of 1 Appendix C

Time History Graphs





Date and Time

24421/TH1





Date and Time

24421/TH2