JOB TITLE:	JOB NUMBER / FILE:	CALCULATION NUMBER:		Form	
68 Elsworthy Road NW3 3BP	233950	001			
CALCULATION:	CALCULATION BY:	DATE:	CHECKED BY:		
Preliminary calculations -350mm garden front slab	Rob M	Jan. 24			

CALCULATIO	NS:									
REF	Design check area.	on 350	mm slab	over ba	sement to	o front gar	den			
	Slab will be d 19kN/M³	esigned	to supp	ort minim	านm 1.0m	n of soil @				
	Finishes allov	vance o	f 2.5kN/I	M <sup>2</sup>			_			
	Imposed allow	vance o	f 5.0kN/	M <sup>2.</sup>			_			-
	RC SLAB DESIGN In accordance with EN1	992-1-1:2004	SSL: 46.600 TBC	corrigendum Jac	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	the UK national and Tedds calcu	nnex liation version 1.0.22			
	Design summary Description	Unit	Provided	Required	Utilisation	Result	_			
	Short span Reinf, at midspan	mm²/m	1340	1134	0.846	PASS	_			
	Bar spacing at midspan	mm	150	209	0.716	PASS				
	Shear at discont. supp Deflection ratio	kN/m	160.2 20.36	116.3 36.61	0.726	PASS				
	Long span		1				_			
	<ul> <li>Reinf. at midspan</li> <li>Bar spacing at midspan</li> </ul>	mm²/m mm	1340 150	617 300	0.460	PASS				
	Shear at discont. supp	kN/m	156.5	116.3	0.743	PASS	-			_
	Cover Min cover bottom	mm	35	21	0.600	PASS	_			_
		11111	35	21	0.000	FA33	_			
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JOB TITLE:	JOB NUMBER / FILE:	CALCULATION NUMBER:	Form	
68 Elsworthy Road NW3 3BP	233950	002		
CALCULATION:	CALCULATION BY:	DATE:	CHECKED BY:	
Preliminary calculations -350mm garden front slab	Rob M	Jan. 24		

<b>A</b> .	TIONS:			
	Slab definition			
	Slab reference name	garden slab		
	Type of slab	Two way unrestrained edges	Overall slab depth	h = <b>350</b> mm
	Shorter effective span of panel	l <sub>x</sub> = <b>6250</b> mm	Longer effective span of panel	l <sub>y</sub> = <b>8750</b> mm
	Support conditions	Four edges simply supported	I	—
			Bottom outer layer of reinft	Short span direction
	Loading			
	Charac permanent action	$G_k = 22.0 \text{ kN/m}^2$	Charac variable action	$Q_k = 5.0 \text{ kN/m}^2$
	Partial factor for perm action	$v_{c} = 1.35$	Partial factor for var action	$v_0 = 1.50$
	Quasi-perm value of var action		$w_2 = 0.30$	
			φ2 ••••	
	Concrete properties			
	Concrete strength class	C32/40	Partial factor	γc = <b>1.50</b>
	Compressive strength factor	α <sub>cc</sub> = <b>0.85</b>	Maximum aggregate size	d <sub>g</sub> = <b>20</b> mm
	Reinforcement properties			
	Characteristic yield strength	f <sub>yk</sub> = <b>500</b> N/mm <sup>2</sup>	Partial factor	γs = <b>1.15</b>
	Concrete cover to reinforcem	ant		
	Nom cover to htm roinft	a = 35  mm	Fire resistance to htm of slab	$\mathbf{P}_{i} = 60$ min
	Reinforcement fabrication	$C_{nom_b} = 33$ mm	Min read nom cover htm reinft	$C_{\text{num}} = 30 \text{ mm}$
	Remorcement labitcation		S - There is sufficient cover to	the bottom reinforcement
	<b>1</b>		5 - There is Sumclent Cover to	
	Slab definition			—
	Slab reference name	garden slab		
	Type of slab	Two way unrestrained edges	Overall slab depth	h = <b>350</b> mm
	Shorter effective span of panel	l <sub>x</sub> = <b>6250</b> mm	Longer effective span of panel	l <sub>v</sub> = <b>8750</b> mm
	Support conditions	Four edges simply supported	g	
		· · · · · · · · · · · · · · · · · · ·	Bottom outer layer of reinft	Short span direction
	Looding		2	• –
	Charge permanent action	$C_{1} = 22.0 \text{ kN/m}^{2}$	Charge veriable action	$O_{1} = 5.0  k N l/m^{2}$
	Dential factor for normal action	$G_k = 22.0 \text{ km/m}^2$	Charac variable action	Qk = 5.0 KN/III-
		γG – 1.35		γο – 1.50
	Quasi-perm. value of var.action	1	$\psi_2 = 0.30$	
	Concrete properties			
	Concrete strength class	C32/40	Partial factor	γc = <b>1.50</b>
	Compressive strength factor	α <sub>cc</sub> = <b>0.85</b>	Maximum aggregate size	d <sub>g</sub> = <b>20</b> mm
	Poinforcomont proportios			_
	Characteristic viold strength	$f = \mathbf{E} \mathbf{O} \mathbf{O} \mathbf{N} / \mathbf{m} \mathbf{m}^2$	Dortial factor	
		lyk – <b>300</b> N/IIIII		γs – 1.15
	Concrete cover to reinforcem	ient		
	Nom cover to btm reinft	c <sub>nom_b</sub> = <b>35</b> mm	Fire resistance to btm of slab	R <sub>btm</sub> = <b>60</b> min
	Reinforcement fabrication	Subject to QA system	Min reqd nom cover btm reinft	C <sub>nom_b_min</sub> = <b>21.0</b> mm
		PAS	S - There is sufficient cover to	o the bottom reinforcement
1	Reinforcement design at mid	span in short span direction		—
	Design bending moment	M <sub>x_p</sub> = <b>143.9</b> kNm/m		—
	Reinforcement provided	16 mm dia. bars at 150 mm c	entres (1340 mm²/m)	—
			K < K' - Compression re	inforcement is not required
	Area of reinft reqd for bending	A <sub>sx_p_m</sub> = <b>1134</b> mm <sup>2</sup> /m	Minimum area required	A <sub>sx_p_min</sub> = <b>483</b> mm <sup>2</sup> /m
		PASS - Ar	ea of tension reinforcement p	rovided is adequate (0.846)
-	Check reinforcement spacing			—
ł	Max allowable spacing	s <sub>max x n</sub> = <b>209</b> mm	Actual bar spacing	s <sub>x n</sub> = <b>150</b> mm
			PASS - Reinforcement sr	$a_{A_{P}}$ $a_{A$
				······································

JOB TITLE:			JOB NUMBER / FILE:	CALCULATION NUMBER:		Form
68 Elsworthy Road NW	3 3BP		233950	003		
CALCULATION:			CALCULATION BY:	DATE:	CHECKED BY:	
Preliminary calculations	-350mr	m garden front slab	Rob M	Jan. 24		
CALCULATIONS:						
REF					OUTPUT	
Shear check at short spa	n discont	tinuous support				_
Shear force	$V_{x\_d}$	= <b>116.3</b> kN/m	Shear resistanc	e \	$/_{Rd,c_x_d} = 160.2$	2 kN/m
			P	PASS - Shear cap	pacity is adeq	uate (0.726)
Shear check at long spar	n disconti	inuous support				
Shear force	$V_{y\_d}$	= <b>116.3</b> kN/m	Shear resistanc		/ <sub>Rd,c_y_d</sub> = 156.	5 kN/m
			P	ASS - Snear cap	bacity is adeq	uate (0.743)
Basic span-to-depth def	ection rat	tio check				
Limit span-to-depth ratio	ratio	D <sub>lim_x</sub> = <b>36.61</b>	Actual span-to-	depth ratio	ratio <sub>act_x</sub> = <b>20.3</b>	6
		PASS	- Actual span-to-	effective depth i	ratio is accept	table (0.556)
Reinforcement summary						
Midspan in short span dire	ction	16 mm d	ia. bars at 150 m	m centres B1		
Midspan in long span dire	ction	16 mm d	ia. bars at 150 m	m centres B2		
Discontinuous support in s	short span	direction 16 mm di	ia. bars at 150 m	m centres B1		
	ong span		ia. Dais at 150 m	in centres b2		
Reinforcement sketch		h. Nata that additional vai				
$\begin{array}{c} \text{The following sketch is ind} \\ 0.212, 0.214 \text{ and } 0.214 \end{array}$	5 of EN 10	$392-1-1\cdot2004$ to meet deta	niorcement may t viling rules	be required in acc	cordance with d	lauses
5.2.1.2, 5.2.1. <del>4</del> and 5.2.1.		552-1-1.2004 to meet deta	lining rules.			
			16mm bars @	0 150 ctrs B1		
		×	——— 16mm bars @	150 ctrs B1		
			$\overline{\neg}$			
		/	——— 16mm bars @	) 150 ctrs B1		
	, B2 -	B2 -				
	0 ctrs	0 ctrs ) ctrs				
	<u> </u> 315	8 15 9 15	2			
	ars (	ars (				
	q mu		2			
	16n	16n 16m				
FORM Structural Design Ltd.						

JOB TITLE:	JOB NUMBER / FILE:	CALCULATION NUMBER:		Form
68 Elsworthy Road NW3 3BP	233950	004		
CALCULATION: Preliminary calculations - 350mm rear	CALCULATION BY:	DATE:	CHECKED BY:	
slab at ground floor	Rob M	Jan. 24		



JOB TITLE:	JOB NUMBER / FILE:	JOB NUMBER / FILE: CALCULATION NUMBER:		Form
68 Elsworthy Road NW3 3BP	233950	005		1 Unit
CALCULATION: Preliminary calculations - 350mm rear	CALCULATION BY:	DATE:	CHECKED BY:	
slab at ground floor	Rob M	Jan. 24		



JOB TITLE:		JOB NUME	ER / FILE:	CALCULATION NUMBER:	Form
68 E	Isworthy Road NW3 3BP	2	33950	006	
CALCULATION	* Proliminany colculations 250mm ro	CALCULA	TION BY:	DATE: CHECKED BY:	-
	slab at ground floor	R	ob M	Jan. 24	
CALCU	ILATIONS:				
REF				OUTPUT	
	KN 153.2 116.1	Shear Force Envelope		109.1	
	00-	74.0		78.3	
	-180.136	6750		-180.1	
		1		B 2 C	
	Support conditions				
	Support A	Vertically restrair	ed		
		Rotationally free			
	Support B	Vertically restrain	ed		
	Support C	Rotationally free			
	Support	Rotationally free			
	Applied loading	, <b>,</b>			
	Applica loading	Dead self weight	of beam $ imes$ 1		
	finisihes	Dead full UDL 2.	5 kN/m		
	imposed	Imposed full UDL	. 1.5 kN/m		
	PL cavity wall	Dead point load	13 kN at 3400	) mm	
	PL col 1 gk	Imposed point load	i0 kN at 3400 ad 40 kN at 3	400 mm	
	PL col 2 gk	Dead point load	14.1 kN at 77	00 mm	
	PL 2 col 2 qk	Imposed point lo	ad 12 kN at 7	700 mm	
	PL3 cav wall	Dead point load 2	21 kN at 7700	) mm	
		Dead partial UDL	. 10.5 kN/m fi 10.5 kN/m fi	rom 2100 mm to 3400 mm	
	PARTIAL CAV WALL	Dead partial UDL	. 10.5 kN/m fi	om 6750 mm to 7900 mm	
	Load combinations	·			
	Load combination 1	Support A		Dead  imes 1.40	
				Imposed $ imes$ 1.60	
	-	Span 1		$\text{Dead}\times 1.40$	
				Imposed $\times$ 1.60	
		Support B		$Dead \times 1.40$	
	-	Spop 2		Imposed $\times$ 1.60	
	-	opan z		Imposed v 1.60	
	-	Support C		Dead $\times 1.40$	
				Imposed × 1.60	
	Analysis results				
	Maximum moment support A	M <sub>A_max</sub> = <b>0</b> kNm		M <sub>A_red</sub> = <b>0</b> kNm	
	Maximum moment span 1 at 3400 mm	M <sub>s1_max</sub> = <b>406</b> kN	n	M <sub>s1_red</sub> = <b>406</b> kNm	
	Maximum moment support B	M <sub>B_max</sub> = -91 kNm	l	M <sub>B_red</sub> = -91 kNm	
	Maximum moment span 2 at support Maximum moment support C	$VI_{s2_{max}} = \mathbf{U} KNM$ M <sub>C max</sub> = <b>0</b> kNm		$VIs2_{red} = 0 \text{ kNm}$ M <sub>C red</sub> = <b>0</b> kNm	
			+ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$		
			+ $+$ $+$ $+$		
			+		++++



	JOB NUMBER / FILE:	CALCULATION NUMBER:		For
Elsworthy Road NW3 3BP	233950	008		
<sup>™</sup> Proliminany colculations 250mm ro	CALCULATION BY:	DATE:	CHECKED BY:	
slab at ground floor	Rob M	Jan. 24		
ULATIONS:			OUTPUT	
PASS - A	Area of shear reinforcemen	t provided exceeds	minimum require	d
Max longitudinal spacing s <sub>vl,max</sub> = <b>221</b> mm			inininani require	
PASS - Longitudina	l spacing of shear reinforc	ement provided is le	ess than maximur	n
Mid span 1				
		x 16+ bars		
320-	2	x $10_{\varphi}$ shear legs at 150	c/c	
	8	x $25_{\phi}$ bars		
◀────1000──	►			
Design moment resistance of rectangular section (	(cl. 3.4.4)	d = 200	mm	+++-
K = 0.119		-ππ. α = <b>292</b> K' = <b>0</b> .1!	56	+
	K' > K - No c	ompression reinford	cement is require	d
Lever arm z = <b>247</b> mm	Depth of neutral as	xis x = <b>102</b>	mm	
Area of tension reinf req'd $A_{s,req} = 3784 \text{ mm}^2$	Tension reinf provi	ded $8 \times 25\phi$	bars	
Area of tension reinf prov $A_{s,prov} = 3927 \text{ mm}^2$ Maximum area of reinf $A_{s,max} = 14000 \text{ mm}^2$	Minimum area of r	einf $A_{s,min} = 2$	155 mm²	
PASS - Area of reinfo	orcement provided is great	er than area of reinfo	orcement require	d
Rectangular section in shear				
Shear reinforcement provided $2 \times 10\phi$ legs at 150 c/c	C			
Area of shear reinf provided $A_{sv,prov} = 1047 \text{ mm}^2/\text{m}^2$	Minimum area of s	hear reinf $A_{sv,min} =$	920 mm²/m	
PASS - A Max longitudinal spacing Sulmax = 219 mm	Area of shear reinforcemen	t provided exceeds i	minimum require	a
PASS - Longitudina	I spacing of shear reinforc	ement provided is le	ess than maximur	n
Spacing of reinforcement (cl 3.12.11)				
Actual dist between bars s = <b>106</b> mm	Min dist between b	ears s <sub>min</sub> = <b>25</b>	5 mm	+-+-+-
Design convice stress from 2 and a life 2	PASS - S	Satisfies the minimu	m spacing criteri	a
Design service stress $T_s = 321.2 \text{ N/mm}^2$	iviax distance betw <b>PASS - S</b>	een pars s <sub>max</sub> = 14 Satisfies the maximu	40 mm Im spacina criteri	a
Span to depth ratio (cl. 3.4.6)			,	
Span to depth ratio (T.3.9) span_to_depth <sub>basic</sub> = 2	26.0 Service stress in te	ension rein $f_s = 321$ .	. <b>2</b> N/mm <sup>2</sup>	+++-
Modification for tension reinf $f_{tens} = 0.780$	Modification for co	mp reinf f <sub>comp</sub> = <b>1</b>	.155	+++-
Modification for span > 10m $f_{iong} = 1.000$	Allowable span to	depth ratio span_to	_depth <sub>allow</sub> = <b>23.4</b>	
	PASS - Actual span to r	depth ratio is within	the allowable lim	it

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		JOB NOPIBER / FILE:	CALCOD THOMAS INC.		F
Isworthy Road NW3 3	3P	233950	009		
* Preliminary calculatic	ne - 350mm roor	CALCULATION BY:	DATE:	CHECKED BY:	
slab at ground floor	ns - 550mm real	Rob M	Jan. 24		
JLATIONS:					
				OUTPUT	
Support B					
- <u> </u>					
	• • • •	8 x 200	bars		
		040		-	
35		2 x 10q	silear legs at 150 G	C	
		• • 8 x 25	bars		
-	1000	<b>&gt;</b>			
_	1000	•			
Design moment resistance o	f rectangular section (cl. 3.4.4	4) Depth to togeth to the second for		100	
Design bending moment	IVI = 91 KINM K = 0.026	Deptn to tension reinf.	d = <b>295</b> m k' - 0 156	m	
_	K - 0.026	K' > K - No comp	ression reinforce	ment is required	
Lever arm	z = <b>280</b> mm	Depth of neutral axis	x = 33 mm	1 1	
Area of tension reinf req'd	A <sub>s,req</sub> <b>= 744</b> mm <sup>2</sup>	Tension reinf provided	$8 imes 20\phi$ ba	irs	
Area of tension reinf prov	A <sub>s,prov</sub> = 2513 mm <sup>2</sup>	Minimum area of reinf	A <sub>s,min</sub> = <b>45</b>	<b>5</b> mm²	
<ul> <li>Maximum area of reinf</li> </ul>	A <sub>s,max</sub> = <b>14000</b> mm <sup>2</sup>				
-	PASS - Area of reinforcement	nt provided is greater th	an area of reinfor	cement required	
Rectangular section in shear	,				
Shear - span 1 at 6455 mm	V = <b>175</b> kN	Shear stress	v = <b>0.593</b>	N/mm²	
<ul> <li>Allowable design shear stress</li> </ul>	v <sub>max</sub> = 5.000 N/mm <sup>2</sup>	CC Desim share street	- i- l 4h		
-	$\mathbf{PA}$	SS - Design snear stres	s is less than may	cimum allowable	
Design shear resistance regid	$V_{c} = 0.400 \text{ N/mm}^{2}$	Area of shear reinf reg	$A_{avrag} = 92$	<b>20</b> mm <sup>2</sup> /m	
Shear reinforcement provided	$2 \times 100$ legs at 150 c/c	Area of shear reinf, prov	$A_{\text{sv,req}} = \mathbf{J}\mathbf{I}$	047 mm²/m	
	PASS - Area of	shear reinforcement pro	vided exceeds m	inimum required	
Max longitudinal spacing	s <sub>vl,max</sub> = <b>221</b> mm				
	PASS - Longitudinal spacir	ng of shear reinforceme	nt provided is les	s than maximum	
Shear - span 2 at 295 mm	V = 100 kN	Shear stress	v = <b>0.337</b>	N/mm²	
Allowable design shear stress	v <sub>max</sub> = 5.000 N/mm <sup>2</sup>	CC Desim share street	- i- l 4h		
Value of v from Table 3.7	<b>ΡΑ</b>	ی - Design snear stres	s is less than may	unum allowable	
Design shear resistance regid	v <sub>s</sub> = <b>0.400</b> N/mm <sup>2</sup>	Area of shear reinf reg?		20 mm²/m	
Shear reinforcement provided	$2 \times 10\phi$ legs at 150 c/c	Area of shear reinf. prov	$v \qquad A_{sv,prov} = 1$	<b>047</b> mm²/m	++-
-	PASS - Area of	shear reinforcement pro	vided exceeds m	inimum required	
<ul> <li>Max longitudinal spacing</li> </ul>	s <sub>vl,max</sub> = <b>221</b> mm				++-
-	PASS - Longitudinal spacir	ng of shear reinforcemen	nt provided is less	s than maximum	+
Spacing of reinforcement (cl	3.12.11)				++-
<ul> <li>Actual dist between bars</li> </ul>	s = 111 mm	Min dist between bars	s <sub>min</sub> = <b>25</b> n	nm	+
-	$f = 0.07 \text{ N}/mm^2$	PASS - Satis	ties the minimum	spacing criteria	
- Design service stress	is – 30.1 IN/MM-	PASS - Satisf	uars s <sub>max</sub> = 300 fies the maximum	spacing criteria	
		, AGG - GallSI		-paoning criteria	
<ul> <li>Span to depth ratio (CI. 3.4.6)</li> <li>Span to depth ratio (T 3.0)</li> </ul>	span to depthenin - 70	Service stress in tensio	n rein f. = <b>08.7</b> N	l/mm <sup>2</sup>	
– Modification for tension reinf	f <sub>tens</sub> = 2.000	Modification for comp re	einf $f_{comp} = 1_{\cdot}3$	07	

JOB TITLE:			JOB NUMBER / FILE:	CALCULATION NUMBER:	Form
68 Els	sworthy Road NW3 3BP		233950	010	
CALCULATION:	Proliminany colculations	250mm roor	CALCULATION BY:	DATE: CHECKED BY:	-
	slab at ground floor	- SSUMM real	Rob M	Jan. 24	
CALCUL	ATIONS:				
REF				OUTPUT	
	Modification for span > 10m	f <sub>long</sub> = <b>1.000</b>	Allowable span	to depth ratio span_to_depth	n <sub>allow</sub> = 18.3
	Actual span to depth ratio	span_to_depth <sub>actual</sub> = <b>4.6</b>			
		P	ASS - Actual span	to depth ratio is within the all	owable limit
	Mid span 2				
		• • • •	• 1	8 x 16 $_{\phi}$ bars	
	0			0 x 10 Labor land at 150 a/a	
	36			2 x 100 shear legs at 150 c/c	
				8 x 20∳ bars	
	▼			·	
		1000			
		1000			
	Design moment resistance o	f rectangular section (cl. 3) $M = 56$ kNm	.4.4)	n roinf d <b>- 207</b> mm	
	Design bending moment	K = 0.016	Depth to tensio	K' = 0,156	
			K' > K - N	o compression reinforcemen	t is required
	Lever arm	z = <b>282</b> mm	Depth of neutra	l axis x = <b>33</b> mm	
	Area of tension reinf req'd	A <sub>s,req</sub> = <b>454</b> mm <sup>2</sup>	Tension reinf pr	ovided $8 \times 16\phi$ bars	
	Area of tension reinf prov	A <sub>s,prov</sub> = 1608 mm <sup>2</sup>	Minimum area o	of reinf A <sub>s,min</sub> = <b>455</b> mr	n²
	Maximum area of reinf	A <sub>s,max</sub> = <b>14000</b> mm <sup>2</sup>			
		PASS - Area of reinforcen	nent provided is gr	eater than area of reinforcem	ent required
	Rectangular section in shear				
	Snear reinforcement provided	$2 \times 10\phi$ legs at 150 c/c	Minimum area	= 0.00  m	m <sup>2</sup> /m
	Area of shear term provided	PASS - Area	of shear reinforcer	nent provided exceeds minim	um required
	Max longitudinal spacing	s <sub>vl,max</sub> = <b>223</b> mm		p	
		PASS - Longitudinal spa	cing of shear reinfo	prcement provided is less that	an maximum
	Spacing of reinforcement (cl	3.12.11)			
	Actual dist between bars	s = <b>116</b> mm	Min dist betwee	en bars s <sub>min</sub> = <b>25</b> mm	
			PASS	S - Satisfies the minimum spa	cing criteria
	Design service stress	f <sub>s</sub> = <b>94.2</b> N/mm <sup>2</sup>	Max distance b	etween bars s <sub>max</sub> = <b>300</b> mm	
			PA33	- Sausnes the maximum spa	
			+ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$		
			+ + + + + +		
			+ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$ $+$		
			+ + + + +		
FORM	Structural Design Ltd.				

JOB TITLE:	JOB NUMBER / FILE:	CALCULATION NUMBER:		Form
68 Elsworthy Road NW3 3BP	233950	011		
CALCULATION: Preliminary calculations - RC liner wall to	CALCULATION BY:	DATE:	CHECKED BY:	
deeper basement area, 300mm thick.	Rob M	Jan. 24		



FORM Structural Design Ltd.

	JOB TITLE:	JOB NUMBER / FILE:	CALCULATION NUMBER:		Form
	68 Elsworthy Road NW3 3BP	233950			
CAL	CALCULATION: Preliminary calculations - RC liner wall to deeper basement area, 300mm thick.	CALCULATION BY:	DATE:	CHECKED BY:	
		Rob M	Jan. 24		

