

Plot 5 & 6, Central Somers Town, London, NW1 1DN

Planning Condition Statement

This statement has been produced in order to discharge condition 29 of planning application ref.: 2022/2855/P for Plot 5 and Plot 6 of the Central Somers Town development in the London Borough of Camden.

The decision notice references the below documents previously issued by Price & Myers.

- Polygon Residential, Plot 5 SuDS Drainage Statement version 1 (prepared by Price & Myers) 20.11.15
- Polygon Residential, Plot 6 SuDS Drainage Statement version 1 (prepared by Price & Myers) 20.11.15

This statement should therefore be read in conjunction with the abovementioned reports.

Planning History

The original planning application reference was 2015/2740/P, in which these documents were first submitted in support of. They were referenced in this planning approval decision notice. Following this there was a submission made to the London Borough of Camden, ref.: 2018/2856/P which refers to the discharge of conditions relating to Plots 1 and 4. In 2022 a submission, ref.: 2022/2855/P, was made for variation or removal of conditions to Section 106 legal agreement relating to Plots 5 and 6. It is condition 29 of this decision notice that this statement has been compiled in order to discharge.

Condition 29

"SuDS

Plot 1 - The SuDS shall be built in line with the details approved under planning reference 2018/2856/P dated 25 August 2020 and shall remain in accordance thereafter.

Other plots - Prior to commencement of the relevant part of the development details of a sustainable urban drainage system shall be submitted to and approved by the local planning authority in writing. Such details shall include details of the following features:

- Permeable surfacing to all hard standing areas, with a minimum 250mm sub-base, totalling 390m³ attenuation discharging to the public sewer at a reduced rate.
- Details of any weirs required within the sub-base to ensure that the full storage volume is utilised and to avoid lower areas becoming overwhelmed.

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- Details of how rainfall falling on impermeable pathways or roads is shed and attenuated in adjacent grassed or planted areas to include swales or bio-retention / rain gardens and details of how these are connected to the sub-base of the paving areas to provide an even greater storage volume.
- A network of perforated pipes collecting the filtered runoff and conveying it to the public sewer.
- Details of permeable surfacing to all play areas.
- Full details of wetland areas.

SuDS will be implemented prior to the opening of the relevant parts of the development.

Reason: To reduce the rate of surface water run-off from the buildings and limit the impact on the storm-water drainage system in accordance with policy CC1 of the Camden Local Plan 2017."

Approved SuDS Strategy

The two SuDS Drainage Statements referred to in the decision notice, were produced by Price & Myers for the original planning application submission back in 2015 for Plots 5 and 6.

These statements set out the following drainage strategies:

- Surface water system designed for 1 in 100 year + 30% climate change.
- Infiltration is not feasible on site due to the site being underlain by London Clay.
- Each plot will discharge at 5 l/s (total 10 l/s), the minimum that can be achieved due to the risk of blockages, via new direct connections to the public sewer in Purchese Street.
- Plot 5 requires a 16m³ attenuation tank.
- Plot 6 requires a 16m³ attenuation tank.

These strategies were approved as part of the planning application approval.

Final SuDS Strategy

The design was developed in accordance with the above approved strategy.

Due to discoveries on site it was found that Plot 5 and Plot 6 could combine prior to their final discharge point to the public sewer. This reduced the requirement for two new direct connections to one single direct connection. In making the S106 application to Thames Water the proposed discharge rate of 10 l/s was questioned, and it was requested for this to be reduced as much as possible. It was therefore agreed that each site would discharge at 2.5 l/s, with a total surface water discharge of 5 l/s from the entire development site.

This resulted in an increased in the attenuation tank sizes. Plot 5's attenuation tank increased from 16m³ to 19.5m³, and Plot 6's tank increased from 16m³ to 27.5m³.

The Plots also utilise permeable paving, bound gravel, in the external areas. The Landscape Architects drawing should be referred to for the proposed surface finishes locations. As shown on the drainage layout drawings, perforated pipes are to be constructed within the sub-base of the permeable paving in order to drain the surface water from these areas that is not able to infiltrate into the ground. There is no requirement for weirs within the sub-base of the permeable paving based on the proposed levels and gradients across the site. Gullies are proposed within the lightwells which are set at a lower level. Where permeable paving is not proposed in the external ground floor areas, slot drains have been proposed. Small hardstanding paths which are adjacent to soft landscaping areas, can drain directly into the soft landscaping.

Refer to the proposed drainage layout drawings appended to the rear of this document. The below ground drainage network was modelled in MicroDrainage, the calculations of which have been appended to this document.

Play Areas

There are no play areas within Plot 5 or 6 of this development.

Appendices

P&M Drawings:

- TM54A008-PAM-Z5-ZZ-DR-C-6000 Below Ground Drainage Layout Plot 5
- TM54A008-PAM-Z6-ZZ-DR-C-6001 Below Ground Drainage Layout Plot 6
- TM54A008-PAM-ZZ-ZZ-DR-C-6100 Below Ground Drainage Details Sheet 1
- TM54A008-PAM-ZZ-ZZ-DR-C-6101 Below Ground Drainage Details Sheet 2
- TM54A008-PAM-ZZ-ZZ-DR-C-6102 Below Ground Drainage Details Sheet 3
- TM54A008-PAM-ZZ-ZZ-DR-C-6103 Below Ground Drainage Details Sheet 4
- TM54A008-PAM-ZZ-ZZ-SH-C-6200 Manhole Schedule

Calculations:

- 30198_CST_Plot 5_MD_Calculations
- 30198_CST_Plot 6_MD_Calculations

Prepared by:	Kirsty Burwood MEng CEng MICE MCIHT
Job Number:	30198
Date:	28.03.2024
Version:	2



REFER TO DRAWING 30198 / 6001

NOTES :

- This drawing is to be read in conjunction with all relevant Architect's, Engineer's and specialists' drawings and specifications.
- 2. Do not scale from this drawing in either paper or digital form. Use written dimensions only. To check that this drawing has been printed to the intended scale this bar should be 50mm long @ A1 or 25mm long @ A3.
- 3. Health & Safety : All specific drawing notes are to be read in conjunction with the project "Information Pack" and "Site Rules".
- 4. Setting out of all drain point positions to be provided by M&E Engineer and Architect.
- 5. Refer to general notes drawing 30198/05/0001.

DRAINAGE LEGEN	DRAINAGE LEGEND					
Existing Combined S New FW Drain New SW Drain Perforated Pipework New Combined Drair Existing Drainage to Demolished	ewer					
	Rainwater Down Pipe					
FWP	Foul Waste Pipe					
S1 🔘 🔲	Surface Water Manhole Chamber					
F1	Foul Water Manhole Chamber					
FCMH1	Flow Control Chamber (SW only)					
\otimes	Non-return flap valve					
	Attenuation Cells					
FG	Floor Gully					
SD	Slot Drain with Sump Unit					
RE	Rodding Eye					
ABBREVIATIONS						
IL - Invert CL - Cover RA - Above CP - Catch	Level Level Ground Rodding Access Pit Manhole					

C04	21.09.23	FG	JL	Issued for Construction
C03	25.08.23	DLa	JL	Issued for Construction
C02	21.07.23	SE	JL	Issued for Construction
C01	12.07.23	SE	JL	Issued for Construction
P03	11.05.23	FG	JL	issued for Information
P02	21.04.23	FG	JL	Stage 4 - Issued for DT Review
P01	28.10.22	TP	JL	Issued for Stage 3
Rev	Date	Drawn	Eng	Amendment

CENTRAL SOMERS TOWN PLOT 5 & 6

BELOW GROUND

DRAINAGE LAYOUT

Status

FOR CONSTRUCTION

Drawn TP	Eng JL				
Scales 1:100 at A1	1:200 at A3				
Drawing No	Rev				
30198/6000	C04				
110134A000-FA101-23-22-DR-0-0000					



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<u> </u>	Thames W	ater culvert			
	drawings fo	or sections	relative to	D	
	proposed id	Junuations			
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- 5. Refer to general notes drawing 30198/05/0001.

DRAINAGE LEGEN	DRAINAGE LEGEND					
Existing Combined Sewer						
New FW Drain	```````					
New SW Drain						
Perforated Pipework	>					
New Combined Drai						
Existing Drainage to Demolished	be <u>*********</u>					
DRAINAGE KEY						
RWP	Rainwater Down Pipe					
•FWP	Foul Waste Pipe					
S1 🔘 🔲	Surface Water Manhole Chamber					
F1	Foul Water Manhole Chamber					
FCMH1	Flow Control Chamber (SW only)					
\otimes	Non-return flap valve					
	Attenuation Cells					
FG	Floor Gully					
SD	Slot Drain with Sump Unit					
RE	Rodding Eye					
ABBREVIATIONS						
IL - Invert CL - Cover RA - Above CP - Catch	Level Level Ground Rodding Access Pit Manhole					

C03	25.08.23	DLa	JL	Issued for Construction
C02	21.07.23	SE	JL	Issued for Construction
C01	06.07.23	TP	JL	Issued for Construction
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P01	28.10.22	SE	JL	Issued for Stage 3
Rev	Date	Drawn	Eng	Amendment

CENTRAL SOMERS TOWN PLOT 5 & 6

DRAINAGE LAYOUT

FOR CONSTRUCTION

Status

Drawn TP

Drawing No

Doc Ref.

Scales 1:100 at A1

BELOW GROUND

C03 30198/6001 TM54A008-PAM-Z6-ZZ-DR-C-6001

Eng JL

Rev

1:200 at A3



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	Rocker pipe	
IN		

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C02	25.08.23	TP	JL	Issued for Construction
C01	05.07.23	ΤP	JL	Issued for Construction
P03	11.05.23	FG	JL	Issued for Information
P02	21.04.23	FG	JL	Stage 4 - Issued for DT Review
P01	28.10.22	TP	JL	Issued for Stage 3
Rev	Date	Drawn	Eng	Amendment

CENTRAL SOMERS TOWN PLOT 5 & 6

BELOW GROUND

SHEET 1

Status

Drawn TP

Drawing No

Doc Ref.

Scales 1:20 at A1

30198/6100

DRAINAGE DETAILS

FOR CONSTRUCTION

TM54A008-PAM-ZZ-ZZ-DR-C-6100

C01	05.07.23	TP	JL	Issued for Construction
P03	11.05.23	FG	JL	Issued for Information
P02	21.04.23	FG	JL	Stage 4 - Issued for DT Review
P01	28.10.22	TP	JL	Issued for Stage 3
Rev	Date	Drawn	Eng	Amendment

CENTRAL SOMERS TOWN						
Rev	Date	Drawn	Eng	Amendment		
P01	28.10.22	ΤP	JL	Issued for Stage 3		

C02	25.08.23	IP	JL	Issued for Construction
C01	05.07.23	TP	JL	Issued for Construction
P03	11.05.23	FG	JL	Issued for Information
P02	21.04.23	FG	JL	Stage 4 - Issued for DT Review
P01	28.10.22	TP	JL	Issued for Stage 3



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Eng JL

1:40 at A3

Rev

C02







SCALE 1:10

NOTES :

relevant Architect's, Engineer's and specialists' drawings

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CLASS S SURROUND

GRANULAR SURROUND & BACKFILL FOR AREAS SUBJECT TO VEHICLE LOADING

Backfill with Type 1 granular sub-base material compacted in 150 thick layers

Ferram 1000 to bed and surround shall be used where pipes are laid in fill material, soft ground and below the water table

Coarse aggregate for pipe bedding and surround material to BS EN 13242. Refer to R12/667



Backfill with material excavated from trench

Selected as dug fill R12 / 616

Terram 1000 to bed and surround shall be used where pipes are laid in fill material, soft ground and below the water table.

Coarse aggregate for pipe bedding and surround material to BS EN 13242. Refer to R12/667

CLASS S SURROUND

GRANULAR SURROUND & BACKFILL FOR SOFT OR HARD LANDSCAPING AREAS NOT SUBJECT TO VEHICLE LOADING

> Class Y surround for cover <300 Class W surround for cover >300

TABLE 1

DN	Minimum trench	Minimum trench width (OD + x)				
	Supported	Unsupported tre	Unsupported trench			
	uench	# > 60°	# < 60°			
less 225	600	600	600			
225 to 350	800	800	800			
350 to 700	OD + 700	OD + 700	OD + 400			
700 to 1200	OD + 850	OD + 850				
greater 1200	OD + 1000	OD + 1000	OD + 400			

In the values OD + x, x/2 equals the minimum working space between the pipe and the trench wall or support, where:

OD is external diameter. # is angle of unsupported trench side measured to the horizontal.

MINIMUM TRENCH WIDTH IN RELATION TO NORMAL SIZE DN

Trench depth	Minimum trench width
ess 1000	As Table 1
1000 to 1750	800
1750 to 4000	900
greater 4000	1000

The minimum trench width shall be the greater of the values taken from tables 1 & 2.

MINIMUM TRENCH WIDTH IN **RELATION TO TRENCH DEPTH**

pipe

pile cap

PIPE THROUGH PILE CAP DETAIL





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Doc Ref. TM54A008-PAM-ZZ-ZZ-DR-C-6102

Drawn	TP	Eng JL
Scales	1:20 at A1	1:40 at A3
Drawing	No	Rev
3019	98/6102	C02

Status FOR CONSTRUCTION

BELOW GROUND DRAINAGE DETAILS SHEET 3

CENTRAL SOMERS TOWN PLOT 5 & 6

21.07.23	ΤP	JL	Issued for Construction
05.07.23	ΤP	JL	Issued for Construction
11.05.23	FG	JL	Issued for Information
21.04.23	FG	JL	Stage 4 - Issued for DT Review
28.10.22	TP	JL	Issued for Stage 3
Date	Drawn	Eng	Amendment
	21.07.23 05.07.23 11.05.23 21.04.23 28.10.22 Date	21.07.23 TP 05.07.23 TP 11.05.23 FG 21.04.23 FG 28.10.22 TP Date Drawn	21.07.23 TP JL 05.07.23 TP JL 11.05.23 FG JL 21.04.23 FG JL 28.10.22 TP JL Date Drawn Eng

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C0125.08.23TPJLIssued for Stage 3RevDateDrawnEngAmendment

BELOW GROUND

DRAINAGE DETAILS

FOR CONSTRUCTION

TM54A008-PAM-ZZ-ZZ-DR-C-6102

PLOT 5 & 6

SHEET 4

Status

Drawn TP

Drawing No

Doc Ref.

Scales 1:20 at A1

30198/6103

CENTRAL SOMERS TOWN



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Eng JL

1:40 at A3

Rev

C01

Manhole / IC	Cover	Invert Level m	Chamber	r Chamber depth (m)	Internal Chamber Size	Cover Clear Opening and Cover Grade	Notes To Building Regulations Part H unless noted
F01	17,900	16,450	PC	1.450	750x600 Rectangular	600x600 cover with 300x300 clear opening	Reduced access inspection chamber
	10000	1.00.000	RAIC		Precast Concrete Blocks	BS EN 124 CLASS B125	Recessed cover finish to match adjacent
	*		27. 28. 88. 79.			ter ter omen 8. Stern in 19. den ster en ter Sternisti	Double sealed and bolted cover
F02	17.040	16.330	PC	0.710	750x600 Rectangular	750x600 Rectangular	
	-		IC		Precast Concrete Blocks	BS EN 124 CLASS B125	Recessed cover finish to match adjacent Double sealed and bolted cover
F03	17.900	16.550	PC	1.350	1000x675 Rectangular	600x600 cover with 300x300 clear opening	Reduced access inspection chamber
			RAIC		Precast Concrete Blocks	BS EN 124 CLASS B125	Recessed cover finish to match adjacent
	T				· · · · · · · · · · · · · · · · · · ·		Double sealed and bolted cover
F04	17.040	16.210	PC	0.830	750x600 Rectangular	750x600 Rectangular	
	1		IC		Precast Concrete Blocks	BS EN 124 CLASS B125	Recessed cover finish to match adjacent
	T				2		Double sealed and bolted cover
F05	18.410	17.500	Plastic	0.910	450mm Polypropylene	600x600 cover	
			IC		Ring	BS EN 124 CLASS B125	Recessed cover finish to match adjacent
	1						Double sealed and bolted cover
F06	18.400	17.450	Plastic	0.950	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	1		. P				
F07	18.400	17.215	Plastic	1.185	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
F08	18.400	16.900	Plastic	1.500	450mm Polypropylene	350 diameter restrictor	Reduced access inspection chamber
			RAIC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	<u> </u>						
F09	18.400	16.860	Plastic	1.540	450mm Polypropylene	350 diameter restrictor	Reduced access inspection chamber
	1		RAIC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
F 40	10,400	17 600	Disstia	1 800	450mm Dolymronylono	250 diameter restrictor	Deduced access increation chember
F10	19.400	17.600	Plastic	1.800	450mm Polypropylene		Reduced access inspection champer
	+		RAIC		King	OSMA 4D945 Square Recessed	Recessed cover linish to match adjacent
F 44	10,400	17 500	Diactio	1 000	450mm Dolynronylono	250 diameter restrictor	Poduced access increation chember
F11	19.400	17.500	Plastic	1.900	Ping	OSMA 4D045 Square Beaccord	Reduced access inspection chamber
	+		RAIC		rxing	OSIMA 4D945 Square Recessed	Recessed cover infisit to match adjacent
E12	18 400	17 350	Plastic	1 050	450mm Polypropylene	450 diameter	
F 12	10.400	17.000	IC	1.000	Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	•		10				
F13	18 400	17 300	Plastic	1 100	450mm Polypropylene	450 diameter	
1 10	10.100	11.000	IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	+				1		
F13A	18,400	17.250	Plastic	1,150	450mm Polypropylene	450 diameter	
	•		IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	*						
F14	18.400	16.750	Plastic	1.650	450mm Polypropylene	350 diameter restrictor	Reduced access inspection chamber
			RAIC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	*						· · · · ·
C01	19.450	16.600	TYPE 2	2.850	1200 diameter precast	600x600 eccentric	Steps Required
			Manhole		concrete rings	BS EN 124 CLASS D400	Recessed cover finish to match adjacent
	*	I.	And Annual Providence				
C02	19.850	16.100	TYPE 1	3.750	1200 diameter precast	600x600 eccentric	Ladder required
			Manhole		concrete rings	BS EN 124 CLASS D400	Recessed cover finish to match adjacent
	*						· · · · ·

FOUL WATER ACCESS CHAMBER SCHEDULE

Manhole / IC	Cover Level m	Invert Level m	ChamberTy pe	Chamber depth (m)	Internal Chamber Size	Cover Clear Opening and Cover Grade	Notes To Building Regulations Part H unless note
S01	17.850	17.275	Plastic	0.575	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
S02A	17.800	17.150	Plastic	0.650	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
S02	17.800	17.135	Plastic	0.665	450mm Polypropylene	450 diameter	
	1		IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
S03	17.900	16.900	Plastic	1.000	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
<u>504</u>	17.900	16.700	Plastic	1.200	450mm Polypropylene	350 diameter restrictor	Reduced access inspection chamber
			RAIC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
S05]						
						OMITTED	
506	19.775	16.580	CATCHPIT	3.645	1200 Diameter Precast	600x600 eccentric	Ladder required
			CHAMBER		Concrete Rings	BS EN 124 CLASS B125	Recessed cover finish to match adjacent
	<u> </u>						450mm Deep sump catch pit
508	18.400	17.410	Plastic	0.990	450mm Polypropylene	450 diameter	
	1		IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
S09	18.400	17.310	Plastic	1.090	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
510	19.350	17.230	Plastic	2.120	450mm Polypropylene	350 diameter restrictor	Reduced access inspection chamber
			RAIC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
511	19.350	17.130	CATCHPIT	2.670	1200 Diameter Precast	600x600 eccentric	Steps Required
	1		CHAMBER		Concrete Rings	BS EN 124 CLASS B125	Recessed cover finish to match adjacent
			-				450mm Deep sump catch pit
512	18.400	17.700	Plastic	0.700	450mm Polypropylene	450 diameter	
	•		IC		Ring	USIVIA 40940 Square Recessed	Recessed cover inish to match adjacent
S13	18.400	17.450	Plastic	0.950	450mm Polypropylene	450 diameter	
			IC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
S14	19.250	17.200	Plastic	2.500	450mm Polypropylene	350 diameter restrictor	Reduced access inspection chamber
			RAIC		Ring	OSMA 4D945 Square Recessed	Recessed cover finish to match adjacent
	N						450mm Deep sump catch pit

SURFACE WATER ACCESS CHAMBER SCHEDULE

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- Health & Safety : All specific drawing notes are to be read in conjunction with the project "Information Pack" and "Site Rules".
- All internal manholes and manholes in hard paved areas to have recessed covers. Cover levels shown on the schedule are indicative. Final cover levels to match landscape architects levels proposals.
- 5. For general notes refer to drawing 30198/05/0001

C04	25.00.00			locued for Construction
C04	10 07 23			Issued for Construction
C02	12.07.23	TP	JL	Issued for Construction
C01	05.07.23	TP	JL	Issued for Construction
P03	11.05.23	JL	JL	Issued for Information
P02	28.10.22	JL	JL	Stage 4 - Issued for DT Review
P01	28.10.22	JL	JL	Issued for Stage 3
Ver	Date	Drawn	Eng	Amendment

CENTRAL SOMERS TOWN PLOTS 5 & 6

MANHOLE SCHEDULE

FOR CONSTRUCTION

Drawn JL

Eng JL

Scales N/A Drawing No

Ver

30198/6200

C04

Doc Ref. TM54A008-PAM-ZZ-ZZ-SH-C-6200



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Price & Myers	Page 1	
37 Alfred Place		
London		
WC1E 7DP		Micco
Date 25/08/2023 15:39	Designed by tempuser	
File Plot 5 NetworkMDX	Checked by	Dialitacje
Innovyze	Network 2018.1.1	

STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FEH Rainfall Model

Return Period (years)

			PIMP (%)	100
FEH Rainfall Version		2013	Add Flow / Climate Change (%)	0
Site Location GB	3 530511 182470 TQ 30	511 82470	Minimum Backdrop Height (m)	0.200
Data Type		Point	Maximum Backdrop Height (m)	1.500
Maximum Rainfall (mm/hr)		50	Min Design Depth for Optimisation (m)	1.200
Maximum Time of Concentration (mins)		30	Min Vel for Auto Design only (m/s)	1.00
Foul Sewage (l/s/ha)		0.000	Min Slope for Optimisation (1:X)	500

100

Volumetric Runoff Coeff. 0.750

Designed with Level Soffits

Network Design Table for Storm

- Indicates pipe length does not match coordinates^ - Indicates Time of Concentration is too low and the pipe is not sized using the rainfall

PN Length Fall Slope I.Area T.E. Base k HYD DIA Section Type Auto (m) (m) (1:X) (ha) (mins) Flow (l/s) (mm) SECT (mm) Design

Network Results Table

Price & Myers		Page 2
37 Alfred Place		
London		
WC1E 7DP		Micco
Date 25/08/2023 15:39	Designed by tempuser	
File Plot 5 NetworkMDX	Checked by	Diamaye
Innovyze	Network 2018.1.1	
N PN Rain T.C. US/I (mm/hr) (mins) (m)	etwork Design Table for Storm L E I.Area E Base Foul Add Flow Vel Cap Flow (ha) Flow (l/s) (l/s) (l/s) (m/s) (l/s) (l/s)	
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Network Design Table for Storm

PN	Length	Fall	Slope	I.Area	T.E.	Ba	ise	k	HYD	DIA	Section Type	Auto
	(m)	(m)	(1:X)	(ha)	(mins)	Flow	(l/s)	(mm)	SECT	(mm)		Design
S1.000	12.261	0.125	98.1	0.014	4.00		0.0	0.600	0	150	Pipe/Conduit	A
S1.001	1.332	0.015	88.8	0.013	0.00		0.0	0.600	0	150	Pipe/Conduit	Ä
S1.002	14.153	0.235	60.2	0.005	0.00		0.0	0.600	0	150	Pipe/Conduit	ď
S1.003	15.777	0.200	78.9	0.005	0.00		0.0	0.600	0	150	Pipe/Conduit	- The second sec
S1.004	4.239	0.100	42.4	0.003	0.00		0.0	0.600	0	150	Pipe/Conduit	ē
S1.005	4.129	0.071	57.8	0.003	0.00		0.0	0.600	0	150	Pipe/Conduit	ē
S1.006	0.500#	0.050	10.0	0.000	0.00		0.0	0.600	0	150	Pipe/Conduit	ē
												_
S2.000	10.230	0.051	200.0	0.004	4.00		0.0	0.600	0	100	Pipe/Conduit	8

Network Results Table

PN	Rain	T.C.	US/IL	Σ I.Area	Σ Base	Foul	Add Flow	Vel	Cap	Flow
	(mm/hr)	(mins)	(m)	(ha)	Flow (l/s)	(l/s)	(1/s)	(m/s)	(l/s)	(l/s)
S1.000	0.00	4.20^	17.275	0.014	0.0	0.0	0.0	1.01	17.9	0.0
S1.001	0.00	4.22^	17.150	0.026	0.0	0.0	0.0	1.07	18.9	0.0
S1.002	0.00	4.40^	17.135	0.031	0.0	0.0	0.0	1.30	22.9	0.0
S1.003	0.00	4.64^	16.900	0.036	0.0	0.0	0.0	1.13	20.0	0.0
S1.004	0.00	4.68^	16.700	0.039	0.0	0.0	0.0	1.55	27.4	0.0
S1.005	0.00	4.73^	16.580	0.042	0.0	0.0	0.0	1.33	23.4	0.0
S1.006	0.00	4.74^	16.350	0.042	0.0	0.0	0.0	3.20	56.6	0.0
S2.000	0.00	4.32^	18.700	0.004	0.0	0.0	0.0	0.54	4.2	0.0

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File Plot 5 NetworkMDX	Checked by	Diamage
Innovyze	Network 2018.1.1	
Networ		
PN Length Fall Slope I.Area (m) (m) (1:X) (ha)	T.E. Base k HYD DIA Section Type Auto (mins) Flow (l/s) (mm) SECT (mm) Design	
S1.007 5.853 0.117 50.0 0.016	0.00 0.0 0.600 o 150 Pipe/Conduit 💣	
N	etwork Results Table	
PN Rain T.C. US/IL X (mm/hr) (mins) (m)	I.Area Σ Base Foul Add Flow Vel Cap Flow (ha) Flow (l/s) (l/s) (l/s) (m/s) (l/s) (l/s)	
S1.007 0.00 4.80^ 16.300	0.062 0.0 0.0 0.0 1.43 25.2 0.0	
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				PI	PELINE	SCHEDULI	ES for	Storm		
					IInc	troom M	anhala			
					<u>ops</u>	LIEAM M				
		#	- Ind	licate	s pipe l	ength doe	es not m	atch coordina	tes	
	PN	Hvd	Diam	мн	C Level	T Level I) Depth	МН	мн ртам т.*w	
		Sect	(mm)	Name	(m)	(m)	(m)	Connection	(mm)	
	S1.000	0	150	S1	17.850	17.275	0.425	Open Manhole	1200	
	S1.001	0	150	S2	17.850	17.150	0.550	Open Manhole	1200	
	S1.002	0	150	S3	17.900	17.135	0.615	Open Manhole	1200	
	S1.003	0	150	S3	17.900	16.900	0.850	Open Manhole	1200	
	S1.004	0	150	S4	17.900	16.700	1.050	Open Manhole	1200	
	S1.005	0	150	S5	19.600	16.580	2.870	Open Manhole	1200	
	S1.006	0	150	S7	19.600	16.350	3.100	Open Manhole	1200	
					Down	stream 1	Manhol	e		
	PN 1	Lenath	Slope	- мн	C Level	I T Level	D Dent	ь мн	MH DTAM T.*W	
	EM 1	(m)	(1:X)	Name	e (m)	(m)	(m)	Connection	(mm)	
	S1.000	12.261	98.1	L S2	2 17.850) 17.150	0.55	0 Open Manhol	e 1200	

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S5 **19.600** 16.600

S7 **19.600** 16.509

0.615 Open Manhole

0.850 Open Manhole

1.050 Open Manhole

2.850 Open Manhole

2.941 Open Manhole

3.150 Open Manhole

1200

1200

1200

1200

1200

1200

S1.001 1.332 88.8 S3 17.900 17.135

S1.002 14.153 60.2 S3 17.900 16.900

S1.003 15.777 78.9 S4 17.900 16.700

S1.006 0.500# 10.0 S9 19.600 16.300

S1.004 4.239 42.4

S1.005 4.129 57.8

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File Plot 5 NetworkMDX					Che	cked by			Drainage		
Innovyze					Net	work 201	8.1.1				
PIPELINE SCHEDULES for Storm											
Upstream Manhole											
	PN	Hyd Sect	Diam (mm)	MH Name	C.Level (m)	I.Level I (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)		
	S2.00) 0	100	S9	19.600	18.700	0.800	Open Manhole	1200		
	S1.00	7 о	150	S9	19.600	16.300	3.150	Open Manhole	1200		
					Down	istream l	Manhole	2			
	PN	Length (m)	Slope (1:X)	e MH Name	C.Leve (m)	l I.Level (m)	D.Depth (m)	n MH Connection	MH DIAM., L*W (mm)		
	S2.000	10.230	200.0) S	19.60	0 18.649	0.851	l Open Manhol	e 1200		
	S1.007	5.853	50.0) 5	19.60	0 16.183	3.26	7 Open Manhol	e 0		
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File Plot 5 NetworkMDX	Checked by	Drainage								
Innovyze	Network 2018.1.1									
Simul	ation Criteria for Storm									
Volumetric Runoff Coeff 0.750 Manhole Head Areal Reduction Factor 1.000 Foul Sewage Hot Start (mins) 0 Additional Flow Hot Start Level (mm) 0 MADD Factor	loss Coeff (Global) 0.500 Inlet Coefficcien e per hectare (l/s) 0.000 Flow per Person per Day (l/per/day w - % of Total Flow 0.000 Run Time (mins r * 10m³/ha Storage 2 000 Output Interval (mins	t 0.800) 0.000) 60								
Hot Start Level (mm) 0 MADD Factor * 10m³/ha Storage 2.000 Output Interval (mins) 1 Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0 Number of Online Controls 1 Number of Storage Structures 3 Number of Real Time Controls 0										
Synthetic Rainfall Details										
Rainfall Model Return Period (years) FEH Rainfall Version Site Location GB 5305 Data Type	FEH Summer Storms Yes 100 Winter Storms Yes 2013 Cv (Summer) 0.750 11 182470 TQ 30511 82470 Cv (Winter) 0.840 Point Storm Duration (mins) 30									
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Innovyze	Network 2018.1.1	
	Online Controls for Storm	
Hydro-Brake® Optimu	Manhole: S9, DS/PN: S1.007, Volume (m³): 3	.8
Unit Reference MD-SHE-00	70-2500-1400-2500 Sump Available	Yes
Design Head (m)	1.400 Diameter (mm)	70
Design Flow (1/s)	2.5 Invert Level (m)	16.300
Flush-Flom Objective Minimise	upstream storage Suggested Manhole Diameter (mm)	1200
Application	Surface	
Control Points Head	(m) Flow (l/s) Control Points Head (m) F	low (l/s)
Design Point (Calculated) 1	.400 2.5 Kick-Flo® 0.621	1.7
Flush-Flo™ 0	.307 2.1 Mean Flow over Head Range -	2.0
The hydrological calculations have been based on the	Head/Discharge relationship for the Hydro-Brake® Opt	imum as specified. Should
another type of control device other than a Hydro-Br	ake Optimum® be utilised then these storage routing c	alculations will be invalidated
Depth (m) Flow (1/s) Depth (m) Flow (1/s) Depth	(m) Flow (1/s) Depth (m) Flow (1/s) Depth (m) Flow	(1/s) Depth (m) Flow (1/s)
0.100 1.8 0.600 1.8 1	.600 2.7 2.600 3.3 5.000	4.5 7.500 5.4
0.200 2.1 0.800 1.9 1	.800 2.8 3.000 3.5 5.500	4.7 8.000 5.6

0.200 2.1 0.800 1.9 1.800 2.8 3.000 3.5 5.500 4.7 8.000 0.300 3.500 8.500 2.1 2.1 2.000 2.9 3.8 6.000 4.9 1.000 0.400 2.1 3.1 4.000 4.1 5.1 9.000 1.200 2.3 2.200 6.500 0.500 2.0 1.400 2.5 2.400 3.2 4.500 4.3 7.000 5.3 9.500

5.8

5.9

6.1

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Innovyze	Network 2018.1.1	
Stor	age Structures for Storm	
Porous Car	Park Manhole: S3, DS/PN: S1.002	
Infiltration Coefficient Base (m/hr) (Membrane Percolation (mm/hr) Max Percolation (l/s) Safety Factor	.00360 Porosity 0.30 Slope (1:X) 0.0 1000 Invert Level (m) 17.450 Depression Storage (mm) 5 28.2 Width (m) 3.5 Evaporation (mm/day) 3 2.0 Length (m) 29.0 Cap Volume Depth (m) 0.250	
Cellular Sto	rage Manhole: S7, DS/PN: S1.006	
Invert Level (m) 16 Infiltration Coefficient Base (m/hr) 0.0 Depth (m) Area (m ²) Inf. Area (m ²) Depth	.350 Infiltration Coefficient Side (m/hr) 0.00000 Porosity 0. 0000 Safety Factor 2.0 (m) Area (m ²) Inf. Area (m ²) Depth (m) Area (m ²) Inf. Area	. 95 (m²)
0.000 16.6 16.0 1	200 16.6 35.7 1.201 0.0 3	35.7
Porous Car	Park Manhole: S9, DS/PN: S2.000	
Infiltration Coefficient Base (m/hr) Membrane Percolation (mm/hr) Max Percolation (l/s) Safety Factor	0.00360 Porosity 0.30 Slope (1:X) 60.0 1000 Invert Level (m) 19.300 Depression Storage (mm) 5 20.8 Width (m) 6.5 Evaporation (mm/day) 3 2.0 Length (m) 11.5 Membrane Depth (mm) 0	
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Innovyze	Network 2018.1.1										
30 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm											
Simulation CriteriaAreal Reduction Factor 1.000Manhole Headloss Coeff (Global) 0.500MADD Factor * 10m³/ha Storage 2.000 Inlet Coefficcient 0.800 Hot Start Level (mm)Number of Input Hydrographs 0Number of Offline Controls 0Number of Time/Area Diagrams 0 Number of Online Controls 1 Number of Storage Structures 3 Number of Real Time Controls 0											
Rainfall Model	FEH Data Type Point										
FEH Rainfall Version	2013 Cv (Summer) 0.750										
Site Location GB	530511 182470 TQ 30511 82470 Cv (Winter) 0.840										
Margin for Flood Risk Warning (m	m) 0.0 DVD Status OFF										
Analysis Timest	ep 2.5 Second Increment (Extended) Inertia Status OFF										
DTS Stat	us ON										
Profile(s) Duration(s) (mins) 15, 3 Return Period(s) (years) Climate Change (%)	Summer and Winter 0, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440 30, 100 0, 40										
US/MH Return Climate First (X) First PN Name Storm Period Change Surcharge Flo	Water Surcharged Flooded Pipe (Y) First (Z) Overflow Level Depth Volume Flow / Overflow Flow od Overflow Act. (m) (m) (m ³) Cap. (l/s) (l/s) Status										
S1.000 S1 15 Winter 30 +0% 100/15 Summer	17.341 -0.084 0.000 0.39 6.3 OK										
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US/MH Level PN Name Exceeded

S1.000 S1

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PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)
S1.001	S2	15 Winter	30	+0%	30/15 Summer				17.314	0.014	0.000	1.04		11.3
S1.002	S3	15 Summer	30	+0%	100/15 Summer				17.223	-0.062	0.000	0.63		13.3
S1.003	S3	15 Winter	30	+0%	100/15 Summer				17.006	-0.044	0.000	0.83		15.4
S1.004	S4	120 Winter	30	+0%	30/15 Winter				17.000	0.150	0.000	0.27		5.4
S1.005	S5	120 Winter	30	+0%	30/15 Summer				16.998	0.268	0.000	0.33		5.5
S1.006	s7	120 Winter	30	+0%	30/15 Summer				16.996	0.496	0.000	0.15		2.1
S2.000	S9	15 Summer	30	+0%					18.752	-0.048	0.000	0.47		1.9
S1.007	S9	120 Winter	30	+0%	30/15 Summer				16.996	0.546	0.000	0.10		2.1

	US/MH		Level
PN	Name	Status	Exceeded
S1.001	S2	SURCHARGED	
S1.002	S3	OK	
S1.003	S3	OK	
S1.004	S4	SURCHARGED	
S1.005	S5	SURCHARGED	
S1.006	s7	SURCHARGED	
S2.000	S9	OK	
S1.007	S9	SURCHARGED	
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Innovyze	Network 2018.1.1			
100 year Return Period Summary of	Critical Results by Max	imum Level (Rank	1) for Stor	<u>cm</u>
Areal Reduction Factor 1.000 Manhole Headl Hot Start (mins) 0 Foul Sewage Hot Start Level (mm) 0 Additional Flow Number of Input Hydrographs 0 Nur Number of Online Controls 1 Number	Simulation Criteria oss Coeff (Global) 0.500 per hectare (1/s) 0.000 - % of Total Flow 0.000 Flo mber of Offline Controls 0 N er of Storage Structures 3 N	MADD Factor * 10 Inlet w per Person per Da umber of Time/Area 1 umber of Beal Time ()m³/ha Storage : Coeffiecient wy (l/per/day) Diagrams 0 Controls 0	2.000 0.800 0.000
	er of Storage Structures 5 N	uniber of itear fine (concrors o	
Sy Sy	nthetic Rainfall Details			
Rainfall Model FEH Rainfall Version	FEH 2013	Data Type Point Cv (Summer) 0.750		
Site Location GB	530511 182470 TQ 30511 82470	Cv (Winter) 0.840		
Margin for Flood Risk Warning (m Analysis Timest DTS Stat	um) sep 2.5 Second Increment (Ext sus	0.0 DVD Stat cended) Inertia Stat ON	tus OFF tus OFF	
Profile(s) Duration(s) (mins) 15, 3 Return Period(s) (years) Climate Change (%)	30, 60, 120, 180, 240, 360, 4	Summer and Wi 480, 600, 720, 960, 30, (inter 1440 , 100 0, 40	
US/MH Return Climate First (X) F PN Name Storm Period Change Surcharge	First (Y) First (Z) Overflow Flood Overflow Act.	Water Surcharged Level Depth (m) (m)	Flooded Volume Flow, (m³) Cap.	Pipe / Overflow Flow (l/s) (l/s)
S1.000 S1 180 Winter 100 +40% 100/15 Summer		17.598 0.173	0.000 0.1	7 2.7
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100 year Return Period Summary of PN S1.00	Critical Results by Maximum Level (Rank 1) for Sto US/MH Level Name Status Exceeded 0 S1 SURCHARGED	<u>rm</u>

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Innovyze	Network 2018.1.1	

PN	US/MH Name	Storm	Return Period	Climate Change	First (X) Surcharge	First (Y) Flood	First (Z) Overflow	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (l/s)	Pipe Flow (l/s)
S1.001	S2	180 Winter	100	+40%	30/15 Summer				17.596	0.296	0.000	0.48		5.2
S1.002	S3	180 Winter	100	+40%	100/15 Summer				17.595	0.310	0.000	0.29		6.2
S1.003	S3	180 Winter	100	+40%	100/15 Summer				17.590	0.540	0.000	0.34		6.4
S1.004	S4	180 Winter	100	+40%	30/15 Winter				17.584	0.734	0.000	0.31		6.2
S1.005	S5	180 Winter	100	+40%	30/15 Summer				17.582	0.852	0.000	0.38		6.3
S1.006	S7	180 Winter	100	+40%	30/15 Summer				17.579	1.079	0.000	0.20		2.8
S2.000	S9	15 Summer	100	+40%					18.779	-0.021	0.000	0.97		3.8
S1.007	S9	180 Winter	100	+40%	30/15 Summer				17.579	1.129	0.000	0.11		2.4

	US/MH		Level
PN	Name	Status	Exceeded
S1.001	S2	SURCHARGED	
S1.002	S3	SURCHARGED	
S1.003	S3	SURCHARGED	
S1.004	S4	SURCHARGED	
S1.005	S5	SURCHARGED	
S1.006	s7	SURCHARGED	
S2.000	S9	OK	
S1.007	S9	SURCHARGED	

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STORM SEWER DESIGN by the Modified Rational Method

Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FEH Rainfall Model

100

Volumetric Runoff Coeff. 0.750

Return Period (years)

		PIMP (%) 100
FEH Rainfall Version	2013	Add Flow / Climate Change (%) 0
Site Location GB 530511 182470 TQ 3051	1 82470	Minimum Backdrop Height (m) 0.200
Data Type	Point	Maximum Backdrop Height (m) 1.500
Maximum Rainfall (mm/hr)	50	Min Design Depth for Optimisation (m) 1.200
Maximum Time of Concentration (mins)	30	Min Vel for Auto Design only (m/s) 1.00
Foul Sewage (l/s/ha)	0.000	Min Slope for Optimisation (1:X) 500

Designed with Level Soffits

Network Design Table for Storm

^ - Indicates Time of Concentration is too low and the pipe is not sized using the rainfall

PN Length Fall Slope I.Area T.E. Base k HYD DIA Section Type Auto (m) (m) (1:X) (ha) (mins) Flow (1/s) (mm) SECT (mm) Design

Network Results Table

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WC1E 7DP		Micco									
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Innovyze	Network 2018.1.1										
Network Design Table for Storm											
PN Rain T.C. US/IL Σ I.Area Σ Base Foul Add Flow Vel Cap Flow (mm/hr) (mins) (m) (ha) Flow (l/s) (l/s) (l/s) (m/s) (l/s) (l/s)											
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Innovyze	Network 2018.1.1	

Network Design Table for Storm

PN	Length	Fall	Slope	I.Area	T.E.	Base		k	HYD	DIA	Section Type	Auto
	(m)	(m)	(1:X)	(ha)	(mins)	Flow	(1/s)	(mm)	SECT	(mm)		Design
S1.000	10.882	0.100	108.8	0.008	4.00		0.0	0.600	0	150	Pipe/Conduit	8
S1.001	7.359	0.080	92.0	0.008	0.00		0.0	0.600	0	150	Pipe/Conduit	Ð
S1.002	4.496	0.055	82.0	0.011	0.00		0.0	0.600	0	150	Pipe/Conduit	0
S2.000	6.662	0.044	150.2	0.002	4.00		0.0	0.600	0	100	Pipe/Conduit	ď
S1.003	3.226	0.038	84.9	0.010	0.00		0.0	0.600	0	225	Pipe/Conduit	<u>A</u>
S1.004	11.370	0.050	227.4	0.000	0.00		0.0	0.600	0	150	Pipe/Conduit	ŏ
S3.000	18.190	0.250	72.8	0.006	4.00		0.0	0.600	0	150	Pipe/Conduit	Ô

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)	Foul (1/s)	Add Flow (1/s)	Vel (m/s)	Cap (1/s)	Flow (1/s)	
S1.000	0.00	4.19^	17.410	0.008	0.0	0.0	0.0	0.96	17.0	0.0	
S1.001	0.00	4.31^	17.310	0.016	0.0	0.0	0.0	1.05	18.5	0.0	
S1.002	0.00	4.37^	17.230	0.027	0.0	0.0	0.0	1.11	19.6	0.0	
S2.000	0.00	4.18^	18.600	0.002	0.0	0.0	0.0	0.63	4.9	0.0	
S1.003	0.00	4.41^	17.130	0.039	0.0	0.0	0.0	1.42	56.5	0.0	
S1.004	0.00	4.70^	16.850	0.039	0.0	0.0	0.0	0.66	11.7	0.0	
S3.000	0.00	4.26^	17.700	0.006	0.0	0.0	0.0	1.18	20.9	0.0	
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Network Design Table for Storm

PN	Length	Fall	Slope	I.Area	T.E.	Ba	ase	k	HYD	DIA	Section Type	Auto
	(m)	(m)	(1:X)	(ha)	(mins)	Flow	(l/s)	(mm)	SECT	(mm)		Design
C2 001	20 624	0 250	00 F	0 010	0 00		0 0	0 600	<u>_</u>	150	Dino (Conduit	ھ
S3.001	20.024	0.250	82.5 45 0	0.010	0.00		0.0	0.600	0	150	Pipe/Conduit	
33.002	5.701	0.004	43.0	0.009	0.00		0.0	0.000	0	100	ripe/conduit	
S1.005	4.919	0.080	61.5	0.000	0.00		0.0	0.600	0	150	Pipe/Conduit	đ

Network Results Table

PN	Rain	T.C.	US/IL	Σ I.Area	Σ Bas	e	Foul	Add Flow	Vel	Cap	Flow
	(mm/hr)	(mins)	(m)	(ha)	Flow (1	/s)	(l/s)	(1/s)	(m/s)	(1/s)	(l/s)
C2 001	0 00	1 574	17 450	0 024		0 0	0 0	0 0	1 1 1	10 C	0 0
53.001	0.00	4.57	17.450	0.024		0.0	0.0	0.0	1.11	19.0	0.0
S3.002	0.00	4.61^	17.200	0.033		0.0	0.0	0.0	1.50	26.6	0.0
S1.005	0.00	4.76^	16.800	0.072		0.0	0.0	0.0	1.28	22.7	0.0

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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd	Diam	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W
	Sect	(mm)	Name	(m)	(m)	(m)	Connection	(mm)
S1.000	0	150	S1	18.400	17.410	0.840	Open Manhole	1200
S1.001	0	150	S2	19.200	17.310	1.740	Open Manhole	1200
S1.002	0	150	S3	19.400	17.230	2.020	Open Manhole	1200
S2.000	0	100	S4	19.200	18.600	0.500	Open Manhole	1200
S1.003	0	225	S4	19.400	17.130	2.045	Open Manhole	1200
S1.004	0	150	S5	19.400	16.850	2.400	Open Manhole	1200

Downstream Manhole

PN	Length	Slope	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W
	(m)	(1:X)	Name	(m)	(m)	(m)	Connection	(mm)
S1.000	10.882	108.8	S2	19.200	17.310	1.740	Open Manhole	1200
S1.001	7.359	92.0	S3	19.400	17.230	2.020	Open Manhole	1200
S1.002	4.496	82.0	S4	19.400	17.175	2.075	Open Manhole	1200
S2.000	6.662	150.2	S4	19.400	18.556	0.744	Open Manhole	1200
S1.003	3.226	84.9	S5	19.400	17.092	2.083	Open Manhole	1200
S1.004	11.370	227.4	S6	19.550	16.800	2.600	Open Manhole	1200

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PIPELINE SCHEDULES for Storm

Upstream Manhole

PN	Hyd	Diam	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W
	Sect	(mm)	Name	(m)	(m)	(m)	Connection	(mm)
s3.000	0	150	S6	18.400	17.700	0.550	Open Manhole	1200
S3.001	0	150	S7	18.400	17.450	0.800	Open Manhole	1200
S3.002	0	150	S8	19.400	17.200	2.050	Open Manhole	1200
S1.005	0	150	S6	19.550	16.800	2.600	Open Manhole	1200

Downstream Manhole

PN	Length	Slope	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W
	(m)	(1:X)	Name	(m)	(m)	(m)	Connection	(mm)
S3.000	18.190	72.8	S7	18.400	17.450	0.800	Open Manhole	1200
S3.001	20.624	82.5	S8	19.400	17.200	2.050	Open Manhole	1200
S3.002	3.781	45.0	S6	19.550	17.116	2.284	Open Manhole	1200
S1.005	4.919	61.5	S	19.400	16.720	2.530	Open Manhole	0

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Simul	ation Criteria for Storm							
Volumetric Runoff Coeff 0.750 Manhole Head Areal Reduction Factor 1.000 Foul Sewag	loss Coeff (Global) 0.500 Inlet Coeffiecien e per hectare (l/s) 0.000 Flow per Person per Day (l/per/day	t 0.800) 0.000						
Hot Start (mins) U Additional Flor Hot Start Level (mm) 0 MADD Facto	w - % of Total Flow 0.000 Run Time (mins r * 10m³/ha Storage 2.000 Output Interval (mins) 60						
Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0 Number of Online Controls 1 Number of Storage Structures 2 Number of Real Time Controls 0								
Synt	chetic Rainfall Details							
Rainfall Model Return Period (years) FEH Rainfall Version Site Location GB 5305. Data Type	FEH Summer Storms Yes 100 Winter Storms Yes 2013 Cv (Summer) 0.750 11 182470 TQ 30511 82470 Cv (Winter) 0.840 Point Storm Duration (mins) 30							
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<u><u> </u></u>	nline Controls for Storm							
Hydro-Brake® Optimum Manhole: S6, DS/PN: S1.005, Volume (m³): 3.3								
Unit Reference MD-SHE-007	-2500-1400-2500 Sump Available Ye	es						
Design Head (m)	1.400 Diameter (mm)	70						
Design Flow (1/S)	2.5 Invert Level (M) 16.80 Calculated Minimum Outlet Pipe Diameter (mm) 10	00						
Objective Minimise	pstream storage Suggested Manhole Diameter (mm) 120	00						
Application	Surface							
Control Points Head	m) Flow (l/s) Control Points Head (m) Flow	(1/s)						
Design Point (Calculated) 1.4	00 2.5 Kick-Flo® 0.621	1.7						
Flush-Flo™ 0.3	07 2.1 Mean Flow over Head Range -	2.0						
The hydrological calculations have been based on the H another type of control device other than a Hydro-Brak	ead/Discharge relationship for the Hydro-Brake® Optimum e Optimum® be utilised then these storage routing calcu	as specified. Should lations will be invalidated						
Depth (m) Flow (1/s) Depth (m) Flow (1/s) Depth	m) Flow (l/s) Depth (m) Flow (l/s) Depth (m) Flow (l/s) Depth (m) Flow (l/s)						
0.100 1.8 0.600 1.8 1.6	00 2.7 2.600 3.3 5.000 4.	5 7.500 5.4						
0.200 2.1 0.800 1.9 1.8	00 2.8 3.000 3.5 5.500 4.	7 8.000 5.6						

2.1 0.800 1.800 3.000 5.500 8.000 1.9 2.8 3.5 4.7 0.300 2.000 3.500 2.1 2.1 2.9 6.000 8.500 1.000 3.8 4.9 0.400 2.1 2.3 2.200 3.1 4.000 4.1 6.500 5.1 9.000 1.200 0.500 2.0 1.400 2.5 2.400 3.2 4.500 4.3 7.000 5.3 9.500

5.8

5.9

6.1

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Stora	age Structures for Storm	
Porous Car E	Park Manhole: S4, DS/PN: S2.000	
Infiltration Coefficient Base (m/hr) (Membrane Percolation (mm/hr) Max Percolation (1/s) Safety Factor <u>Cellular Sto</u> Invert Level (m) 16. Infiltration Coefficient Base (m/hr) 0.00 Depth (m) Area (m ²) Inf. Area (m ²) Depth	<pre>0.00000 Porosity 0.30 Slope (1:X) 50.0 1000 Invert Level (m) 18.850 Depression Storage (mm) 5 28.8 Width (m) 4.5 Evaporation (mm/day) 3 2.0 Length (m) 23.0 Membrane Depth (mm) 0 rage Manhole: S5, DS/PN: S1.004 .850 Infiltration Coefficient Side (m/hr) 0.00000 Porosity 0 0000 Safety Factor 2.0 (m) Area (m²) Inf. Area (m²) Depth (m) Area (m²) Inf. Area</pre>	. 95 (m²)
0.000 29.0 24.0 1.	000 29.0 52.0 1.001 0.0	52.0
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30 year Return Period Summary of (Critical Results by Maximum Level (Rank 1) for Storm
Areal Reduction Factor 1.000 Manhole Headl Hot Start (mins) 0 Foul Sewage Hot Start Level (mm) 0 Additional Flow Number of Input Hydrographs 0 Num Number of Online Controls 1 Number	Simulation Criteriaoss Coeff (Global) 0.500MADD Factor * 10m³/ha Storage 2.000per hectare (1/s) 0.000Inlet Coefficcient 0.800- % of Total Flow 0.000Flow per Person per Day (1/per/day) 0.000mber of Offline Controls 0Number of Time/Area Diagrams 0er of Storage Structures 2Number of Real Time Controls 0
Rainfall Model	FEH Data Type Point
FEH Rainfall Version	2013 Cv (Summer) 0.750
Site Location GB	530511 182470 TQ 30511 82470 Cv (Winter) 0.840
Margin for Flood Risk Warning (m	um) 0.0 DVD Status OFF
Analysis Timest	ep 2.5 Second Increment (Extended) Inertia Status OFF
DTS Stat	CUS ON
Profile(s) Duration(s) (mins) 15, 3 Return Period(s) (years) Climate Change (%)	Summer and Winter 30, 60, 120, 180, 240, 360, 480, 600, 720, 960, 1440 30, 100 0, 40
US/MH Return Climate First (X) First PN Name Storm Period Change Surcharge Flo	Water Surcharged FloodedPipet (Y) First (Z) Overflow Level Depth Volume Flow / Overflow Flowbod Overflow Act. (m) (m) (m³) Cap. (1/s) (1/s) Status
S1.000 S1 15 Summer 30 +0% 100/15 Winter	17.461 -0.099 0.000 0.25 3.8 OK
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US/MH Level PN Name Exceeded

S1.000 S1

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PN	US/MH Name	Sto	orm	Return Period	Climate Change	First () Surchar	X) First ge Flood	Y) First (Z) I Overflow	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (1/s)	Pipe Flow (l/s)
S1.001	S2	15 Sı	ummer	30	+0%	100/15 Su	ummer			17.381	-0.079	0.000	0.46		7.3
S1.002	S3	120 W	inter	30	+0%	100/15 Su	ummer			17.367	-0.013	0.000	0.25		3.7
S2.000	S4	120 W	inter	30	+0%					18.616	-0.084	0.000	0.06		0.3
S1.003	S4	120 W:	inter	30	+0%	30/120 Wi	inter			17.366	0.011	0.000	0.17		5.1
S1.004	S5	120 W:	inter	30	+0%	30/15 Su	ummer			17.365	0.365	0.000	0.19		2.0
S3.000	S6	15 W:	inter	30	+0%	100/120 Wi	inter			17.737	-0.113	0.000	0.14		2.7
S3.001	s7	15 W:	inter	30	+0%	100/15 Su	ummer			17.535	-0.065	0.000	0.61		11.2
S3.002	S8	120 W	inter	30	+0%	30/120 Wi	inter			17.363	0.013	0.000	0.25		4.6
S1.005	S6	120 W	inter	30	+0%	30/15 Su	ummer			17.367	0.417	0.000	0.12		2.1

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File Plot 6 NetworkMDX	Checked by			Diamage
Innovyze	Network 2018.1.1			
100 year Return Period Summary of	Critical Results by Maxi	imum Level (Rank	1) for Stor	<u>rm</u>
Areal Reduction Factor 1.000 Manhole Headl Hot Start (mins) 0 Foul Sewage Hot Start Level (mm) 0 Additional Flow Number of Input Hydrographs 0 Nur Number of Online Controls 1 Numbe	Simulation Criteria oss Coeff (Global) 0.500 per hectare (1/s) 0.000 - % of Total Flow 0.000 Flo wher of Offline Controls 0 Nu er of Storage Structures 2 Nu	MADD Factor * 10 Inlet w per Person per Da umber of Time/Area I umber of Real Time (m ³ /ha Storage Coeffiecient y (l/per/day) Diagrams 0 Controls 0	2.000 0.800 0.000
	2			
Bainfall Model	nthetic Rainfall Details	Data Type Point		
FEH Rainfall Version	2013	Cv (Summer) 0.750		
Site Location GB	530511 182470 TQ 30511 82470	Cv (Winter) 0.840		
Margin for Flood Risk Warning (n Analysis Timest DTS Stat	m) ep 2.5 Second Increment (Ext us	0.0 DVD Stat ended) Inertia Stat ON	cus OFF cus OFF	
Profile(s) Duration(s) (mins) 15, Return Period(s) (years) Climate Change (%)	30, 60, 120, 180, 240, 360, 4	Summer and Wi 180, 600, 720, 960, 30, C	inter 1440 , 100), 40	
US/MH Return Climate First (X) H PN Name Storm Period Change Surcharge	'irst (Y) First (Z) Overflow Flood Overflow Act.	Water Surcharged Level Depth (m) (m)	Flooded Volume Flow , (m³) Cap.	Pipe / Overflow Flow (l/s) (l/s)
S1.000 S1 180 Winter 100 +40% 100/15 Winter		18.250 0.690	0.000 0.10	1.6
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Innovyze		Network 2018.1	.1		
100 year Beturn P	eriod Summary of (Critical Result	s by Maximum Leve	l (Bank 1) for Sto	rm
100 year keturn Pe	eriod Summary of (Critical Result	s by Maximum Leve	(RANK I) IOI SLO	
			Iovol		
	PN	Name Status	Exceeded		
	01.000				
	51.000) SI SURCHARGEL			
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PN	US/MH Name	Stor	rm	Return Period	Climate Change	First (X Surcharg	() First (Y) Me Flood	First (Z) Overflow	Overflow Act.	Water Level (m)	Surcharged Depth (m)	Flooded Volume (m³)	Flow / Cap.	Overflow (1/s)	Pipe Flow (l/s)
S1.001	S2	180 Wi	nter	100	+40%	100/15 Sum	mmer			18.249	0.789	0.000	0.18		2.8
S1.002	S3	180 Wi	nter	100	+40%	100/15 Sum	mmer			18.248	0.868	0.000	0.31		4.5
S2.000	S4	15 Wi	nter	100	+40%					18.642	-0.058	0.000	0.31		1.4
S1.003	S4	180 Wi	nter	100	+40%	30/120 Wir	nter			18.246	0.891	0.000	0.20		6.1
S1.004	S5	180 Wi	nter	100	+40%	30/15 Sum	mmer			18.245	1.245	0.000	0.18		1.9
S3.000	S6	180 Wi	nter	100	+40%	100/120 Wir	nter			18.247	0.397	0.000	0.06		1.2
S3.001	s7	180 Wi	nter	100	+40%	100/15 Sum	mmer			18.246	0.646	0.000	0.26		4.8
S3.002	S8	180 Wi	nter	100	+40%	30/120 Wir	nter			18.242	0.892	0.000	0.31		5.7
S1.005	S6	180 Wi	nter	100	+40%	30/15 Sum	mmer			18.240	1.290	0.000	0.14		2.5

	US/MH		Level
PN	Name	Status	Exceeded
S1.001	S2	SURCHARGED	
S1.002	S3	SURCHARGED	
S2.000	S4	OK	
S1.003	S4	SURCHARGED	
S1.004	S5	SURCHARGED	
S3.000	S6	SURCHARGED	
\$3.001	S7	SURCHARGED	
\$3.002	S8	SURCHARGED	
S1.005	S6	SURCHARGED	
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