



# Drainage Statement & Flood Risk Assessment **20 Crediton Hill, Camden**

SD Structures Project Reference

**SDS1585**

Issuing Date

**19/04/2023**

Revision Number

**Rev P01**

# CONTENTS

<b>1.0</b>	<b>Introduction .....</b>	<b>3</b>
<b>2.0</b>	<b>Existing Site &amp; Proposed Site .....</b>	<b>3</b>
<b>3.0</b>	<b>Policy and Climate Change .....</b>	<b>4</b>
<b>4.0</b>	<b>Flood Risk Assessment .....</b>	<b>5</b>
<b>5.0</b>	<b>Drainage Hierarchy.....</b>	<b>6</b>
<b>6.0</b>	<b>Surface Water Drainage Strategy.....</b>	<b>7</b>
<b>7.0</b>	<b>Management and Maintenance .....</b>	<b>9</b>
<b>8.0</b>	<b>Summary .....</b>	<b>10</b>
	<b>APPENDIX A .....</b>	<b>11</b>
	<b>APPENDIX B1 .....</b>	<b>12</b>
	<b>APPENDIX B2 .....</b>	<b>13</b>
	<b>APPENDIX B3 .....</b>	<b>14</b>
	<b>APPENDIX C .....</b>	<b>15</b>
	<b>APPENDIX D .....</b>	<b>16</b>

## 1.0 Introduction

- 1.1. SD Structures have been commissioned by Scenario Architecture to undertake a Flood Risk Assessment & Drainage Strategy to be submitted along with the additional documents to request planning approval for a residential development located at 20 Crediton Hill, Camden, London, NW6 1HP.
- 1.2. The report has been completed in accordance with guidance presented within the National Planning Policy Framework and its associated Planning Practice Guidance.

## 2.0 Existing Site & Proposed Site

- 2.1. The site is located at 20 Crediton Hill, Camden (Coordinate reference: E: 525732, N: 185068) with a total site area of 0.016ha. An extract of the redline boundary can be seen in Figure 1 below.

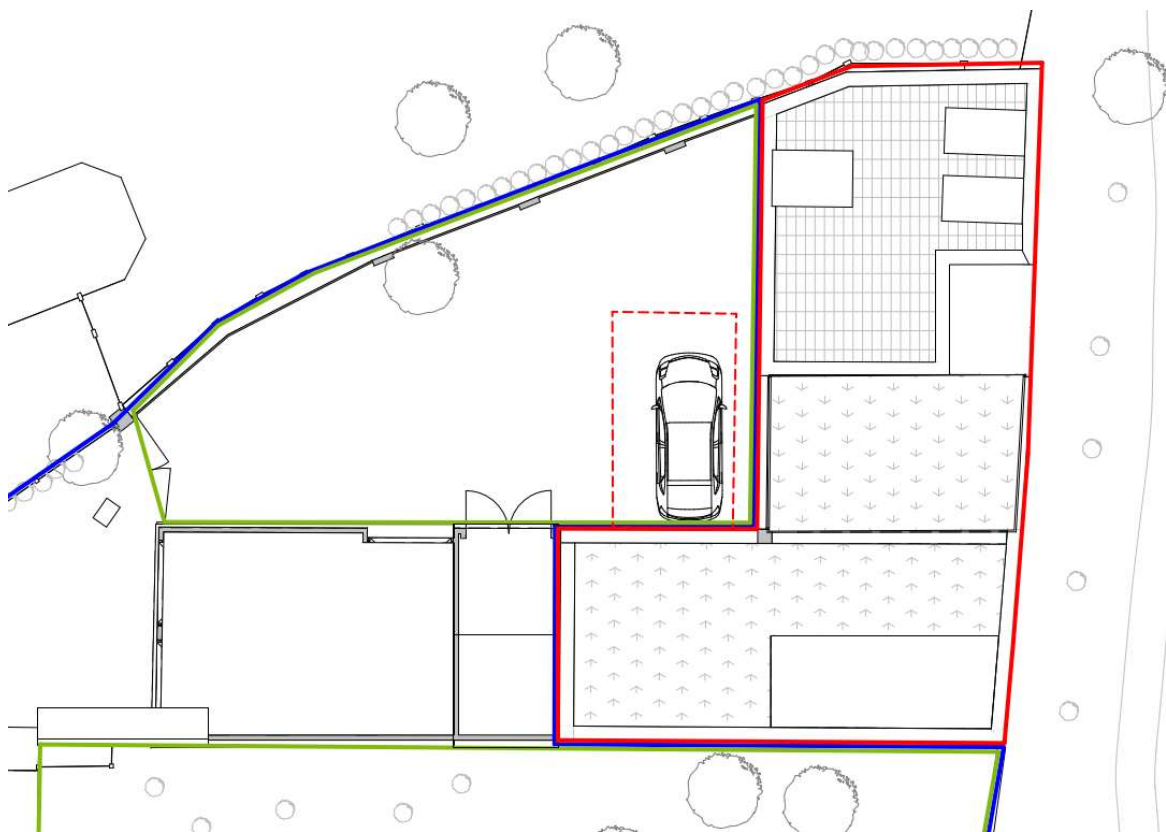


Figure 1 - Proposed redline boundary.

- 2.2. The site is currently consisting of a single residential dwelling and is made up of 100% impermeable area.
- 2.3. Based on the British Geological Survey mappings, the underlying geology is made up of London Clay Formation Bedrock with no overlying superficial deposit.

- 2.4. The proposed development comprises of the demolition of the existing residential dwelling and the erecting of a new 2 story dwelling, which will also include a new basement.
- 2.5. The existing drainage on site has been surveyed. From the survey it is evident that the existing drainage from the development discharged into a private combined network, discharging into a public combined sewer within Crediton Hill. The survey has been included within the appendices.
- 2.6. Greenfield and Pre-development discharge rates have been calculated using synthetic rainfall data derived from the Flood Study Report (FSR).
- 2.7. Greenfield runoff rates have been calculated using the IH124 methodology, whereas Pre-development rates have been calculated using the Modified Rational Method. These rates are outlined in Table 1 below.

Return Period	Greenfield Runoff Rates (l/s/ha)	Pre-Development Discharge Rates (l/s)
1:1yr	0.49	3.2
QBAR	0.58	N/A
1:30yr	1.33	7.8
1:100yr	1.85	10.1

Table 1 - Existing discharge rates

## 3.0 Policy and Climate Change

- 3.1. The proposed development is smaller than 1000m<sup>2</sup> in total floor space making the proposed development a minor development.
- 3.2. The Royal Borough of Camden's Local Plan states under Policy CC3 that developments will be required to utilise Sustainable Drainage Systems in line with the drainage hierarchy to achieve a greenfield runoff rate where feasible.
- 3.3. Additionally, due to the development being located within a Critical Drainage Area, the proposed development will also require a Flood Risk Assessment addressing the potential risk of all sources of flooding.
- 3.4. In addition to Royal Borough of Camden's Local Plan Policy SI13 of the London Plan will also apply to this development.
- 3.5. From the online data provided by the Department for Environment Food & Rural Affairs states that the proposed development is in the London Catchment. This catchment will require developments to increase their peak discharge rate by 40% to allow for future climatic changes.

## 4.0 Flood Risk Assessment

- 4.1. **Risk of Tidal Flooding:** The site is located a significant distance inland and is elevated above predicted extreme tide levels. Consequently, the risk of flooding from this source is considered to be low.
- 4.2. **Risk of Flooding from Fluvial Sources:** Inspection of the EA's 'Flood Map for Planning' identifies that the site is situated in Flood Zone 1 and OS mapping shows that there are no main rivers, ordinary or manmade watercourses near to the site. Consequently, the risk of flooding to the site from rivers is considered to be low.
- 4.3. **Risk of Flooding from Pluvial Sources:** After inspection of the EA's 'Extent of flooding from Surface Water' it is evident that the site is not located within an area of very low risk of surface water flooding. The EA's mapping is a national dataset which can provide an indication of the surface water flood risk to an area.

The London Borough of Camden has also undertaken detailed modelling of the extent of surface water flooding within the borough. From this mapping it is evident that the proposed development is located outside of the modelling extent. Therefore, it is concluded that the risk of flooding from this source is low.

- 4.4. **Risk of Flooding from Sewer:** From the CCTV survey it is assumed that the public sewer network within Crediton Hill is a combined system. During an unlikely event of a combined sewer surcharging, i.e., following an extreme rainfall event or a blockage within the system, surcharging sewer water would likely leave the system at a location lower than the development. Nonetheless the proposed development will be fitted with a non-return valve and positive pump device for any basement drainage. Consequently, it is concluded that the risk of flooding from this source is low.
- 4.5. **Risk of Flooding from Groundwater:** From the mappings provided within the Strategic Flood Risk Assessment developed by London Borough of Camden, show that the development is in a location of low risk of groundwater flooding. Nonetheless, to reduce the risk of groundwater flooding to the proposed development a two-tier waterproofing system will be implemented within the basement construction, consisting out of a Type A or B system in combination with a Type C system. Consequently, with the inclusion of the mitigation measure the risk of flooding from this source is considered to be low.
- 4.6. The proposed development has been asset for all sources of flooding, and it has been concluded the risk is considered to be low from these sources.

## 5.0 Drainage Hierarchy

- 5.1. Policy S13 of the London Plan set out a drainage hierarchy to provide the most sustainable method of discharging surface water runoff from developments. Policy S13 states that the preferred method of managing surface water runoff is by utilising it on site. If this is not feasible, discharging it via infiltration, or discharging it into a watercourse should be considered. The least favourable method of discharging surface water runoff is to connect it into a public sewer system, with a surface water sewer being more favourable than a public foul sewer.
- 5.2. **Infiltration:** The underlying geology has been assessed using the mapping provided by the British geological Survey. From the mapping it is evident that the underlying geology is made up of London Clay formation with no overlying superficial deposit. London Clay is commonly associated with very low infiltration rates, due this discharging all surface water runoff via infiltration-based SuDS has been deemed not viable for this development.
- 5.3. **Connection into Watercourse:** There is no watercourse or drainage ditch located in close proximity to the development. Due to this discharging surface water runoff via a connection into a watercourse or drainage ditch has been discounted.
- 5.4. **Connection into Public Sewer:** From the CCTV survey it is evident that the existing development has an existing connection into the assumed public combined sewer running along Crediton Hill. The existing connection into this sewer will be utilised to discharge all surface water runoff from the development.

## 6.0 Surface Water Drainage Strategy

- 6.1. From Figure 1, it is evident that the proposed redline boundary only covers the extent of the development and does not include any open space or garden areas. Due to this there is limited opportunity to implement SuDS within the development.
- 6.2. The Architectural layout has suggested the utilisation of green roofs for the development. To provide benefits regarding water quantity controls a minimum of 80mm sub-base should be provided. These are designed by a specialist to delay the peak discharge rate by slowing down infiltrating surface water. The green roof should be design with an adequate drainage layer to avoid stagnation within the sub-base, additionally and overflow should be designed to reduce the risk of overflowing surface water runoff in the event the downpipe becomes blocked. In Figure 2 below the areas of green roof have been shown. The proposed green roof will also provide a betterment regarding biodiversity and water quality.

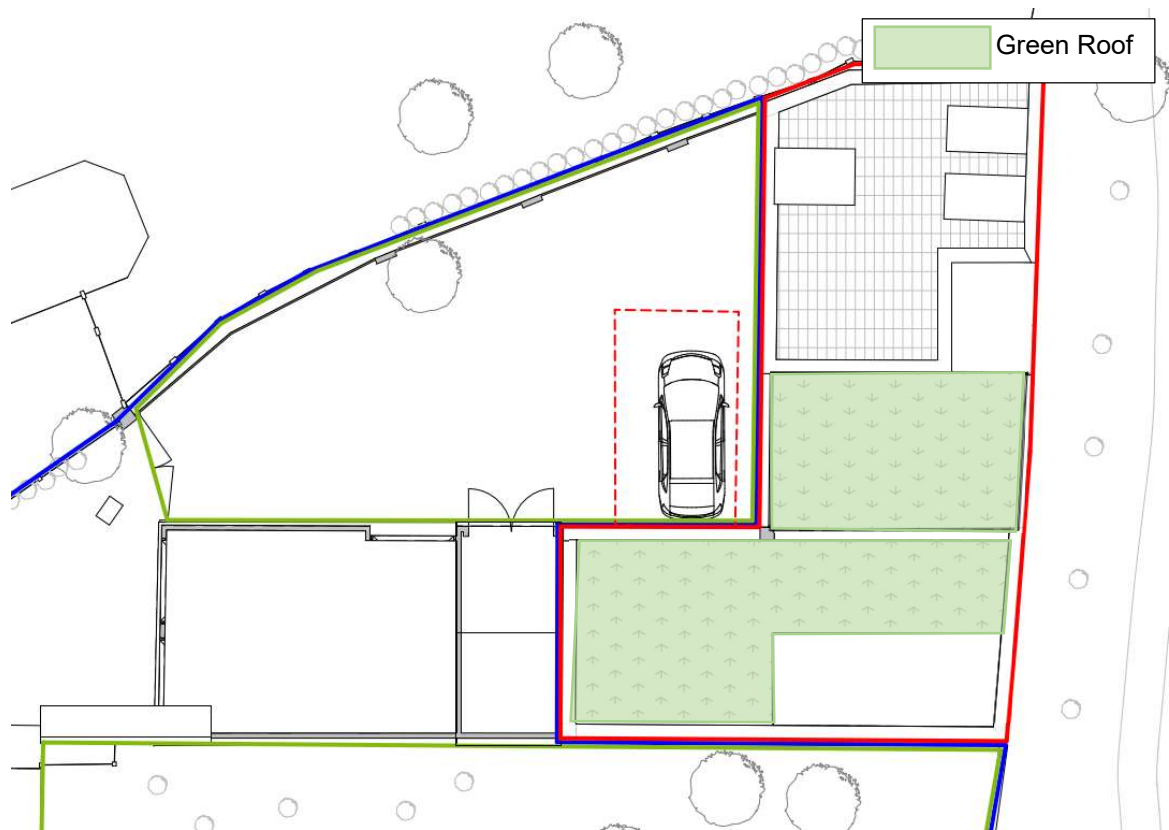


Figure 2 - Location of proposed green roofs.

- 6.3. The proposed drainage system has been modelled using the industry standard Causeway Flow+ software. The undertaken hydraulic calculations use synthetic rainfall data derived using the Flood Estimation Report (FSR). A 40% allowance in rainfall has been made to allow for any future climatic changes.
- 6.4. To represent the green roof's ability to delay peak discharge rates within the hydraulic model, a time of entry of 10 minutes for the green roof catchments has been used.
- 6.5. In Table 2 the proposed and existing discharge rates have been provided.

Return Period	Greenfield Runoff Rates (l/s)	Proposed Runoff Rates (l/s)
1:1yr	3.2	2.3
1:30yr	7.8	5.6
1:100yr	10.1	7.2
1:100yr+CC	14.2	9.6

*Table 2 – Pre & post discharge rates.*

6.6. Based on the above table and the included results of the hydraulic model it is evident that the proposed drainage system can accommodate up to and including the design event. Additionally, with the inclusion of the proposed green roofs the proposed development will provide a reduction in discharge rates when compared to the existing situation.



## 7.0 Management and Maintenance

- 7.1. The proposed drainage system will be located within a private garden; therefore, the owner of the development will be required to manage and maintain the proposed SuDS.
- 7.2. Typical management requirements have been outlined in Table 4 below. The management company should also refer to any manufacture’s specific management and maintenance requirements.

Drainage Asset	Responsible Organisation	Maintenance Work	Frequency
General Pipework and manholes	Private ownership	Inspect pipework and manholes and clear any blockages; Repair to any defects over long-term usage	Annually or after severe storm events
Green Roof	Private ownership	Inspect all components including soil substrate, vegetation, drains, irrigation systems (if applicable), membranes and roof structure for proper operation, integrity of waterproofing and structural stability	Annually or after severe storm events
		Remove fallen leaves and debris from deciduous plant foliage	Six monthly or as required
		Remove nuisance and invasive vegetation, including weeds	Six monthly or as required
		If erosion channels are evident, these should be stabilised with extra soil substrate like the original material, and sources of erosion damage should be identified and controlled	As required
		Inspect underside of roof for evidence of leakage	Annually and after severe Storms

Table 3 – Maintenance Schedule

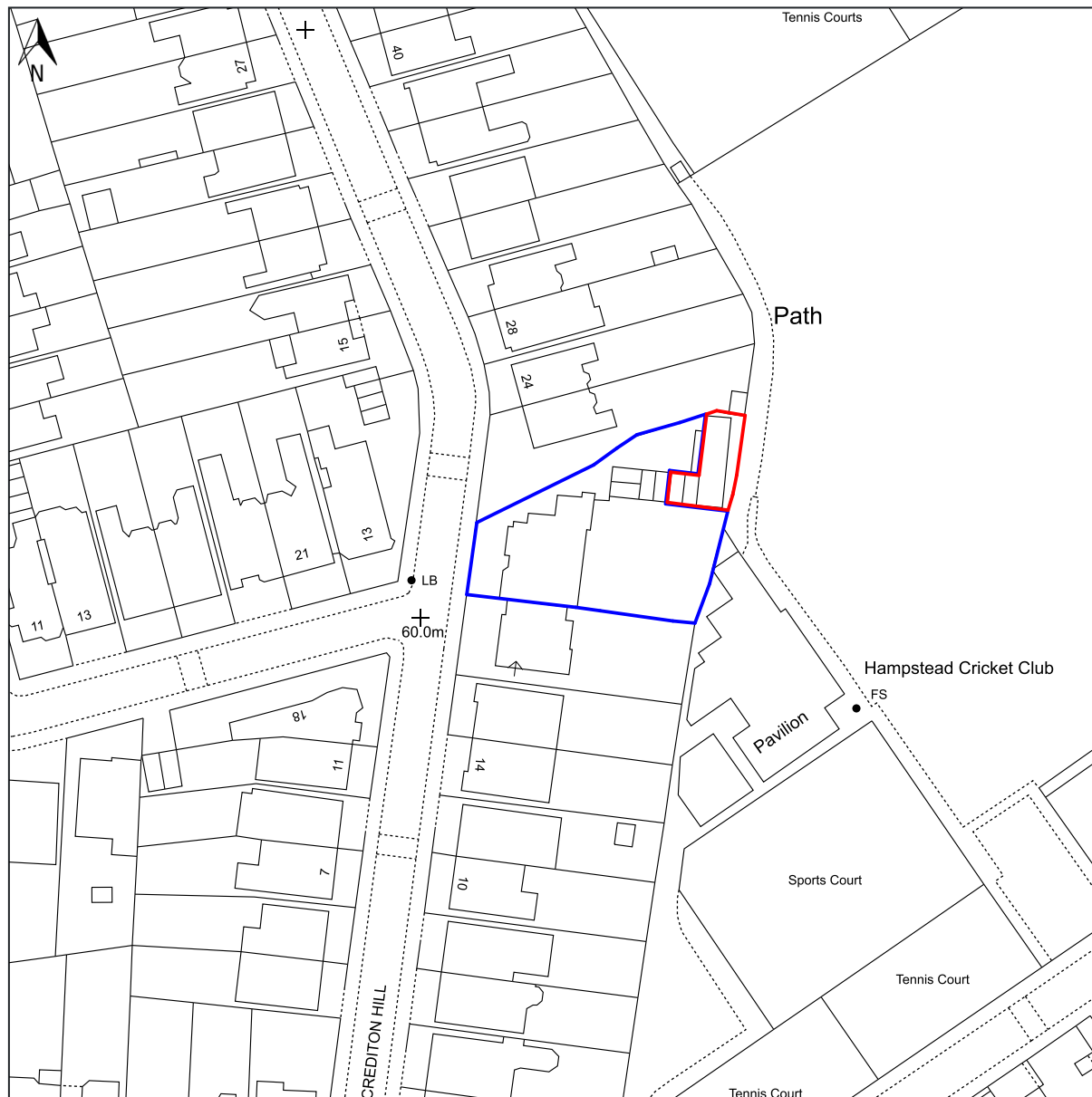
- 7.3. The manufacturers management and maintenance requirements for the green roof should be provided to the owners and should be followed for the lifetime of the development.

## 8.0 Summary

- 8.1. This report has been undertaken to be accompanied for the planning application for the development located at land off 20 Crediton Hill, Camden, London, NW6 1HP.
- 8.2. As part of the assessment, the risk of flooding from a wide range of sources has been assessed, it has been identified that the risk of the proposed development is low. In order to minimise the impact of offsite flooding from the proposed development, the opportunities for managing surface water at the site have been analysed.
- 8.3. The report outlines that the most viable method of discharging surface water runoff is via the existing connection into the public combined sewer system.
- 8.4. Due to the limited space within the redline boundary, there has been a limited possibility to include SuDS within the development. Nonetheless green roofs have been proposed for the roof area to provide a reduction in peak runoff rates and increase biodiversity within the development.
- 8.5. Typical management and maintenance requirements have been included within this report. Before commissioning the development, a manual outlining the management and maintenance requirements for each proposed SuDS system should be provided to the end owner and user.

# APPENDIX A

## ARCHITECTURAL DRAWINGS



**01** Location Plan  
Scale 1:1250

S A

10b Branch Place  
London N1 5PH  
p: 0207 686 3445  
e: info@scenarioarchitecture.com  
w: www.scenarioarchitecture.com

Project Name:  
**20 Crediton Hill**

Client:  
**Sendi & Daniel Young**

Site Location:  
**20 Crediton Hill, London NW6  
1HP London UK**

Drawing not to be used other than the purpose for which it was prepared. It's supplied without liability for errors or omissions. All dimensions are to be checked on site. This drawing is to be read in conjunction with all other drawings. Notes on this drawing will apply to all other drawings where a similar position exists.

Scale @ A4 <b>1:1250</b>	Project No. <b>168</b>
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Drawing Name  
**Location Plan**

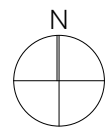
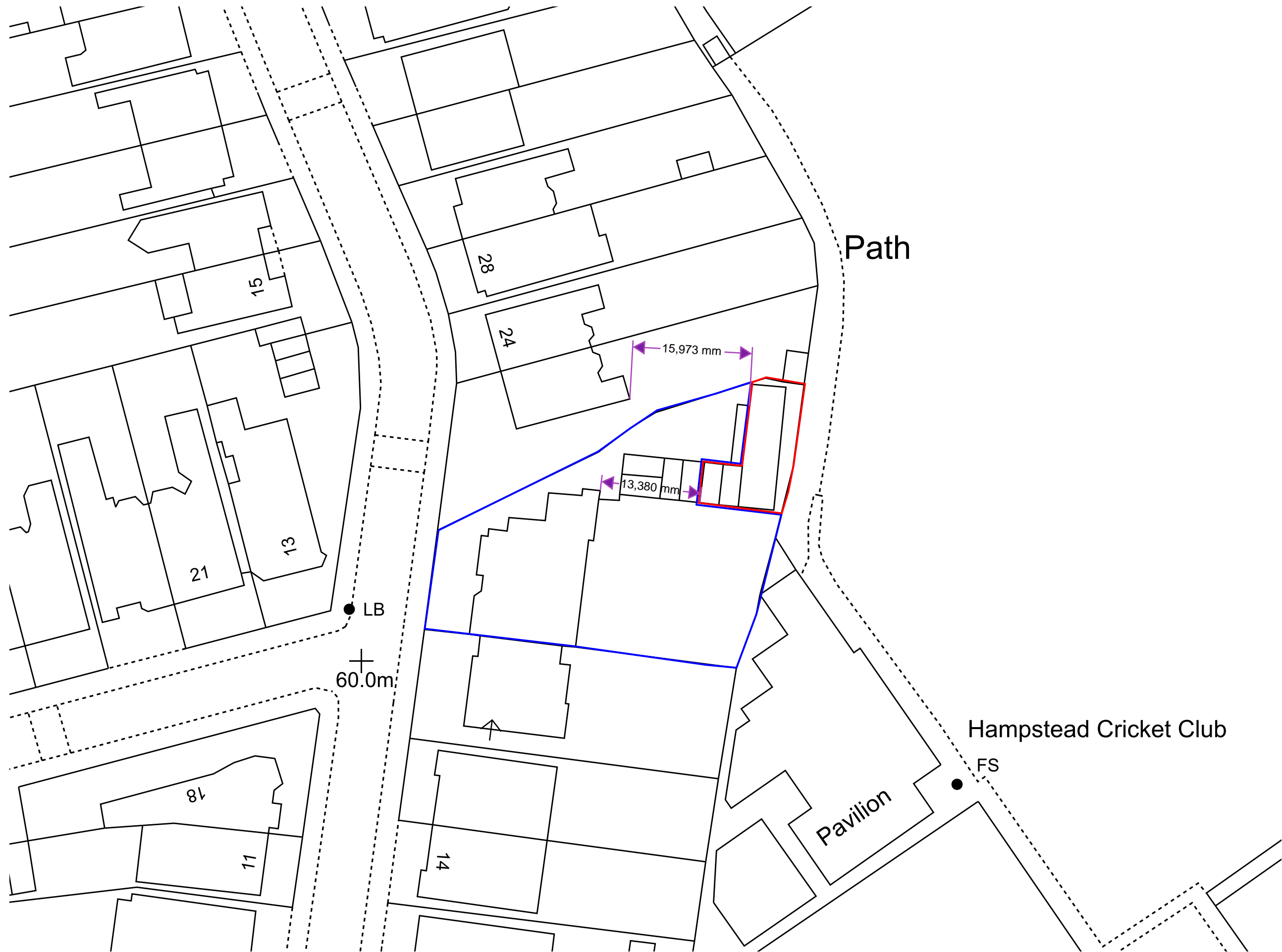
Drawing Number	Rev
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**LO-A-01**

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EXISTING  
Not For Construction

Rev	Date



S/A

10b Branch Place  
London N1 5PH  
p: 0207 686 3445  
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Scale @ A3  
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Project No.  
**168**

Drawing Name  
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Drawing Number  
**LO-A-02**

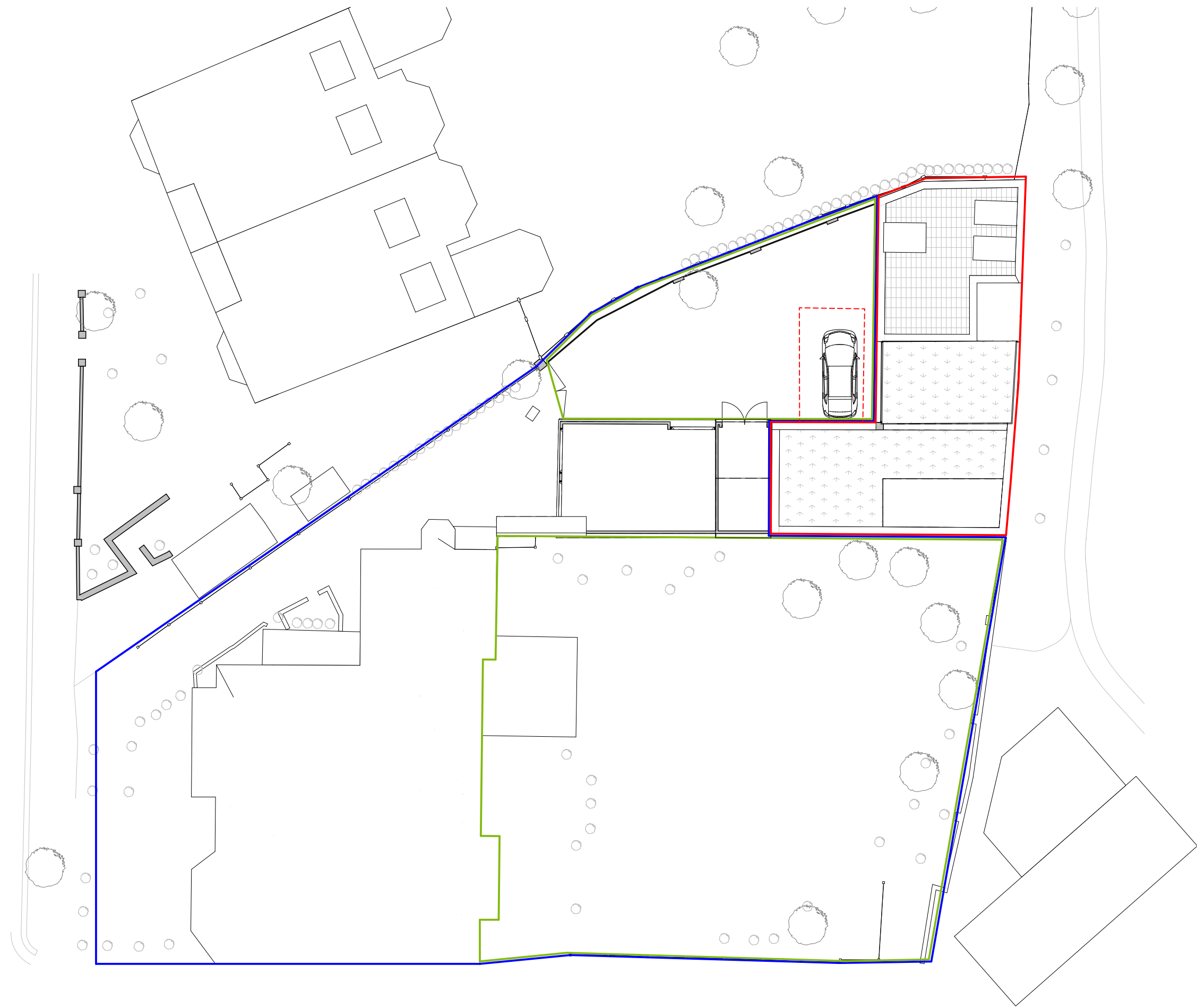
Rev

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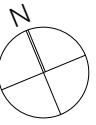
BIMcloud: scenarioarchitecture - BIMcloud as a Service | 10b Branch Place, London N1 5PH | 0207 686 3445 | info@scenarioarchitecture.com

Rev	Date



**LEGEND**

- Area of Freehold Site and Premises subject of Application
- Ownership form below existing ground level
- Adjacent land over which Application Site and Premises have the established full unconditional legal rights of pedestrian and vehicular access, parking/garaging, all other general uses, full use of Communal Gardens, own Services: Gas, Mains Water, Mains Electricity, Drainage, Cable Services, communal General Waste and Recycle Waste Bin facilities, own CCTV Security system
- Full use of Communal Gardens



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Site Location:  
**20 Crediton Hill, London NW6  
1HP London UK**

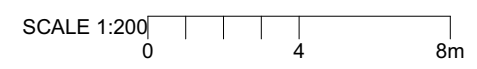
Drawing not to be used other than the purpose for which it was prepared. It's supplied without liability for errors or omissions. All dimensions are to be checked on site. This drawing is to be read in conjunction with all other drawings. Notes on this drawing will apply to all other drawings where a similar position exists.

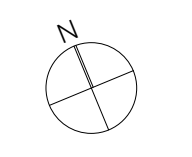
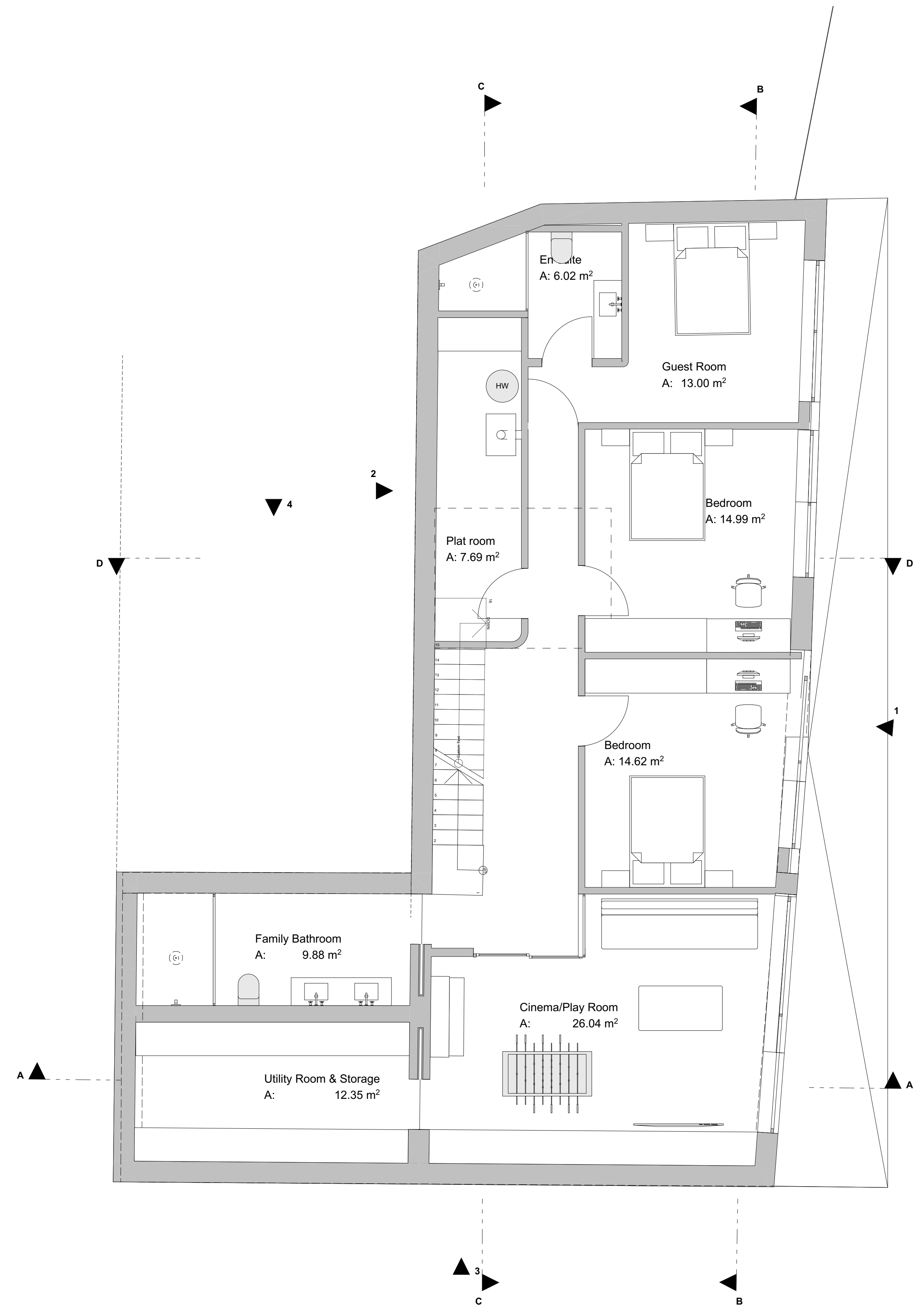
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Drawing Name  
**Site Plan**

Drawing Number Rev

**PR-A0.01**





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Client:  
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Scale @ A1  
**1:50**

Project No.  
**168**

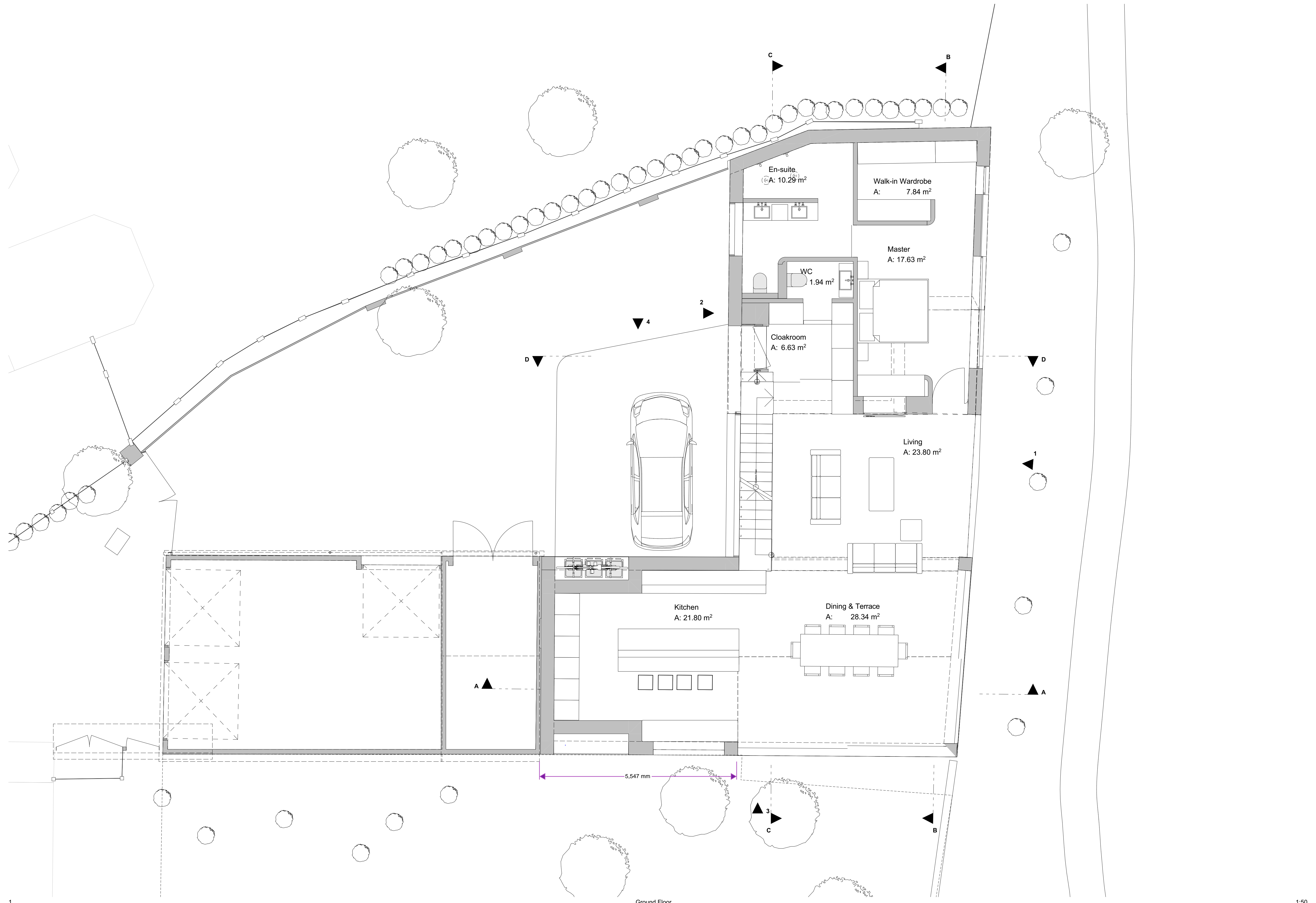
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**Proposed Basement Floor Plan**

Drawing Number Rev

**PR-A1.01**

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1

Ground Floor

1:50

SCALE 1:50  
0 1000 2000mm

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Scale @ A1  
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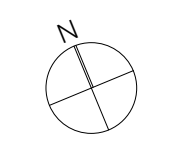
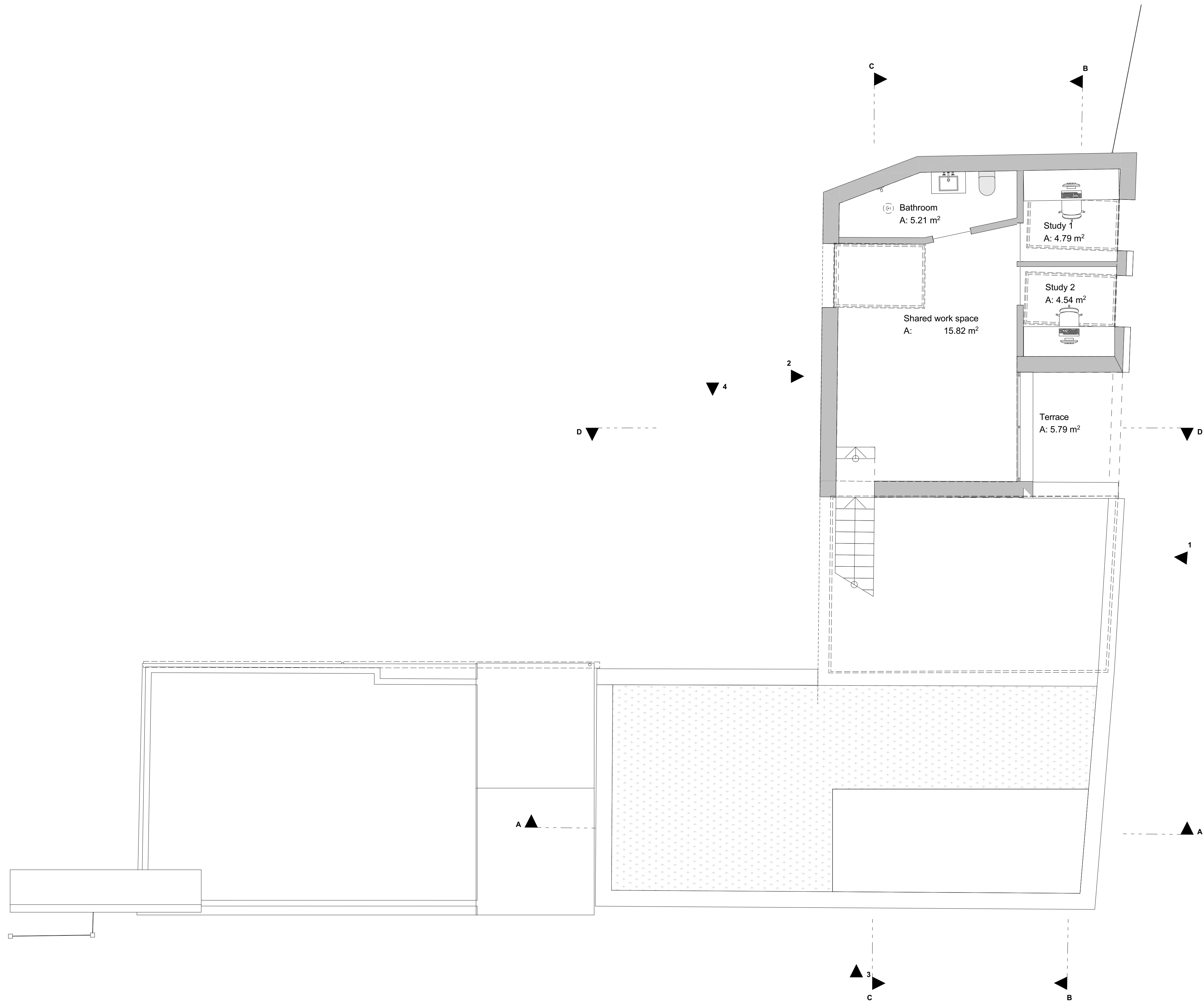
Project No.  
**168**

Drawing Name  
**Proposed Ground Floor Plan**

Drawing Number | Rev  
**PR-A1.02**

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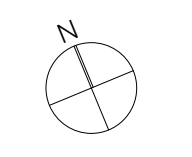
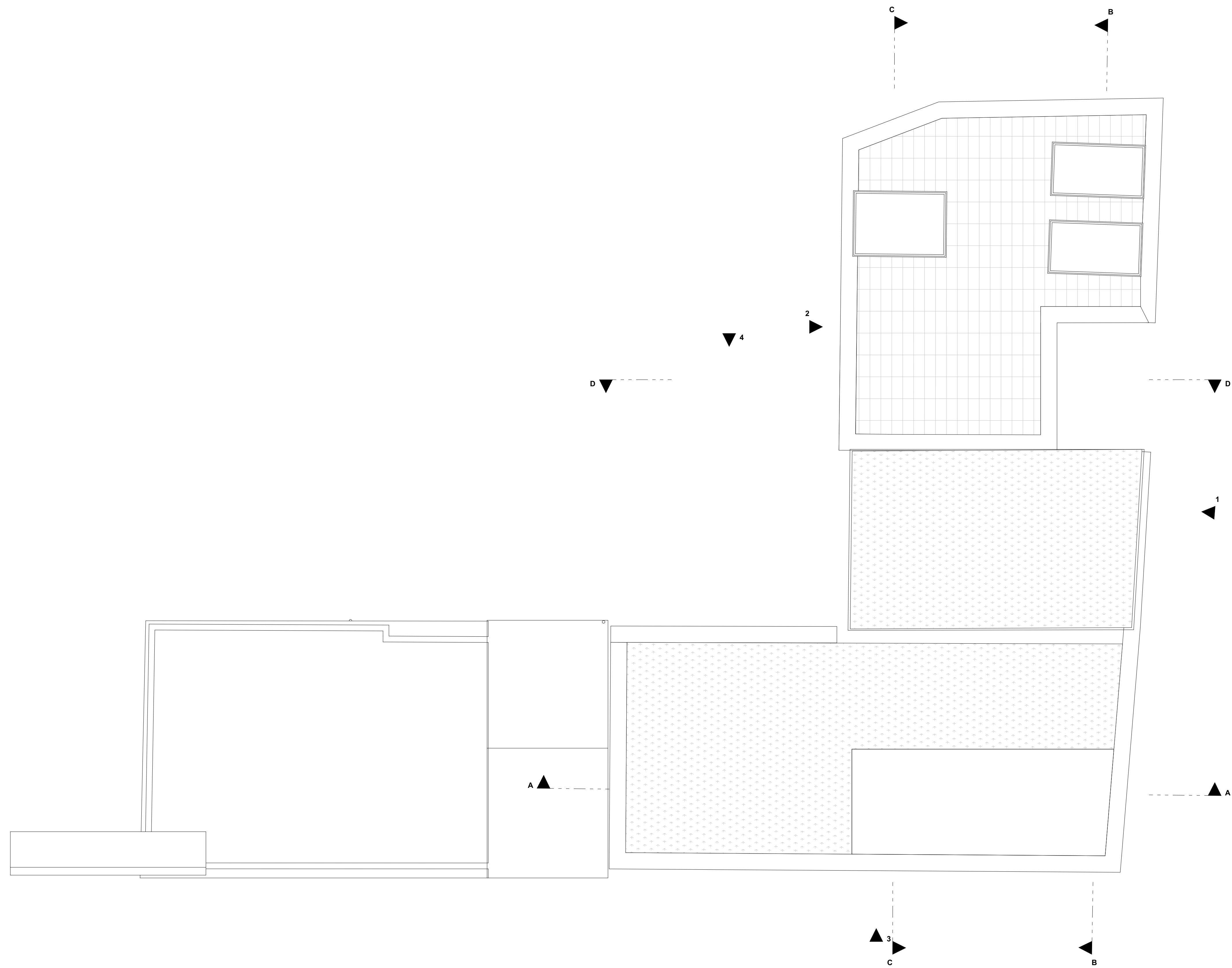
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Project No.  
**168**

Drawing Name  
**Proposed First Floor Plan**

Drawing Number  
**PR-A1.03**

Rev



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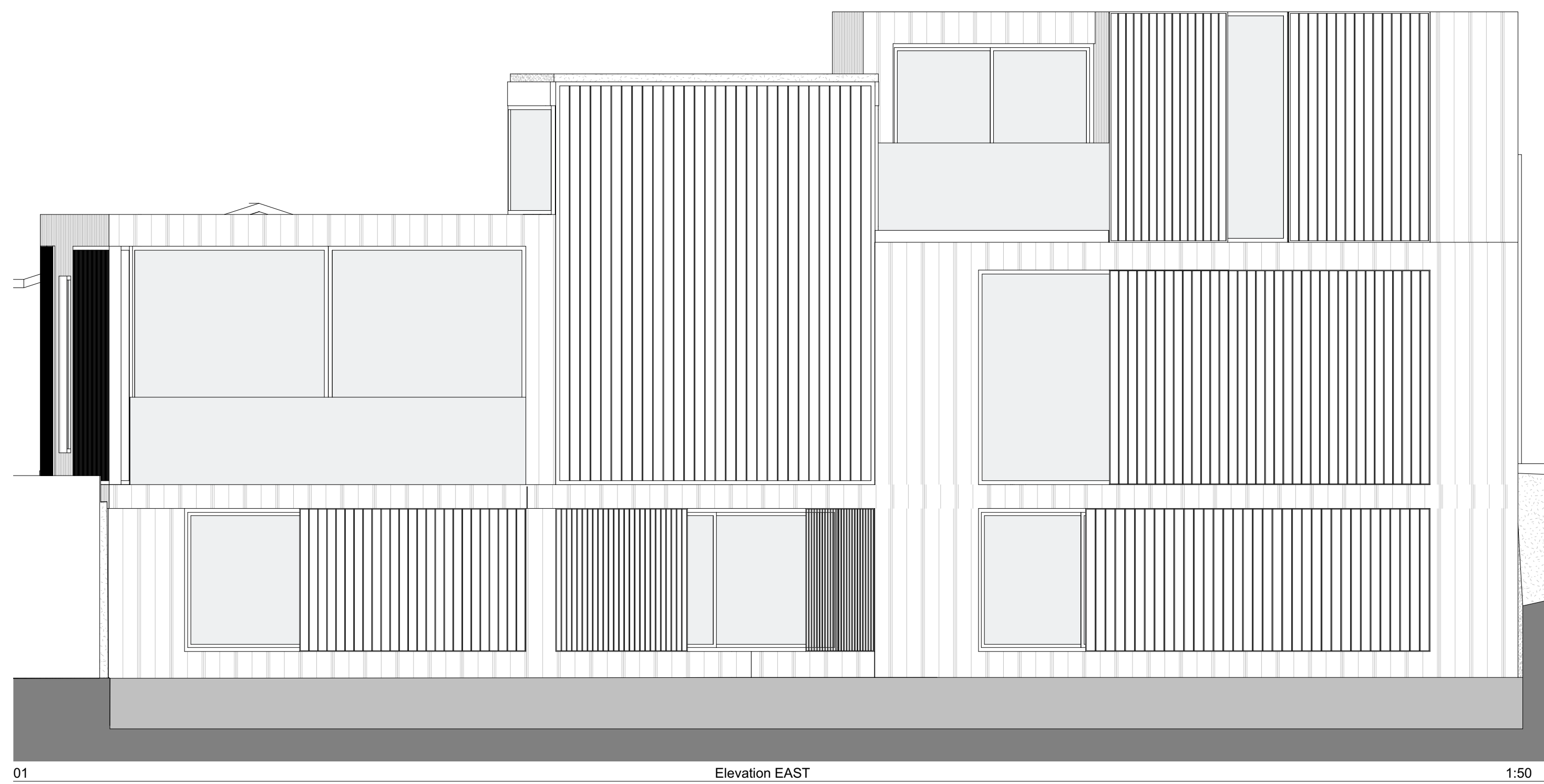
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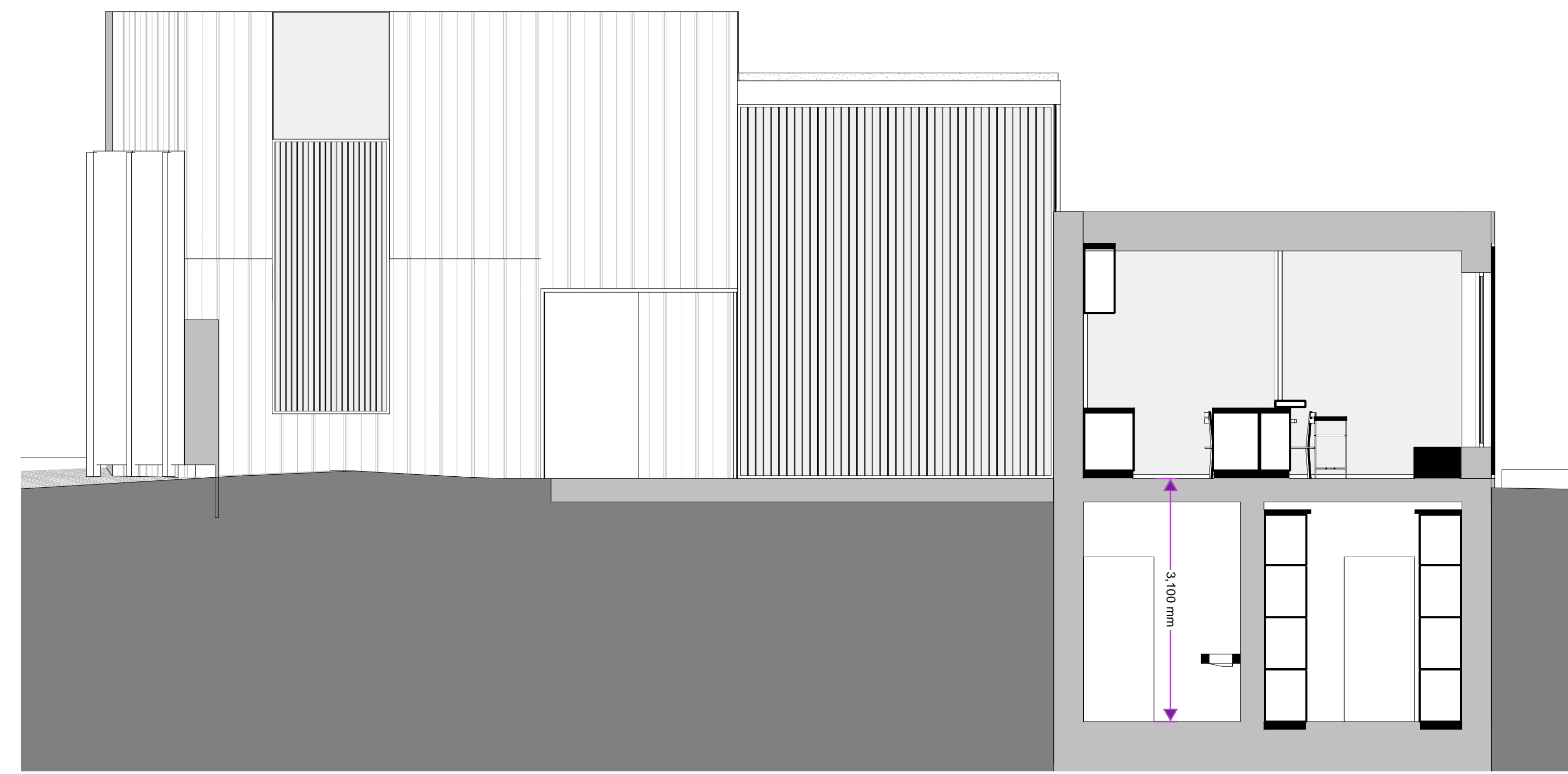
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Drawing Number  
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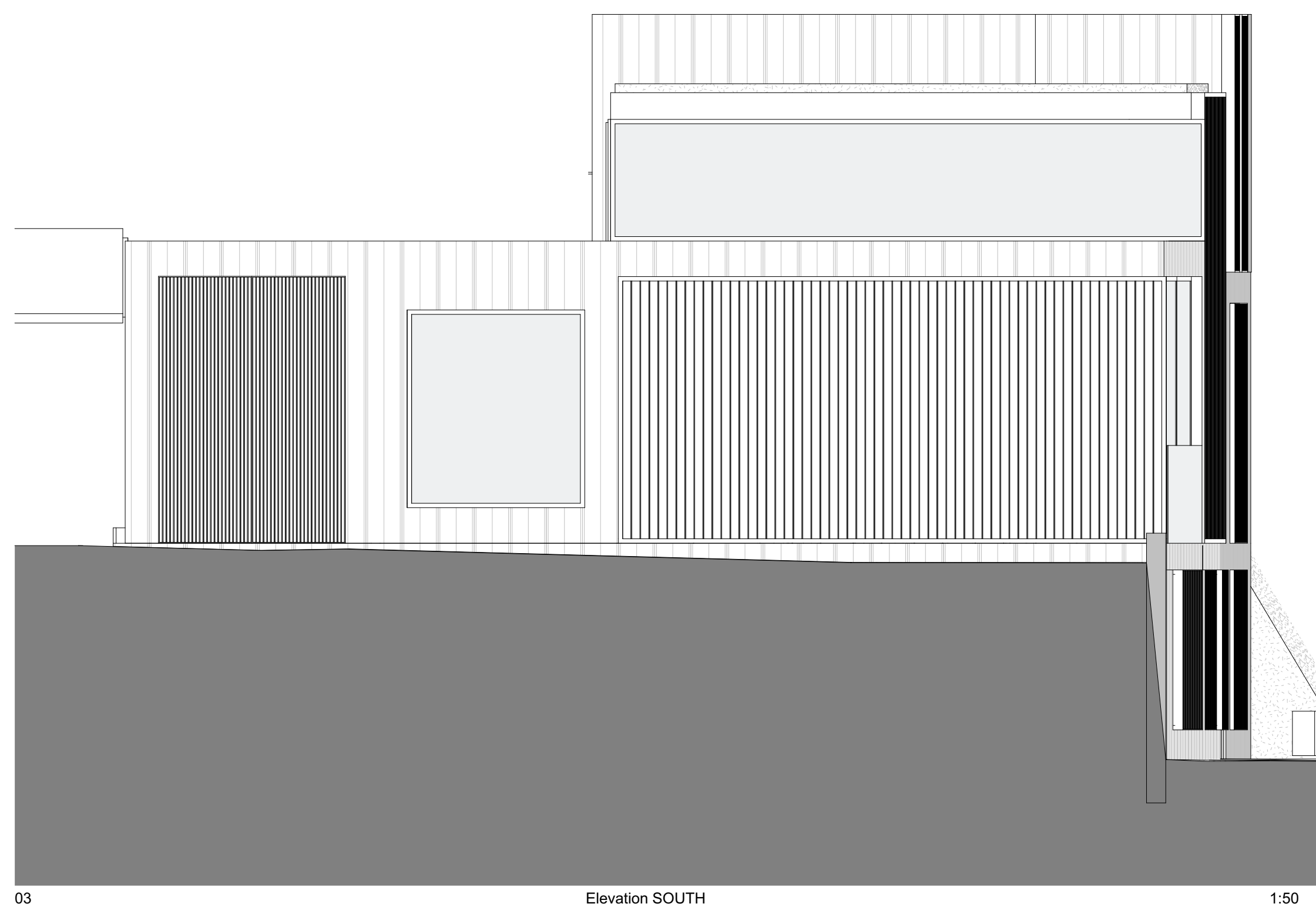
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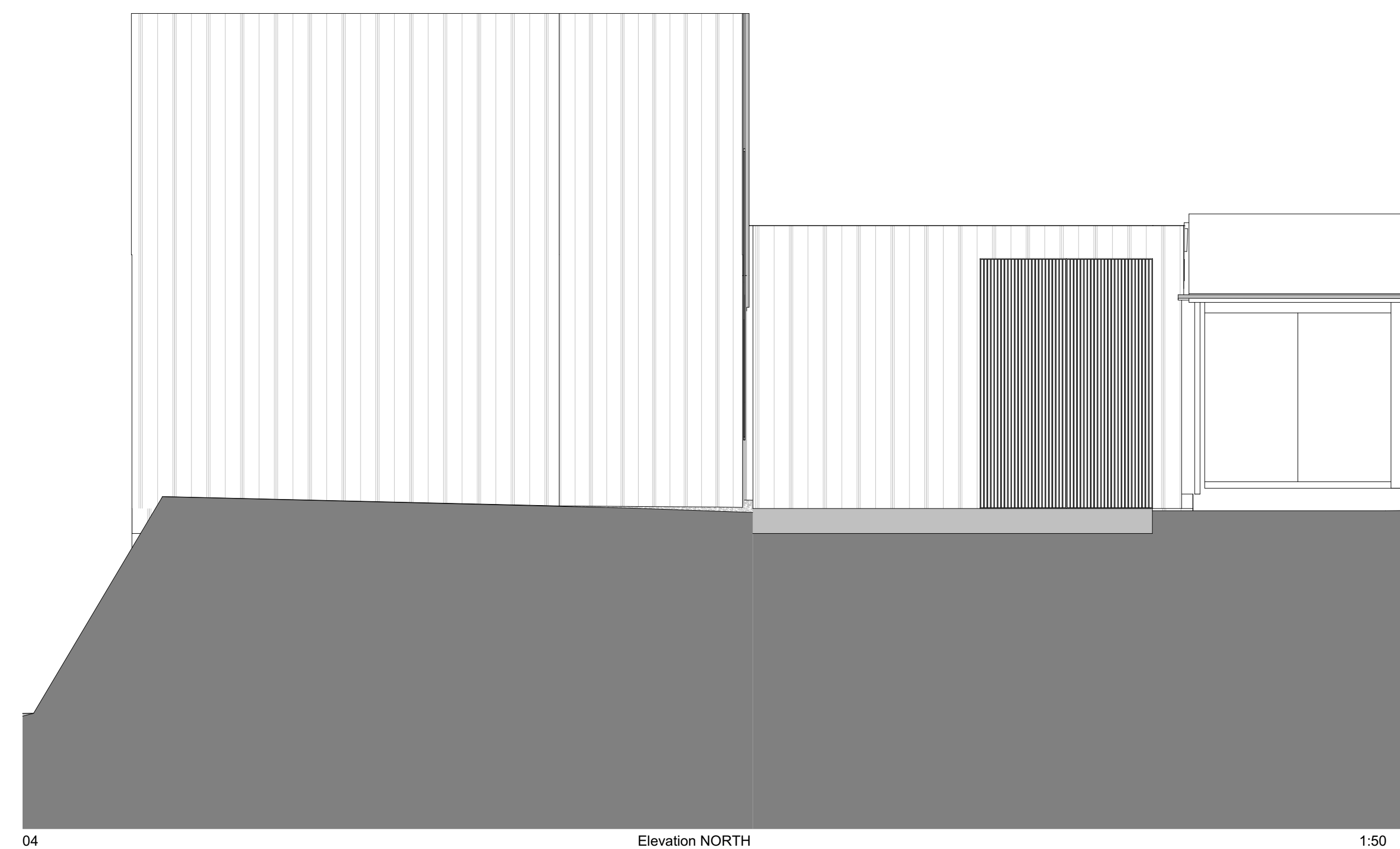
01 Elevation EAST 1:50



02 Elevation WEST 1:50



03 Elevation SOUTH 1:50



04 Elevation NORTH 1:50

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**S/A**  
106 Branch Place  
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Project Name:  
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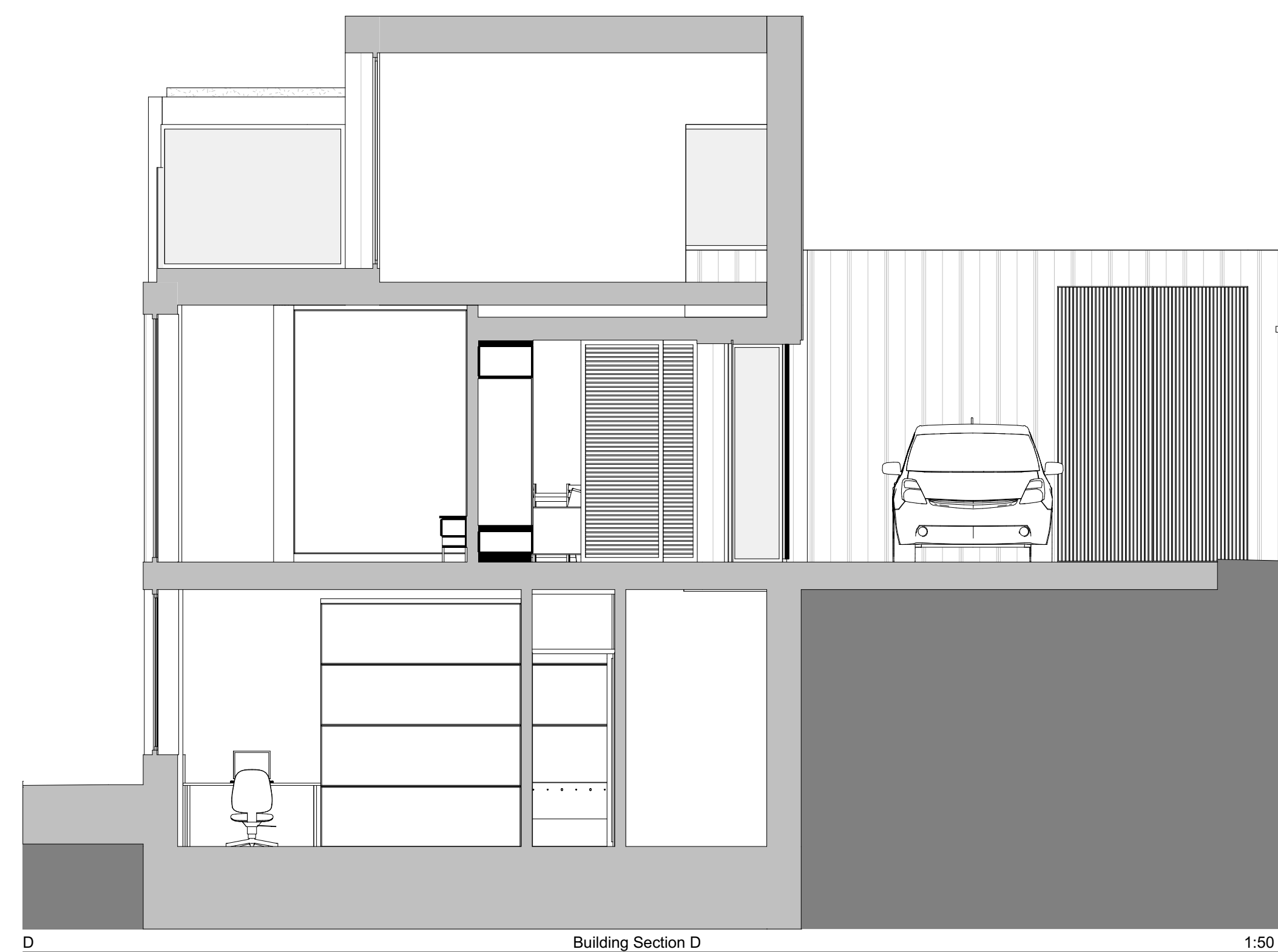
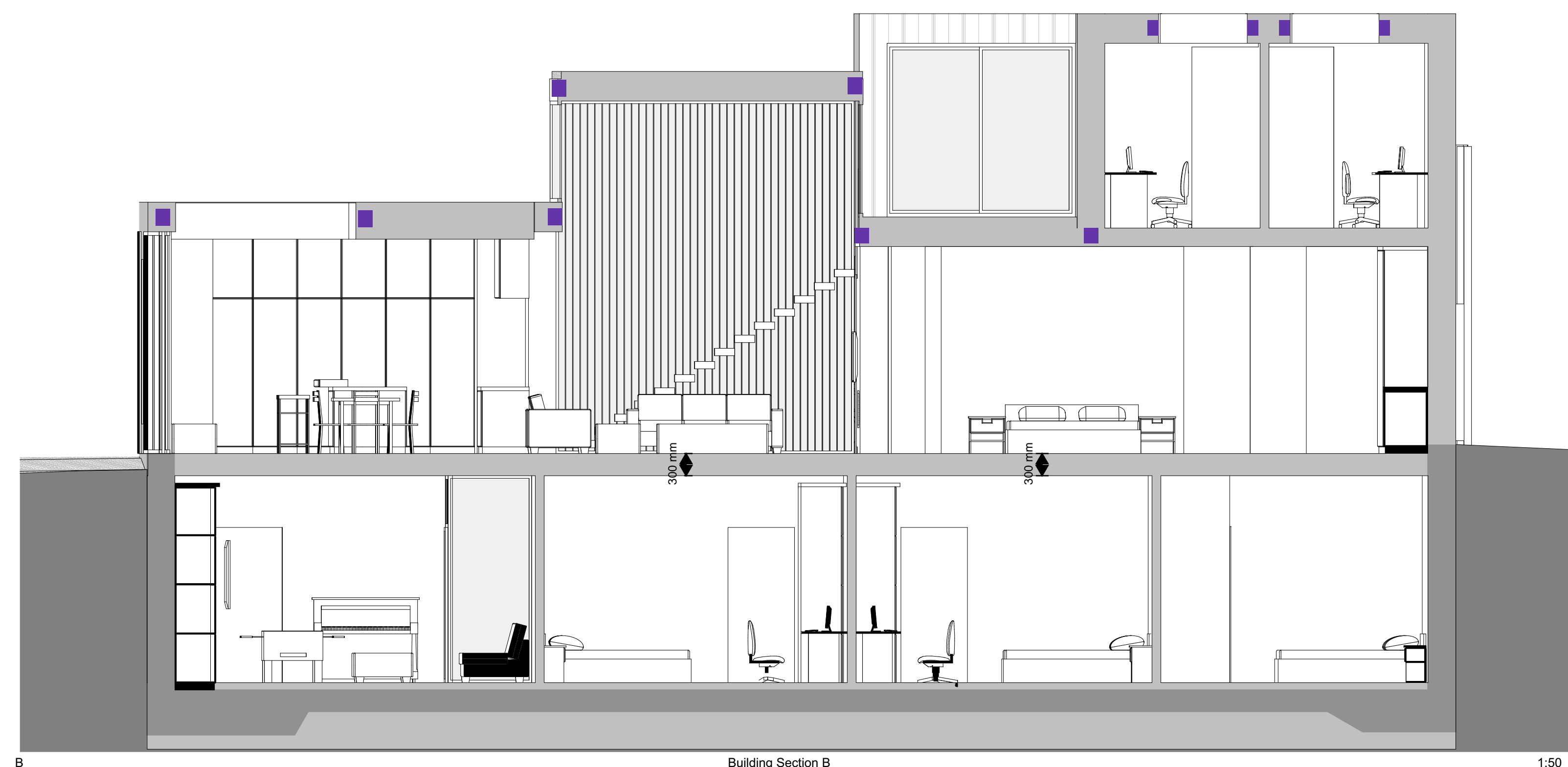
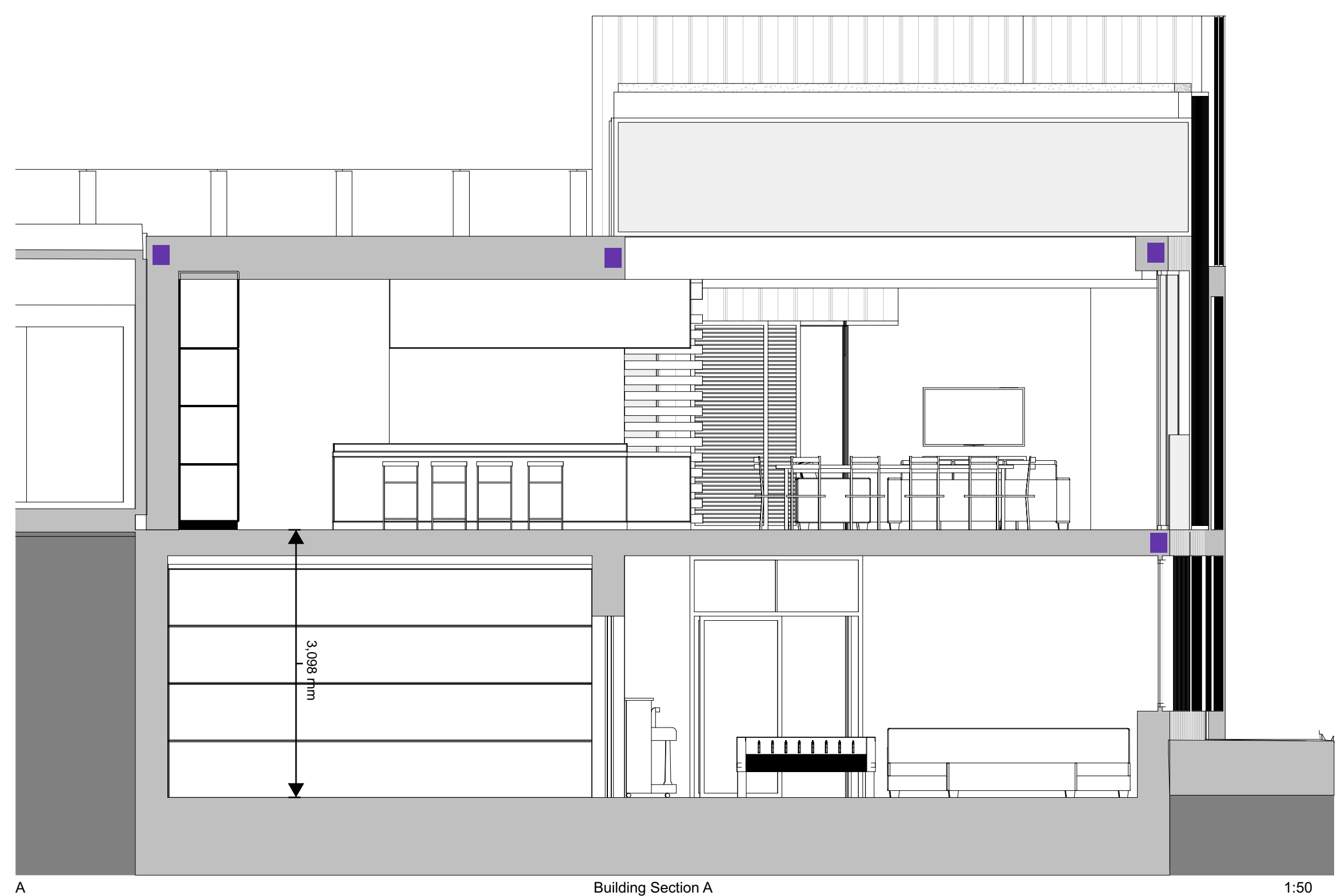
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Project No.  
**168**

Drawing Name  
**Proposed Elevations**

Drawing Number  
**PR-A2.01**

Rev



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Scale @ A1  
**1:50** Project No.  
**168**

Drawing Name  
**Proposed Sections**

Drawing Number Rev  
**PR-A3.01**

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# APPENDIX B1

## CALCULATIONS: Greenfield rates

Print

Close Report



# Greenfield runoff rate estimation for sites

www.uksubs.com | Greenfield runoff tool

Calculated by:

Site name:

Site location:

### Site Details

Latitude:

Longitude:

Reference:

Date:

This is an estimation of the greenfield runoff rates that are used to meet normal best practice criteria in line with Environment Agency guidance "Rainfall runoff management for developments", SC030219 (2013), the SuDS Manual C753 (Ciria, 2015) and the non-statutory standards for SuDS (Defra, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Runoff estimation approach

### Site characteristics

Total site area (ha):

### Methodology

Q<sub>BAR</sub> estimation method:

SPR estimation method:

Soil characteristics	Default	Edited
SOIL type:	<input type="text" value="4"/>	<input type="text" value="4"/>
HOST class:	<input type="text" value="N/A"/>	<input type="text" value="N/A"/>
SPR/SPRHOST:	<input type="text" value="0.47"/>	<input type="text" value="0.47"/>

### Hydrological characteristics

	Default	Edited
SAAR (mm):	<input type="text" value="650"/>	<input type="text" value="650"/>
Hydrological region:	<input type="text" value="6"/>	<input type="text" value="6"/>
Growth curve factor 1 year:	<input type="text" value="0.85"/>	<input type="text" value="0.85"/>
Growth curve factor 30 years:	<input type="text" value="2.3"/>	<input type="text" value="2.3"/>
Growth curve factor 100 years:	<input type="text" value="3.19"/>	<input type="text" value="3.19"/>
Growth curve factor 200 years:	<input type="text" value="3.74"/>	<input type="text" value="3.74"/>

### Notes

#### (1) Is Q<sub>BAR</sub> < 2.0 l/s/ha?

When Q<sub>BAR</sub> is < 2.0 l/s/ha then limiting discharge rates are set at 2.0 l/s/ha.

#### (2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consent for discharge is usually set at 5.0 l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set where the blockage risk is addressed by using appropriate drainage elements.

#### (3) Is SPR/SPRHOST ≤ 0.3?

Where groundwater levels are low enough the use of soakaways to avoid discharge offsite would normally be preferred for disposal of surface water runoff.

Greenfield runoff rates	Default	Edited
Q <sub>BAR</sub> (l/s):	<input type="text" value="0.58"/>	<input type="text" value="0.58"/>
1 in 1 year (l/s):	<input type="text" value="0.49"/>	<input type="text" value="0.49"/>
1 in 30 years (l/s):	<input type="text" value="1.33"/>	<input type="text" value="1.33"/>
1 in 100 year (l/s):	<input type="text" value="1.85"/>	<input type="text" value="1.85"/>
1 in 200 years (l/s):	<input type="text" value="2.17"/>	<input type="text" value="2.17"/>

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at [www.uksuds.com](http://www.uksuds.com). The use of this tool is subject to the UK SuDS terms and conditions and licence agreement , which can both be found at [www.uksuds.com/terms-and-conditions.htm](http://www.uksuds.com/terms-and-conditions.htm). The outputs from this tool are estimates of greenfield runoff rates. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for the use of this data in the design or operational characteristics of any drainage scheme.

# APPENDIX B2

## CALCULATIONS: Pre-Development rates





**Design Settings**

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	100	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	40	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.650
Ratio-R	0.400	Preferred Cover Depth (m)	0.000
CV	1.000	Include Intermediate Ground	✓
Time of Entry (mins)	4.00	Enforce best practice design rules	✓

**Nodes**

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
Modified Rational Method	0.016	4.00	10.000	1900	0.000	0.000	1.000
Outlet			9.900	1900	10.000	0.000	1.900

**Links**

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1	Modified Rational Method	Outlet	10.000	0.600	9.000	8.000	1.000	10.0	1000	4.02	50.0

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)	Pro Depth (mm)	Pro Velocity (m/s)
1	10.602	8327.0	4.0	0.000	0.900	0.016	0.0	17	1.443

**Pipeline Schedule**

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1	10.000	10.0	1000	Circular	10.000	9.000	0.000	9.900	8.000	0.900

Link	US Node	Dia (mm)	Node Type	MH Type	DS Node	Dia (mm)	Node Type	MH Type
1	Modified Rational Method	1900	Manhole	Adoptable	Outlet	1900	Manhole	Adoptable

**Manhole Schedule**

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
Modified Rational Method	0.000	0.000	10.000	1.000	1900				
Outlet	10.000	0.000	9.900	1.900	1900		0 1	9.000	1000
							1 1	8.000	1000



**Simulation Settings**

Rainfall Methodology	FSR	Analysis Speed	Normal
FSR Region	England and Wales	Skip Steady State	x
M5-60 (mm)	20.000	Drain Down Time (mins)	240
Ratio-R	0.400	Additional Storage (m <sup>3</sup> /ha)	20.0
Summer CV	1.000	Check Discharge Rate(s)	x
Winter CV	1.000	Check Discharge Volume	x

**Storm Durations**

15	60	180	360	600	960	2160	4320	7200	10080
30	120	240	480	720	1440	2880	5760	8640	

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
30	0	0	0
100	0	0	0
100	40	0	0



**Results for 1 year Critical Storm Duration. Lowest mass balance: 100.00%**

<b>Node Event</b>	<b>US Node</b>	<b>Peak (mins)</b>	<b>Level (m)</b>	<b>Depth (m)</b>	<b>Inflow (l/s)</b>	<b>Node Vol (m<sup>3</sup>)</b>	<b>Flood (m<sup>3</sup>)</b>	<b>Status</b>
15 minute summer	Modified Rational Method	10	9.016	0.016	3.2	0.0513	0.0000	OK
15 minute summer	Outlet	10	8.014	0.014	3.2	0.0000	0.0000	OK

<b>Link Event (Upstream Depth)</b>	<b>US Node</b>	<b>Link</b>	<b>DS Node</b>	<b>Outflow (l/s)</b>	<b>Velocity (m/s)</b>	<b>Flow/Cap</b>	<b>Link Vol (m<sup>3</sup>)</b>	<b>Discharge Vol (m<sup>3</sup>)</b>
15 minute summer	Modified Rational Method	1	Outlet	3.2	1.363	0.000	0.0235	1.2



**Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%**

<b>Node Event</b>	<b>US Node</b>	<b>Peak (mins)</b>	<b>Level (m)</b>	<b>Depth (m)</b>	<b>Inflow (l/s)</b>	<b>Node Vol (m<sup>3</sup>)</b>	<b>Flood (m<sup>3</sup>)</b>	<b>Status</b>
15 minute summer	Modified Rational Method	10	9.024	0.024	7.8	0.0767	0.0000	OK
15 minute summer	Outlet	10	8.024	0.024	7.8	0.0000	0.0000	OK

<b>Link Event (Upstream Depth)</b>	<b>US Node</b>	<b>Link</b>	<b>DS Node</b>	<b>Outflow (l/s)</b>	<b>Velocity (m/s)</b>	<b>Flow/Cap</b>	<b>Link Vol (m<sup>3</sup>)</b>	<b>Discharge Vol (m<sup>3</sup>)</b>
15 minute summer	Modified Rational Method	1	Outlet	7.8	1.718	0.001	0.0454	3.0



**Results for 100 year Critical Storm Duration. Lowest mass balance: 100.00%**

<b>Node Event</b>	<b>US Node</b>	<b>Peak (mins)</b>	<b>Level (m)</b>	<b>Depth (m)</b>	<b>Inflow (l/s)</b>	<b>Node Vol (m<sup>3</sup>)</b>	<b>Flood (m<sup>3</sup>)</b>	<b>Status</b>
15 minute summer	Modified Rational Method	10	9.027	0.027	10.1	0.0862	0.0000	OK
15 minute summer	Outlet	10	8.026	0.026	10.1	0.0000	0.0000	OK

<b>Link Event (Upstream Depth)</b>	<b>US Node</b>	<b>Link</b>	<b>DS Node</b>	<b>Outflow (l/s)</b>	<b>Velocity (m/s)</b>	<b>Flow/Cap</b>	<b>Link Vol (m<sup>3</sup>)</b>	<b>Discharge Vol (m<sup>3</sup>)</b>
15 minute summer	Modified Rational Method	1	Outlet	10.1	1.861	0.001	0.0543	3.9



**Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%**

<b>Node Event</b>	<b>US Node</b>	<b>Peak (mins)</b>	<b>Level (m)</b>	<b>Depth (m)</b>	<b>Inflow (l/s)</b>	<b>Node Vol (m<sup>3</sup>)</b>	<b>Flood (m<sup>3</sup>)</b>	<b>Status</b>
15 minute summer	Modified Rational Method	10	9.032	0.032	14.2	0.1008	0.0000	OK
15 minute summer	Outlet	10	8.030	0.030	14.2	0.0000	0.0000	OK

<b>Link Event (Upstream Depth)</b>	<b>US Node</b>	<b>Link</b>	<b>DS Node</b>	<b>Outflow (l/s)</b>	<b>Velocity (m/s)</b>	<b>Flow/Cap</b>	<b>Link Vol (m<sup>3</sup>)</b>	<b>Discharge Vol (m<sup>3</sup>)</b>
15 minute summer	Modified Rational Method	1	Outlet	14.2	2.061	0.002	0.0689	5.5

# APPENDIX B3

## CALCULATIONS: Proposed rates



**Design Settings**

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	100	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	40	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.960
Ratio-R	0.400	Preferred Cover Depth (m)	0.750
CV	1.000	Include Intermediate Ground	✓
Time of Entry (mins)	4.00	Enforce best practice design rules	✓

**Nodes**

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
green roof 1	0.006	10.00	10.000	1200	0.000	0.000	0.850
Green roof 2	0.003	10.00	10.000	1200	0.000	10.000	0.850
3	0.007	4.00	10.000	1200	0.000	20.000	0.850
Combined manhole			9.000	1200	10.943	9.416	0.850
5			9.000	1200	17.016	9.374	0.953

**Links**

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.000	3	Combined manhole	15.224	0.600	9.150	8.150	1.000	15.2	100	4.13	50.0
3.000	Green roof 2	Combined manhole	10.959	0.600	9.150	8.150	1.000	11.0	100	10.08	50.0
2.000	green roof 1	Combined manhole	14.436	0.600	9.150	8.150	1.000	14.4	100	10.12	50.0
1.001	Combined manhole	5	6.073	0.600	8.150	8.047	0.103	59.0	100	10.22	50.0

Name	Vel (m/s)	Cap (l/s)	Flow (l/s)	US Depth (m)	DS Depth (m)	Σ Area (ha)	Σ Add Inflow (l/s)	Pro Depth (mm)	Pro Velocity (m/s)
1.000	1.990	15.6	1.8	0.750	0.750	0.007	0.0	23	1.328
3.000	2.347	18.4	0.8	0.750	0.750	0.003	0.0	14	1.134
2.000	2.044	16.1	1.5	0.750	0.750	0.006	0.0	21	1.280
1.001	1.005	7.9	4.0	0.750	0.853	0.016	0.0	50	1.008

**Pipeline Schedule**

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1.000	15.224	15.2	100	Circular	10.000	9.150	0.750	9.000	8.150	0.750
3.000	10.959	11.0	100	Circular	10.000	9.150	0.750	9.000	8.150	0.750
2.000	14.436	14.4	100	Circular	10.000	9.150	0.750	9.000	8.150	0.750
1.001	6.073	59.0	100	Circular	9.000	8.150	0.750	9.000	8.047	0.853

Link	US Node	Dia (mm)	Node Type	MH Type	DS Node	Dia (mm)	Node Type	MH Type
1.000	3	1200	Manhole	Adoptable	Combined manhole	1200	Manhole	Adoptable
3.000	Green roof 2	1200	Manhole	Adoptable	Combined manhole	1200	Manhole	Adoptable
2.000	green roof 1	1200	Manhole	Adoptable	Combined manhole	1200	Manhole	Adoptable
1.001	Combined manhole	1200	Manhole	Adoptable	5	1200	Manhole	Adoptable





**Manhole Schedule**

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
green roof 1	0.000	0.000	10.000	0.850	1200				
						0	2.000	9.150	100
Green roof 2	0.000	10.000	10.000	0.850	1200				
						0	3.000	9.150	100
3	0.000	20.000	10.000	0.850	1200				
						0	1.000	9.150	100
Combined manhole	10.943	9.416	9.000	0.850	1200		1	3.000	8.150
						2	2.000	8.150	100
						3	1.000	8.150	100
						0	1.001	8.150	100
5	17.016	9.374	9.000	0.953	1200		1	1.001	8.047
									100

**Simulation Settings**

Rainfall Methodology	FSR	Analysis Speed	Normal
FSR Region	England and Wales	Skip Steady State	x
M5-60 (mm)	20.000	Drain Down Time (mins)	240
Ratio-R	0.400	Additional Storage (m <sup>3</sup> /ha)	20.0
Summer CV	1.000	Check Discharge Rate(s)	x
Winter CV	0.840	Check Discharge Volume	x

**Storm Durations**

15	60	180	360	600	960	2160	4320	7200	10080
30	120	240	480	720	1440	2880	5760	8640	

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
30	0	0	0
100	0	0	0
100	40	0	0



**Results for 1 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	green roof 1	14	9.164	0.014	0.7	0.0182	0.0000	OK
30 minute summer	Green roof 2	20	9.160	0.010	0.4	0.0119	0.0000	OK
15 minute summer	3	10	9.170	0.020	1.4	0.0263	0.0000	OK
15 minute summer	Combined manhole	11	8.189	0.039	2.4	0.0437	0.0000	OK
15 minute summer	5	11	8.084	0.037	2.3	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	green roof 1	2.000	Combined manhole	0.7	0.569	0.044	0.0251	
30 minute summer	Green roof 2	3.000	Combined manhole	0.4	0.312	0.020	0.0162	
15 minute summer	3	1.000	Combined manhole	1.4	0.826	0.090	0.0299	
15 minute summer	Combined manhole	1.001	5	2.3	0.841	0.288	0.0164	1.2



**Results for 30 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	green roof 1	13	9.172	0.022	1.7	0.0281	0.0000	OK
30 minute summer	Green roof 2	20	9.165	0.015	0.9	0.0180	0.0000	OK
15 minute summer	3	10	9.182	0.032	3.4	0.0412	0.0000	OK
15 minute summer	Combined manhole	10	8.218	0.068	5.8	0.0773	0.0000	OK
15 minute summer	5	10	8.109	0.062	5.6	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	green roof 1	2.000	Combined manhole	1.7	0.687	0.106	0.0500	
30 minute summer	Green roof 2	3.000	Combined manhole	0.9	0.390	0.048	0.0332	
15 minute summer	3	1.000	Combined manhole	3.4	0.937	0.218	0.0597	
15 minute summer	Combined manhole	1.001	5	5.6	1.035	0.707	0.0328	3.0



**Results for 100 year Critical Storm Duration. Lowest mass balance: 100.00%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
30 minute summer	green roof 1	20	9.175	0.025	2.2	0.0319	0.0000	OK
30 minute summer	Green roof 2	21	9.167	0.017	1.1	0.0200	0.0000	OK
15 minute summer	3	10	9.186	0.036	4.4	0.0472	0.0000	OK
15 minute summer	Combined manhole	11	8.235	0.085	7.4	0.0962	0.0000	OK
15 minute summer	5	11	8.122	0.075	7.2	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
30 minute summer	green roof 1	2.000	Combined manhole	2.2	0.691	0.137	0.0595	
30 minute summer	Green roof 2	3.000	Combined manhole	1.1	0.403	0.060	0.0417	
15 minute summer	3	1.000	Combined manhole	4.4	0.997	0.282	0.0733	
15 minute summer	Combined manhole	1.001	5	7.2	1.073	0.913	0.0407	3.9



**Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%**

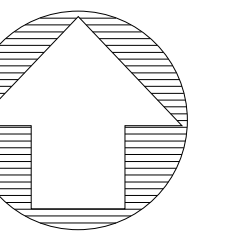
Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
30 minute summer	green roof 1	20	9.180	0.030	3.1	0.0380	0.0000	OK
30 minute summer	Green roof 2	20	9.170	0.020	1.6	0.0240	0.0000	OK
15 minute summer	3	10	9.194	0.044	6.2	0.0569	0.0000	OK
15 minute summer	Combined manhole	11	8.340	0.190	10.5	0.2151	0.0000	SURCHARGED
15 minute summer	5	11	8.141	0.094	9.6	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
30 minute summer	green roof 1	2.000	Combined manhole	3.1	0.729	0.193	0.0706	
30 minute summer	Green roof 2	3.000	Combined manhole	1.6	0.408	0.087	0.0490	
15 minute summer	3	1.000	Combined manhole	6.2	1.090	0.397	0.0847	
15 minute summer	Combined manhole	1.001	5	9.6	1.231	1.221	0.0469	5.5

# APPENDIX C

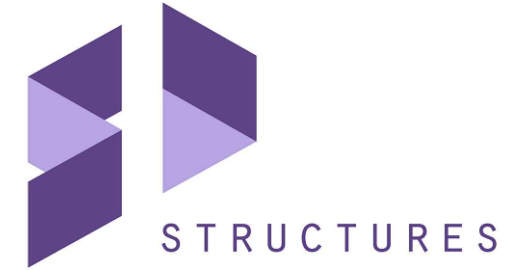
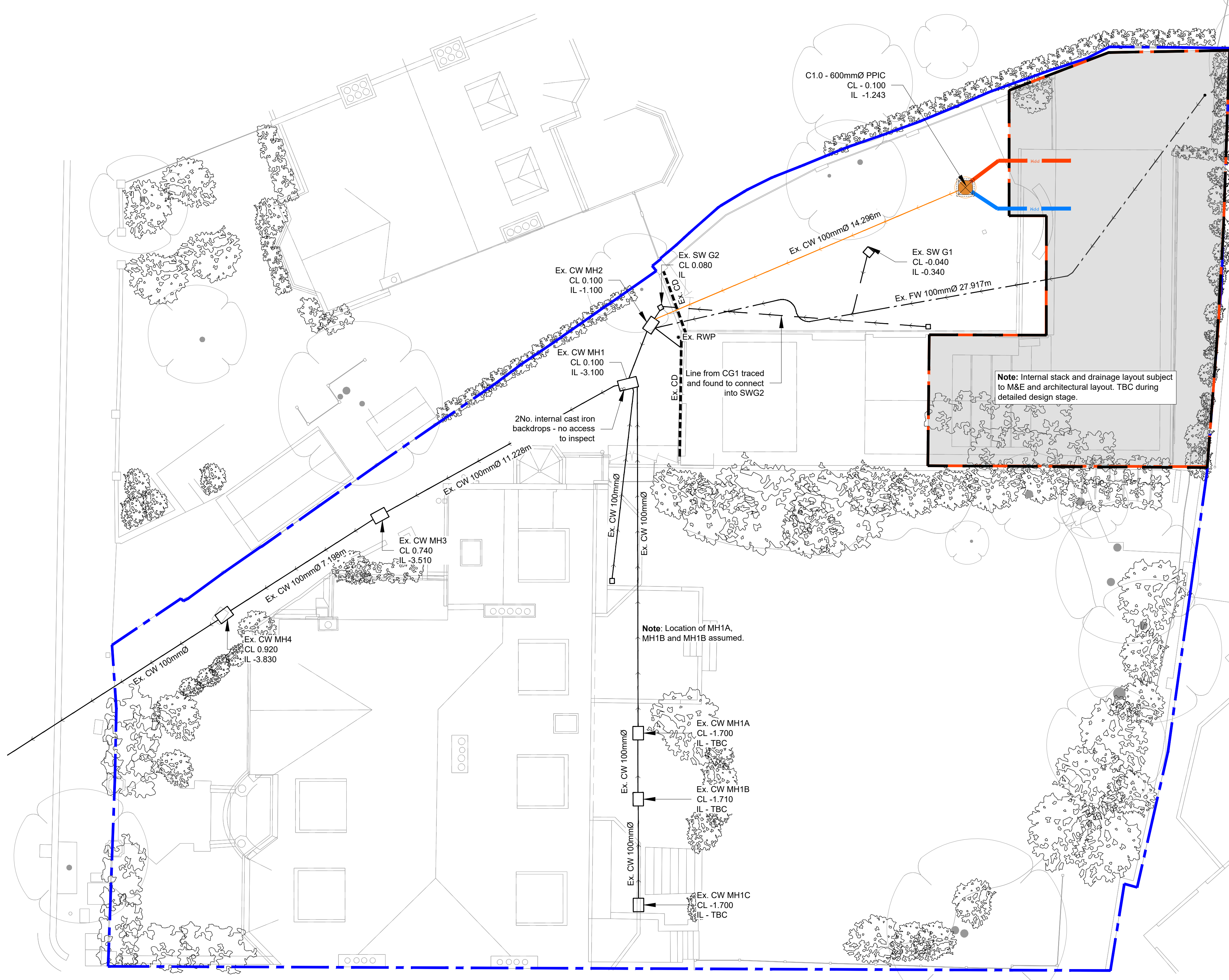
## DRAINAGE DRAWINGS





Below Ground Drainage Key	
<b>General Notation</b>	
100mmØ ID (pipe diameter) at 1/80 (approximate gradient)	Pipework other than that covered by the general drainage notes will be identified as adjacent BD - Backdrop connection UIL - Upper Invert Level
<b>Existing Drainage</b>	
	Existing Drainage - Combined Water
	Existing Drainage - Foul Water
	Existing Drainage - Surface Water
	Existing Drainage - to be abandoned
	Existing Drainage - Manholes Sizes as shown on plan / schedules Information as per services survey
	Existing Drainage - Pump and Rising Main Sizes shown indicatively Information as per services survey
<b>Combined Water</b>	
	Proposed Drainage - Combined Water drain
	Proposed Drainage - Combined Water Manholes Sizes are per plan and schedules PPIC - Polypropylene Inspection Chamber PCC - Pre-Cast Concrete
<b>Foul Water</b>	
	Proposed Drainage - Foul Water drain
	Proposed Drainage - Foul Water Manholes Sizes are per plan and schedules PPIC - Polypropylene Inspection Chamber PCC - Pre-Cast Concrete
	Proposed Drainage - Foul Water Pumping Chamber and Rising Main Sizes shown indicatively Refer to pump manufacturers' specification
	Foul Connection: SVP - Soil Vent Pipe SS - Stub Stack AAV - Air Admittance Valve FA - From Above (refer to Architectural / M&E plans) FS - Floor Socket (for internal gullies / shower drains)
	FG - Foul Gully (trapped and roddable)
<b>Surface Water</b>	
	Proposed Drainage - Surface Water drain
	Proposed Drainage - Surface Water land drain Perforated pipe laid within sub-base material
	Proposed Drainage - Surface Water channel drain (ACO or similar approved)
	Proposed Drainage - Foul Water Manholes Sizes are per plan and schedules PPIC - Polypropylene Inspection Chamber PCC - Pre-Cast Concrete FC - Flow Control chamber (Hydro-Brake™ by Hydro International or similar approved) CP - Catch Pit chamber
	Proposed Drainage - Surface Water Pumping Chamber and Rising Main Sizes shown indicatively Refer to pump manufacturers' specification
	Proposed Drainage - Cellular storage structure or soakaway Sizes as per plan and schedules Refer to crate manufacturers' specification
	Proposed Drainage - Permeable surfacing Permeable paving / permeable asphalt Refer to Landscape Architect's / Construction build-ups drawings for more information
	RWP - Rain Water Pipe
	YG - Yard Gully (trapped and roddable) RG - Road Gully

- General Notes:**
- Do not scale from this drawing manually or electronically. Written permission must be obtained from SD Structures prior to scaling.
  - Contact SD Structures in the event of any discrepancies between findings on site and these drawings.
  - This drawing is also to be read in conjunction with all relevant Architect's, Engineer's and Specialist's drawings and specifications.
  - 3D views are indicative only and any conflicting 2D information should take precedence. If in doubt contact SD Structures prior to starting work.
  - All work is to be carried out in accordance with the relevant British Standards, European norms, codes of practice and building practice.
  - The Contractor shall obtain licences from the Highway Authority prior to carrying out any workings within the existing Public Highway.



INFORMATION	
Client	Scenario Architecture
Project Name	20 Crediton Hill
Drawing Title	Proposed Drainage Layout
SD Ref	SDS1584
Rev	CC ES

P01	Issued for information	19/04/2023	ES	CC	Scale:	1:100 @ A1	Proj	Orig	Vol	Lev	Typ	Rol	No	Status	Rev
Rev	Amendment	Date	Drawn	Eng			1584-SDS-00-XX-DR-C-1000								P01







# APPENDIX D

## CCTV SURVEY

