

Report VA4664.230831.NIA1.1

**16-24 Whitfield Street & 55 Tottenham
Court Road, London**

Noise Impact Assessment

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Attachments

VA4664/SP1	Indicative Site Plan
VA4664/TH1-TH4	Environmental Noise Time Histories
VA4664/NM1	Noise Map
Appendix A	Acoustic Terminology

1. Introduction

It is proposed to install new plant 1st floor and roof level as part of the works at 16-24 Whitfield Street & 55 Tottenham Court Road, London.

Venta Acoustics has been commissioned by Taylor Project Services LLP to undertake an assessment of the potential noise impact of these proposals in support of an application for planning permission.

An environmental noise survey has been undertaken to determine the background noise levels at the most affected noise sensitive receptors. These levels are used to undertake an assessment of the likely impact with reference to the planning requirements of Camden Council.

2. Design Criterion and Assessment Methodology

2.1 Camden Council Requirements

Camden Council’s Local Plan (adopted June 2017), Appendix 3, provides the following guidance regarding noise from Industrial and Commercial Noise Sources

A relevant standard or guidance document should be referenced when determining values for LOAEL and SOAEL for non-anonymous noise. Where appropriate and within the scope of the document it is expected that British Standard 4142:2014 ‘Methods for rating and assessing industrial and commercial sound’ (BS 4142) will be used. For such cases a ‘Rating Level’ of 10 dB below background (15dB if tonal components are present) should be considered as the design criterion).

Existing Noise sensitive receiver	Assessment Location	Design Period	LOAEL (Green)	LOAEL to SOAEL (Amber)	SOAL (Red)
Dwellings**	Garden used for main amenity (free field) and Outside living or dining or bedroom window (façade)	Day	‘Rating level’ 10dB* below background	‘Rating level’ between 9dB below and 5dB above background	‘Rating level’ greater than 5dB above background
Dwellings**	Outside bedroom window (façade)	Night	‘Rating level’ 10dB* below background and no events exceeding 57dB _{L_{max}}	‘Rating level’ between 9dB below and 5dB above background or noise events between 57dB and 88dB L _{max}	‘Rating level’ greater than 5dB above background and/or events exceeding 88dB _{L_{max}}

**10dB should be increased to 15dB if the noise contains audible tonal elements. (day and night). However, if it can be demonstrated that there is no significant difference in the character of the residual background noise and the specific noise from the proposed development then this reduction may not be required.*

In addition, a frequency analysis (to include, the use of Noise Rating (NR) curves or other criteria curves) for the assessment of tonal or low frequency noise may be required.

***levels given are for dwellings, however, levels are use specific and different levels will apply dependent on the use of the premises.*

The periods in Table C correspond to 0700 hours to 2300 hours for the day and 2300 hours to 0700 hours for the night. The Council will take into account the likely times of occupation for types of development and will be amended according to the times of operation of the establishment under consideration.

There are certain smaller pieces of equipment on commercial premises, such as extract ventilation, air conditioning units and condensers, where achievement of the rating levels (ordinarily determined by a BS:4142 assessment) may not afford the necessary protection. In these cases, the Council will generally also require a NR curve specification of NR35 or below, dependant on the room (based upon measured or predicted $L_{eq,5mins}$ noise levels in octave bands) 1 metre from the façade of affected premises, where the noise sensitive premise is located in a quiet background area.

2.2 BS8233:2014

BS8233 *Guidance on sound insulation and noise reduction for buildings* provides guidance as to suitable internal noise levels for different areas within residential buildings.

The relevant section of the standard is shown below in Table 2.1.

Activity	Location	07:00 to 23:00	23:00 to 07:00
Resting	Living Room	35 dB $L_{Aeq, 16 \text{ hour}}$	-
Dining	Dining Room	40 dB $L_{Aeq, 16 \text{ hour}}$	-
Sleeping (daytime resting)	Bedroom	35 dB $L_{Aeq, 16 \text{ hour}}$	30 dB $L_{Aeq, 8 \text{ hour}}$

Table 2.1 - Excerpt from BS8233: 2014

[dB ref. 20µPa]

3. Site Description

As illustrated on attached site plan VA4664/SP1, the site building is located to the east of Whitfield Street and runs across to Tottenham Court Road to the east. The site houses an existing M&S Simply food and has offices above.

The most affected noise sensitive receivers are expected to be the apartments above the retail uses on Tottenham Court Road located to the north east of the building.

Existing building services plant was noted on several of the neighbouring rooftops.

4. Environmental Noise Survey

4.1 Survey Procedure & Equipment

In order to establish the existing background noise levels at the site, a noise survey was carried out between Tuesday 25th and Friday 28th April 2023 at the location shown in site plan VA4664/SP1. This location was chosen to be representative of the background noise level at the most affected noise sensitive receivers.

Continuous 5-minute samples of the L_{Aeq} , L_{Amax} , L_{A10} and L_{A90} sound pressure levels were undertaken at the measurement location.

The weather during the survey period was generally dry with light winds. The background noise data is not considered to have been compromised by these conditions.

Measurements were made generally in accordance with ISO 1996 2:2017 *Acoustics - Description, measurement and assessment of environmental noise – Part 2: Determination of sound pressure levels*.

The following equipment was used in the course of the survey:

Manufacturer	Model Type	Serial No	Calibration	
			Certificate No.	Date
NTi Class 1 Integrating SLM	XL2	A2A-15993-E0	1504971-2	28/3/23
Larson Davis calibrator	CAL200	13049	1504971-3	28/3/23

Table 4.1 – Equipment used for the tests

The calibration of the sound level meter was verified before and after use with no significant calibration drift observed.

4.2 Results

The measured sound levels are shown as time-history plots on the attached charts VA4664/TH1-4.

The background noise level is determined by existing plant in the area, and road traffic in the surrounding roads.

The minimum background noise levels measured were:

Monitoring Period	Typical ¹ $L_{A90,5min}$
07:00 – 23:00 hours	46 dB
23:00 – 07:00 hours	42 dB

Table 4.2 – Minimum background noise levels

[dB ref. 20 μ Pa]

¹The typical L_{A90} value is taken as the 10th percentile of all L_{A90} values measured during the relevant period.

4.3 Plant Noise Emission Limits

On the basis of the measured noise levels and the planning requirements of the Local Authority, and considering that it is not expected that tonal noise will be generated by the proposed plant units, the following plant specific sound levels should not be exceeded at the most affected noise sensitive receivers:

Monitoring Period	Design Criterion (L _{Aeq})
07:00 – 23:00 hours	33 dB
23:00 – 07:00 hours	32 dB

Table 4.3 – Specific sound pressure levels not to be exceeded at most affected noise sensitive receivers

5. Predicted Noise Impact

Calculations have been undertaken based upon the provided plant noise information at the time of writing. It has not been possible to confirm the model or noise levels for the M&S Gas Cooler which will be located at roof level at this stage. To allow for this unit, plant noise has been mitigated to achieve a maximum level of 28dB(A) at the most affected receiver, which provides an allowance for the gas cooler of 30dB(A) at the nearest receiver, which will be evaluated against once the necessary information becomes available.

5.1 Proposed plant

The following plant is proposed for installation at first floor and roof level at the locations indicated on site plan VA4664/SP1.

Plant Item	Quantity	Proposed Model	Notes
AHU	1	Systemair Topvex SR80-R-EL19	First floor
AHU	1	Daikin EDT05FCD	Roof level
VRF Units	2	Mitsubishi PURY-P350YNW-A1	
Condenser Units	6	Daikin RXYSCQ8	
Toilet Extract	1	Nuaire DE7-ES	

Table 5.1 – Indicative plant selections assumed for this assessment.

Consulting the manufacturer’s datasheets, the following noise emissions levels are attributed to the proposed plant items:

Plant Item	Octave Band Centre Frequency (Hz)								dB(A)
	Sound Pressure/Power Level, L _p @1m, L _w (dB)								
	63	125	250	500	1k	2k	4k	8k	
	Sound Power Level, L _w (dB)								
Systemair – Intake	83	81	64	63	56	50	46	42	67
Systemair – Exhaust	83	77	65	66	65	60	56	42	69
Systemair – Breakout	71	75	65	57	49	44	42	35	62
Daikin - Intake	70	61	64	60	58	57	57	64	67
Daikin – Exhaust	75	64	76	71	72	70	68	71	78
DE7-ES – Induct Exhaust	96	91	75	71	68	63	59	55	78
DE7-ES -Breakout	75	72	69	57	55	45	40	37	63
	Sound Pressure Level, L _p @1m (dB)								
Daikin – Breakout	55	44	49	42	43	39	37	26	48
PURY-P350YNW-A1	72	71	64	62	57	54	52	48	64
Daikin RXYSCQ6	54	55	52	52	49	43	37	29	53

Table 5.2 – Advised plant noise data used for the assessment.

5.2 Recommended Mitigation Measures

The atmospheric side ductwork of the Systemair AHU will need to be fitted with attenuators providing the minimum insertion losses shown in Table 5.3. Alternative attenuation performance shape curves may be suitable and should be confirmed prior to installation.

Attenuation Component	Octave Band Centre Frequency (Hz)							
	Minimum Insertion Loss (dB)							
	63	125	250	500	1k	2k	4k	8k
Systemair attenuators	15	30	20	50	50	50	50	50
Nuaire exhaust attenuator	9	18	30	47	50	50	50	50
Daikin AHU exhaust attenuator	9	18	30	47	50	50	50	50

Table 5.3 – Minimum attenuator insertion loss

Should the above insertion loss be achieved using multiple silencers, these should be separated from each other by a distance of minimum 3-4 x D, where D is the largest internal dimension of the duct work (e.g. D is 0.5m, so a minimum of 1.5-2m apart) or a bend of at least 90°. Attenuators should be fitted as close to the fan as possible, and attached to the ductwork using flexible connections.

The rooftop plant area is to be enclosed by a plant screen. This should be a 0.7m taller than the top of the largest item of plant, nominally 2.5 metre high, formed of a continuous and imperforate material with a minimum mass per unit area of 15kg/m².

The first floor AHU is to be located within a plant room, with the atmospheric side servers ducted to atmosphere.

All plant and ductwork should be fitted with anti-vibration mounts in accordance with the manufacturer guidelines. This is expected to control structureborne noise to the building to acceptable levels.

Please note that the above recommendations relate to acoustic issues only. It is recommended that professional advice confirming the suitability of these measures be sought from others with regards to issues such as airflow, structural stability and visual impact.

5.3 Predicted noise levels

Due to the complexity of the building interaction in this locale and the likelihood of noise both reflecting off and being screened by the surrounding buildings, 3D noise mapping was implemented to ensure the most accurate prediction of plant noise levels at the nearest noise sensitive receivers.

The model was run allowing for five reflections off the surrounding surfaces.

This process uses several different calculation protocols to derive accurate noise analysis predictions. Noise propagation and barrier attenuation are calculated in accordance with ISO 9613-1:1993 *Acoustics - Attenuation of sound during propagation outdoors - Part 1: Calculation of the absorption of sound by the atmosphere* and ISO 9613-2:1996 *Acoustics - Attenuation of sound during propagation outdoors - Part 2: General method of calculation*.

Description	dB(A)
Plant noise criterion	31
L _p 1m from receiver	28

Table 5.4 – Predicted noise and level and design criteria at noise sensitive location

5.4 Comparison to NR35 Curve

As can be seen from the following comparison in Table 5.5, the predicted noise levels at 1m from the most affected receiver are comfortably below the NR35 curve.

Frequency (Hz)	63	125	250	500	1k	2k	4k	8k
NR35	63	52	45	39	35	35	30	28
L _p 1m from receiver	48	39	30	22	14	9	8	6

Table 5.5 – Comparison of predicted noise levels against the NR35 criterion

5.5 Comparison to BS8233:2014 Criteria

BS8233 assumes a loss of approximately 15dB for a partially open window. The external noise level shown in Table 5.4 would result in internal noise levels that achieve the guidelines shown in Table 2.1.

6. Terraces

Predictions of the noise levels due to the various different terraces have been calculated to the façade of the nearest building, with the following assumptions.

- Terraces would be occupied with 1 person per 2m²
- One person in four talking at a time
- People talking at ‘normal’ level, with levels based upon those stated in ANSI 3.5/BB93.

- Distance, screening and reflections off the surrounding building form to the receivers
- No amplified music or speech.

The terraces are understood to only be used during the daytime, with some occasional evening use. Noise levels at the most affected receiver are up to 50dB(A) down to 29dB(A) at the least affected receiver. These levels are significantly lower than the average daytime noise level of 58dB(A) measured during the survey. Assuming a loss of 15dB, as stated in section 5.5, maximum internal noise levels would be up to 35B(A), meeting the internal noise criterion stated in BS8233 for daytime periods.

7. Conclusion

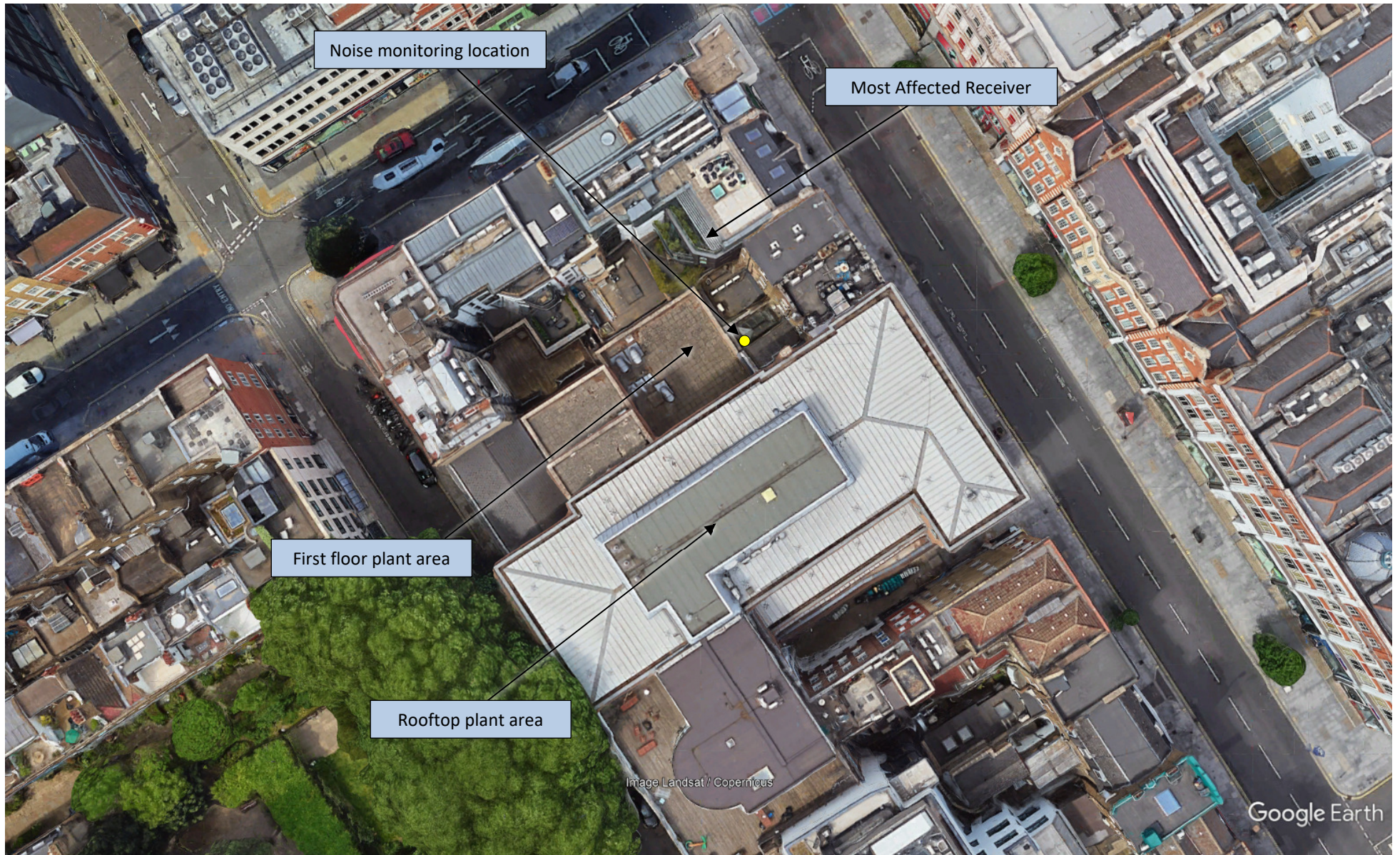
A baseline noise survey has been undertaken by Venta Acoustics to establish the background noise climate in the locality of 16-24 Whitfield Street & 55 Tottenham Court Road, London in support of a planning application for the proposed introduction of new building services plant.

This has enabled noise emission limits to be set at the most affected noise sensitive receiver such that the proposed installation meets the requirements of Camden Council .

The cumulative noise emission levels from the proposed plant have been assessed to be compliant with the plant noise emission limits, with necessary mitigation measures specified.

The proposed scheme is not expected to have a significant adverse noise impact and the relevant plant noise requirements have been shown to be met.

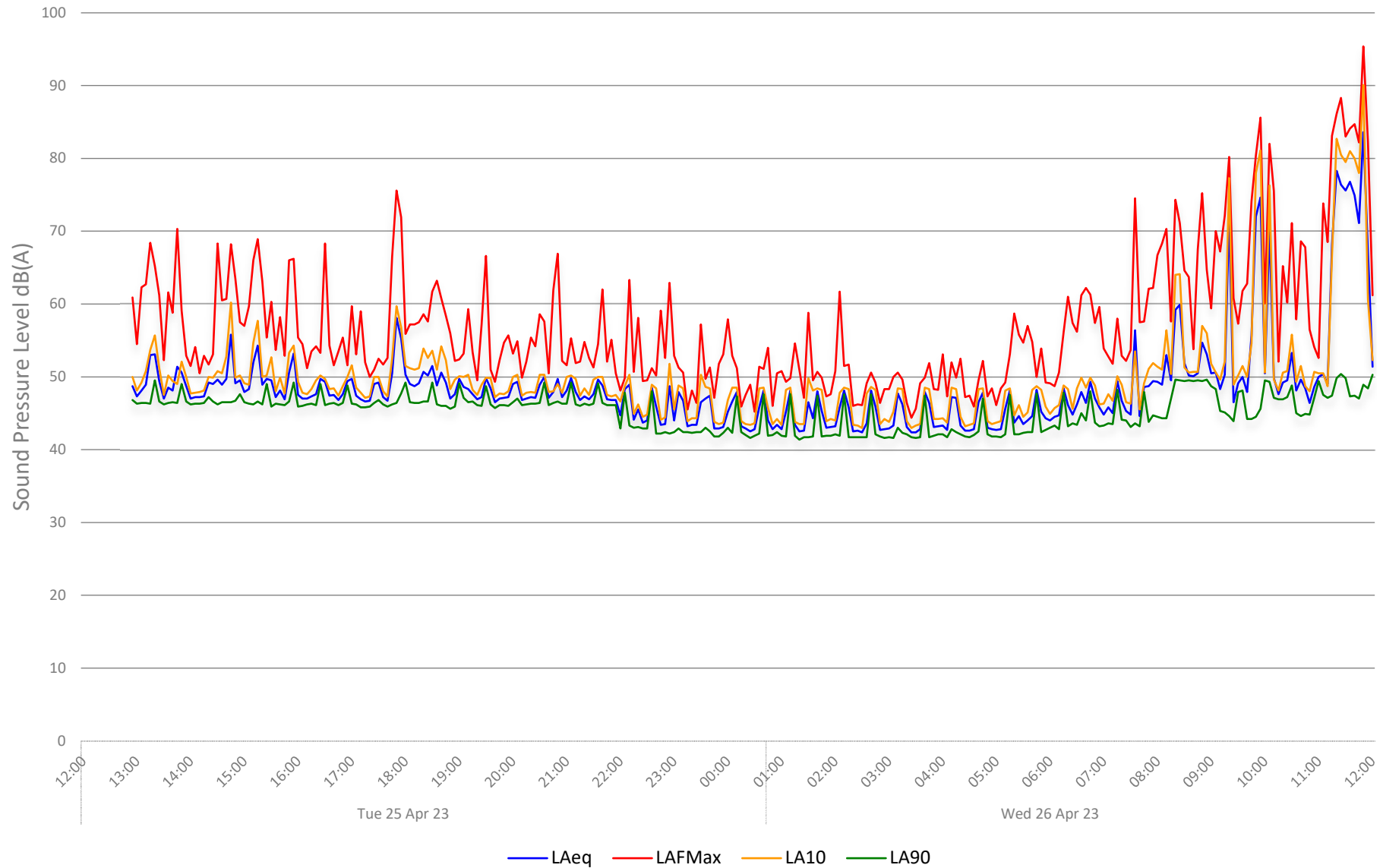
Jamie Duncan MIOA



16-24 Whitfield Street & 55 Tottenham Court Road
Environmental Noise Time History: 1



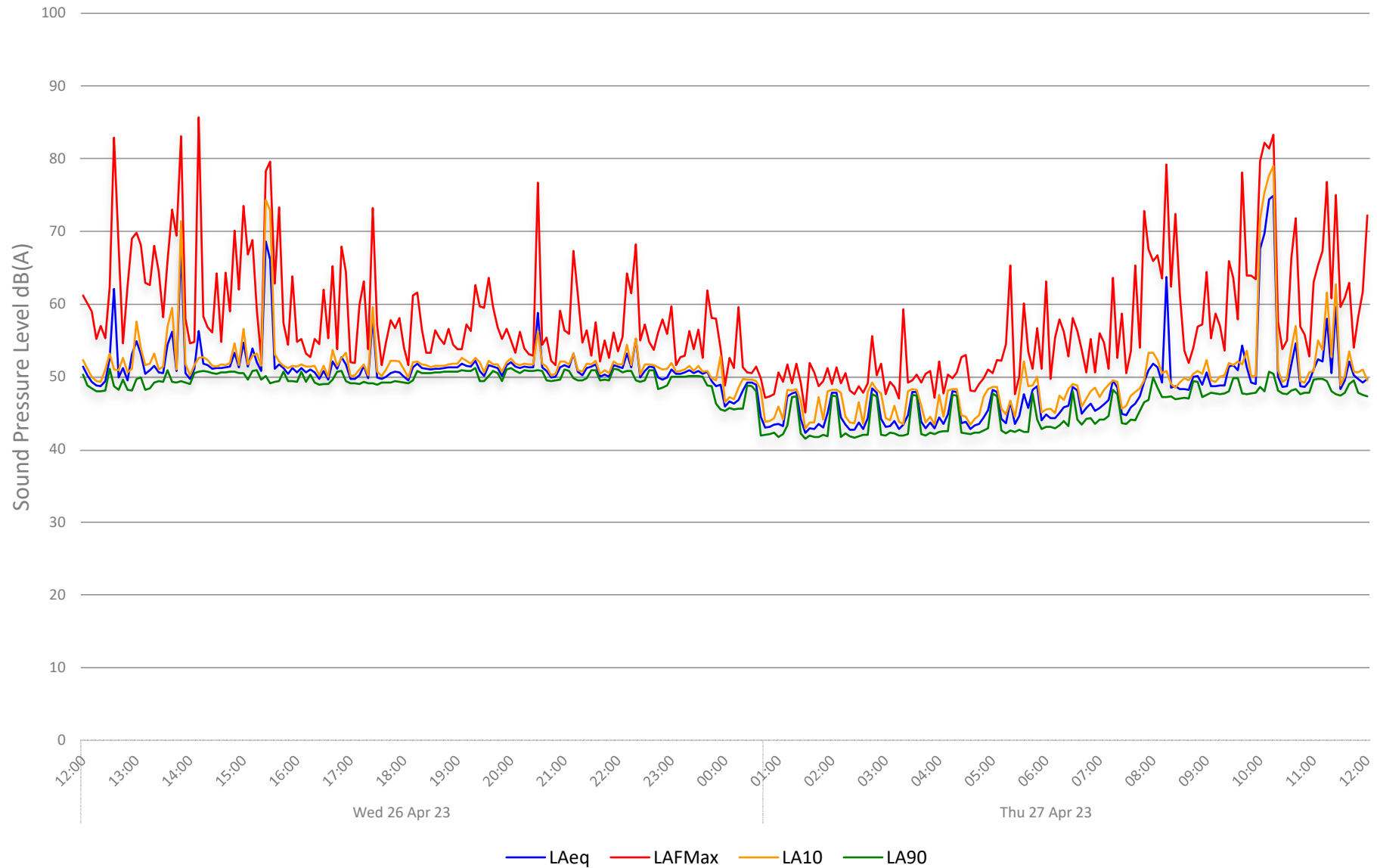
Figure VA4664/TH1



16-24 Whitfield Street & 55 Tottenham Court Road
Environmental Noise Time History: 2



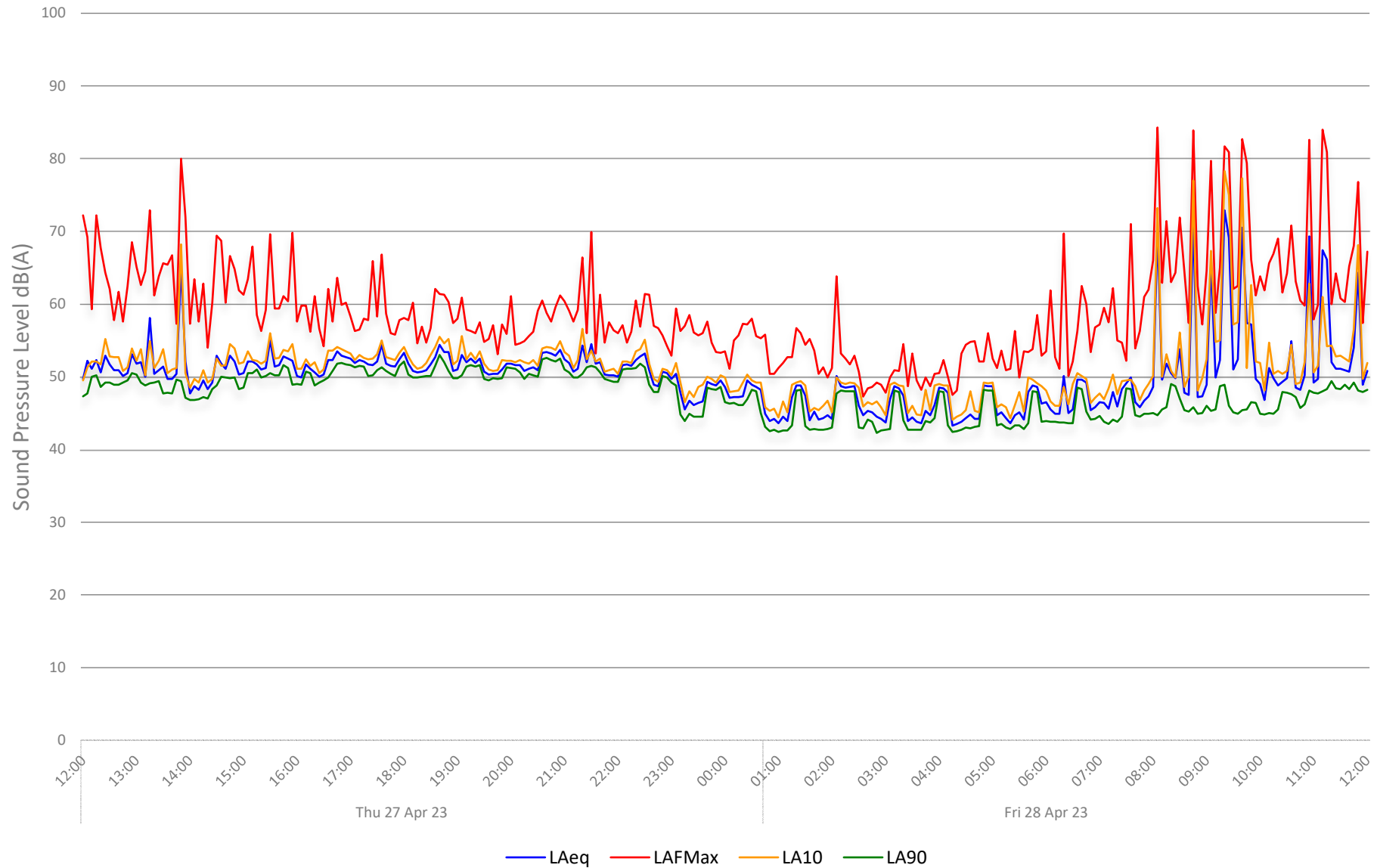
Figure VA4664/TH2



16-24 Whitfield Street & 55 Tottenham Court Road
Environmental Noise Time History: 3



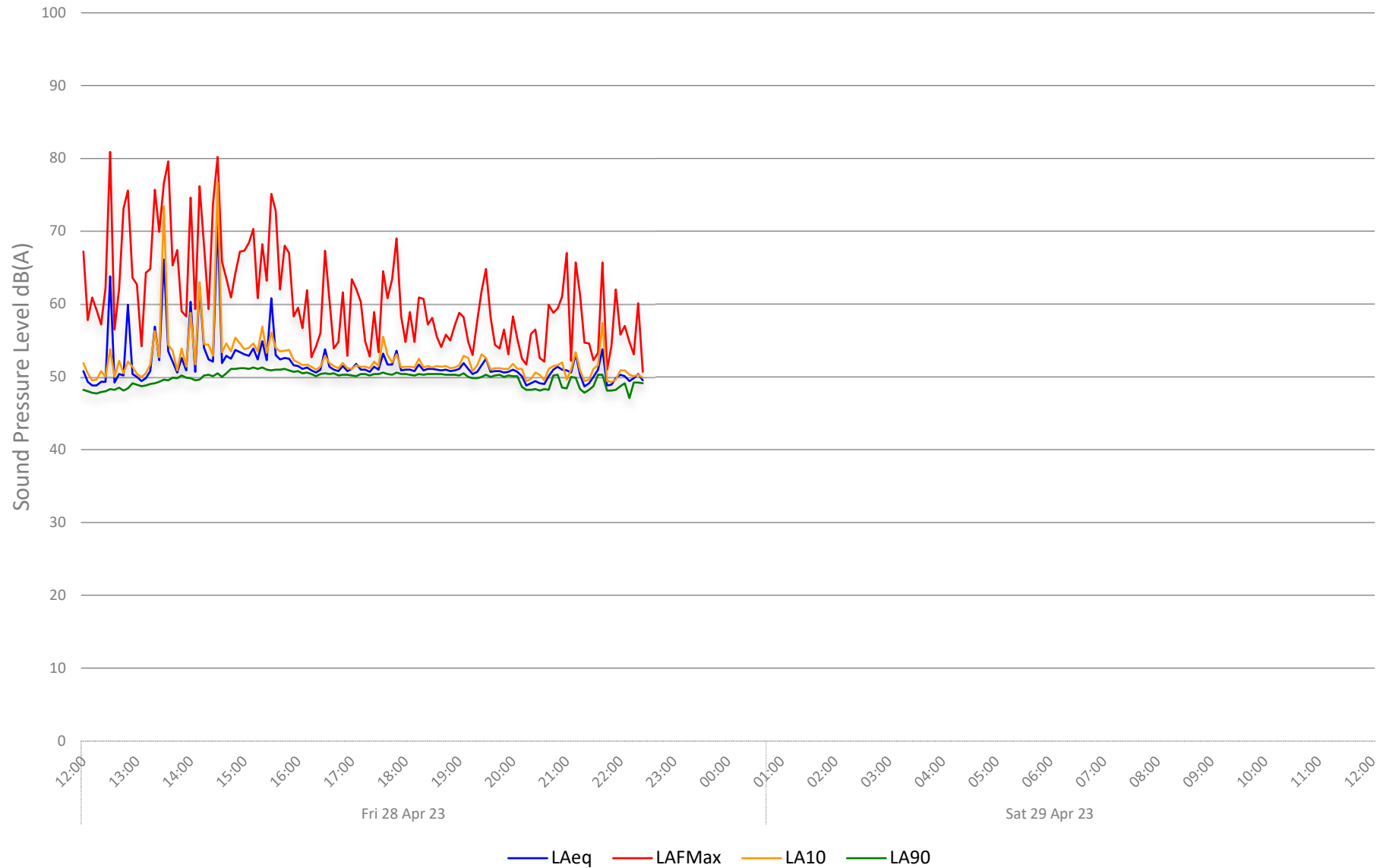
Figure VA4664/TH3

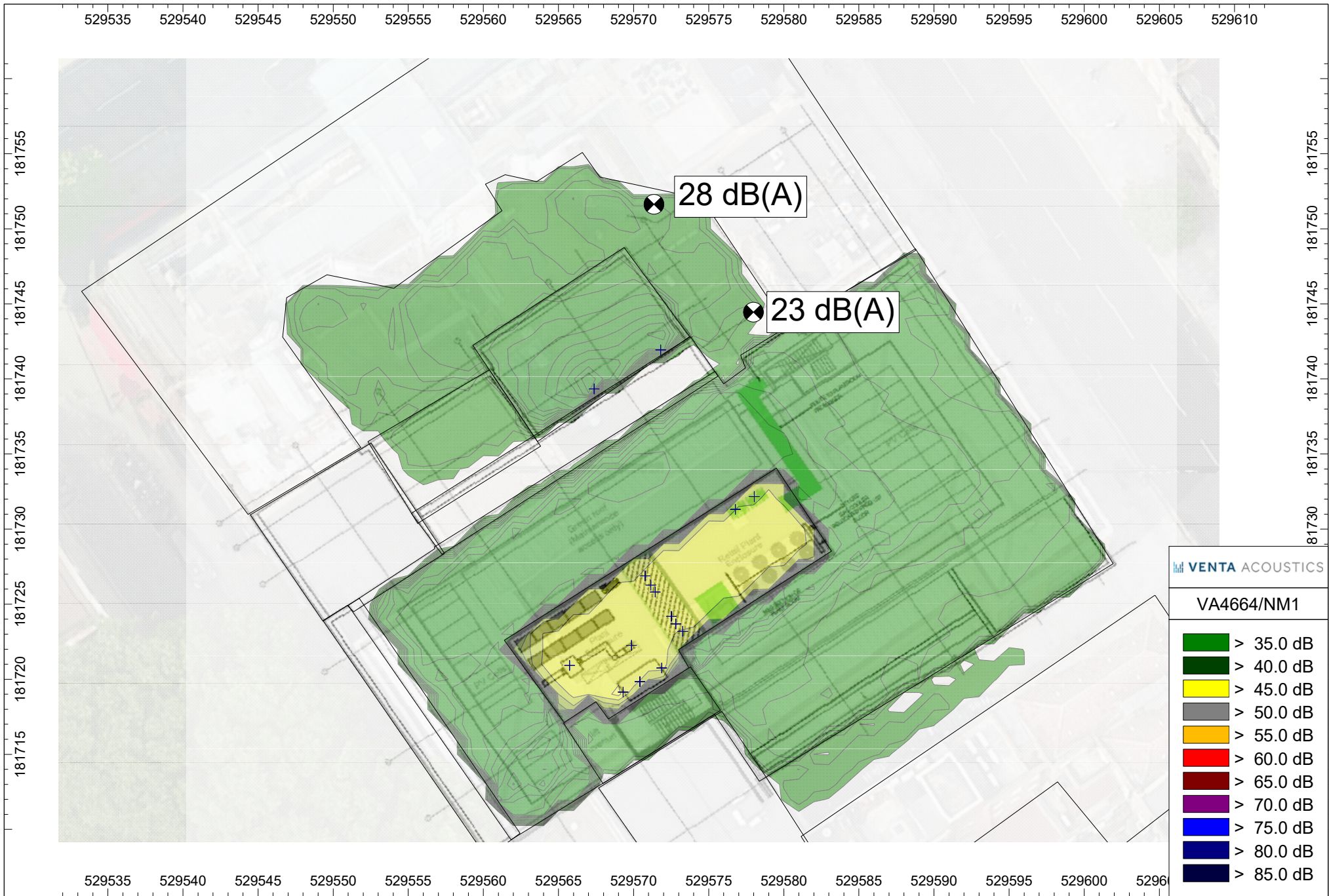


16-24 Whitfield Street & 55 Tottenham Court Road
Environmental Noise Time History: 4



Figure VA4664/TH4





VENTA ACOUSTICS

VA4664/NM1

28 dB(A)

23 dB(A)

529535 529540 529545 529550 529555 529560 529565 529570 529575 529580 529585 529590 529595 529600 529605 529610

181715 181720 181725 181730 181735 181740 181745 181750 181755

181715 181720 181725 181730 181735 181740 181745 181750 181755

529535 529540 529545 529550 529555 529560 529565 529570 529575 529580 529585 529590 529595 529600 529605 529610

APPENDIX A

Acoustic Terminology & Human Response to Broadband Sound

1.1 Acoustic Terminology

The human impact of sounds is dependent upon many complex interrelated factors such as 'loudness', its frequency (or pitch) and variation in level. In order to have some objective measure of the annoyance, scales have been derived to allow for these subjective factors.

Sound	Vibrations propagating through a medium (air, water, etc.) that are detectable by the auditory system.
Noise	Sound that is unwanted by or disturbing to the perceiver.
Frequency	The rate per second of vibration constituting a wave, measured in Hertz (Hz), where 1Hz = 1 vibration cycle per second. The human hearing can generally detect sound having frequencies in the range 20Hz to 20kHz. Frequency corresponds to the perception of 'pitch', with low frequencies producing low 'notes' and higher frequencies producing high 'notes'.
dB(A):	Human hearing is more susceptible to mid-frequency sounds than those at high and low frequencies. To take account of this in measurements and predictions, the 'A' weighting scale is used so that the level of sound corresponds roughly to the level as it is typically discerned by humans. The measured or calculated 'A' weighted sound level is designated as dB(A) or L_A . A notional steady sound level which, over a stated period of time, would contain the same amount of acoustical energy as the actual, fluctuating sound measured over that period (e.g. 8 hour, 1 hour, etc).
L_{eq} :	The concept of L_{eq} (equivalent continuous sound level) has primarily been used in assessing noise from industry, although its use is becoming more widespread in defining many other types of sounds, such as from amplified music and environmental sources such as aircraft and construction. Because L_{eq} is effectively a summation of a number of events, it does not in itself limit the magnitude of any individual event, and this is frequently used in conjunction with an absolute sound limit.
L_{10} & L_{90} :	Statistical L_n indices are used to describe the level and the degree of fluctuation of non-steady sound. The term refers to the level exceeded for n% of the time. Hence, L_{10} is the level exceeded for 10% of the time and as such can be regarded as a typical maximum level. Similarly, L_{90} is the typical minimum level and is often used to describe background noise. It is common practice to use the L_{10} index to describe noise from traffic as, being a high average, it takes into account the increased annoyance that results from the non-steady nature of traffic flow.
L_{max} :	The maximum sound pressure level recorded over a given period. L_{max} is sometimes used in assessing environmental noise, where occasional loud events occur which might not be adequately represented by a time-averaged L_{eq} value.

1.2 Octave Band Frequencies

In order to determine the way in which the energy of sound is distributed across the frequency range, the International Standards Organisation has agreed on "preferred" bands of frequency for sound measurement and analysis. The widest and most commonly used band for frequency measurement and analysis is the Octave Band. In these bands, the upper frequency limit is twice the lower frequency limit, with the band being described by its "centre frequency" which is the average (geometric mean) of the upper and lower limits, e.g. 250 Hz octave band extends from 176 Hz to 353 Hz. The most commonly used octave bands are:

Octave Band Centre Frequency Hz | 63 | 125 | 250 | 500 | 1000 | 2000 | 4000 | 8000

APPENDIX A

Acoustic Terminology & Human Response to Broadband Sound

1.3 Human Perception of Broadband Noise

Because of the logarithmic nature of the decibel scale, it should be borne in mind that sound levels in dB(A) do not have a simple linear relationship. For example, 100dB(A) sound level is not twice as loud as 50dB(A). It has been found experimentally that changes in the average level of fluctuating sound, such as from traffic, need to be of the order of 3dB before becoming definitely perceptible to the human ear. Data from other experiments have indicated that a change in sound level of 10dB is perceived by the average listener as a doubling or halving of loudness. Using this information, a guide to the subjective interpretation of changes in environmental sound level can be given.

Change in Sound Level dB	Subjective Impression	Human Response
0 to 2	Imperceptible change in loudness	Marginal
3 to 5	Perceptible change in loudness	Noticeable
6 to 10	Up to a doubling or halving of loudness	Significant
11 to 15	More than a doubling or halving of loudness	Substantial
16 to 20	Up to a quadrupling or quartering of loudness	Substantial
21 or more	More than a quadrupling or quartering of loudness	Very Substantial