



Email: ccconsultw4@gmail.com
Tel: 07793200529

Project No:	S-2930	Calc By:	BC
Project:	161 ARLINGTON ROAD,LONDON NW1 7ET		
Date:	01 February 2024	Rev:	0

Title: Structural Calculations for Proposed Refurbishment of 161 Arlington Road

Section 7 Superstructure elements

Cpe		
Front wall	D/H < 1	0.85
Side wall		-1.3
Roof	A	-1.9
	B	-1.3
	C	-0.7
	D	±0.2

Cpi		Cpi
Two walls preamble		0.2
		-0.3

Cp	parapet without returns	Cp	Length
		A	3.4 0.225 m
		B	2.1 1.5
		C	1.7 3
		D	1.2 3.7

Side Wall qs = 0.33 kPa Ca = 0.97 k = 0.7

$p = qs \cdot Ca \cdot (Cpe - Cpi)$ Cpe-Cpi = 1.15 P= 0.368 kPa windward side
-1.5 P= -0.481 kPa side

Parapet

L 3.7 m < 15h = 11.25 with L/h = 4.933 gives reduction factor
h = Hr = 0.75 m max k = 0.7

$p = qs \cdot Cp \cdot Ca \cdot K$		start	end	length	
	A	Pa = 0.763 kPa	0.00	0.23	0.23
	B	Pb = 0.471 kPa	0.23	1.50	1.28
	C	Pc = 0.381 kPa	1.50	3.00	1.50
	D	Pd = 0.269 kPa	3.00	3.70	0.70

Roof - check for uplift

Roof loads Dead 0.898
Live 1.5

	Cpe	Cpi	Cpe-Cpi	p	
A	-1.90	0.20	-2.10	-0.67	OK
B	-1.30	0.20	-1.50	-0.48	OK
C	-0.70	0.20	-0.90	-0.29	OK
D	-0.20	0.20	-0.40	-0.13	OK
	0.20	-0.30	0.50	0.16	OK



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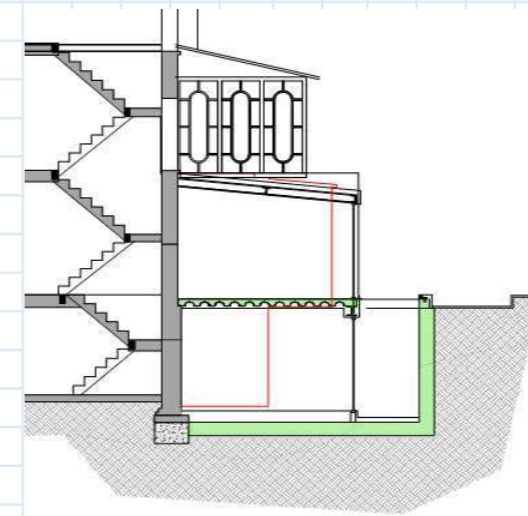
Project No:	S-2930	Calc By:	BC
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Rear Extension Side Walls- masonry design To BS5628-1

Side walls	Width	3700 mm
	Storey Height	2850 mm max
	Parapet	750 mm



Density brick 20 kN/m3 set in type (iii) 1:1:6 mortar
Density block 18 kN/m3

Assume 100 block inner leaf / 100 cavity / 102.5 brick outer leaf


Vertical Capacity

Total height of wall above ground floor 2850 mm
Panel width 3700 mm
effective height = height between support = 2850 mm
effective thickness = 2/3 (ti + to) = 135 mm h/t = 21.11 < 40 - therefore panel ok

$\lambda = 21.11$ less than 27 - okay

Tb7 gives ecc = 0.1 t $\beta = 0.53$ $\gamma_m = 3.1$ t = 100

Vert load resistance $V_r = (\beta \cdot t / \gamma_m) \cdot f_k = 17.1 \times (f_k)$ N/mm



COCHRANE CONSTRUCTION CONSULTANTS
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Section 7 Superstructure elements

					Dead	Live
Self wt of wall = $\rho \cdot t \cdot h =$					5.13	
Beams - assume to act as udl along full length						
	R dead	R live	width =			
B5	4.15	3.08	3.7 m		1.122	0.832
B4	2.17	1.54			0.586	0.416
				SLS	6.838	1.249
Yf	dead 1.4	live 1.6		ULS	9.573	1.998
Vd =	11.57 kN/m			stress vd =	0.116 N/mm ²	

vr = vd, gives fk reqd = 0.677 N/mm² **Try 2.8N block**

Block
 Tb 2c with type (iii) mortar gives reqd compressive strength of unit = 2.8 N/mm² **Block**

fk =	2.8 N/mm ²	fk = 2.8
fkx parallel	0.25 N/mm ²	fkx par= 0.25
fkx perpendicular	0.4 N/mm ²	fkx prp 0.4

Brick
 20N brick in type(iii)0 mortar water absorption between 7% and 12% **Brick**

fk =	5.8 N/mm ²	fk = 5.8
fkx parallel	0.4 N/mm ²	fkx par= 0.4
fkx perpendicular	1.1 N/mm ²	fkx prp 1.1


Padstones
 To CP 111, using 2.8N block in 1:1:6 mortar, comp stress = 0.28 N/mm²

t =	100 mm	Ym =	3.1
-----	--------	------	-----

	R dead	R live	Total kN	Bearing factor	Local cap	Area reqd	L reqd (mm)
B5	4.15	3.08	7.23	1.5	1.355	5336	53
B4	2.17	1.54	3.71	1.25	1.129	3286	33

Lateral Loading

Assume wall is: simply supported at ground floor
 simply supported at existing rear wall
 continuous over first floor and roof
 free on rear edge **Tb 9 - case L**



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Section 7 Superstructure elements

Wind Loading

From wind loading (see above)	Wk =	0.368 kPa
	Yf =	1.4

Panel

L =	3700	h/L =	0.77
h =	2850		
teff =	135		
	μ	α	α from Tb9 / L
Brick	0.364	0.06	
Block	0.625	0.043	

Ck panel (cl 36.3)
 $hl < 1350 teff^2$

10545000	<	24603750	OK
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Design Moment Md

Assume wall spans vertically
 $Md = W_{kYf} h^2 / 8 = 0.524$ kNm

Moment of resistance Mr

$Mr = \frac{f_{kx} Z}{\gamma_m}$
 $Ym = \text{special / normal} = 3.1$ $Z = bd^2/6$

fkx parallel enhanced by self weight over
 enhanced $fkx = fkx' = fkx + Ym (gd \cdot Yfg)$ $Yfg = 0.9$

Use masonry stress at mid height of panels

	Ht m	Density kN/m ³	tk mm	Load kN/m	gd N/mm ²	Ym.gd.Yfg N/mm ²	fkx N/mm ²	fkx' N/mm ²	Z mm ³	Mr kNm
Grd	4.81	brick 20	102.5	9.8605	0.096	0.268	0.4	0.668	1751041.7	0.38
	4.81	block 18	100	8.658	0.087	0.242	0.25	0.492	1666666.7	0.26
										0.64

Mr ground 0.64 kNm > Design Moment Md 0.524 kNm

Main panels okay

Parapet Treat as freestanding wall (cantilever)

750 mm $M_d = Y_f w l^2 / 2$ $Y_f = 1$
 Maximum height =

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Title: Structural Calculations for Proposed Refurbishment of 161 Arlington Road
 Section 7 Superstructure elements

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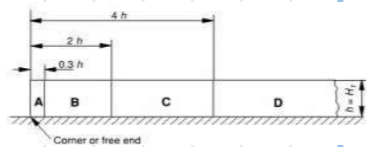
Design Moment Md

Wind loading from above

	p	start	end	length	Md
Zone A	0.763	0.225	1.500	1.275	0.185
Zone B	0.471	1.500	3.000	1.500	0.15
Zone C	0.381	3.000	3.700	0.700	0.106
Zone D	0.269	m	m	m	kNm

kPa

$\gamma_m = 3.1$



Moment of Resistance Mr

	Tk	Z	fkx	Mr
brick	102.5	1751041.7	0.4	0.226
block	100	1666666.7	0.25	0.134

0.360 kNm **Panel okay for all zones**
 UF = 0.833 (zone A)

Support to leading edge

Double exposure of parapet and cyclic nature of loading on leading edge - add windpost on leading edge fixed to steels

Design loading

Wind Loading $(0.225) \cdot \text{zone A} + (1-0.225) \cdot \text{zone B}$
 = 0.537 kPa $\gamma_f = 1.6$ $l = 1000$ mm
 $Wk = 0.859$

$M = wl^2/2 = 0.268$ $Z_{reqd} = M/\sigma$ $\sigma = 275$ N/mm²
 $Z_{reqd} = 975.62052$ mm³ $\delta = wk l^4/8EI$ $\delta_{limit} = \text{span} / 500$
 2 mm

$I_{reqd} = w l^4/8E\delta$ ## mm⁴
 60x60x5 SHS Z 18100 mm³
 I 544000 mm⁴ $\delta = 0.96$ mm

Deflection of beam will give deflection on windpost

152x89UB (Initial B4 section)

w	1.55	kN/m
I	838	cm ⁴ 8380000 mm ⁴
e	205000	

L 4100

Slope $wl^3 / 24 EI = 0.002591$ radians = 148.5 degrees
 3.139 = 31.54 deg from horz

Wind post 1000 mm long

beam deflection = 2.59
 post deflection = 0.96
 total deflection = 3.55 mm Deflection = span / ##

Try 152UC23

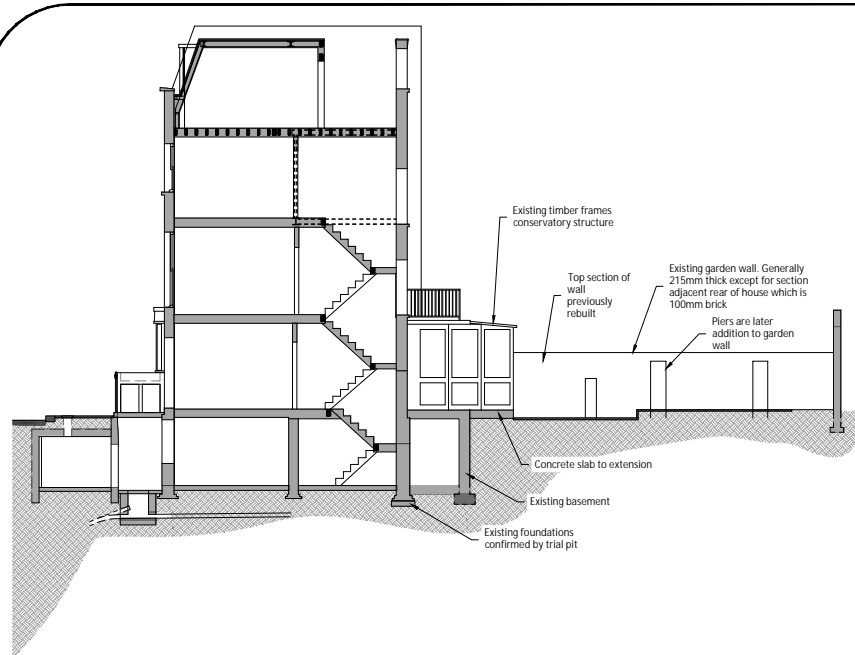
w	1.55	kN/m
I	1250	cm ⁴ 12500000 mm ⁴
e	205000	
L	4100	

Slope $wl^3 / 24 EI = 0.001737$ radians = 0.1 degrees
 3.140 = 179.9 deg from horz

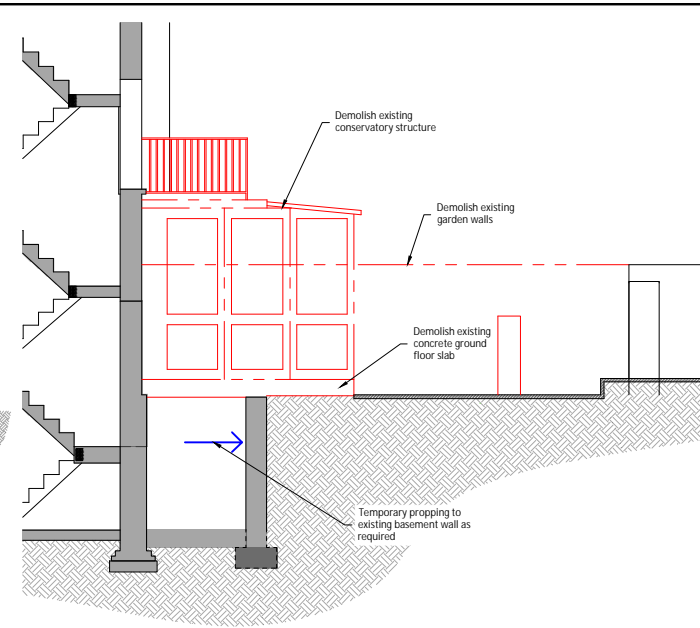
beam deflection = 1.74
 post deflection = 0.96
 total deflection = 2.70 mm Deflection = span / 370.5

Change B4 to 152UC23

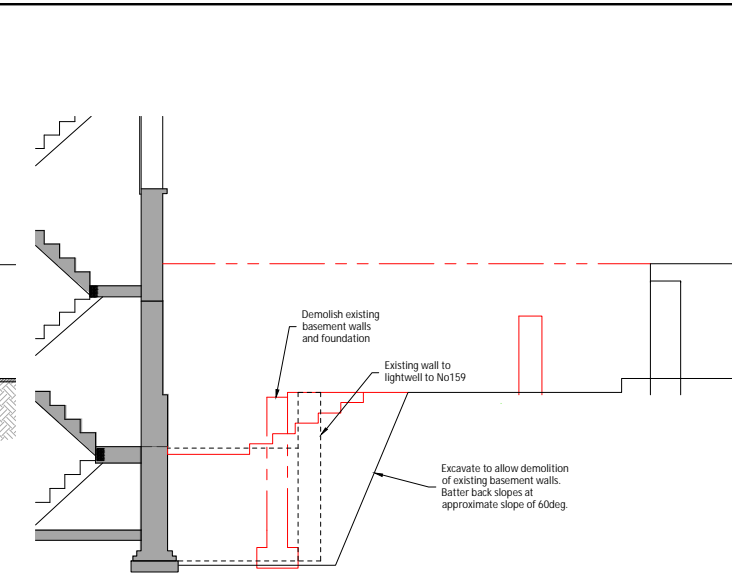
APPENDIX D – CONSTRUCTION SEQUENCE



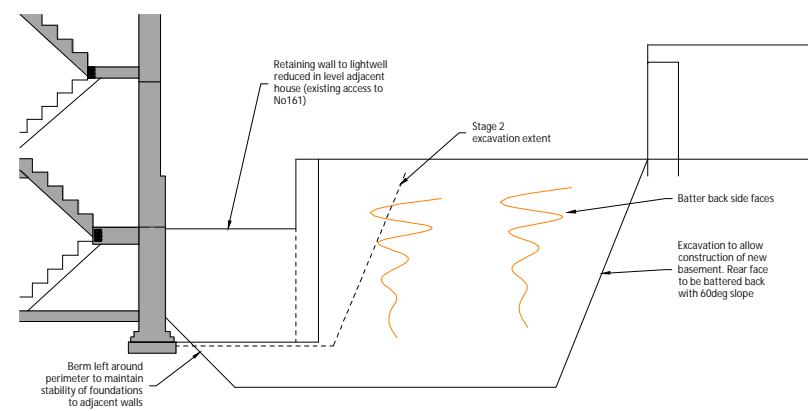
STAGE 0 - EXISTING BUILDING



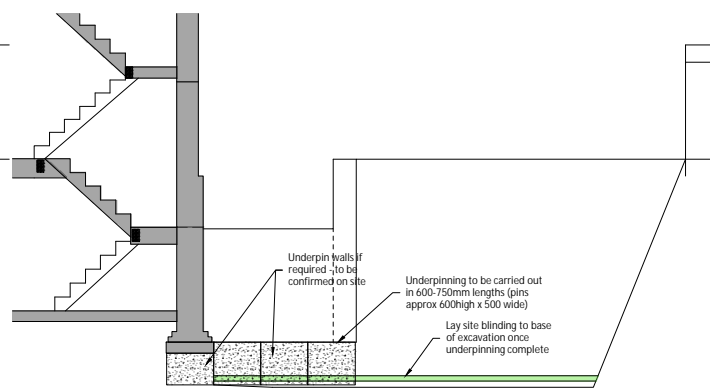
STAGE 1 - SITE PREPARATION & INITIAL DEMOLITION



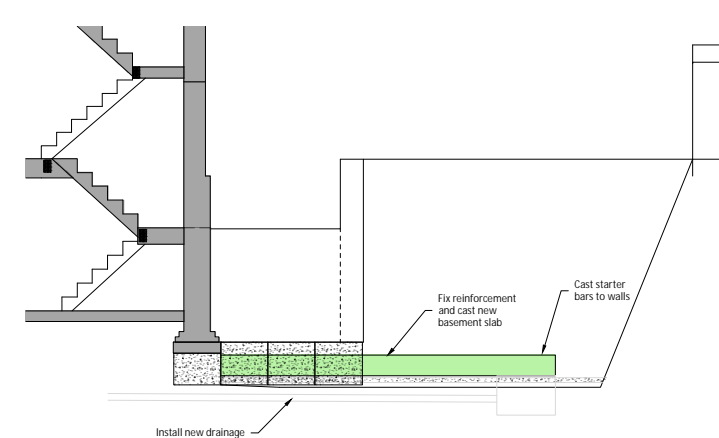
STAGE 2 - COMPLETION OF DEMOLITION



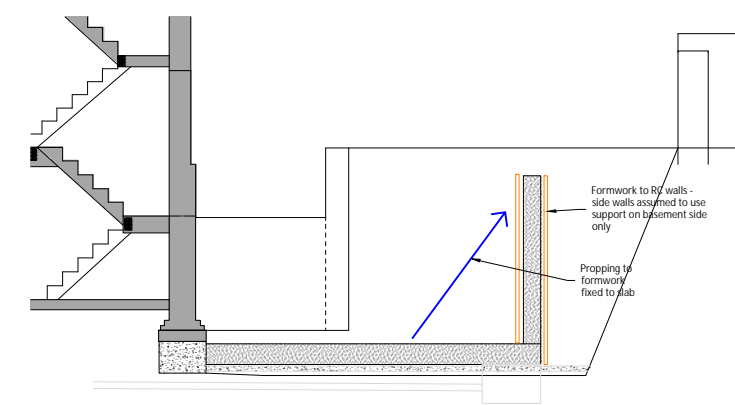
STAGE 3 - EXCAVATION



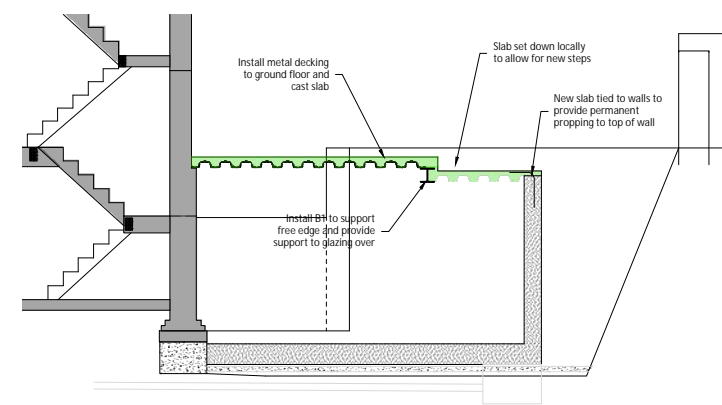
STAGE 4 - UNDERPINNING



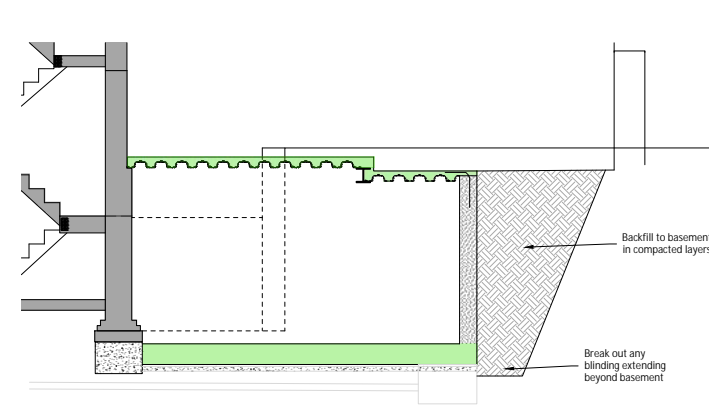
STAGE 5 - CAST BASEMENT SLAB



STAGE 6 - CAST BASEMENT WALLS



STAGE 7 - CONSTRUCT GROUND FLOOR SLAB



STAGE 8 - BACKFILL

General Notes

NOTES
 Sequence shown is that assumed in the design for the rebuilding of the rear extension to 161 Arlington Road and referenced in the Basement Impact Assessment submitted as part of the planning application to Camden.
 Existing foundations shown are based on site investigation carried out by Fastrak.
 Extent of works to garden walls to be agreed with neighbouring properties under Party Wall process.

No.	Revision/Issue	Date

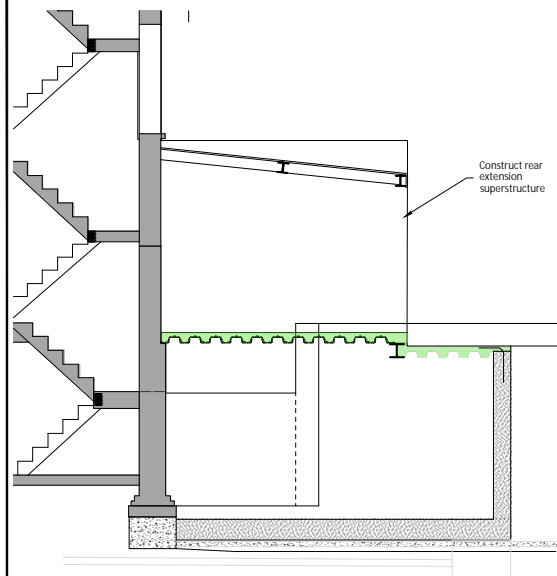
CCC COCHRANE CONSTRUCTION CONSULTANTS
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 Email: ccconsultw4@gmail.com

Client

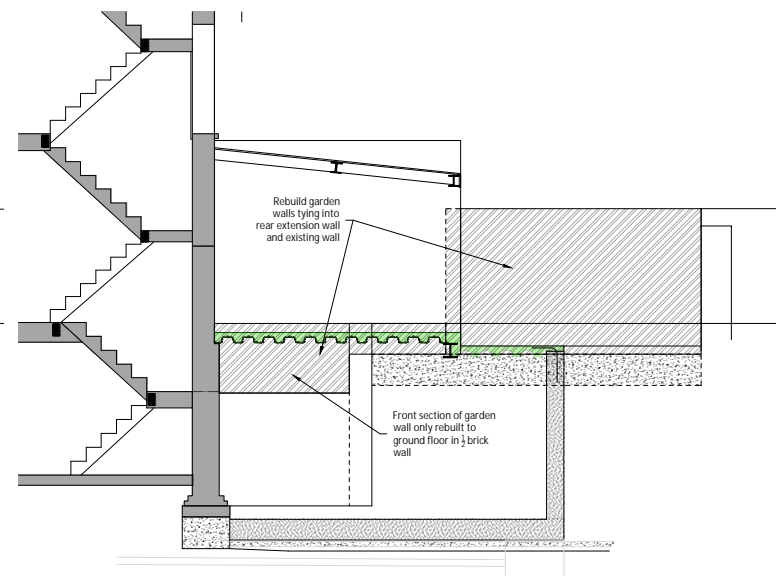
Project Name and Address
**161 ARLINGTON ROAD
 LONDON NW1 7ET**
 Proposed Structure
 Sequence of Construction
 1 of 2

Drawn	BC	Project	S 2930
Date	20.01.2024	Sheet	TW 001
Scale	1:50 @ A1 1:100 @ A3		--

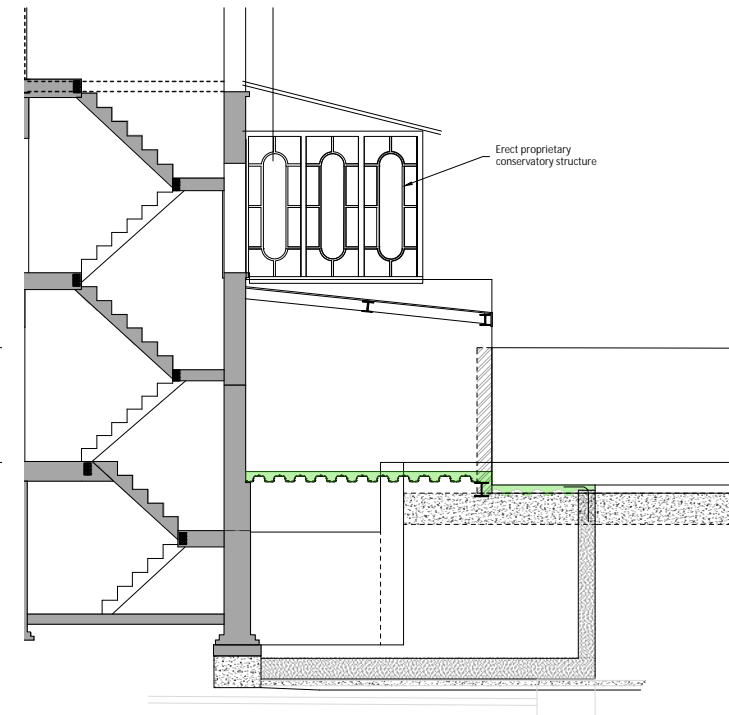
S 2930 - 161 AR Sequence.dwg
8 April 2024



STAGE 9 - CONSTRUCT SUPERSTRUCTURE



STAGE 10 - REBUILD GARDEN WALLS



STAGE 11 - COMPLETION

General Notes

No.	Revision/Issue	Date



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Client

Project Name and Address
161 ARLINGTON ROAD
LONDON NW1 7ET

Proposed Structure
Sequence of Construction
2 of 2

Drawn BC	Project S 2930
Date 20.01.2024	Sheet TW 002
Scale 1:50 @ A1 1:100 @ A3	Rev --

APPENDIX E – SITE INVESTIGATION REPORT



Geotechnical Survey Report

FSI Ref: 27798
 Issue Date: January 2024
 Risk Address: 161 Arlington Road,
 Camden,
 London,
 NW1 7ET

Managing Director: Martin Rush MSc FGS
 Finance Director: Louise Banks BSc (Hons)
 Laboratory Manager: Jade McLellan
 Senior Geologist: Thomas Lee BSc (Hons)
 Assistant Geologist: Sarah Brand
 Geotechnical Assistant: Bradley Webb



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Appendix No: 1
 FSI Ref: 27798

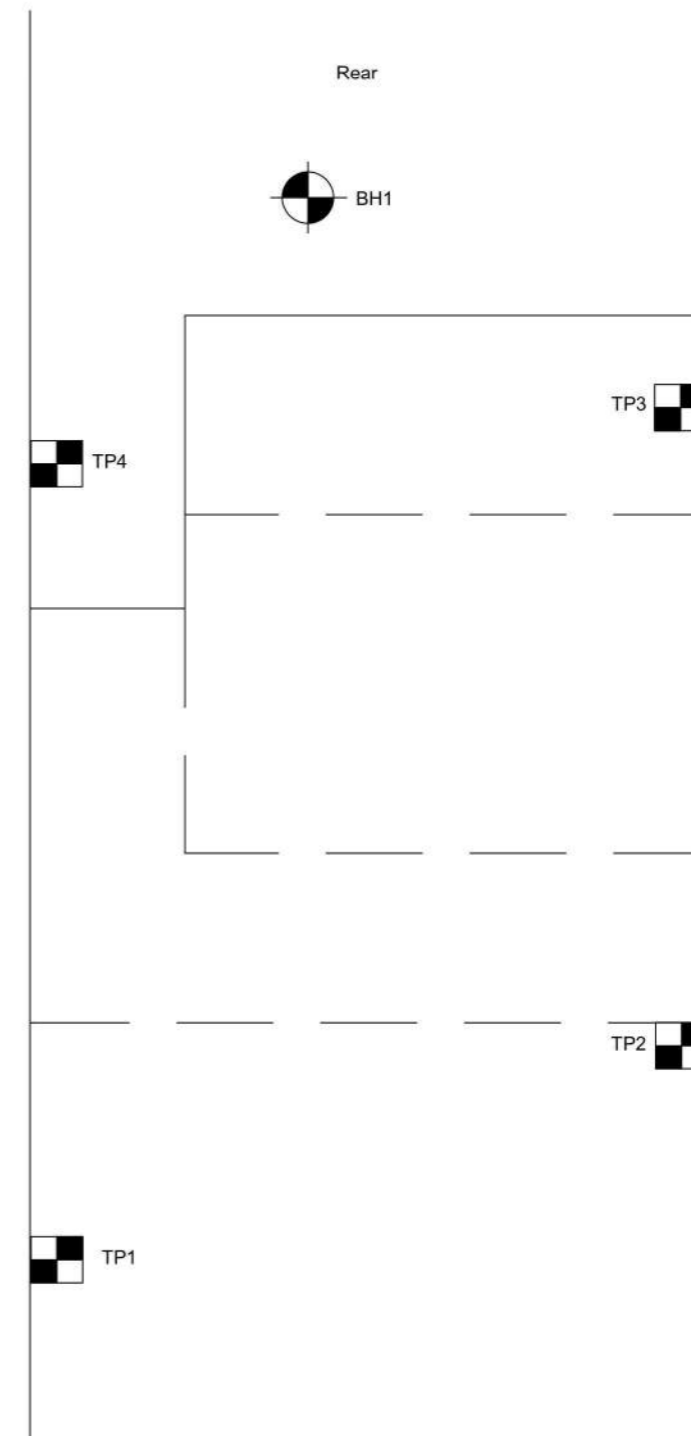
SITE PLAN

Property Address: 161 Arlington Road, Camden, London, NW1 7ET

Client Claim Ref: N/A

Survey date: 12/02/2024

Operative: SE1



Scale: NTS	Drawn by: TL	Key:	Trial Pit	Manholes	Rain Water Pipe	Surface Water Gully	Soil & Vent Pipe	Foul Water Gully	Shrub	Tree (Conifer)	Tree (Deciduous)
----------------------	------------------------	-------------	-----------	----------	-----------------	---------------------	------------------	------------------	-------	----------------	------------------

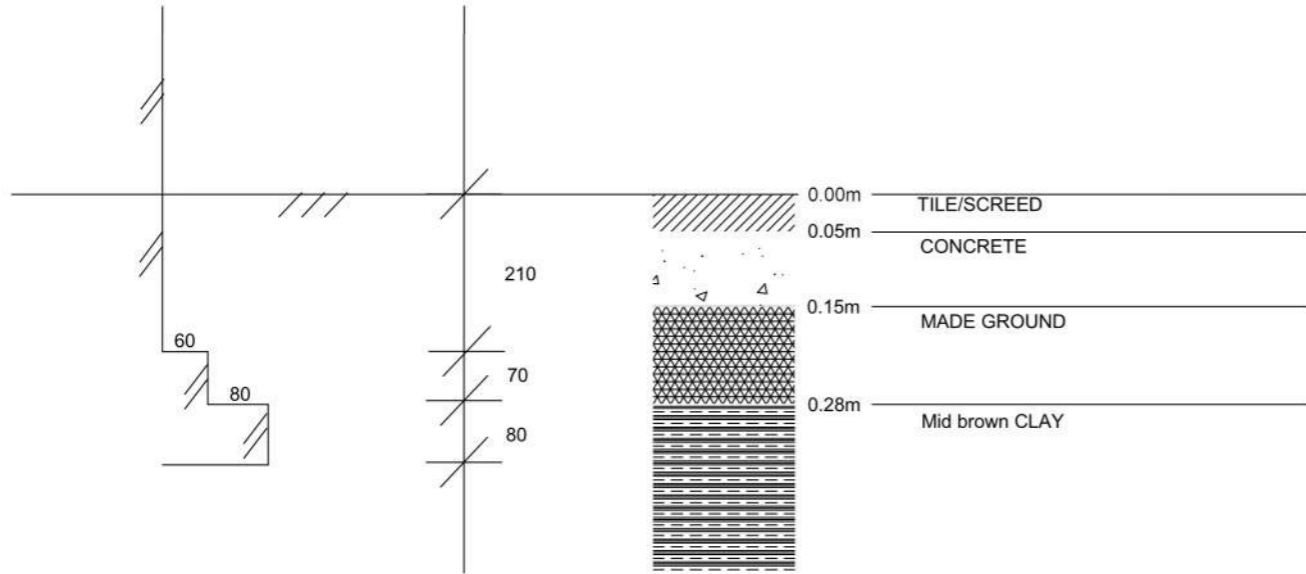
TRIAL PIT 1

Property Address: 161 Arlington Road, Camden, London, NW1 7ET

Client Claim Ref: N/A

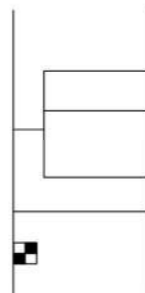
Survey date:12/02/2024

Operative: SE1



D1 @ F.L. (0.42m)
 Founding strata: Mid brown CLAY

Trial Pit Location:



Drawn by:

TL

Scale:

1:10

D= small disturbed sample, B= large bulk sample, U= undisturbed sample,
 MP= mackintosh probe blow counts, V= shear vane reading (kPa)

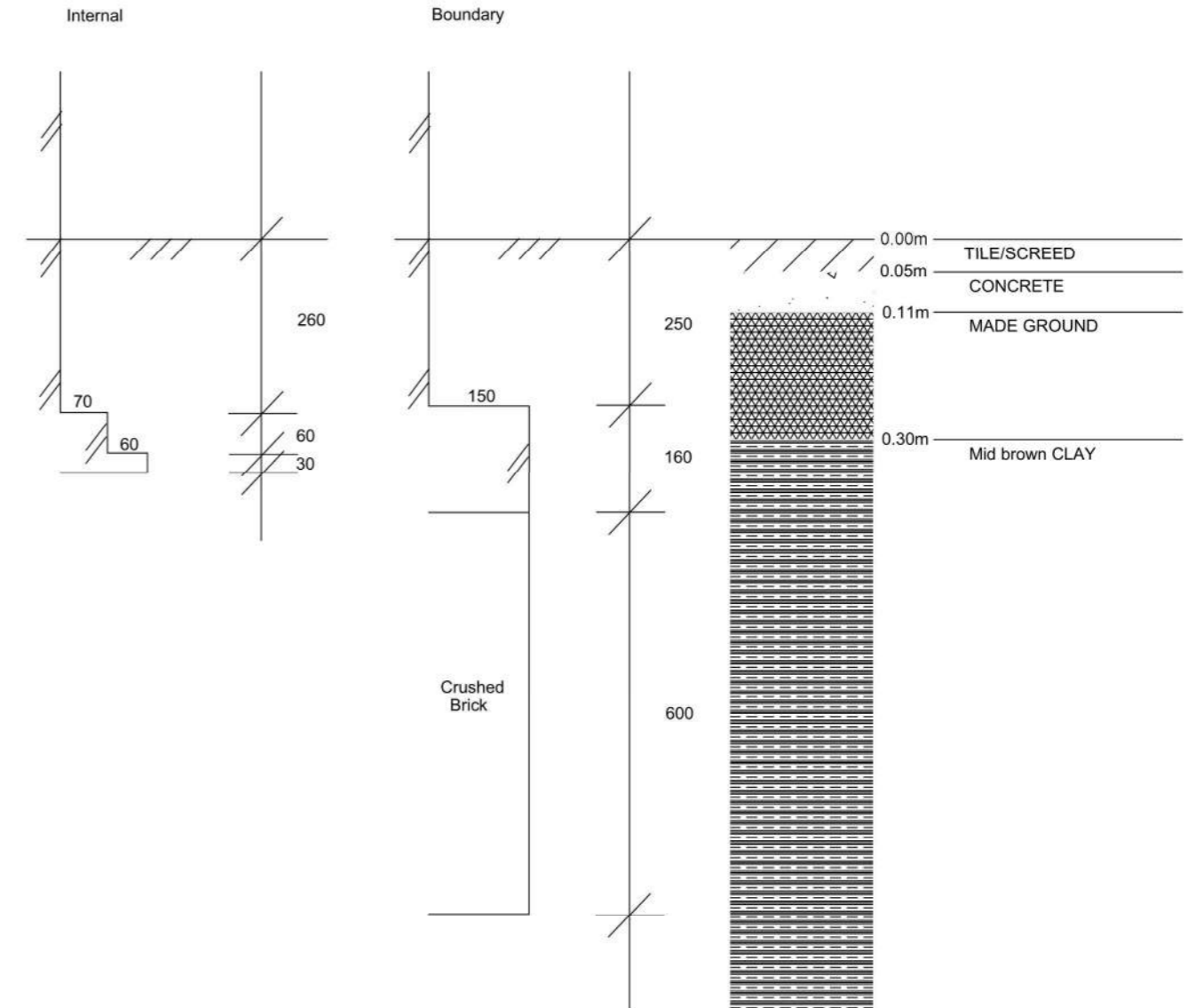
TRIAL PIT 2

Property Address: 161 Arlington Road, Camden, London, NW1 7ET

Client Claim Ref: N/A

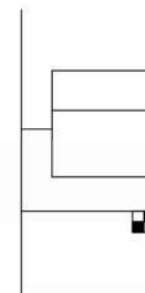
Survey date:12/02/2024

Operative: SE1



D1 @ F.L. (1.01m)
 Founding strata: Mid brown CLAY

Trial Pit Location:



Drawn by:

TL

Scale:

1:10

D= small disturbed sample, B= large bulk sample, U= undisturbed sample,
 MP= mackintosh probe blow counts, V= shear vane reading (kPa)

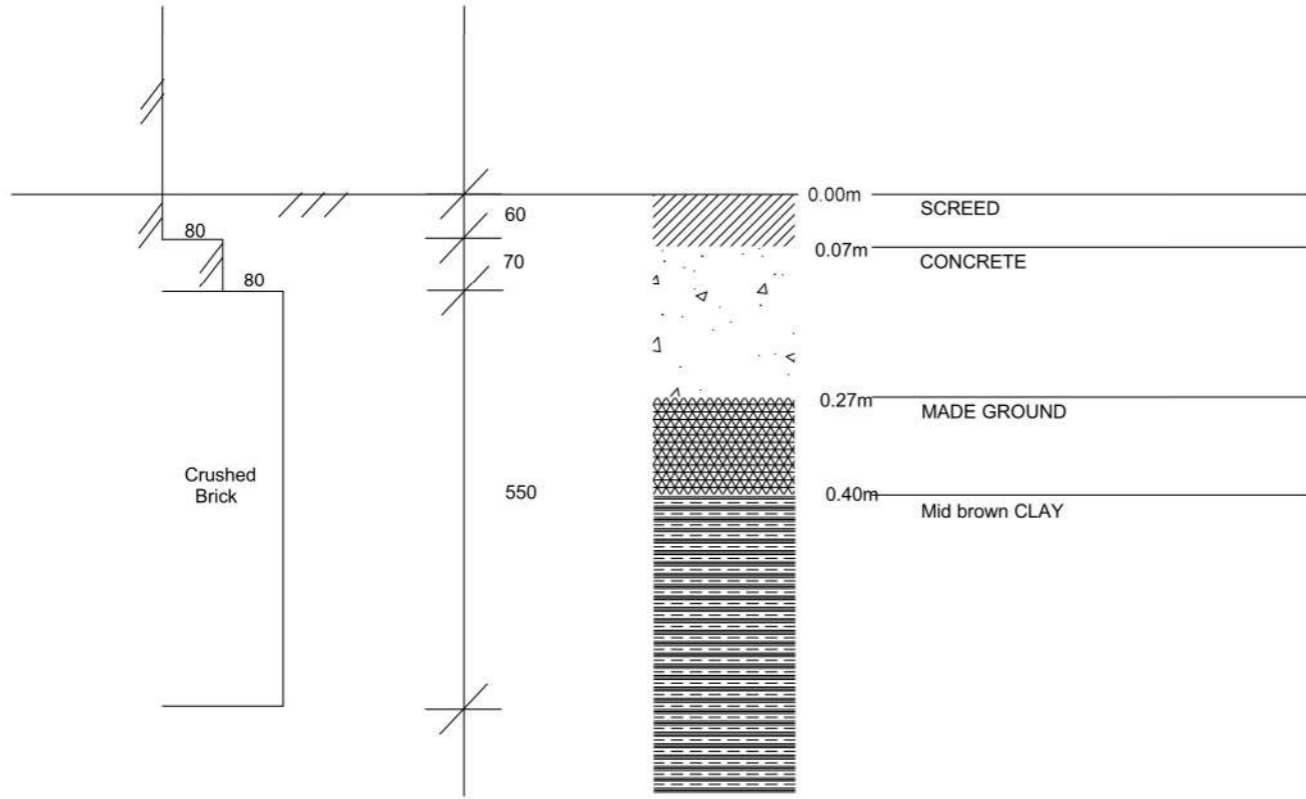
TRIAL PIT 3

Property Address: 161 Arlington Road, Camden, London, NW1 7ET

Client Claim Ref: N/A

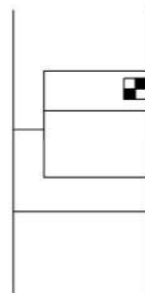
Survey date:12/02/2024

Operative: SE1



D1 @ F.L. (0.68m)
 Founding strata: Mid brown CLAY

Trial Pit Location:



Drawn by:

TL

Scale:

1:10

D= small disturbed sample, B= large bulk sample, U= undisturbed sample,
 MP= mackintosh probe blow counts, V= shear vane reading (kPa)

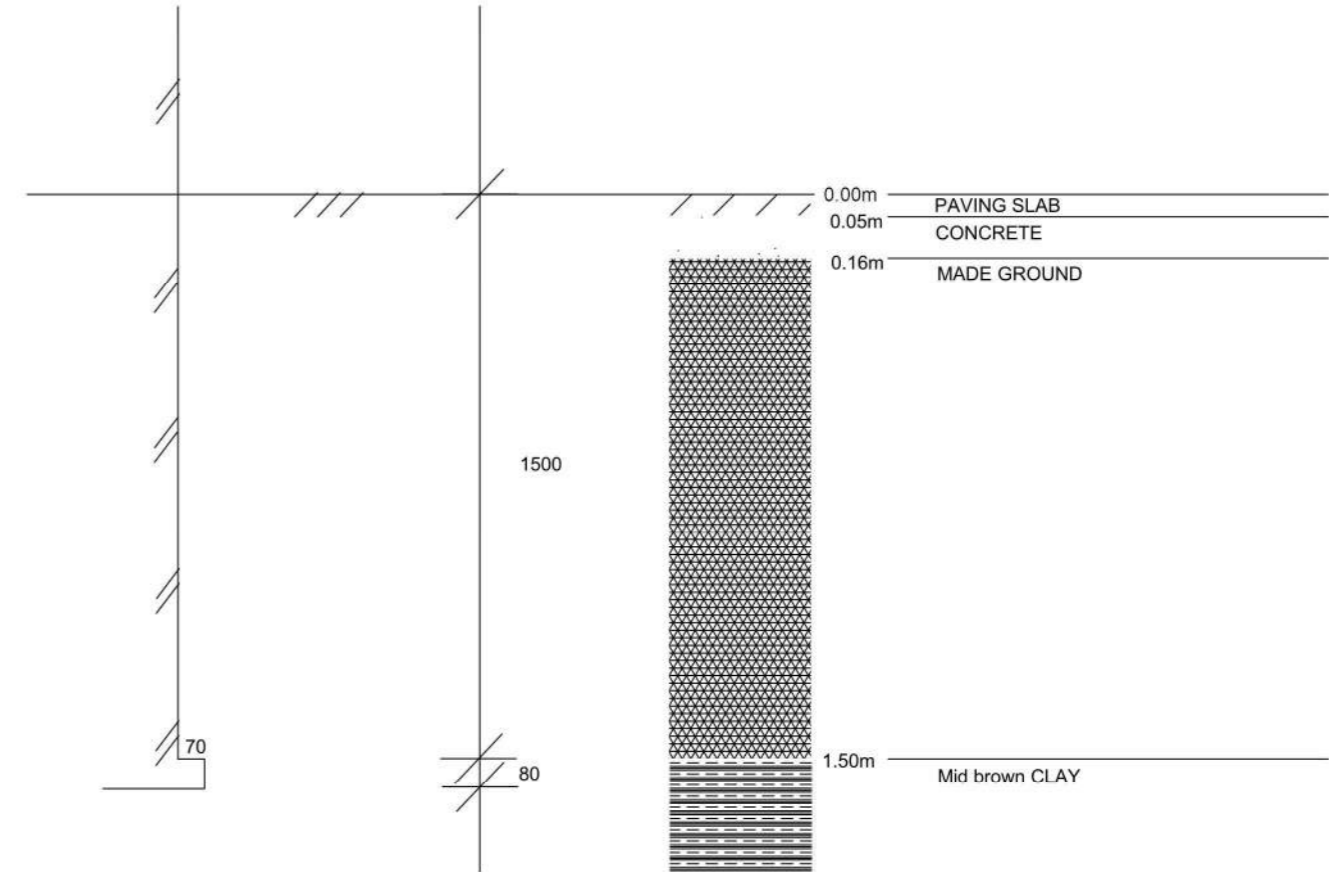
TRIAL PIT 4

Property Address: 161 Arlington Road, Camden, London, NW1 7ET

Client Claim Ref: N/A

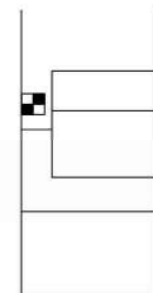
Survey date:12/02/2024

Operative: SE1



D1 @ F.L. (1.58m)
 Founding strata: Mid brown CLAY

Trial Pit Location:



Drawn by:

TL

Scale:

1:20

D= small disturbed sample, B= large bulk sample, U= undisturbed sample,
 MP= mackintosh probe blow counts, V= shear vane reading (kPa)

		Fastrack Site Investigations Ltd Unit 9, Tyndales Farm Southend Road Maldon CM9 6TQ		<h1>Borehole Log</h1>		Borehole No. BH1	
Project Name: 161 Arlington Road		Project No. 27798		Site Date:		Sheet 1 of 1	
Location: 161 Arlington Road, Camden, London, NW1 7ET						Hole Type BH	
Client: Fourwalls London Construction Ltd						Scale 1:27	
						Logged By SE1	
Water Strikes	Sample and In Situ Testing			Depth (m)	Legend	Stratum Description	
	Depth (m)	Type	Results				
				0.12		TOPSOIL	
				0.45		MADE GROUND	
	0.50	D	V (kPa) = 38 V (kPa) = 38	0.45		Mid brown CLAY	
	1.00	D	V (kPa) = 60 V (kPa) = 62				1
	1.50	D	V (kPa) = 76 V (kPa) = 80				
	2.00	D	V (kPa) = 100 V (kPa) = 104	2.20		Mid brown sandy CLAY	2
	2.50	D	V (kPa) = 124 V (kPa) = 130				
	3.00	D	V (kPa) = 138 V (kPa) = 140				3
	3.50	D	V (kPa) = 140				
	4.00	D	V (kPa) = 140				4
	4.50	D	V (kPa) = 140				
	5.00	D	V (kPa) = 140	5.00		4.90m - Standing water	5
						End of Borehole at 5.000m	
Key: D - Disturbed Sample V - Insitu Vane Test MP - Mackintosh Probe Test							
Remarks: Borehole closed at 5.00m upon completion. No roots observed.							

	Tel: 01245 223033	Appendix No: 3
	Fax: 0844 3358907	FSI Ref: 27798
	Email: enquiries@fastrackgroup.co.uk	
	Web: www.fastracksiteinvestigations.co.uk	
197 High Street, Maldon, Essex, CM9 5BU		
LABORATORY RESULTS		
Property Address:	161 Arlington Road, Camden, London, NW1 7ET	

SAMPLE DETAILS		ANALYSIS REQUESTED	
Investigation date:	12/02/2024	Moisture Content	<input checked="" type="checkbox"/> PSD <input checked="" type="checkbox"/>
Sample details:	Bags as received	Liquid Limit	<input checked="" type="checkbox"/> Soil Suction <input type="checkbox"/>
Samples received:	13/02/2024	Plastic Limit	<input checked="" type="checkbox"/> Shear Strength <input type="checkbox"/>
Schedule received:	13/02/2024	Plasticity Index	<input checked="" type="checkbox"/> Contamination <input type="checkbox"/>
Samples tested:	14/02/2024-19/02/2024	Root ID	<input type="checkbox"/> Root/Tree DNA <input type="checkbox"/>
Results reported:	19/02/2024	No roots found	

TEST DETAILS

General

Sample descriptions were written in accordance with BS 5930:1999.

Samples were prepared in accordance with BS 1377: Part 1: 1990, section 7

Samples from this contract will be retained for 1 calendar month following the issue of this report unless otherwise notified

Written approval is required from Fastrack Site Investigations Limited to reproduce report in full. The results shown within this report only relate to the samples tested

Moisture Content

Samples were tested in accordance with BS 1377: Part 2: 1990, section 3.2 (Oven drying method)

In accordance with Note 1 to paragraph 3.2.4 of BS 1377 Part 2 1990; these moisture contents have been corrected to give the equivalent moisture content of the fraction passing the 425µm sieve, to enable comparison with the liquid & plastic limits. (If condition of test is 'natural' the retained percentage is an estimated value, if condition is 'washed' the percentage is a measured value).

Samples are dried at 105-110°C unless otherwise stated.

Atterberg Limits

Samples were tested in accordance with BS 1377: Part 2: 1990, section 4.3 (4 drop LL), 4.4 (1 drop LL), 5.3 (PL) and 5.4 (PI) Test results on samples with a sand content, may show less accurate results. If condition of test is 'washed' results relate to the fraction passing the 425µm sieve only.

* Driscoll's rules deem the soil to be desiccated where the moisture content is less than the value calculated using driscoll's rule 1 and/or 2

Particle Size Distribution

Samples were tested in accordance with BS 1377: Part 2: 1990 section 9.2 (Wet sieving method)

Undrained Shear Strength

Samples were prepared in accordance with BS 1377: Part 7: 1990 section 8.3 and testing in accordance with BS 1377: Part 7: 1990: section 8.4 (undrained shear strength in triaxial compression without measurement of pore pressure (UU))

Soil Suction

Samples were prepared and tested based on the BRE digest No:IP4/93 (Corrected). 'A method of determining the state of desiccation in clay soils.' (Filter paper method).

Test results on samples with a sand or silt content, may show less accurate results. Deviation to standard procedure - Polythene bags are not used from weighing filter papers.

LABORATORY RESULTS

Property Address: 161 Arlington Road, Camden, London, NW1 7ET
Client Claim Ref: 0

BOREHOLE 1

Depth (m)	MC (%)	Corr. MC (%)	LL (%)	PL (%)	PI (%)	Class	% Retained (425µm)	Soil Suction (kPa)	Condition of test	Soil Description
0.50	37.5	37.5					0		Natural	Brown silty CLAY
1.00	35	37.12	63	27	36	CH	5.72		Natural	Brown silty CLAY containing grey and orange mottle and gravel
2.00	28.4	28.4					0		Natural	Brown silty CLAY containing grey and orange mottle
3.00	31.4	31.4	75	30	45	CV	0		Natural	Brown silty CLAY containing grey mottle
4.00	30.9	30.9					0		Natural	Brown silty CLAY containing grey mottle
5.00	30.8	30.8	74	28	46	CV	0		Natural	Brown silty CLAY containing grey mottle and gypsum



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Certificate of Analysis

THE ENVIRONMENTAL LABORATORY LTD

Analytical Report Number: 24-52393

Issue: 1

Date of Issue: 21/02/2024

Contact: Martin Rush

Customer Details: Fastrack Site Investigations Ltd
197-199 High Street
Maldon
Essex CM9 5BU

Quotation No: Q24-04367

Order No: 5000/27798

Customer Reference: 27798

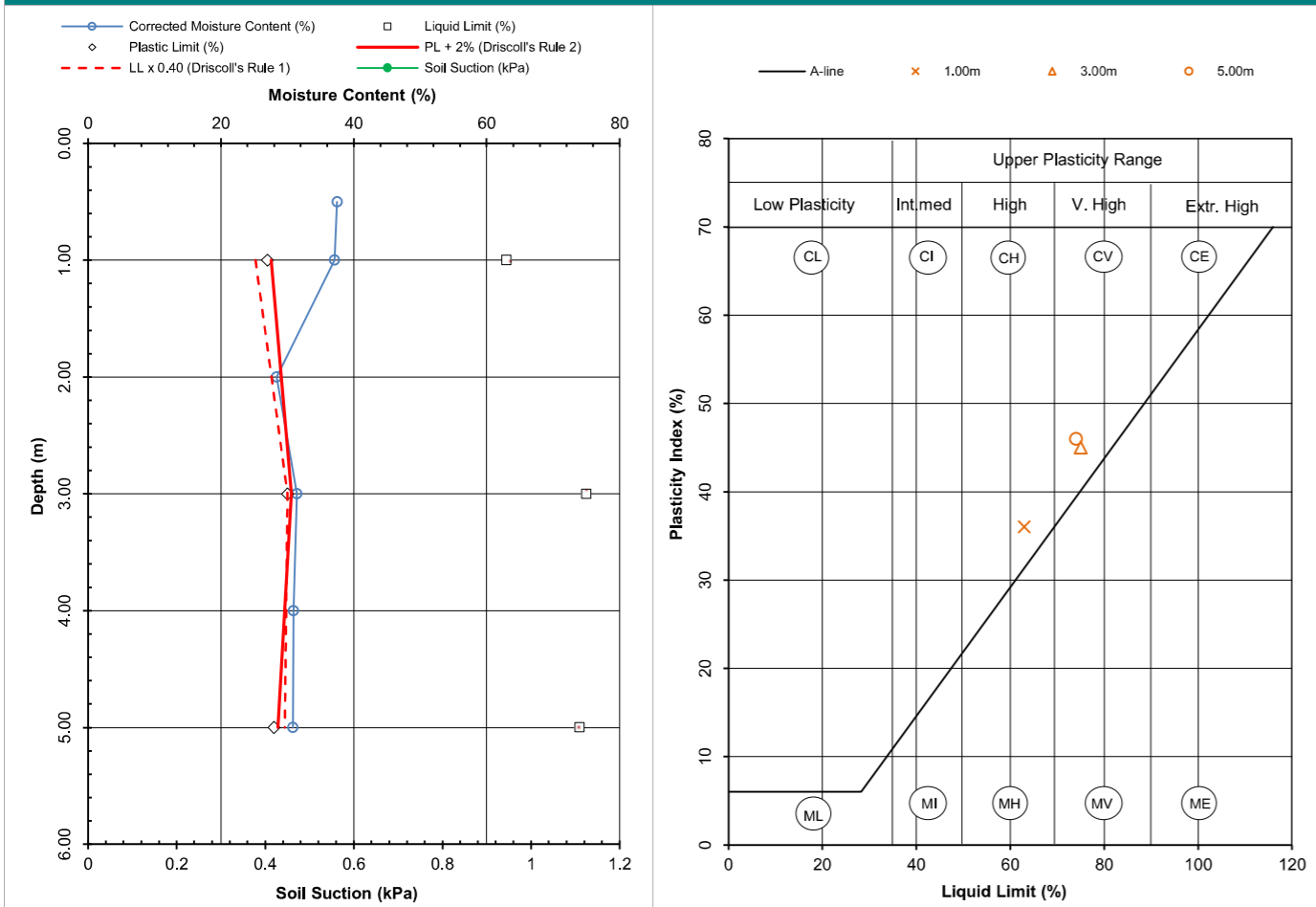
Date Received: 16/02/2024

Date Approved: 21/02/2024

Details: 161 Arlington Road, Camden, London, WW1 7ET

Approved by:

Tim Reeve, Technical Coordinator



Comments: Samples dried in 75° due to the presence of gypsum

Reported by: Issy Acerbis

Checked by: Jade McLellan

Sample Summary

Report No.: 24-52393, issue number 1

Elab No.	Client's Ref.	Date Sampled	Date Scheduled	Description	Deviations
353075	BH1 D2 1.00	12/02/2024	16/02/2024	Silty clayey loam	
353076	BH1 D4 2.50	12/02/2024	16/02/2024	Silty clayey loam	



Results Summary

Report No.: 24-52393, issue number 1

ELAB Reference	353075	353076
Customer Reference	D2	D4
Sample ID		
Sample Type	SOIL	SOIL
Sample Location	BH1	BH1
Sample Depth (m)	1.00	2.50
Sampling Date	12/02/2024	12/02/2024

Determinand	Codes	Units	LOD		
Soil sample preparation parameters					
Moisture Content	N	%	0.1	25.1	20.5
Material removed	N	%	0.1	< 0.1	< 0.1
Description of Inert material removed	N		0	None	None
Anions					
Water Soluble Sulphate	M	g/l	0.02	0.04	2.01
Miscellaneous					
pH	M	pH units	0.1	9.8	8.9

Tests marked N are not UKAS accredited.
The Environmental Laboratory Ltd, Reg. No. 3882193

Method Summary

Report No.: 24-52393, issue number 1

Parameter	Codes	Analysis Undertaken On	Date Tested	Method Number	Technique
Soil					
pH	M	Air dried sample	19/02/2024	113	Electromeric
Water soluble anions	M	Air dried sample	19/02/2024	172	Ion Chromatography

Report Information

Report No.: 24-52393, issue number 1

Key

U	hold UKAS accreditation
M	hold MCERTS and UKAS accreditation
N	do not currently hold UKAS accreditation
^	MCERTS accreditation not applicable for sample matrix
*	UKAS accreditation not applicable for sample matrix
S	Subcontracted to approved laboratory UKAS Accredited for the test
SM	Subcontracted to approved laboratory MCERTS/UKAS Accredited for the test
NS	Subcontracted to approved laboratory. UKAS accreditation is not applicable.
I/S	Insufficient Sample
U/S	Unsuitable sample
n/t	Not tested
<	means "less than"
>	means "greater than"
LOD	LOD refers to limit of detection, except in the case of pH soils and pH waters where it means limit of discrimination. Soil sample results are expressed on an air dried basis (dried at < 30°C), and are uncorrected for inert material removed. ELAB are unable to provide an interpretation or opinion on the content of this report. The results relate only to the sample received. PCB congener results may include any coeluting PCBs Uncertainty of measurement for the determinands tested are available upon request Unless otherwise stated, sample information has been provided by the client. This may affect the validity of the results.

Deviation Codes

a	No date of sampling supplied
b	No time of sampling supplied (Waters Only)
c	Sample not received in appropriate containers
d	Sample not received in cooled condition
e	The container has been incorrectly filled
f	Sample age exceeds stability time (sampling to receipt)
g	Sample age exceeds stability time (sampling to analysis)

Where a sample has a deviation code, the applicable test result may be invalid.

Sample Retention and Disposal

All soil samples will be retained for a period of one month
All water samples will be retained for 7 days following the date of the test report
Charges may apply to extended sample storage

TPH Classification - HWOL Acronym System

HS	Headspace analysis
EH	Extractable Hydrocarbons - i.e. everything extracted by the solvent
CU	Clean-up - e.g. by florisil, silica gel
1D	GC - Single coil gas chromatography
Total	Aliphatics & Aromatics
AL	Aliphatics only
AR	Aromatics only
2D	GC-GC - Double coil gas chromatography
#1	EH_Total but with humics mathematically subtracted
#2	EH_Total but with fatty acids mathematically subtracted
_	Operator - underscore to separate acronyms (exception for +)
+	Operator to indicate cumulative e.g. EH+HS_Total or EH_CU+HS_Total
MS	Mass Spectrometry

End of Report

