

Site Investigation Report



Job Information	
Client	[Redacted]
Client ref	[Redacted]
Visit date	31/10/2022
Report date	03/11/2022

Job Summary	
✓	CCTV survey undertaken. Read more.
!	Further Investigations required. Read more.
✓	3 trial holes undertaken. Read more.
✓	No drainage defects found. Read more.



Job Information

Overview

Brief

Auger were commissioned by Questgates to undertake a site investigation and CCTV inspection of the underground drainage within the area of concern (AOC) at the property.

Findings

Trial Hole Findings

TH1 was completed in the proposed location and reached the required depth, soil and root samples were taken. The footing was determined by probing to a depth below 1m, if deemed necessary we can return with two men to dig a larger hole and fully expose the footing.

TH2 was completed in the proposed location and revealed the footing. Soil and root samples were taken. Within TH2 we also took readings from the garage wall, these measurements can be shown in trial hole log 2b below

TH3 was completed in the proposed location and revealed the footing. Soil and root samples were taken.

Drain Survey

We carried out a CCTV survey of the below ground drainage system, our findings of which are as follows:

Line 1 - From IC1 downstream to MH

Our survey of line 1 revealed no significant defects to the pipework on this line which could be allowing an escape of water.

Line 2 - From IC1 upstream to RWG1

Our survey of line 2 revealed no significant defects to the pipework on this line which could be allowing an escape of water.

Line 3 - From IC1 upstream to WP1

Our survey of line 3 revealed no significant defects to the pipework on this line which could be allowing an escape of water.

Line 4 - From SWG1 downstream to D/S

We were unable to survey line 4 properly due to severe root ingress within the pipework.

Line 5 - From MH1 downstream to Main

Our survey of line 5 revealed no significant defects to the pipework on this line which could be allowing an escape of water.

Line 4 - From SWG1 downstream to D/S

We were unable to complete a full CCTV survey of line 4 due to an unknown blockage in the pipework.

Recommendations	
Refer Back to Client	<p>It is recommended that the following further investigation works are carried out to confirm the condition of all pipework at the property:</p> <p>Line 4 Excavate at a depth no greater than 1.0m through concrete directly downstream of RWG to break into and access the pipework on this line. We need to perform high pressure jetting of the drains for approximately 2 hours to clear the roots. We will then need to conduct a further CCTV investigation downstream on this line.</p> <p>Please note The further CCTV investigation may reveal additional defects to the drainage system. This will be reported whilst on-site and could potentially cause an increase in repair costs and provide further inconvenience to the customer/occupants.</p> <p>We will now refer the claim back to the client in order to progress the claim.</p>
	<p><i>Once repairs have been undertaken the customer should ensure the drainage system is periodically inspected in the future for any deterioration and kept free flowing / free of blockages. Any damage noted during future inspections should be repaired immediately in accordance with current Building Regulations.</i></p> <p><i>With any repair process, complications and unforeseen circumstances can arise. These scenarios will be reported whilst on-site and could potentially cause an increase in repair costs and inconvenience.</i></p> <p><i>If any of the above lining recommendations fail then excavation and replacement of the pipework would be required. This would severely increase the cost of repairs and would provide greater inconvenience to the residents.</i></p> <p><i>Recommendations have been made to reline or patch reline sections of the drainage system at the property. This process combines a number of chemicals in a resin, which then harden in a fibreglass matting to create a new section of drain within the original. The reaction creates a strong smell which can linger for up to 72 hours once works are completed - this is not harmful. It is recommended that any areas where smells are experienced are kept well ventilated until the odour subsides.</i></p>

Photographs

Trial Hole 1	
Fig 1.1: Trial Hole 1 Location	Fig 1.2: Trial Hole 1 Footing
	

Trial Hole 2

Fig 2.1: Trial Hole 2 Location



Fig 2.2: Trial Hole 2 Footing



Trial Hole 3

Fig 3.1: Trial Hole 3 Location



Fig 3.2: Trial Hole 3 Footing



CCTV Survey – Inspection Listings (WRc Guidelines Applied)

L1			
Direction	Downstream	From	IC1
Pipe Size (mm)	100	Depth (m)	0.80
Pipe Material	PVC	To	MAIN
0.0m	Start of Survey Length		
0.1m	Material Change (TO VC)		
3.3m	Finish of Survey Length (ENTER LARGE MH1)		

L2			
Direction	Upstream	From	IC1
Pipe Size (mm)	100	Depth (m)	0.80
Pipe Material	PVC	To	RWG1
0.0m	Start of Survey Length		
3.2m	Junction (TO ACO)		
9.5m	Manhole (TO BIC2)		
9.9m	Junction (TO RWG2)		
12.3m	Line of Sewer Deviates Left		

17.4m

Finish of Survey Length (AT RWG1)

L3

Direction	Upstream	From	IC1
Pipe Size (mm)	100	Depth (m)	0.80
Pipe Material	PVC	To	WP1

0.0m	Start of Survey Length
0.2m	Material Change (TO VC)
3.2m	Material Change (TO PVC)
3.5m	Line of Sewer Deviates Left
4.5m	Junction
5.2m	Line of Sewer Deviates Right
6.3m	Finish of Survey Length

L4

Direction	Downstream	From	SWG1
Pipe Size (mm)	100	Depth (m)	0.0
Pipe Material	PVC	To	DS

0.0m	Start of Survey Length
0.0m	Survey Abandoned (Mass Roots)

L5

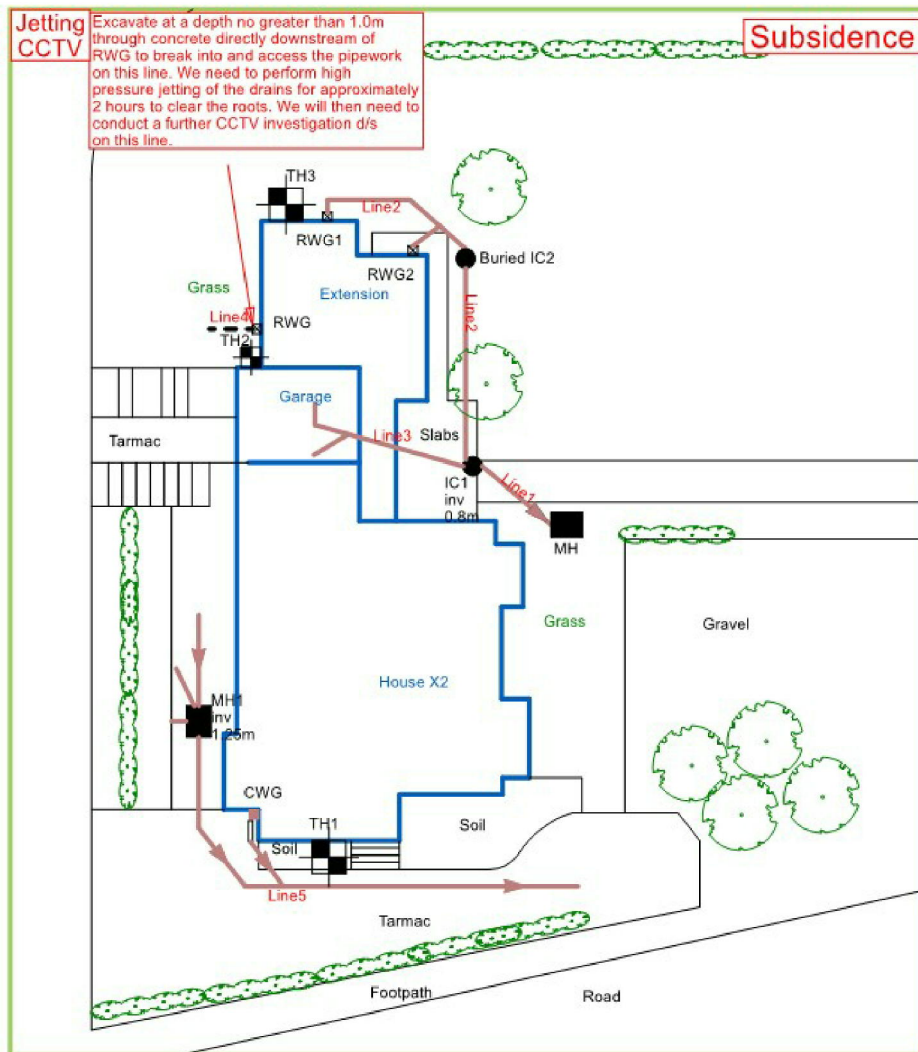
Direction	Downstream	From	MH1
Pipe Size (mm)	100	Depth (m)	1.25
Pipe Material	VC	To	MAIN

0.0m	Start of Survey Length
3.8m	Line of Sewer Deviates Left
5.7m	Line of Sewer Deviates Left
6.6m	Junction (TO CWG/SWG)
20.6m	Finish of Survey Length

Jetting CCTV




















Excavate at a depth no greater than 1.0m through concrete directly downstream of RWG to break into and access the pipework on this line. We need to perform high pressure jetting of the drains for approximately 2 hours to clear the roots. We will then need to conduct a further CCTV investigation d/s on this line.

Subsidence



FRONT OF PROPERTY

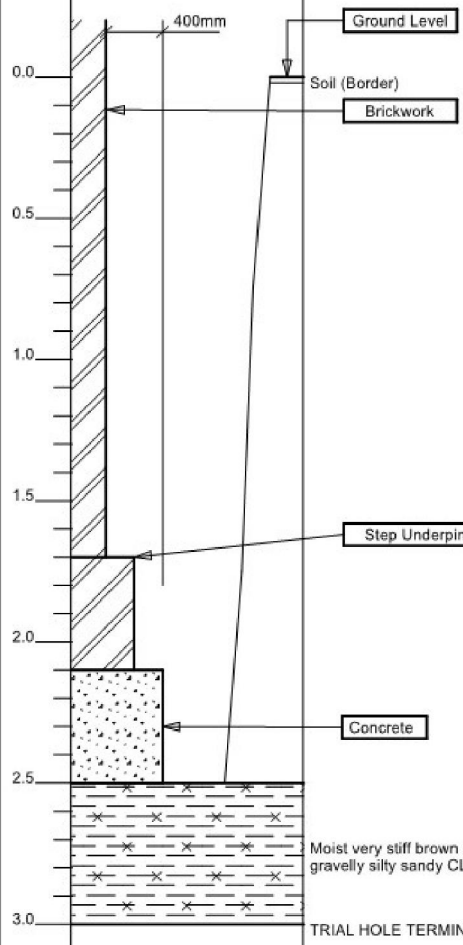
This drawing should be used for diagrammatic purposes only. Auger are not responsible or liable for any 3rd party works undertaken using the details outlined in this drawing. Confirmation of the drainage configuration can only be confirmed by excavation or detailed technical survey.

LEGEND			
	= Manhole (MH)		= Blockage / Collapse
	= Inspection Chamber (IC)		= Soil Vent Pipe (SVP) / WC
	= Inspection Point (IP)		= Combined Waste Gully (CWG) / Foul Waste Gully (FWG)
	= Rainwater Gully (RWG)		= Rainwater Pipe (RWP)
	= Lines not to be repaired		= Trial hole
	= Lines to be repaired		= Borehole
	= Assumed water mains feed		= Direction of flow
	= Walls		= Gate / Door
	= Fences		= Steps
	= Building Outline		



Trial Hole Log No.1

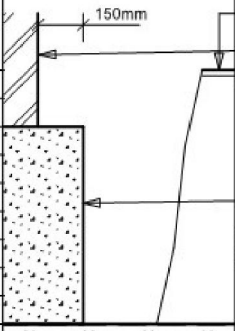
Location: Front left of front entrance

Depth (m)	Symbolic Log	Strata Description	Insitu Tests		Soil Sample	Root Sample
			SV(19)			
0.0		Ground Level				
		Soil (Border)				
0.5		Brickwork				
1.0						
1.5		Step Underpinned				
2.0						
2.5		Concrete	82kpa		Soil @ 2.5m	Root @ 2.5m
3.0		Moist very stiff brown slightly fine gravelly silty sandy CLAY				
		TRIAL HOLE TERMINATED	88kpa		Soil @ 3m	



Trial Hole Log No.2

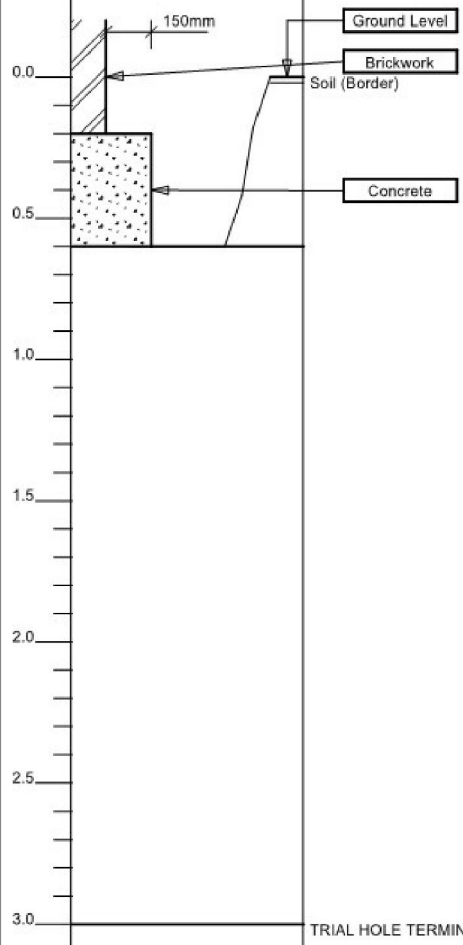
Location: JN between extension and garage (A)
extension

Depth (m)	Symbolic Log	Strata Description	Insitu Tests		Soil Sample	Root Sample
			SV(19)			
0.0		Ground Level Brickwork Soil (Border) Concrete				
0.5		Moist stiff brown fine gravelly silty sandy CLAY			Soil @ 0.6m	
1.0		Moist stiff brown fine gravelly silty sandy CLAY	62kpa		Soil @ 0.9m	Root @ 0.9m
1.5		Moist stiff brown fine gravelly silty sandy CLAY	76kpa		Soil @ 1.4m	
2.0		Moist stiff brown fine gravelly silty sandy CLAY	74kpa		Soil @ 1.9m	
2.5		Moist stiff brown fine gravelly silty sandy CLAY	64kpa		Soil @ 2.4m	
3.0		Moist stiff brown slightly fine gravelly silty sandy CLAY	60kpa		Soil @ 2.9m	
		TRIAL HOLE TERMINATED	60kpa			



Trial Hole Log No.2b


Location: Garage wall

Depth (m)	Symbolic Log	Strata Description	Insitu Tests		Soil Sample	Root Sample
			SV(19)			
0.0		Ground Level				
		Brickwork				
		Soil (Border)				
0.5		Concrete				
1.0						
1.5						
2.0						
2.5						
3.0		TRIAL HOLE TERMINATED				



Trial Hole Log No.3

Location: Rear of extension

Depth (m)	Symbolic Log	Strata Description	Insitu Tests		Soil Sample	Root Sample
			SV(19)			
0.0		Ground Level				
		Gravel				
		Brickwork				
		Concrete (No Proj)				
0.5						
1.0		Moist very stiff brown silty sandy CLAY	82kpa		Soil @ 1.2m	Root @ 1.2m
1.5		Moist very stiff brown fine gravelly silty sandy CLAY	84kpa		Soil @ 1.7m	
2.0		Moist very stiff brown fine gravelly silty sandy CLAY	86kpa		Soil @ 2.2m	
2.5		Moist very stiff brown slightly fine gravelly silty sandy CLAY	78kpa		Soil @ 2.7m	
3.0		TRIAL HOLE TERMINATED	80kpa			



Root identification
Vegetation surveys
Tree/Building Investigations
Plant taxonomy

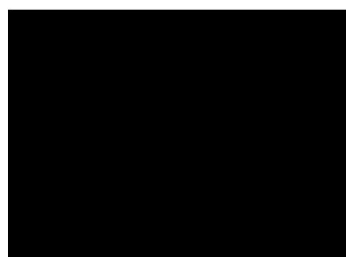
Richardson's Botanical Identifications

Dr Ian B K Richardson
BSc, MSc, PhD, MRSB, FLS
James Richardson
BSc (Hons. Biology)

Auger Solutions



15/11/2022



Dear Sirs

Root ID

The samples you sent in relation to the above on 31/10/2022 have been examined. Their structures were referable as follows:

TH1, 2.50m		
2 no.	Examined root: similar in many ways to PLATANUS (Plane). Less than 0.9mm in diameter.	Alive, recently*.
4 no.	All pieces of BARK only - not enough material for identification.	
TH2, 0.90m		
3 no.	Examined root; also under 0.9mm in diameter. Referable to the family Rosaceae, subfamily POMOIDEAE (a group of closely related trees: Malus (Apple), Pyrus (Pear), Crataegus (Hawthorn), Sorbus (Rowan, Whitebeam, Service tree), Mespilus (Medlar), and some shrubs (Pyracantha (Firethorn), Chaenomeles (Japonica), Cydonia (Quince), Amelanchier, Cotoneaster)).	Alive, recently*.
TH3, 1.20m		
2 no.	Examined root: the family LEGUMINOSAE (a group of closely related trees: Robinia (False Acacia), Laburnum, Sophora (Pagoda tree), Gleditsia (Honey Locust), Cercis (Judas tree/Redbud), Albizia (Silk tree), Acacia (Mimosa), as well as such shrubs as Wisteria, Lupins, Gorse and Brooms). Again, not more than 0.9mm in diameter.	Alive, recently*.

Click here for more information: [LEGUMINOSAE](#) [PLATANUS](#) [POMOIDEAE](#)

I trust this is of help. Please call us if you have any queries; our Invoice is enclosed.

Yours faithfully



Dr Ian B K Richardson

* Based mainly on the Iodine test for starch. Starch is present in some cells of a living woody root, but is more or less rapidly broken down by soil micro-organisms on death of the root, sometimes before decay is evident. This result need not reflect the state of the parent tree.

Identified with no information on vegetation, on or off site.

Report commissioned by





Geotechnical Testing Analysis Report



*The testing results contained within this report have been performed by GSTL a UKAS accredited laboratory on behalf of Auger.

Summary Of Claim Details

Policy Holder	Unknown
Risk Address	Unknown
SI Date	31/10/2022
Issue Date	31/10/2022
Report Date	21/11/2022
Auger Reference	
Insurance Company	
LA Claim Reference	
LA Co. Reference	

This certificate is issued in accordance with the accreditation requirements of the United Kingdom Accreditation Service. The results reported herein relate only to the material supplied to the laboratory. This certificate shall not be reproduced except in full, without the prior written approval of the laboratory.

Checked and approved

21/11/2022

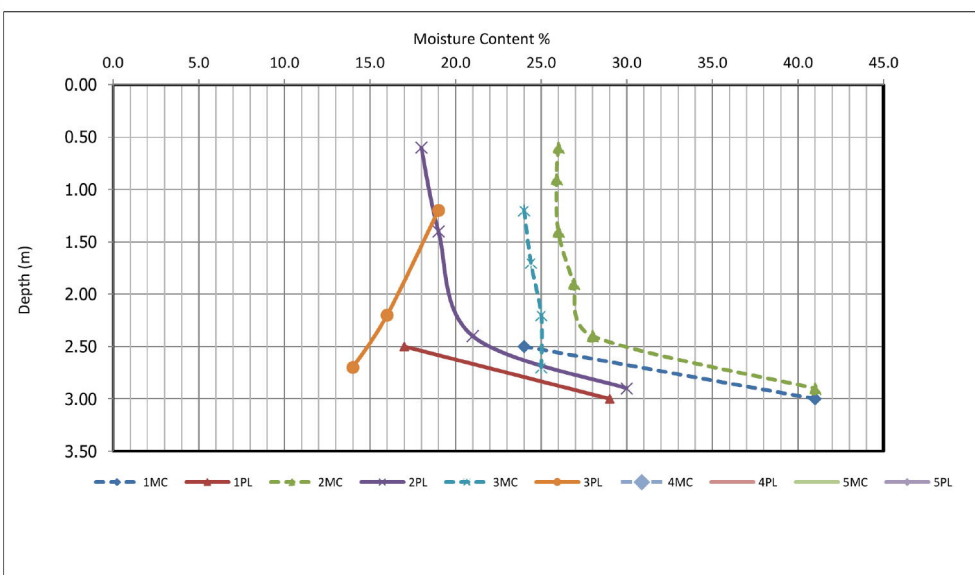
Wayne Honey



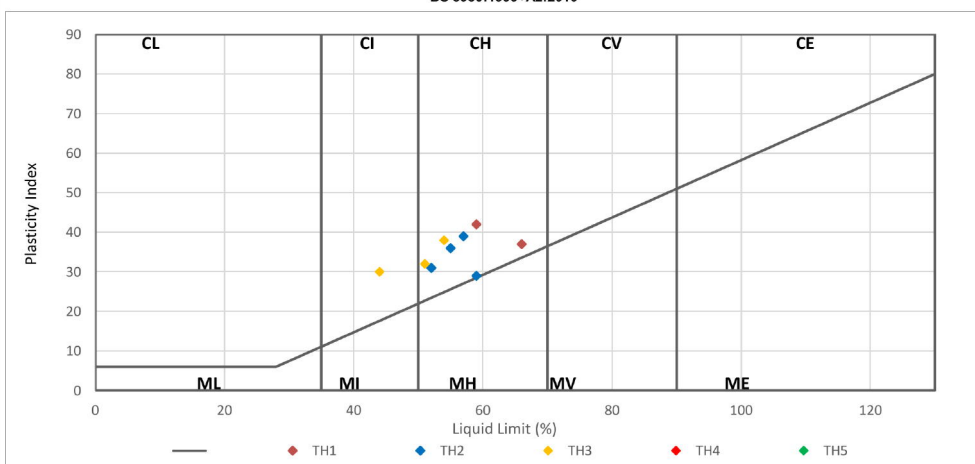




Test Operator
Jason Smith



PLASTICITY CHART FOR CASAGRANDE CLASSIFICATION
BS 5930:1999+A2:2010



Modified Plasticity Index (PI) <10 : Non Classified
 Modified PI = 10 to <20 : Low volume change potential (LOW VCP)
 Modified PI = 20 to <40 : Medium volume change potential (Med VCP)
 Modified PI = 40 or greater : High volume change potential (HIGH VCP)

The Atterberg Limits May also be used to classify the volume change potential of fine soils using the National House building system, as given in the NHBC's Standards Chapter 4.2 (2003) "Building Near Trees"

Test Operator
 Jason Smith



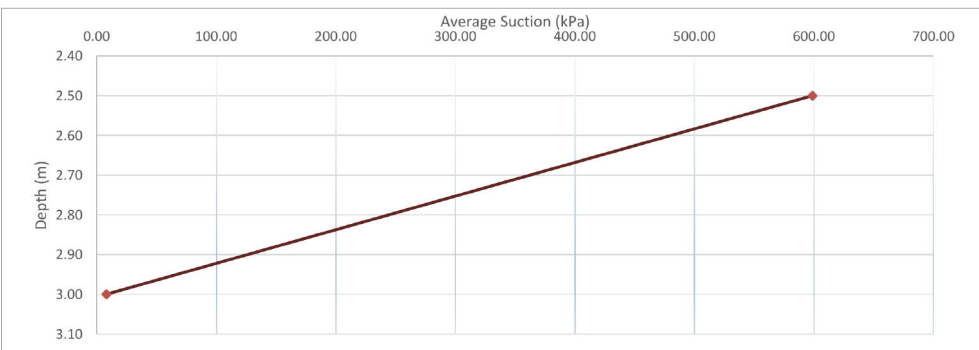
GSTL Contract Number		
Risk Address	Unknown	
Auger Reference		
Remarks	D - Disturbed (Recompacted 2.5kg Rammer), U - Undisturbed Sample	

[illegible]



Heave potential is calculated from the bottom of the hole and heaves above the bottom of the hole are reported as a cumulative value.

The values reported for heave above only apply to the strata the suction and plasticity have been performed on. The shallowest depth reported is assumed to be a strata thickness to GL and Heave is calculated based on that layer thickness, if the next sample is in 0.5m increments the heave is calculated based on the layer thickness of 0.5m and depths 1m from the sample above will include heave over 1m.

Consideration should be made for other stratas where values are not reported and when working out the heave potential over the entire trial hole.



Test Operator
Jason Smith

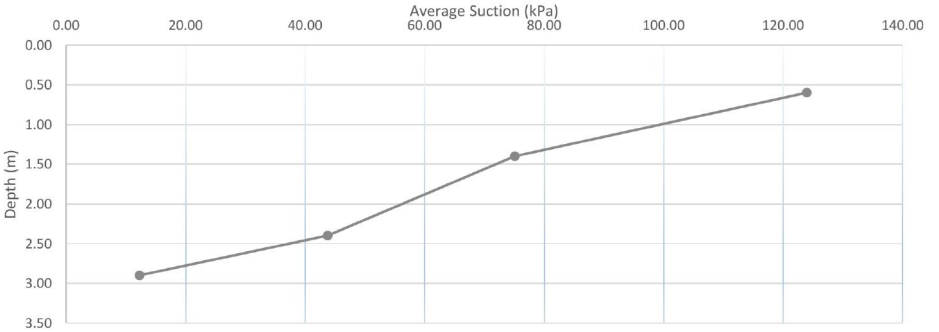
 SUMMARY OF SOIL CLASSIFICATION TESTS, Information Paper IP 4/93 February 1993 (CI/SfB p1), Information Paper Digest 412 ci/sFb (A3s) February 1996		BRE BRE		 <small>environmental claims mgmt subsidence drainage</small>	
GSTL Contract Number					
Risk Address		Unknown			
Auger Reference					
Remarks		D - Disturbed (Recompacted 2.5kg Rammer), U - Undisturbed Sample			

TH Trial Hole	Depth (m)	Filter Paper Location	Filter Paper	Sample Prep Method	Test Duration (Days)	Water Content (%)	Soil Suction Pk (kPa)	Average Soil Suction Pk (kPa)	Cumulative Heave Potential (mm) from bottom of the hole
TH2	0.60	Top	I	D	5	45.3	105	124	5
TH2	0.60	Middle	II	D	5	45.5	102		
TH2	0.60	Bottom	III	D	5	42.1	166		
TH2	0.90								
TH2	0.90								
TH2	0.90								
TH2	1.40	Top	I	D	5	48.1	76	75.1	0
TH2	1.40	Middle	II	D	5	48.2	75		
TH2	1.40	Bottom	III	D	5	48.4	74		
TH2	1.90								
TH2	1.90								
TH2	1.90								
TH2	2.40	Top	I	D	5	59.6	44	43.8	0
TH2	2.40	Middle	II	D	5	59.9	44		
TH2	2.40	Bottom	III	D	5	60.3	43		
TH2	2.90	Top	I	D	5	127.0	7	12.3	0
TH2	2.90	Middle	II	D	5	92.1	15		
TH2	2.90	Bottom	III	D	5	92.5	15		

Heave potential is calculated from the bottom of the hole and heaves above the bottom of the hole are reported as a cumulative value.

The values reported for heave above only apply to the strata the suction and plasticity have been performed on. The shallowest depth reported is assumed to be a strata thickness to GL and Heave is calculated based on that layer thickness, if the next sample is in 0.5m increments the heave is calculated based on the layer thickness of 0.5m and depths 1m from the sample above will include heave over 1m.

Consideration should be made for other stratas where values are not reported and when working out the heave potential over the entire trial hole.



Test Operator
Jason Smith



Test Operator
Jason Smith