

47 PLATT'S LANE

For Mr Gert-Jan Breukink

BUILDING DAMAGE ASSESSMENT REPORT

April 2024

Prepared by Articlus Limited



Client Name: Mr Gert-Jan Breukink Project Name: 47 Platt's Lane, London, NW3 7NL Project No: 15670 Document No: EWGCE-15670-XX-R-BDA-001

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This document has been prepared and checked in accordance with Articlus internal management procedures.

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Issue 1 – First issue.

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1. Introduction

Articlus has been instructed by UPP on behalf of Mr Gert-Jan Breukink to prepare building damage assessment (BDA) report for the proposed development at 47 Platt's Lane, London.

1.1 Study Aims and Objectives

This report aims to give a degree of certainty to the asset owner and the developer to understand the predicted ground movements and magnitude of potential impact at the location of the assets.

This ground movement assessment has included the following assets in the assessment:

- Key Facades of 45 Platt's Lane.
- Key Facades of 49 Platt's Lane.

1.2 Limitations

This report is based upon information obtained from third party sources. The third-party data has been accepted at face value and has not been independently verified. Articlus can therefore give no warranty, representation, or assurance as to the accuracy or completeness of such information.

This report has been prepared for the sole internal use and reliance of the Client, Mr Gert-Jan Breukink, and shall not be relied upon by other parties without the express written authority of Articlus. If an unauthorised third party comes into possession of this report, then they rely on it at their own risk.

2. Site Location and Description

2.1 Site Location

The site is located at street address of 47 Platt's Lane, London NW3 7NL with a grid reference of 525276, 186151. The site has an approximate area of 0.03ha. Figure 1 presents the current site layout.



Figure 1: Current site layout (courtesy of google map)

2.2 Current Site and Surrounding Land Uses

The site is currently occupied by a double-storey Victorian semi-detached house with a partial basement (as shown in Figure 1).

The site surrounding is predominantly consisting of residential buildings.

2.3 Proposed Development

The proposed to construct a light well to front of the existing house by extending existing basement.

The new building structure will be as follows:

- A hit and miss sequence of underpinning to form light well/extension of existing basement.
- A 350mm thick raft foundation to support wall loading.



Figure 2: Proposed lightwell/basement extension plan (extract from UPP drawing)



Figure 3: Proposed section (extract from UPP drawing)

3. Third Party Assets

The following neighbouring building has been included in this assessment.

- 45 Platt's Lane.
- 49 Platt's Lane.

The third-party assets are shown in Figure 4.



Figure 4: Adjacent building included in this BDA

3.1 Building Damage Assessment (BDA)

A building damage assessment has been undertaken to assess the potential impact of the proposed development on the adjacent 45 & 49 Platt's Lane buildings, due to the following key construction stages:

- Underpinning of existing building
- Excavation to Basement
- Long-term structural loading

The overall aim of this study is to evaluate the potential impact of the proposed redevelopment on the neighbouring building. The building damage assessment has been undertaken in accordance with the Burland (2001) assessment criteria presented in CIRIA C760.

The damage criteria limiting tensile strain, description of the damage categories and associated approximate crack

widths are presented in Figure 5. According to the various London borough councils, the acceptable damage categories are "0 Negligible" to "2 Slight" and are highlighted in Figure 5.

Category of damage	Description of typical damage (ease of repair is underlined)	Approximate crack width (mm)	Limiting tensile strain, $\varepsilon_{\rm sim}$ (%)
0 Negligible	Hairline cracks of less than about 0.1 mm are classed as negligible	<0.1	0.0 to 0.05
1 Very slight	Fine cracks that can easily be treated during normal decoration. Perhaps isolated slight fracture in building. Cracks in external brickwork visible on inspection	<1	0.05 to 0.075
2 Slight	Cracks easily filled. Redecoration probably required. Several slight fractures showing inside of building. Cracks are visible externally and some repointing may be required externally to ensure weathertightness. Doors and windows may stick slightly.	<5	0.075 to 0.15
3 Moderate	The cracks require some opening up and can be patched by a mason. Recurrent cracks can be masked by suitable lining. Repointing of external brickwork and possibly a small amount of brickwork to be replaced. Doors and windows sticking. Service pipes may fracture. Weathertightness often impaired.	5 to 15 or a number of cracks >3	0.15 to 0.3
4 Severe	Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows. Windows and frames distorted, floor sloping noticeably. Walls leaning or bulging noticeably, some loss of bearing in beams. Services pipes disrupted.	15 to 25, but also depends on number of cracks	>0.3
5 Very severe	This requires a major repair, involving partial or complete rebuilding. Beams lose bearings, walls lean badly and require shoring. Windows broken with distortion. Danger of instability.	Usually >25, but depends on numbers of cracks	

Figure 5:Damage category classification - CIRIA C760 Table 6.4: Classification of visible damage to walls
(after Burland et al., 1977, Boscardin and Cording, 1989 and Burland, 2001)

4. Ground Model and Parameters

4.1 Ground Model and Geotechnical Parameters

Ground model and geotechnical parameters have been evaluated based on the information from the nearby site and borehole logs available from BGS archives.

A summary of ground condition and geotechnical parameters used in design are presented in Table 1.

Stratum	Thickness (m)	Undrained Young's Modulus (MN/m²)	Drained Young's Modulus (MN/m²)	Drained Poisson's Ratio
Made Ground	1.5	-	5.0	0.2
Downwash Deposits	2.0	14	11.2	0.2
Claygate Member	>3.0	17.5	14.0	0.2

Table 1: Ground model and geotechnical parameters summary

- The undrained stiffness for cohesive strata has been obtained by correlation with the undrained shear strength for the anticipated range of strain in the respective analytical models. The drained stiffness for cohesive strata has been taken as 80% of the undrained stiffness, following principles of elasticity theory (assuming a Poisson's Ratio of 0.2).
- The Made Ground stiffness has been assumed based on experience in the area and the conditions observed in the site-specific ground investigation.
- The Clay stiffness profiles indicated are based on the relationship Eu=350Cu corresponding to strain levels associated with unloading due to excavation/ demolition and subsequent loading on raft foundation.

4.2 Groundwater

No water strikes were noted during drilling of the borehole. The results from a return visit of the groundwater monitoring installation shows groundwater encountered at 3.5m bgl. Therefore, it should be assumed that a perched water table may be present at site.

Notes:

5. Loading Information

To represent the phasing of proposed development, the loading has been provided in terms of underpinning loading during deepening of existing foundations, excavation loading (removal of soil) and proposed development loading (new building loading, which has been applied to corresponding stages in the modelling.

The underpinning loading during deepening of foundation to create new basement has been considered considering additional weight of concrete. Excavation loading has been considered equivalent to removal of 4m of soil to achieve required basement level. The loading for the new built has been considered as maximum 100kPa at the underpinning location and approximately 56kPa in the general area.

6. Assessment Methodology

6.1 Pdisp Modelling Methodology

A series of greenfield ground movement analyses have been carried out, using the commercial software Oasys Pdisp, to evaluate the short and long-term movements induced by the proposed construction works. The construction scheme comprises the underpinning of the existing foundation to enable basement excavation, excavation to the proposed formation level and the construction of the proposed structure. The analyses have been undertaken assuming undrained and drained conditions for the cohesive strata, in order to evaluate the short and long-term effects, respectively. Excavation stage has been modelled as upwards uniform surface loads at the formation level.

Pdisp calculates the displacements and changes in vertical stress in a linear elastic soil medium, which arise from uniform normal or tangential pressures applied on a specific level. The analysis has been carried out using the Boussinesq (1885) method. This method calculates the stress distribution assuming a uniform isotropic material with a constant user-defined Poisson's ratio.

The following analyses have been carried out:

- Model 1 Pdisp Underpinning Short Term (ST) conditions.
- Model 2 Pdisp Underpinning and Excavation ST conditions.
- Model 3 Pdisp Underpinning + Excavation + Proposed Building Loading Long Term (LT) conditions.

6.2 Xdisp Modelling Methodology

A building potential damage assessment has been carried out using Oasys Xdisp. The software calculates the "local" greenfield ground movements induced by the embedded wall installation and excavation in addition to the imported global movements from Pdisp models. The software uses the Burland strain criteria (2001) to evaluate the building damage category of each façade of the building. The Burland building damage assessment criteria are presented in Section 3.1.

The building damage assessment uses the work described in Burland et al (2001) and Gaba et al (2003). In this approach the façades of the buildings are represented by simple linear elastic beam with E/G of 2.6 for a Poisson ratio of 0.3, whose foundations are assumed to follow the "greenfield" soil movements at ground surface. The height of the buildings is also an input for the assessment and has been derived based on the visual assessment from google maps and site visit.

Although, this stage of assessment is relatively detailed, the assumptions made are moderately conservative. Consequently, the categories of damage derived in this level of assessment are only potential degrees of damage. The actual damage should be less than the predicted due to the inherent stiffness of the structures and their foundations, which tend to redistribute and reduce both the deflection ratio and the horizontal strains.

The following combined analyses have been carried out in Xdisp in order to simulate the ground movements occurring following existing building demolition, basement excavation and subsequent structural loading in shortand long-term conditions.

- Model 4 Xdisp Underpinning ST model based on results from Model 1.
- Model 5 Xdisp Underpinning and Excavation ST model based on results from Model 2.
- Model 6 Xdisp Combined Loading LT model based on results from Model 3.

7. Results

7.1 Potential Building Damage Assessment

The view of the potential building damage assessment model is shown in Figure 6. The simplified shape of four façades of 45 & 49 Platt's Lane buildings have been modelled. The potential building damage category for each façade is summarised in Table 2 to Table 4.

It is worth noting that the assessment carried out involves a number of conservative assumptions in terms of greenfield movements and no allowance for structural stiffness and therefore the anticipated ground movements are likely to be of smaller magnitude.

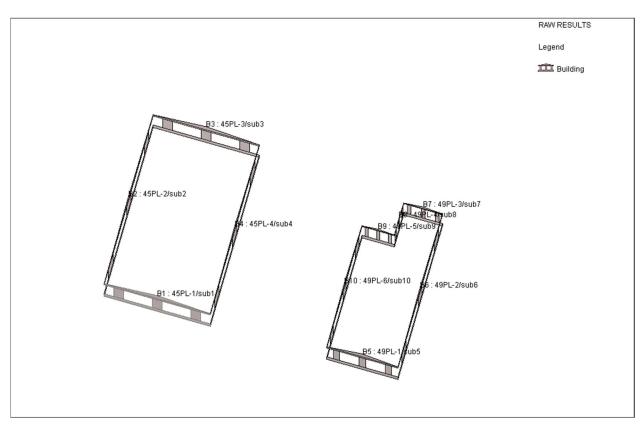


Figure 6: Potential building damage assessment model view

Table 2:	Building damage assessment results summary [Model 4]
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Building ID	Façade ID	Damage category	Maximum vertical displacement [1] [mm]	Max tensile strain [%]
	45PL-1	0 (Negligible)	<1	0.002
45 Platt's Lane	45PL-2	0 (Negligible)	<1	0.00
	45PL-3	0 (Negligible)	<1	0.00

Building ID	Façade ID	Damage category	Maximum vertical displacement [1]	Max tensile strain
			[mm]	[%]
	45PL-4	0 (Negligible)	<1	0.002
	49PL-1	0 (Negligible)	<1	0.005
_	49PL-2	0 (Negligible)	<1	0.0005
-	49PL-3	0 (Negligible)	<1	0.00
49 Platt's Lane –	49PL-4	0 (Negligible)	<1	0.00
-	49PL-5	0 (Negligible)	<1	0.00
	49PL-6	0 (Negligible)	1.2	0.004

Table 3:	Building damage	assessment results	summary	[Model 5
Table 3.	Building damage	assessment results	Summary	[iviouel 5

Building ID	Façade ID	Damage category	Maximum vertical displacement [mm]	Max tensile strain [%]
	45PL-1	0 (Negligible)	1.0	0.004
45 Platt's Lane	45PL-2	0 (Negligible)	<1	0.00
	45PL-3	0 (Negligible)	<1	0.00
	45PL-4	0 (Negligible)	1.1	0.003
	49PL-1	0 (Negligible)	2.3	0.01
	49PL-2	0 (Negligible)	<1	0.001
40 Diatt's Loss	49PL-3	0 (Negligible)	<1	0.00
49 Platt's Lane	49PL-4	0 (Negligible)	<1	0.004
	49PL-5	0 (Negligible)	<1	0.00
	49PL-6	0 (Negligible)	2.6	0.01

Table 4: Building damage assessment results summary [Model 6]

Building ID	Façade ID	Damage category	Maximum vertical displacement [1] [mm]	Max tensile strain [%]
45 Platt's Lane –	45PL-1	0 (Negligible)	-3.8	0.014
45 Platt S Laile –	45PL-2	0 (Negligible)	<1	0.001

Building ID	Façade ID	Damage category	Maximum vertical displacement [1] [mm]	Max tensile strain [%]
	45PL-3	0 (Negligible)	<1	0.001
-	45PL-4	0 (Negligible)	-3.9	0.01
	49PL-1	0 (Negligible)	-8.3	0.03
-	49PL-2	0 (Negligible)	-1.8	0.004
40 Diattic Lana	49PL-3	0 (Negligible)	-1.0	0.0002
49 Platt's Lane -	49PL-4	0 (Negligible)	-1.6	0.001
-	49PL-5	0 (Negligible)	-2.2	0.00
-	49PL-6	0 (Negligible)	-8.4	0.03

Notes:

- +ve displacement is heave.
- -ve displacement is settlement.

8. Conclusions

Articlus Limited has been instructed by UPP on behalf of Mr Gert-Jan Breukink to undertake a ground movement assessment (GMA) to evaluate the potential impacts of the proposed development on the adjacent buildings. This report aims to provide a degree of certainty to the asset owners and the developer in relation to the ground movement and the magnitude of potential impact induced by construction, at the location of these assets.

Ground model and geotechnical parameters have been evaluated based on the experience in the proximity of proposed development and using BGS borehole archives.

Some of the information and conclusions presented in this report are based on information provided by others. Articlus has endeavoured to assess all information provided to them but makes no guarantees or warranties as to the accuracy or completeness of this information.

A combination of analyses has been carried out, using the commercial software Oasys Xdisp and Oasys Pdisp, in order to evaluate the greenfield ground movements due to underpinning, excavation for the proposed basement construction and the long-term loading from the proposed structure.

The results from the GMA analyses are presented in Table 2 to Table 4 for adjacent buildings at 45 & 49 Platt's Lane. The predicted potential damage to the adjacent building has been predicted to be Category 0 Negligible.

The resulting damage categories predicted as part of this GMA are within the allowable limits adopted for such assessments and industry wide practice. It is noted that the predicted ground movements, the associated wall tensile strains and level of damage categorisation are considered to be conservative, in view of the relatively cautious data assumptions and greenfield nature of the assessment undertaken.

The GMA has been supplemented by a project-specific monitoring regime and Action Plan, which delineate lines of responsibility, trigger levels in accordance with the ground movements predicted as part of this study and appropriate mitigation measures (if required). The assessment presented herein is dependent and reliant on the works being undertaken by an experienced contractor, high quality workmanship and appropriate supervision of construction means and methods by experienced personnel.

It is recommended that this report is reviewed and understood in full by the project team and relevant stakeholders. Where significant changes are made to items such as construction sequencing and scheme design the engineer should thoroughly review the discrepancy and evaluate any potential impacts on ground movement and building damage.

It is critical that the permanent and temporary works designs are carried out in a coordinated manner between performance specified elements and substructure contractors, with the aim to ensure that such design elements are in alignment with the assumptions/findings of the GMA and overall design intent.

9. References

- 1. Articlus, ground investigation report, June 2023
- 2. British Geological Survey borehole archives.
- 3. CIRIA R143 (1995) The Standard Penetration Test (SPT): Methods and Use.
- 4. CIRIA C760 (2017) Guidance on embedded retaining wall design.
- 5. Jardine, RJ et al. (1986) Studies of the influence of non-linear stress strain characteristics in soil structure interaction. Geotechnique, Vol 36, No 3, pp377-396.
- 6. Oasys Pdisp user manual.
- 7. Oasys Xdisp user manual.

APPENDICES

A. Xdisp Tabular Output

tage: Ref.	Stage: Name	Specific Building: Ref.		Parameter	Critical Sub-Building		Start	End	Curvature	Max Slop	e Max Settlement	Max Tensile Strain		Min Radius of Curvature (Sagging) [m]	Damage Category
							[m]	[m]			[mm]	[4]	[m]	[m]	
	Base Model	0	45PL-1	Max Slope	subl	1	0.0	5.1250	None	131.71E-	6 0.49499	0.0015833	-	-	0 (Negligible)
				Max Settlement	subl	1	0.0	5.1250	None	131.71E-	6 0.49499	0.0015833	-	-	0 (Negligible)
				Max Tensile Strain	subl	1	0.0	5.1250	None	131.71E-	6 0.49499	0.0015833	-	-	0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-	-	-			-	-	-	-
				Min Radius of Curvature (Sagging)		-	-	-	-			-	-	-	-
		0	45PL-2	All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
		0	45PL-3	All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less	than the li	mit sensi	tivity.								
				All vertical displacements are less											
		0	45PL-4	Max Slope	sub4	1	2.0308	6.6781	None	59.484E-	6 0.32196	414.38E-6	-	-	0 (Negligible)
				Max Settlement	sub4	2	6.6781	13.200	None	59.484E-	6 0.50906	0.0014719	-	-	0 (Negligible)
				Max Tensile Strain	sub4	2	6.6781	13,200	None	59.484E-	0.50906	0.0014719	-	-	0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-				-		
				Min Radius of Curvature (Sagging)		-	-	-	-			-	-	-	-
		0	49PL-1	Max Slope	sub5	1	0.0	5.5000	None	374.39E-	6 1 1747	0.0053356	-	-	0 (Negligible)
				Max Settlement	sub5	1		5.5000		374.39E-		0.0053356			0 (Negligible)
				Max Tensile Strain	sub5	1		5.5000		374.39E-		0.0053356			0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-		-		-	-	
				Min Radius of Curvature (Sagging)		-	-		-				-	-	-
		0	49PL-2	Max Slope	sub6	1	0.0	7.4852	None	19.995E-		515.74E-6			0 (Negligible)
		•	1000 0	Max Settlement	sub6	1		7.4852		19.995E-		515.74E-6			0 (Negligible)
				Max Tensile Strain	sub6	1		7.4852		19.995E-		515.74E-6			0 (Negligible)
				Min Radius of Curvature (Hogging)	subc	-	0.0		None				-		
				Min Radius of Curvature (Rogging)		-			-						-
		0	49PL-3	All vertical displacements are less					-			-	-	-	-
		0	4357-3	All vertical displacements are less All vertical displacements are less											
				All vertical displacements are less											
				All vertical displacements are less All vertical displacements are less											
				All vertical displacements are less All vertical displacements are less											
			49PL-4	Max Slope	sub8	nit sensi	1.2500			36.600E-		35.763E-9			0 (Negligible)
		0	4957-4		subs								-		
				Max Settlement Max Tensile Strain	sub8	1	1.2500			36.600E- 36.600E-		35.763E-9			0 (Negligible)
					subs	1	1.2500		None	36.600E-	0.16229	35.763E-9	-	-	0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-			-	-	-	-
				Min Radius of Curvature (Sagging)		-			-			-	-	-	-
		0	49PL-5	Max Slope	sub9	1		2.5000		35.725E-		13.268E-6			0 (Negligible)
				Max Settlement	sub9	1		2.5000		35.725E-		13.268E-6			0 (Negligible)
				Max Tensile Strain	sub9	1	0.0	2.5000		35.725E-	6 0.25090	13.268E-6	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-		-	-	-	-	
				Min Radius of Curvature (Sagging)		-	-		-			-	-	-	
		0	49PL-6	Max Slope	sub10	1		3.5332		216.88E-		0.0016432			0 (Negligible)
				Max Settlement	sub10	2	3.5332			216.88E-		0.0045127	-		0 (Negligible)
				Max Tensile Strain	sub10	2	3.5332			216.88E-	6 1.1982	0.0045127	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-	-	-				-	-	-
				Min Radius of Curvature (Sagging)		-	-	-	-				-	-	-

Short-term Underpinning Stage

tage: Ref.	Stage: Name	Specific Building: Ref.		Parameter	Critical Sub-Building				Curvature		Max Settlement	Strain		Curvature (Sagging)	Damage Category
							[m]	[m]			[mm]	[%]	[m]	[m]	
	Base Model	0	45PL-1	Max Slope	subl	1	0.0	€.1500	None	284.32E-6	1.0736	0.0039124	-	-	0 (Negligible)
				Max Settlement	subl	1	0.0	6.1500		284.32E-6	1.0736	0.0039124	-	-	0 (Negligible)
				Max Tensile Strain	subl	1	0.0	6.1500	None	284.32E-6	1.0736	0.0039124	-	-	0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-	-	-	-	-	-	-	-	-
				Min Radius of Curvature (Sagging)			-		-	-	-	-	-		-
		0	45PL-2	All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
		0	45PL-3	All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les	s than the li	mit sensi	tivity.								
				All vertical displacements are les											
		0	45PL-4	Max Slope	sub4	1	1.0154	7.5834	None	132.09E-6	0.74777	0.0014911	-	-	0 (Negligible)
				Max Settlement	sub4	2	7.5834	13.200	None	132.09E-6	1.1235	0.0033627	-	-	0 (Negligible)
				Max Tensile Strain	sub4	2	7.5834	13.200	None	132.09E-6	1.1235	0.0033627	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-	-	-	-	-	-	-	-	-
				Min Radius of Curvature (Sagging)			-	-	-	-	-	-	-		-
		0	49PL-1	Max Slope	sub5	1	0.0	5.5000	None	679.92E-6	2.3778	0.0094426	-	-	0 (Negligible)
				Max Settlement	sub5	1	0.0	5.5000	None	679.92E-6	2.3778	0.0094426	-	-	0 (Negligible)
				Max Tensile Strain	sub5	1	0.0	5.5000	None	679.92E-6	2.3778	0.0094426	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-	-	-	-	-	-	-	-	
				Min Radius of Curvature (Sagging)		-	-	-	-	-	-	-	-	-	-
		0	49PL-2	Max Slope	sub6	1	0.0	6.8999	None	44.903E-6	0.42589	0.0011836	-	-	0 (Negligible)
				Max Settlement	sub6	1		6.8999		44.903E-6		0.0011836	-		0 (Negligible)
				Max Tensile Strain	sub6	1	0.0	6.8999	None	44.903E-6	0.42589	0.0011836	-	-	0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-	-	-	-	-	-	-		
				Min Radius of Curvature (Sagging)		-	-	-	-	-	-	-	-	-	_
		0	49PL-3	Max Slope	sub7	1	2.0000	3.0000	None	28.065E-6	0.14843	35.763E-9	-	-	0 (Negligible)
				Max Settlement	sub7	1	2.0000			28.065E-6		35.763E-9	-		0 (Negligible)
				Max Tensile Strain	sub7	1	2.0000	3.0000	None	28.0652-6		35.763E-9	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-	-	-	-	-	-	-
				Min Radius of Curvature (Sagging)		-	-	-	-		-	-	-		-
		0	49PL-4	Max Slope	sub8	1	0.0	2.5000	None	72.444E-6	0.30982	373.76E-6	-	-	0 (Negligible)
		101		Max Settlement	sub8	1		2.5000		72.444E-6		373.76E-6	-		0 (Negligible)
				Max Tensile Strain	sub8	1		2.5000		72.4448-6		373.76E-6	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-	-	-	-	-		
				Min Radius of Curvature (Sagging)		-	-	-	-	-	-	-	-	-	-
		0	49PL-5	Max Slope	sub9	1	0.0	2.5000	None	63.230E-6	0.46730	11.337E-6	-	-	0 (Negligible)
				Max Settlement	sub9	1		2.5000		63.230E-6		11.337E-6	-		0 (Negligible)
				Max Tensile Strain	sub9	ĩ		2.5000		63.230E-6		11.337E-6	-		0 (Negligible)
				Min Radius of Curvature (Hogging)		-	-		-		-		-	-	
				Min Radius of Curvature (Sagging)		-	-		-	-	-	-	-	-	
		0	49PL-6	Max Slope	sub10	1		4.8744		411.95E-6	1 6604	0.0031191	-		0 (Negligible)
			1750-0	Max Settlement	sub10	2	4.8744			411.952-6		0.0099229	-		0 (Negligible) 0 (Negligible)
				Max Tensile Strain	sub10	2	4.8744			411.952-6		0.0099229	-		0 (Negligible) 0 (Negligible)
				Min Radius of Curvature (Hogging)	50010	-	4.0/44		-	411.305-0	2.0//4	0.0033223	-	-	
							-		-		-	-		-	
				Min Radius of Curvature (Sagging)		-	-	-	-	-	-	-	-		-

Short-term Underpinning + Excavation Stage

Ref.	Stage: 1		Specific Building: Ref.		Parameter	Critical Sub-Building		[m]	End	Curvature	e Max Slope	Max Settlement	Max Tensile Strain [%]	Min Radius of Curvature (Hogging) [m]		Damage Category
								-	-					-		
	Base Mod	iel	0	45PL-1	Max Slope	subl	1			0 None	875.47E-6					0 (Negligible)
					Max Settlement	subl	1			0 None	875.47E-6					0 (Negligible)
					Max Tensile Strain	subl	1	0.0		0 None	875.47E-6	3.8028	0.014212	-		0 (Negligible)
					Min Radius of Curvature (Hoge		-	-			-	-	-	-		
					Min Radius of Curvature (Sage		-	-			-	-	-	-		
			0	45PL-2	Max Slope	sub2	1			0 None	38.143E-6		996.67E-6			0 (Negligible)
					Max Settlement	sub2	1			.0 None	38.143E-6		996.67E-6			0 (Negligible)
					Max Tensile Strain	sub2	1	0.0		.0 None	38.143E-6		996.67E-6			0 (Negligible)
					Min Radius of Curvature (Hogo		-	-			-	-	-	-		
					Min Radius of Curvature (Sage		-	-			-		-	-		
			0	45PL-3	Max Slope	sub3	1			0 None	80.513E-6		798.40E-6			0 (Negligible)
					Max Settlement	sub3	1			0 None	80.513E-6		798.40E-6			0 (Negligible)
					Max Tensile Strain	sub3	1	0.0		0 None	80.513E-6	0.78739	798.40E-6	-		0 (Negligible)
					Min Radius of Curvature (Hoge	jing)	-	-			-	-	-	-	-	
					Min Radius of Curvature (Sage	(ing)	-	-			-	-	-	-		-
			0	45PL-4	Max Slope	sub4	1	0.0	6.509	9 None	403.16E-6	2.6069	0.0044680	-	- 1	0 (Negligible)
					Max Settlement	sub4	2	6.5099	13.20	0 None	403.16E-6	3.8882	0.0098803	-	- 1	0 (Negligible)
					Max Tensile Strain	sub4	2	6.5099	13.20	0 None	403.16E-6	3.8882	0.0098803	-	- 1	0 (Negligible)
					Min Radius of Curvature (Hoge	(ing)	-	-			-	-	-	-		
					Min Radius of Curvature (Sage		-	-			-		-	-		-
			0	49PL-1	Max Slope	sub5	1	0.0	5.500	0 Hogging	0.0025017	8.3265	0.028938	889.23	- 1	0 (Negligible)
					Max Settlement	sub5	1			0 Hogging	0.0025017					0 (Negligible)
					Max Tensile Strain	sub5	1			0 Hogging	0.0025017		0.028938			0 (Negligible)
					Min Radius of Curvature (Hogo		1			0 Hogging	0.0025017		0.028938			0 (Negligible)
					Min Radius of Curvature (Sage		- 2	-			-	-	_	-		
			0	49PL-2	Max Slope	sub6	1	0.0	7.807	0 None	143.61E-6	1.7974	0.0036833	-	- 1	0 (Negligible)
			-		Max Settlement	sub6	1			0 None	143.61E-6		0.0036833			0 (Negligible)
					Max Tensile Strain	sub6	1			0 None	143.61E-6		0.0036833			0 (Negligible)
					Min Radius of Curvature (Hogo			-						-	-	
					Min Radius of Curvature (Sage		-	-				-		-		-
			0	49PL-3	Max Slope	sub7	1	0.0		0 None	112.14E-6	0 99105	207.60E-6	-		0 (Negligible)
			~	1020 0	Max Settlement	sub7	ĩ			0 None	112.14E-6		207.60E-6			0 (Negligible)
					Max Tensile Strain	sub7	ĩ			0 None	112.14E-6		207.60E-6			0 (Negligible)
					Min Radius of Curvature (Hogo		-					0.00100	207.000 0	-	-	
					Min Radius of Curvature (Sage			-			_			_	-	
			0	49PL-4	Max Slope	sub8	1			0 None	261.94E-6		0.0012182			0 (Negligible)
			•	1725-1	Max Settlement	sub8	1			0 None	261.942-6		0.0012182			0 (Negligible)
					Max Tensile Strain	sub8	1			0 None	261.942-6		0.0012182			0 (Negligible)
					Min Radius of Curvature (Hogo		-	0.0			201.942-0	1.5/16			-	
							-	-			-		-	-	-	
			0	49PL-5	Min Radius of Curvature (Sage		1	-					-	-		
			0	4257-2	Max Slope	sub9	1			0 None	249.93E-6		36.871E-6			0 (Negligible)
					Max Settlement	sub9				0 None	249.93E-6		36.871E-6			0 (Negligible)
					Max Tensile Strain	sub9	1	0.0		0 None	249.93E-6	2.1945	36.871E-6	-		0 (Negligible)
					Min Radius of Curvature (Hoge		-	-			-	-	-	-		
					Min Radius of Curvature (Sage		-	-			-	-	-	-		
			0	49PL-6	Max Slope	sub10	1			1 None	0.0014895		0.011059			0 (Negligible)
					Max Settlement	sub10	2			0 Sagging	0.0014895		0.030341			0 (Negligible)
					Max Tensile Strain	sub10	2			0 Sagging	0.0014895		0.030341			0 (Negligible)
					Min Radius of Curvature (Hogo		-	-			-	-	-	-	-	
					Min Radius of Curvature (Sage	(ing) subl0	2	2 4291	9 500	0 Sagging	0.0014995	9 4116	0.030341	-	2086 4	0 (Negligible)

Long term Underpinning + Excavation + Loading Stage

B. Pdisp Tabular Output

lef.	Name	x	Y	=	δz	Stress: Calc.	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m ²]	[kN/m ²]	[11]
1	45PL-1	-8.20000	2.60000	0.00000	0.49499	-0.18750	0.0	0.0	[µ] 0.
	45PL-1	-9.22500	2.60000	0.00000	0.35998	-0.18750	0.0	0.0	0.
1	45PL-1	-10.25000	2.60000	0.00000	0.26362	-0.18750	0.0	0.0	0.
	45PL-1	-11.27500	2.60000	0.00000	0.19291	-0.18750	0.0	0.0	0.
	45PL-1	-12.30000	2.60000	0.00000	0.14010	-0.18750	0.0	0.0	0.
	45PL-1	-13.32500	2.60000	0.00000	0.10024	-0.18750	0.0	0.0	0.
	45PL-1 45PL-1	-14.35000 -15.37500	2.60000	0.00000	0.06994	-0.18750	0.0	0.0	0.
	45PL-1	-16.40000	2.60000	0.00000	0.02925	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	2.60000	0.00000	0.02925	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	3.61538	0.00000	0.03012	-0.18750	0.0	0.0	0.
2	45PL-2	-16.40000	4.63077	0.00000	0.03000	-0.18750	0.0	0.0	0.
2	45PL-2	-16.40000	5.64615	0.00000	0.02889	-0.18750	0.0	0.0	0.
2	45PL-2	-16.40000	6.66154	0.00000	0.02685	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	7.67692	0.00000	0.02402	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	8.69231	0.00000	0.02054	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	9.70769	0.00000	0.01660	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	10.72308	0.00000	0.01240	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	11.73846	0.00000	0.00813	-0.18750	0.0	0.0	0.
	45PL-2 45PL-2	-16.40000	12.75385 13.76923	0.00000	0.00394	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	14.78462	0.00000	-0.00368	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	15.80000	0.00000	-0.00695	-0.18750	0.0	0.0	0
	45PL-3	-16.40000	15.80000	0.00000	-0.00695	-0.18750	0.0	0.0	0
3	45PL-3	-15.37500	15.80000	0.00000	-0.00257	-0.18750	0.0	0.0	0
3	45PL-3	-14.35000	15.80000	0.00000	0.00277	-0.18750	0.0	0.0	0
	45PL-3	-13.32500	15.80000	0.00000	0.00913	-0.18750	0.0	0.0	0
	45PL-3	-12.30000	15.80000	0.00000	0.01655	-0.18750	0.0	0.0	0
	45PL-3	-11.27500	15.80000	0.00000	0.02504	-0.18750	0.0	0.0	0
	45PL-3	-10.25000	15.80000	0.00000	0.03448	-0.18750	0.0	0.0	0
	45PL-3	-9.22500	15.80000	0.00000	0.04467	-0.18750	0.0	0.0	0
	45PL-3 45PL-4	-8.20000	15.80000	0.00000	0.05525	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	14.78462	0.00000	0.07763	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	13.76923	0.00000	0.10548	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	12.75385	0.00000	0.13976	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	11.73846	0.00000	0.18136	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	10.72208	0.00000	0.22072	-0.18750	0.0	0.0	0
4	45PL-4	-8.20000	9.70769	0.00000	0.28712	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	8.69231	0.00000	0.34752	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	7.67692	0.00000	0.40587	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	6.66154	0.00000	0.45478	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	5.64615	0.00000	0.48911	-0.18750	0.0	0.0	0
	45PL-4 45PL-4	-8.20000	4.63077 3.61538	0.00000	0.50719	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	2.60000	0.00000	0.49499	-0.18750	0.0	0.0	0
	49PL-1	0.80000	2.60000	0.00000	1.17470	-0.18750	0.0	0.0	0
	49PL-1	1.90000	2.60000	0.00000	0.76287	-0.18750	0.0	0.0	0
	49PL-1	3.00000	2.60000	0.00000	0.52760	-0.18750	0.0	0.0	0
5	49PL-1	4.10000	2.60000	0.00000	0.37403	-0.18750	0.0	0.0	0
5	49PL-1	5.20000	2.60000	0.00000	0.26765	-0.18750	0.0	0.0	0
	49PL-1	6.30000	2.60000	0.00000	0.19143	-0.18750	0.0	0.0	0
	49PL-2	6.30000	2.60000	0.00000	0.19143	-0.18750	0.0	0.0	0
	49PL-2	6.30000	3.60000	0.00000	0.19623	-0.18750	0.0	0.0	0
	49PL-2	6.30000	4.60000	0.00000	0.19569	-0.18750	0.0	0.0	0
	49PL-2 49PL-2	6.30000	5.60000	0.00000	0.18986	-0.18750	0.0	0.0	0
	49PL-2	6.30000	7.60000	0.00000	0.16431	-0.18750	0.0	0.0	0
	49PL-2	6.30000	8.60000	0.00000	0.14649	-0.18750	0.0	0.0	0
	49PL-2	6.30000	9.60000	0.00000	0.12694	-0.18750	0.0	0.0	0
	49PL-2		10.60000						0
6	49PL-2	6.30000	11.60000	0.00000	0.08756	-0.18750	0.0		0
	49PL-2	6.30000							0
	49PL-2	6.30000	13.60000	0.00000	0.05334		0.0		0
		6.30000							0
	49PL-3	6.30000	14.60000	0.00000	0.03916		0.0		0
	49PL-3 49PL-3	5.30000	14.60000	0.00000	0.05186				0
		3.30000							0
	49PL-3	3.30000	14.60000			-0.18750			0
	49PL-4		13.35000						0
	49PL-4	3.30000	12.10000		0.16229				0
		3.30000							0
	49PL-5	2.05000	12.10000	0.00000	0.20624	-0.18750	0.0		0
	49PL-5	0.80000	12.10000		0.25090				0
	49PL-6	0.80000	12.10000	0.00000	0.25090				0
	49PL-6	0.80000							0
	49PL-6	0.80000	8.93333	0.00000	0.64708		0.0		0
	49PL-6	0.80000			0.99047				0
	49PL-6	0.80000	5.76667	0.00000	1.15835		0.0		0
	49PL-6 49PL-6	0.80000	4.18333 2.60000	0.00000	1.19849		0.0		0

Short-term Underpinning Stage

£.	Name	×	Y	z	δz	Stress: Calc.	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
						Level			
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m ²]	[kN/m*]	[µ]
	45PL-1	-8.20000	2.60000	0.00000	-1.07357	-0.18750	0.0	0.0	0.
	45PL-1	-9.22500	2.60000	0.00000	-0.78214	-0.18750	0.0	0.0	0.
	45PL-1	-10.25000	2.60000	0.00000	-0.57161	-0.18750	0.0	0.0	0.
	45PL-1 45PL-1	-11.27500	2.60000	0.00000	-0.41642	-0.18750	0.0	0.0	0.
	45PL-1	-13.32500	2.60000	0.00000	-0.21299	-0.18750	0.0	0.0	0.
	45PL-1	-14.35000	2.60000	0.00000	-0.14670	-0.18750	0.0	0.0	0.
	45PL-1	-15.37500	2.60000	0.00000	-0.09633	-0.18750	0.0	0.0	0.
_	45PL-1	-16.40000	2.60000	0.00000	-0.05809	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	2.60000	0.00000	-0.05809	-0.18750	0.0	0.0	0.
2	45PL-2	-16.40000	3.61538	0.00000	-0.06015	-0.18750	0.0	0.0	0.
2	45PL-2	-16.40000	4.63077	0.00000	-0.05987	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	5.64615	0.00000	-0.05724	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	6.66154	0.00000	-0.05247	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	7.67692	0.00000	-0.04588	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	8.69231	0.00000	-0.03789	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	9.70769	0.00000	-0.02898	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	10.72308	0.00000	-0.01961	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	11.73846	0.00000	-0.01020	-0.18750	0.0	0.0	0.
	45PL-2	-16.40000	12.75385 13.76923	0.00000	-0.00113	-0.18750	0.0	0.0	0.
	45PL-2 45PL-2	-16.40000	13.76923	0.00000	0.00735	-0.18750	0.0	0.0	0.
	45PL-2 45PL-2	-16.40000	14.78462	0.00000	0.01503	-0.18750	0.0	0.0	0.
_	45PL-2	-16.40000	15.80000	0.00000	0.02180	-0.18750	0.0	0.0	0.
	45PL-3	-15.37500	15.80000	0.00000	0.01323	-0.18750	0.0	0.0	0.
	45PL-3	-14.35000	15.80000	0.00000	0.00280	-0.18750	0.0	0.0	0.
	45PL-3	-13.32500	15.80000	0.00000	-0.00960	-0.18750	0.0	0.0	0.
	45PL-3	-12.30000	15.80000	0.00000	-0.02403	-0.18750	0.0	0.0	0.
3	45PL-3	-11.27500	15.80000	0.00000	-0.04042	-0.18750	0.0	0.0	0.
3	45PL-3	-10.25000	15.80000	0.00000	-0.05852	-0.18750	0.0	0.0	0.
3	45PL-3	-9.22500	15.80000	0.00000	-0.07792	-0.18750	0.0	0.0	0.
3	45PL-3	-8.20000	15.80000	0.00000	-0.09792	-0.18750	0.0	0.0	0.
4	45PL-4	-8.20000	15.80000	0.00000	-0.09792	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	14.78462	0.00000	-0.14213	-0.18750	0.0	0.0	0.
4	45PL-4	-8.20000	13.76923	0.00000	-0.19715	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	12.75385	0.00000	-0.26485	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	11.73846	0.00000	-0.34697	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	10.72308	0.00000	-0.44473	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	9.70769	0.00000	-0.55812	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	8.69231	0.00000	-0.68493	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	7.67692	0.00000	-0.81905	-0.18750	0.0	0.0	0.
	45PL-4 45PL-4	-8.20000	6.66154 5.64615	0.00000	-0.94821 -1.05380	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	4.63077	0.00000	-1.11642	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	3.61538	0.00000	-1.12349	-0.18750	0.0	0.0	0.
	45PL-4	-8.20000	2.60000	0.00000	-1.07357	-0.18750	0.0	0.0	0.
	49PL-1	0.80000	2.60000	0.00000	-2.37781	-0.18750	0.0	0.0	0.
	49PL-1	1.90000	2.60000	0.00000	-1.62990	-0.18750	0.0	0.0	0.
	49PL-1	3.00000	2.60000	0.00000	-1.14309	-0.18750	0.0	0.0	0.
5	49PL-1	4.10000	2.60000	0.00000	-0.81269	-0.18750	0.0	0.0	0.
5	49PL-1	5.20000	2.60000	0.00000	-0.58043	-0.18750	0.0	0.0	0.
	49PL-1	6.30000	2.60000	0.00000	-0.41318	-0.18750	0.0	0.0	0.
	49PL-2	6.20000	2.60000	0.00000	-0.41318	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	3.60000	0.00000	-0.42595	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	4.60000	0.00000	-0.42451	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	5.60000	0.00000	-0.40903	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	6.60000	0.00000	-0.38132	-0.18750	0.0		0.
	49PL-2	6.30000	7.60000	0.00000	-0.34441	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	8.60000	0.00000	-0.30182	-0.18750	0.0		0.
	49PL-2 49PL-2	6.30000	9.€0000 10.€0000	0.00000	-0.25692	-0.18750	0.0	0.0	0.
	49PL-2 49PL-2	6.30000	11.60000	0.00000	-0.21248	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	12.60000	0.00000	-0.13230	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	13.60000	0.00000	-0.09847	-0.18750	0.0	0.0	0.
	49PL-2	6.30000	14.60000	0.00000	-0.06923	-0.18750	0.0	0.0	0.
	49PL-3	6.30000	14.60000	0.00000	-0.06923	-0.18750	0.0	0.0	0.
	49PL-3	5.30000	14.60000	0.00000	-0.09370	-0.18750	0.0		0.
	49PL-3	4.30000	14.60000	0.00000	-0.12037	-0.18750	0.0	0.0	0.
	49PL-3	3.30000	14.60000	0.00000	-0.14843	-0.18750	0.0	0.0	0.
8	49PL-4	3.30000	14.60000	0.00000	-0.14843	-0.18750	0.0	0.0	0.
8	49PL-4	3.30000	13.35000	0.00000	-0.21927	-0.18750	0.0	0.0	0.
8	49PL-4	3.30000	12.10000	0.00000	-0.20982	-0.18750	0.0	0.0	0.
9	49PL-5	3.30000	12.10000	0.00000	-0.20982	-0.18750	0.0	0.0	0.
	49PL-5	2.05000	12.10000	0.00000	-0.38886	-0.18750	0.0	0.0	0.
	49PL-5	0.80000	12.10000	0.00000	-0.46730	-0.18750	0.0	0.0	0.
	49PL-6	0.80000	12.10000	0.00000	-0.46730	-0.18750	0.0	0.0	0.
	49PL-6	0.80000	10.51667	0.00000	-0.72895	-0.18750	0.0		0.
	49PL-6	0.80000	8.93333	0.00000	-1.10001	-0.18750	0.0	0.0	0.
	49PL-6	0.80000	7.35000	0.00000	-1.60916	-0.18750	0.0	0.0	0.
	49PL-6	0.80000	5.76667	0.00000	-2.26141	-0.18750	0.0	0.0	0.
10	49PL-6	0.80000	4.18333	0.00000	-2.57845	-0.18750	0.0		0.
	49PL-6	0.80000	2.60000	0.00000	-2.37781	-0.18750	0.0	0.0	0.

Short-term Underpinning + Excavation Stage

£.	Name	x	У		ðz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m ²]	[kN/m ²]	[µ]
	45PL-1	-8.20000	2.60000	0.00000	3.80282	-0.18750	0.0	0.0	0.
	45PL-1	-9.22500	2.60000	0.00000	2.90546	-0.18750	0.0	0.0	0.
	45PL-1	-10.25000	2.60000	0.00000	2.25794	-0.18750	0.0	0.0	0.
	45PL-1	-11.27500	2.60000	0.00000	1.77528	-0.18750	0.0	0.0	0.
	45PL-1 45PL-1	-12.30000	2.60000	0.00000	1.40751	-0.18750	0.0	0.0	0
	45PL-1	-14.35000	2.60000	0.00000	0.90003	-0.18750	0.0	0.0	0
	45PL-1	-15.37500	2.60000	0.00000	0.72402	-0.18750	0.0	0.0	0
	45PL-1	-16.40000	2.60000	0.00000	0.58405	-0.18750	0.0	0.0	0
2	45PL-2	-16.40000	2.60000	0.00000	0.58405	-0.18750	0.0	0.0	0
2	45PL-2	-16.40000	3.61538	0.00000	0.59121	-0.18750	0.0	0.0	0
2	45PL-2	-16.40000	4.63077	0.00000	0.59022	-0.18750	0.0	0.0	0
2	45PL-2	-16.40000	5.64615	0.00000	0.58111	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	6.66154	0.00000	0.56436	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	7.67692	0.00000	0.54078	-0.18750	0.0		0
	45PL-2	-16.40000	8.69231	0.00000	0.51149	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	9.70769	0.00000	0.47781	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	10.72308	0.00000	0.44112	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	11.73846	0.00000	0.40279	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	12.75385			-0.18750	0.0	0.0	0
	45PL-2 45PL-2	-16.40000	13.76923 14.78462	0.00000	0.32598	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	15.80000	0.00000	0.25492	-0.18750	0.0	0.0	0
	45PL-2	-16.40000	15.80000	0.00000	0.25492	-0.18750	0.0	0.0	0
	45PL-3	-15.37500	15.80000	0.00000	0.30013	-0.18750	0.0	0.0	0
	45PL-3	-14.35000	15.80000	0.00000	0.35170	-0.18750	0.0	0.0	0
	45PL-3	-13.32500	15.80000	0.00000	0.40998	-0.18750	0.0		0
	45PL-3	-12.30000	15.80000	0.00000	0.47504	-0.18750	0.0	0.0	0
3	45PL-3	-11.27500	15.80000	0.00000	0.54659	-0.18750	0.0	0.0	0
3	45PL-3	-10.25000	15.80000	0.00000	0.62374	-0.18750	0.0	0.0	0
3	45PL-3	-9.22500	15.80000	0.00000	0.70486	-0.18750	0.0	0.0	0
3	45PL-3	-8.20000	15.80000	0.00000	0.78739	-0.18750	0.0	0.0	0
4	45PL-4	-8.20000	15.80000	0.00000	0.78739	-0.18750	0.0	0.0	0
4	45PL-4	-8.20000	14.78462	0.00000	0.95774	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	13.76923	0.00000	1.16373	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	12.75385	0.00000	1.41142	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	11.73846	0.00000	1.70626	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	10.72308	0.00000	2.05057	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	9.70769	0.00000	2.43848	-0.18750	0.0		0
	45PL-4 45PL-4	-8.20000	8.69231	0.00000	2.84784 3.23571	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	6.66154	0.00000	3.55206	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	5.64615	0.00000	3.76680	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	4.63077	0.00000	3.87666	-0.18750	0.0	0.0	0
	45PL-4	-8.20000	3.61538	0.00000	3.88831	-0.18750	0.0	0.0	0
4	45PL-4	-8.20000	2.60000	0.00000	3.80282	-0.18750	0.0	0.0	0
5	49PL-1	0.80000	2.60000	0.00000	8.32649	-0.18750	0.0	0.0	0
5	49PL-1	1.90000	2.60000	0.00000	5.57466	-0.18750	0.0	0.0	0
	49PL-1	3.00000	2.60000	0.00000	4.01871	-0.18750	0.0	0.0	0
	49PL-1	4.10000	2.60000	0.00000	2.99926	-0.18750	0.0	0.0	0
	49PL-1	5.20000	2.60000	0.00000	2.28519	-0.18750	0.0	0.0	0
	49PL-1	6.30000	2.60000	0.00000	1.76510	-0.18750	0.0	0.0	0
	49PL-2	6.20000	2.60000	0.00000	1.76510	-0.18750	0.0	0.0	0
	49PL-2	6.30000	3.60000	0.00000	1.79750	-0.18750	0.0	0.0	0
	49PL-2 49PL-2	6.20000	4.60000 5.60000	0.00000	1.79388	-0.18750	0.0	0.0	0
	49PL-2 49PL-2		6.60000		1.68138		0.0		0
	49PL-2	6.30000	7.60000	0.00000	1.57934		0.0		0
	49PL-2	6.30000			1.45509				0
	49PL-2	6.30000	9.60000	0.00000	1.31694		0.0		0
	49PL-2	6.30000	10.60000		1.17333		0.0		0
	49PL-2	6.30000	11.60000	0.00000	1.03157		0.0		0
	49PL-2		12.60000			-0.18750	0.0		0
	49PL-2	6.30000	13.60000	0.00000	0.77319	-0.18750	0.0	0.0	0
	49PL-2	6.30000	14.60000	0.00000	0.66169		0.0	0.0	0
7	49PL-3	6.30000	14.60000	0.00000	0.66169		0.0	0.0	0
	49PL-3		14.60000		0.76151		0.0		0
	49PL-3	4.30000	14.60000	0.00000	0.86890		0.0		0
	49PL-3		14.60000	0.00000	0.98105		0.0		0
	49PL-4	3.30000	14.60000	0.00000	0.98105		0.0		0
	49PL-4		13.35000			-0.18750			0
	49PL-4	3.30000	12.10000	0.00000	1.57164		0.0		0
	49PL-5		12.10000		1.57164		0.0		0
	49PL-5	2.05000	12.10000	0.00000	1.88211		0.0		0
	49PL-5	0.80000		0.00000	2.19453		0.0		0
	49PL-6	0.80000	12.10000	0.00000	2.19453		0.0		0
	49PL-6		10.51667	0.00000		-0.18750	0.0		0
	49PL-6	0.80000	8.93333	0.00000	4.93464		0.0		0
	49PL-6	0.80000	7.35000	0.00000	7.29293		0.0		0
	49PL-6	0.80000	5.76667	0.00000	8.25726		0.0		0
	49PL-6	0.80000	4.18333	0.00000	8.41272	-0.18750	0.0	0.0	0

Long term Underpinning + Excavation + Loading Stage



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